# thermo Documentation

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#### CHAPTER

## INTRODUCTION TO CUBIC EQUATIONS OF STATE

- Working With Pure Components
- Pure Component Equilibrium
- Working With Mixtures
- Other features
  - Hashing
  - Serialization
- Mixture Equilibrium
- Using Units with Cubic Equations of State

Cubic equations of state provide thermodynamically-consistent and relatively fast models for pure chemicals and mixtures. They are normally used to represent gases and liquids.

The generic three-parameter form is as follows:

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V^2 + \delta V + \epsilon}$$

This forms the basis of the implementation in *thermo*.

Two separate interfaces are provided, thermo. eos for pure component modeling and thermo. eos\_mix for multicomponent modeling. Pure components are quite a bit faster than multicomponent mixtures, because the Van der Waals mixing rules conventionally used take N^2 operations to compute  $\alpha(T)$ :

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

The other slow parts which applies to both types are calculating some basic properties (the list is at  $set\_properties\_from\_solution$ ) that other properties may depend on, and calculating the molar volume given a pair of (T, P) inputs (an entire submodule *thermo.eos\\_volume* discusses and implements this topic). Both of those calculations are constant-time, so their overhead is the same for pure components and multicomponent mixtures.

### **1.1 Working With Pure Components**

We can use the *GCEOS* (short for "General Cubic Equation Of State") interface with any component or implemented equation of state, but for simplicity n-hexane is used with the Peng-Robinson EOS. Its critical temperature is 507.6 K, critical pressure 3.025 MPa, and acentric factor is 0.2975.

The state must be specified along with the critical constants when initializing a *GCEOS* object; we use 400 K and 1e6 Pa here:

```
>>> from thermo import *
>>> eos = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=400., P=1E6)
>>> eos
PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=400.0, P=1000000.0)
```

The \_\_repr\_\_ string is designed to show all the inputs to the object.

We can check the volume solutions with the raw\_volumes attribute:

```
>>> eos.raw_volumes
(0.0001560731847856, 0.002141876816741, 0.000919295474982)
```

At this point there are three real volume, so there is a liquid-like and a vapor-like solution available. The **phase** attribute will have the value of 'l/g' in this state; otherwise it will be 'l' or 'g'.

>>> eos.phase
'1/g'

The basic properties calculated at initialization are directly attributes, and can be accessed as such. Liquid-like properties have "\_l" at the end of their name, and "\_g" is at the end of gas-like properties.

```
>>> eos.H_dep_l
-26111.877
>>> eos.S_dep_g
-6.4394518
>>> eos.dP_dT_l
288501.633
```

All calculations in *thermo.eos* and *thermo.eos\_mix* are on a molar basis; molecular weight is never provided or needed. All outputs are in base SI units (K, Pa, m^3, mole, etc). This simplified development substantially. For working with mass-based units, use the *Phase* interface. The *thermo.eos* and *thermo.eos\_mix* interfaces were developed prior to the *Phase* interface and does have some features not exposed in the *Phase* interface however.

Other properties are either implemented as methods that require arguments, or Python properties which act just like attributes but calculate the results on the fly. For example, the liquid-phase fugacity *fugacity\_l* or the gas isobaric (constant-pressure) expansion coefficient are properties.

```
>>> eos.fugacity_l
421597.00785
>>> eos.beta_g
0.0101232239
```

There are an awful lot of these properties, because many of them are derivatives subject to similar conditions. A full list is in the documentation for *GCEOS*. There are fewer calls that take temperature, such as *Hvap* which calculates the heat of vaporization of the object at a specified temperature:

>>> eos.Hvap(300)
31086.2

Once an object has been created, it can be used to instantiate new *GCEOS* objects at different conditions, without respecifying the critical constants and other parameters that may be needed.

```
>>> eos.to(T=300.0, P=1e5)
PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=300.0, P=100000.0)
>>> eos.to(V=1e2, P=1e5)
PR(Tc=507.6, Pc=3025000.0, omega=0.2975, P=100000.0, V=100.0)
>>> eos.to(V=1e2, T=300)
PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=300, V=100.0)
```

As was seen in the examples above, any two of *T*, *P*, *V* can be used to specify the state of the object. The input variables of the object are stored and can be checked with *state\_specs* :

```
>>> eos.state_specs
{'T': 400.0, 'P': 1000000.0}
```

The individual parts of the generic cubic equation are stored as well. We can use them to check that the pressure equation is satisfied:

```
>>> from thermo.eos import R
>>> R*eos.T/(eos.V_l-eos.b) - eos.a_alpha/(eos.V_l**2 + eos.V_l*eos.delta + eos.epsilon)
1000000.000000
>>> R*eos.T/(eos.V_g-eos.b) - eos.a_alpha/(eos.V_g**2 + eos.V_g*eos.delta + eos.epsilon)
1000000.000000
```

Note that as floating points are not perfectly precise, some small error may be shown but great care has been taken to minimize this.

The value of the gas constant used is 8.31446261815324 J/(mol\*K). This is near the full precision of floating point numbers, but not quite. It is now an exact value used as a "definition" in the SI system. Note that other implementations of equations of state may not use the full value of the gas constant, but the author strongly recommends anyone considering writing their own EOS implementation use the full gas constant. This will allow more interchangeable results.

### **1.2 Pure Component Equilibrium**

Continuing with the same state and example as before, there were two solutions available from the equation of state. However, unless the exact temperature 400 K and pressure 1 MPa happens to be on the saturation line, there is always one more thermodynamically stable state. We need to use the departure Gibbs free energy to determine which state is more stable. For a pure component, the state which minimizes departure Gibbs free energy is the most stable state.

```
>>> eos = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=400., P=1E6)
>>> eos.G_dep_l, eos.G_dep_g
(-2872.498434, -973.5198207)
```

It is easy to see the liquid phase is more stable. This shortcut of using departure Gibbs free energy is valid only for pure components with all phases using the ideal-gas reference state. The full criterial is whichever state minimizes the actual Gibbs free energy.

The method more\_stable\_phase does this check and returns either 'l' or 'g':

>>> eos.more\_stable\_phase '1'

For a pure component, there is a vapor-liquid equilibrium line right up to the critical point which defines the vapor pressure of the fluid. This can be calculated using the *Psat* method:

```
>>> eos.Psat(400.0)
466205.073739
```

The result is accurate to more than 10 digits, and is implemented using some fancy mathematical techniques that allow a direct calculation of the vapor pressure. A few more digits can be obtained by setting *polish* to True, which polishes the result with a newton solver to as much accuracy as a floating point number can provide:

```
>>> 1-eos.Psat(400, polish=True)/eos.Psat(400)
1.6e-14
```

A few more methods of interest are  $V_1$  and  $V_2$  and  $V_2$  are which calculate the saturation liquid and molar volumes; Tsat which calculates the saturation temperature given a specified pressure, and phi\_sat which computes the saturation fugacity coefficient given a temperature.

```
>>> eos.V_l_sat(298.15), eos.V_g_sat(500)
(0.0001303559, 0.0006827569)
>>> eos.Tsat(101325.0)
341.76265
>>> eos.phi_sat(425.0)
0.8349716
```

### **1.3 Working With Mixtures**

Using mixture from thermo.eos\_mix is first illustrated using an equimolar mixture of nitrogen-methane at 115 K and 1 MPa and the Peng-Robinson equation of state:

```
>>> eos = PRMIX(T=115.0, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], omegas=[0.04,
→ 0.011], zs=[0.5, 0.5], kijs=[[0.0, 0.0289], [0.0289, 0.0]])
>>> eos.V_l, eos.V_g
(3.658707770e-05, 0.00070676607)
>>> eos fugacities_1, eos fugacities_g
([838516.99, 78350.27], [438108.61, 359993.48])
```

All of the properties available in GCEOS are also available for GCEOSMIX objects.

New GCEOSMIX objects can be created with the to method, which accepts new mole fractions zs as well as new state variables. If a new composition zs is not provided, the current composition is also used for the new object.

```
>>> eos.to(T=300.0, P=1e5)
PRMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011], kijs=[[0.0,]
→0.0289], [0.0289, 0.0]], zs=[0.5, 0.5], T=300.0, P=100000.0)
>>> eos.to(T=300.0, P=1e5, zs=[.1, .9])
PRMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011], kijs=[[0.0,
→0.0289], [0.0289, 0.0]], zs=[0.1, 0.9], T=300.0, P=100000.0)
>>> eos.to(V=1, P=1e5, zs=[.4, .6])
PRMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011], kijs=[[0.0,]
 →0.0289], [0.0289, 0.0]], zs=[0.4, 0.6], P=100000.0, V=1)
```

(continued from previous page)

It is possible to create new *GCEOSMIX* objects with the *subset* method which uses only some of the initially specified components:

```
>>> kijs = [[0.0, 0.00076, 0.00171], [0.00076, 0.0, 0.00061], [0.00171, 0.00061, 0.0]]
>>> PR3 = PRMIX(Tcs=[469.7, 507.4, 540.3], zs=[0.8168, 0.1501, 0.0331], omegas=[0.249, 0.
...305, 0.349], Pcs=[3.369E6, 3.012E6, 2.736E6], T=322.29, P=101325.0, kijs=kijs)
>>> PR3.subset([1,2])
PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349], kijs=[[0.0, ...
...0.00061], [0.00061, 0.0]], zs=[0.8193231441048, 0.1806768558951], T=322.29, P=101325.0)
>>> PR3.subset([1,2], T=500.0, P=1e5, zs=[.2, .8])
PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349], kijs=[[0.0, ...
...0.00061], [0.00061, 0.0]], zs=[0.2, 0.8], T=500.0, P=100000.0)
>>> PR3.subset([1,2], zs=[.2, .8])
PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349], kijs=[[0.0, ...
...0.00061], [0.00061, 0.0]], zs=[0.2, 0.8], T=500.0, P=100000.0]
>>> PR3.subset([1,2], zs=[.2, .8])
```

It is also possible to create pure GCEOS objects:

```
>>> PR3.pures()
[PR(Tc=469.7, Pc=3369000.0, omega=0.249, T=322.29, P=101325.0), PR(Tc=507.4, Pc=3012000.
→0, omega=0.305, T=322.29, P=101325.0), PR(Tc=540.3, Pc=2736000.0, omega=0.349, T=322.
→29, P=101325.0)]
```

Temperature, pressure, mole number, and mole fraction derivatives of the log fugacity coefficients are available as well with the methods *dlnphis\_dT*, *dlnphis\_dP*, *dlnphis\_dns*, and *dlnphis\_dzs*:

>>> PR3.dlnphis\_dT('l')
[0.029486952019, 0.03514175794, 0.040281845273]
>>> PR3.dlnphis\_dP('l')
[-9.8253779e-06, -9.8189093031e-06, -9.8122598e-06]
>>> PR3.dlnphis\_dns(PR3.Z\_l)
[[-0.0010590517, 0.004153228837, 0.007300114797], [0.0041532288, -0.016918292791, -0.
...0257680231], [0.0073001147, -0.02576802316, -0.0632916462]]
>>> PR3.dlnphis\_dzs(PR3.Z\_l)
[[0.0099380692, 0.0151503498, 0.0182972357], [-0.038517738, -0.059589260, -0.068438990],\_
...[-0.070571069, -0.103639207, -0.141162830]]

# 1.4 Other features

### 1.4.1 Hashing

It is possible to compare the two objects with each other to see if they have the same kijs, model parameters, and components by using the *model\_hash* method:

>>> PR\_case = PRMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], omegas=[0. →04, 0.011], zs=[0.5, 0.5], kijs=[[0,0.41],[0.41,0]]) >>> SRK\_case = SRKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], →omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0.41],[0.41,0]])

```
>>> PR_case.model_hash() == SRK_case.model_hash()
False
```

It is possible to see if both the exact state and the model match between two different objects by using the *state\_hash* method:

And finally it is possible to see if two objects are exactly identical, including cached calculation results, by using the \_\_hash\_\_ method:

```
>>> PR_case3 = PRMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], omegas=[0.

...04, 0.011], zs=[0.5, 0.5], kijs=[[0,0.41],[0.41,0]])

>>> PR_case.state_hash() == PR_case3.state_hash()

True

>>> hash(PR_case) == hash(PR_case3)

True

>>> _ = PR_case.da_alpha_dT_ijs

>>> hash(PR_case) == hash(PR_case3)

False
```

#### 1.4.2 Serialization

All cubic EOS models offer a *as\_json* method and a *from\_json* to serialize the object state for transport over a network, storing to disk, and passing data between processes.

Other json libraries can be used besides the standard json library by design.

Storing and recreating objects with Python's pickle.dumps library is also tested; this can be faster than using JSON at the cost of being binary data.

# 1.5 Mixture Equilibrium

Unlike pure components, it is not straightforward to determine what the equilibrium state is for mixtures. Different algorithms are used such as sequential substitution and Gibbs minimization. All of those require initial guesses, which usually come from simpler thermodynamic models. While in practice it is possible to determine the equilibrium composition to an N-phase problem, in theory a global optimization algorithm must be used.

More details on this topic can be found in the thermo.flash module.

# **1.6 Using Units with Cubic Equations of State**

There is a pint wrapper to use these objects as well.

```
>>> base = IG(T=300.0*u.K, P=1e6*u.Pa)
>>> base.V_g
<Quantity(0.00249433879, 'meter ** 3 / mole')>
```

# INTRODUCTION TO ACTIVITY COEFFICIENT MODELS

- Object Structure
- UNIFAC Example
- Notes on Performance
- Other features
- Activity Coefficient Identities
- References

Vapor-liquid and liquid-liquid equilibria systems can have all sorts of different behavior. Raoult's law can describe only temperature and pressure dependence, so a correction factor that adds dependence on composition called the "activity coefficient" is often used. This is a separate approach to using an equation of state, but because direct vapor pressure correlations are used with the activity coefficients, a higher-accuracy result can be obtained for phase equilibria.

While these models are often called "activity coefficient models", they are in fact actually a prediction for excess Gibbs energy. The activity coefficients that are used for phase equilibria are derived from the partial mole number derivative of excess Gibbs energy according to the following expression:

$$\gamma_i = \exp\left(\frac{\frac{\partial n_i G^E}{\partial n_i}}{RT}\right)$$

There are 5 basic activity coefficient models in thermo:

- NRTL
- Wilson
- UNIQUAC
- RegularSolution
- UNIFAC

Each of these models are object-oriented, and inherit from a base class *GibbsExcess* that provides many common methods. A further dummy class that predicts zero excess Gibbs energy and activity coefficients of 1 is available as *IdealSolution*.

The excess Gibbs energy model is typically fairly simple. A number of derivatives are needed to calculate other properties like activity coefficient so those expressions can seem more complicated than the model really is. In the literature it is common for a model to be shown directly in activity coefficient form without discussion of the Gibbs excess energy model. To illustrate the difference, here is the *NRTL* model Gibbs energy expression and its activity coefficient model:

$$g^E = RT \sum_{i} x_i \frac{\sum_{j} \tau_{ji} G_{ji} x_j}{\sum_{j} G_{ji} x_j}$$

$$\ln(\gamma_i) = \frac{\sum_{j=1}^n x_j \tau_{ji} G_{ji}}{\sum_{k=1}^n x_k G_{ki}} + \sum_{j=1}^n \frac{x_j G_{ij}}{\sum_{k=1}^n x_k G_{kj}} \left( \tau_{ij} - \frac{\sum_{m=1}^n x_m \tau_{mj} G_{mj}}{\sum_{k=1}^n x_k G_{kj}} \right)$$

The models *NRTL*, *Wilson*, and *UNIQUAC* are the most commonly used. Each of them is regression-based - all coefficients must be found in the literature or regressed yourself. Each of these models has extensive temperature dependence parameters in addition to the composition dependence. The temperature dependencies implemented should allow parameters from most other sources to be used here with them.

The model *RegularSolution* is based on the concept of a solubility parameter; with liquid molar volumes and solubility parameters it is a predictive model. It does not show temperature dependence. Additional regression coefficients can be used with that model also.

The UNIFAC model is a predictive group-contribution scheme. In it, each molecule is fragmented into different sections. These sections have interaction parameters with other sections. Usually the fragmentation is not done by hand. One online tool for doing this is the DDBST Online Group Assignment Tool.

# 2.1 Object Structure

The *GibbsExcess* object doesn't know anything about phase equilibria, vapor pressure, or flash routines; it is limited in scope to dealing with excess Gibbs energy. Because of that modularity, an initialized *GibbsExcess* object is designed to be passed in an argument to a cubic equations of state that use excess Gibbs energy such as *PSRK*.

The other place these objects are used are in *GibbsExcessLiquid* objects, which brings the pieces together to construct a thermodynamically (mostly) consistent phase that the *flash algorithms* can work with.

This modularity allows new Gibbs excess models to be written and used anywhere - so the *PSRK* model will happily allow a UNIFAC object configured like VTPR.

## 2.2 UNIFAC Example

The UNIFAC model is a group contribution based predictive model that is works using "fragmentations" of each molecule into a number of different "groups" and their "counts",

The DDBST has published numerous sample problems using UNIFAC; a simple binary system from example P05.22a  $in^2$  with n-hexane and butanone-2 is shown below:

The solution given by the DDBST has the activity coefficient values [1.428, 1.365], which match those calculated by the UNIFAC object:

```
>>> GE.gammas()
[1.4276025835, 1.3646545010]
```

Many other properties are also implemented, a few of which are shown below:

<sup>&</sup>lt;sup>2</sup> Gmehling, Jürgen, Michael Kleiber, Bärbel Kolbe, and Jürgen Rarey. Chemical Thermodynamics for Process Simulation. John Wiley & Sons, 2019.

```
>>> GE.GE(), GE.dGE_dT(), GE.d2GE_dT2()
(923.641197, 0.206721488, -0.00380070204)
>>> GE.HE(), GE.SE(), GE.dHE_dT(), GE.dSE_dT()
(854.77193363, -0.2067214889, 1.266203886, 0.0038007020460)
```

Note that the *UFIP* and *UFSG* variables contain the actual interaction parameters; none are hardcoded with the class, so the class could be used for regression. The *version* parameter controls which variant of UNIFAC to use, as there are quite a few. The different UNIFAC models implemented include original UNIFAC, Dortmund UNIFAC, PSRK, VTPR, Lyngby/Larsen, and UNIFAC KT. Interaction parameters for all models are included as well, but the *version* argument is not connected to the data files.

For convenience, a number of molecule fragmentations are distributed with the UNIFAC code. All fragmentations were obtained through the DDBST online portal, where molecular structure files can be submitted. This has the advantage that what is submitted is unambiguous; there are no worries about CAS numbers like how graphite and diamond have a different CAS number while being the same element or Air having a CAS number despite being a mixture. Accordingly, The index in these distributed data files are InChI keys, which can be obtained from chemicals.identifiers or in various places online.

```
>>> import thermo.unifac
>>> thermo.unifac.load_group_assignments_DDBST()
>>> len(thermo.unifac.DDBST_UNIFAC_assignments)
28846
>>> len(thermo.unifac.DDBST_MODIFIED_UNIFAC_assignments)
29271
>>> len(thermo.unifac.DDBST_PSRK_assignments)
30034
>>> from chemicals import search_chemical
>>> search_chemical('toluene').InChI_key
'YXFVVABEGXRONW-UHFFFAOYSA-N'
>>> thermo.unifac.DDBST_MODIFIED_UNIFAC_assignments['YXFVVABEGXRONW-UHFFFAOYSA-N']
{9: 5, 11: 1}
```

Please note that the identifying integer in these {group: count} elements are not necessarily the same in different UNIFAC versions, making them a royal pain.

# 2.3 Notes on Performance

Initializing the object for the first time is a not a high performance operation as certain checks need to be done and data structures set up. Some pieces of the equations of the Gibbs excess model may depend only on temperature or composition, instead of depending on both. Each model implements the method  $to_T_xs$  which should be used to create a new object at the new temperature and/or composition. The design of the object is to lazy-calculate properties, and to be immutable: calculations at new temperatures and compositions are done in a new object.

Note also that the <u>\_\_repr\_\_</u> string for each model is designed to allow lossless reconstruction of the model. This is very useful when building test cases.

When working with small numbers of components (5 or under), PyPy offers the best performance and using the model with Python lists as inputs is the fastest way to perform the calculations even in CPython.

If working with many components or if Numpy arrays are desired as inputs and outputs, numpy arrays can be provided as inputs. This will have a negative impact on performance unless the *numba* interface is used:

```
>>> import numpy as np
>>> import thermo.numba
>>> N = 3
>>> T = 25.0 + 273.15
>>> xs = np.array([0.7273, 0.0909, 0.1818])
>>> rs = np.array([0.7273, 0.0909, 0.1818])
>>> rs = np.array([.92, 2.1055, 3.1878])
>>> qs = np.array([1.4, 1.972, 2.4])
>>> tausA = tausC = tausD = tausE = tausF = np.array([[0.0]*N for i in range(N)])
>>> tausB = np.array([[0, -526.02, -309.64], [318.06, 0, 91.532], [-1325.1, -302.57, 0]])
>>> ABCDEF = (tausA, tausB, tausC, tausD, tausE, tausF)
>>> from thermo import UNIQUAC
>>> GE2 = UNIQUAC(T=T, xs=xs, rs=rs, qs=qs, ABCDEF=ABCDEF)
>>> GE2.gammas()
array([ 1.57039333, 0.29482416, 18.11432905])
```

The *numba* interface will speed code up and allow calculations with dozens of components. The *numba* interface requires all inputs to be numpy arrays and all of its outputs are also numba arrays.

```
>>> GE3 = thermo.numba.UNIQUAC(T=T, xs=xs, rs=rs, qs=qs, ABCDEF=ABCDEF)
>>> GE3.gammas()
array([ 1.57039333,  0.29482416, 18.11432905])
```

As an example of the performance benefits, a 200-component UNIFAC gamma calculation takes 10.6 ms in CPython and 318 µs when accelerated by Numba. In this case PyPy takes at 664 µs.

When the same benchmark is performed with 10 components, the calculation takes 387 µs in CPython, 88.6 µs with numba, and 36.2 µs with PyPy.

It can be quite important to use the  $to_T_xs$  method re-use parts of the calculation; for UNIFAC, several terms depends only on temperature. If the 200 component calculation is repeated with those already calculated, the timings are 3.26 ms in CPython, 127 µs with numba, and 125 µs with PyPy.

## 2.4 Other features

The limiting infinite-dilution activity coefficients can be obtained with a call to gammas\_infinite\_dilution

```
>>> GE.gammas_infinite_dilution()
[3.5659995166, 4.32849696]
```

All activity coefficient models offer a *as\_json* method and a *from\_json* to serialize the object state for transport over a network, storing to disk, and passing data between processes.

```
>>> from thermo import IdealSolution
>>> import json
>>> model = IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
>>> json_view = model.as_json()
>>> json_str = json.dumps(json_view)
```

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```
>>> model_copy = IdealSolution.from_json(json.loads(json_str))
>>> assert model_copy == model
```

Other json libraries can be used besides the standard json library by design.

Storing and recreating objects with Python's pickle.dumps library is also tested; this can be faster than using JSON at the cost of being binary data.

All models have a <u>hash</u> method that can be used to compare different models to see if they are absolutely identical (including which values have been calculated already).

They also have a *model\_hash* method that can be used to compare different models to see if they have identical model parameters.

They also have a *state\_hash* method that can be used to compare different models to see if they have identical temperature, composition, and model parameters.

# 2.5 Activity Coefficient Identities

A set of useful equations are as follows. For more information, the reader is directed to<sup>1,?,3,4</sup>, and<sup>5</sup>; no one source contains all this information.

-

$$\begin{split} h^{E} &= -T \frac{\partial g^{E}}{\partial T} + g^{E} \\ & \frac{\partial h^{E}}{\partial T} = -T \frac{\partial^{2} g^{E}}{\partial T^{2}} \\ & \frac{\partial h^{E}}{\partial x_{i}} = -T \frac{\partial^{2} g^{E}}{\partial T \partial x_{i}} + \frac{\partial g^{E}}{\partial x_{i}} \\ & s^{E} = \frac{h^{E} - g^{E}}{T} \\ & \frac{\partial s^{E}}{\partial T} = \frac{1}{T} \left( \frac{-\partial g^{E}}{\partial T} + \frac{\partial h^{E}}{\partial T} - \frac{(G+H)}{T} \right) \\ & \frac{\partial S^{E}}{\partial x_{i}} = \frac{1}{T} \left( \frac{\partial h^{E}}{\partial x_{i}} - \frac{\partial g^{E}}{\partial x_{i}} \right) \\ & \frac{\partial \gamma_{i}}{\partial n_{i}} = \gamma_{i} \left( \frac{\frac{\partial^{2} G^{E}}{\partial x_{i} \partial x_{j}}}{RT} \right) \\ & \frac{\partial \gamma_{i}}{\partial T} = \left( \frac{\frac{\partial^{2} n G^{E}}{\partial T \partial n_{i}}}{RT} - \frac{\frac{\partial n_{i} G^{E}}{\partial n_{i}}}{RT^{2}} \right) \exp \left( \frac{\frac{\partial n_{i} G^{E}}{\partial n_{i}}}{RT} \right) \end{split}$$

<sup>4</sup> Elliott, J., and Carl Lira. Introductory Chemical Engineering Thermodynamics. 2nd edition. Upper Saddle River, NJ: Prentice Hall, 2012.

<sup>&</sup>lt;sup>1</sup> Poling, Bruce E., John M. Prausnitz, and John P. O'Connell. The Properties of Gases and Liquids. 5th edition. New York: McGraw-Hill Professional, 2000.

<sup>&</sup>lt;sup>3</sup> Nevers, Noel de. Physical and Chemical Equilibrium for Chemical Engineers. 2nd edition. Wiley, 2012.

<sup>&</sup>lt;sup>5</sup> Walas, Dr Stanley M. Phase Equilibria in Chemical Engineering. Butterworth-Heinemann, 1985.

# 2.6 References

### CHAPTER

### THREE

# INTRODUCTION TO PROPERTY OBJECTS

• Temperature Dependent Properties

- Creating Objects
- Temperature-dependent Methods
- Calculating Properties
- Limits and Extrapolation
- Plotting
- Calculating Temperature From Properties
- Property Derivatives
- Property Integrals
- Using Tabular Data
- Adding New Methods
- Adding New Correlation Coefficient Methods
- Fitting Correlation Coefficients
- Adding New Correlation Coefficient Methods From Data
- Temperature and Pressure Dependent Properties
  - Creating Objects
  - Pressure-dependent Methods
  - Calculating Properties
  - Limits and Extrapolation
  - Plotting
  - Calculating Conditions From Properties
  - Property Derivatives
  - Property Integrals
  - Using Tabular Data
- Mixture Properties
- Notes

For every chemical property, there are lots and lots of methods. The methods can be grouped by which phase they apply to, although some methods are valid for both liquids and gases.

Properties calculations be separated into three categories:

- Properties of chemicals that depend on **temperature**. Some properties have weak dependence on pressure, like surface tension, and others have no dependence on pressure like vapor pressure by definition.
- Properties of chemicals that depend on **temperature** and **pressure**. Some properties have weak dependence on pressure like thermal conductivity, while other properties depend on pressure fundamentally, like gas volume.
- Properties of mixtures, that depend on **temperature** and **pressure** and **composition**. Some properties like gas mixture heat capacity require the pressure as an input but do not use it.

These properties are implemented in an object oriented way, with the actual functional algorithms themselves having been separated out into the chemicals library. The goal of these objects is to make it easy to experiment with different methods.

The base classes for the three respective types of properties are:

- TDependentProperty
- TPDependentProperty
- MixtureProperty

The specific classes for the three respective types of properties are:

- HeatCapacityGas, HeatCapacityLiquid, HeatCapacitySolid, VolumeSolid, VaporPressure, SublimationPressure, EnthalpyVaporization, EnthalpySublimation, Permittivity, SurfaceTension.
- VolumeGas, VolumeLiquid, ViscosityGas, ViscosityLiquid, ThermalConductivityGas, ThermalConductivityLiquid
- HeatCapacityGasMixture, HeatCapacityLiquidMixture, HeatCapacitySolidMixture, VolumeGasMixture, VolumeLiquidMixture, VolumeSolidMixture, ViscosityLiquidMixture, ViscosityGasMixture, ThermalConductivityLiquidMixture, ThermalConductivityGasMixture, SurfaceTensionMixture

# 3.1 Temperature Dependent Properties

The following examples introduce how to use some of the methods of the *TDependentProperty* objects. The API documentation for *TDependentProperty* as well as each specific property such as *VaporPressure* should be consulted for full details.

### 3.1.1 Creating Objects

All arguments and information the property object requires must be provided in the constructor of the object. If a piece of information is not provided, whichever methods require it will not be available for that object.

Various data files will be searched to see if information such as Antoine coefficients is available for the compound during the initialization. This behavior can be avoided by setting the optional *load\_data* argument to False. Loading

data requires *pandas*, uses more RAM, and is a once-per-process procedure that takes 20-1000 ms per property. For some applications it may be advantageous to provide your own data instead of using the provided data files.

```
>>> useless_psat = VaporPressure(CASRN='64-17-5', load_data=False)
```

#### 3.1.2 Temperature-dependent Methods

As many methods may be available, a single method is always selected automatically during initialization. This method can be inspected with the *method* property; if no methods are available, *method* will be None. *method* is also a valid parameter when constructing the object, but if the method specified is not available an exception will be raised.

```
>>> ethanol_psat.method, useless_psat.method
('WAGNER_MCGARRY', None)
```

All available methods can be found by inspecting the all\_methods attribute:

Changing the method is as easy as setting a new value to the attribute:

```
>>> ethanol_psat.method = 'ANTOINE_POLING'
>>> ethanol_psat.method
'ANTOINE_POLING'
>>> ethanol_psat.method = 'WAGNER_MCGARRY'
```

#### 3.1.3 Calculating Properties

Calculation of the property at a specific temperature is as easy as calling the object which triggers the \_\_call\_\_ method:

```
>>> ethanol_psat(300.0)
8753.8160
```

This is actually a cached wrapper around the specific call, *T\_dependent\_property*:

```
>>> ethanol_psat.T_dependent_property(300.0)
8753.8160
```

The caching of  $\_call\_$  is quite basic - the previously specified temperature is stored, and if the new *T* is the same as the previous *T* the previously calculated result is returned.

There is a lower-level interface for calculating properties with a specified method by name, *calculate*. *T\_dependent\_property* is a wrapper around *calculate* that includes validation of the result.

```
>>> ethanol_psat.calculate(T=300.0, method='WAGNER_MCGARRY')
8753.8160
>>> ethanol_psat.calculate(T=300.0, method='DIPPR_PERRY_8E')
8812.9812
```

### 3.1.4 Limits and Extrapolation

Each correlation is associated with temperature limits. These can be inspected as part of the  $T_{limits}$  attribute which is loaded on creation of the property object.

```
>>> ethanol_psat.T_limits
{'WAGNER_MCGARRY': (293.0, 513.92), 'WAGNER_POLING': (159.05, 513.92), 'ANTOINE_POLING': 
→ (276.5, 369.54), 'DIPPR_PERRY_8E': (159.05, 514.0), 'COOLPROP': (159.1, 514.71), 'VDI_
→ TABULAR': (300.0, 513.9), 'VDI_PPDS': (159.05, 513.9), 'BOILING_CRITICAL': (0.01, 514.
→ 0), 'LEE_KESLER_PSAT': (0.01, 514.0), 'AMBROSE_WALTON': (0.01, 514.0), 'SANJARI': (0.
→ 01, 514.0), 'EDALAT': (0.01, 514.0)}
```

Because there is often a need to obtain a property outside the range of the correlation, there are some extrapolation methods available; depending on the method these may be enabled by default. The full list of extrapolation methods can be see *here*.

For vapor pressure, there are actually two separate extrapolation techniques used, one for the low-pressure and thermodynamically reasonable region and another for extrapolating even past the critical point. This can be useful for obtaining initial estimates of phase equilibrium.

The low-pressure region uses  $\log(P_{sat}) = A - B/T$ , where the coefficients A and B are calculated from the low-temperature limit and its temperature derivative. The default high-temperature extrapolation is  $P_{sat} = \exp(A + B/T + C\log(T))$ . The coefficients are also determined from the high-temperature limits and its first two temperature derivatives.

When extrapolation is turned on, it is used automatically if a property is requested out of range:

```
>>> ethanol_psat(100.0), ethanol_psat(1000)
(1.047582e-11, 1779196575.4962692)
```

The default extrapolation methods may be changed in the future, but can be manually specified also by changing the value of the *extrapolation* attribute. For example, if the *linear* extrapolation method is set, extrapolation will be linear instead of using those fit equations. Because not all properties are suitable for linear extrapolation, some methods have a default *transform* to make the property behave as linearly as possible. This is also used in tabular interpolation:

```
>>> ethanol_psat.extrapolation = 'linear'
>>> ethanol_psat(100.0), ethanol_psat(1000)
(1.0475e-11, 385182009.4)
```

The low-temperature linearly extrapolated value is actually the same as before, because it performs a 1/T transform and a log(P) transform on the output, which results in the fit being the same as the default equation for vapor pressure.

To better understand what methods are available, the *valid\_methods* method checks all available correlations against their temperature limits.

```
>>> ethanol_psat.valid_methods(100)
['AMBROSE_WALTON', 'LEE_KESLER_PSAT', 'EDALAT', 'BOILING_CRITICAL', 'SANJARI']
```

If the temperature is not provided, all available methods are returned; the returned value favors the methods by the ranking defined in thermo, with the currently selected method as the first item.

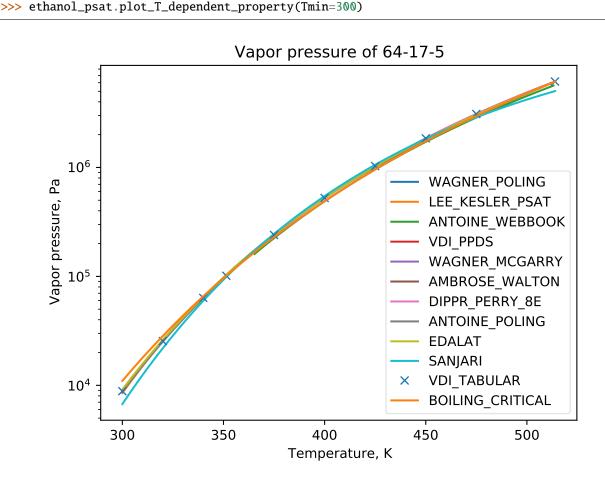
```
>>> ethanol_psat.valid_methods()
['WAGNER_MCGARRY', 'WAGNER_POLING', 'DIPPR_PERRY_8E', 'VDI_PPDS', 'COOLPROP', 'ANTOINE_

→POLING', 'VDI_TABULAR', 'AMBROSE_WALTON', 'LEE_KESLER_PSAT', 'EDALAT', 'BOILING_

→CRITICAL', 'SANJARI']
```

### 3.1.5 Plotting

It is also possible to compare the correlations graphically with the method *plot\_T\_dependent\_property*.



By default all methods are shown in the plot, but a smaller selection of methods can be specified. The following example compares 30 points in the temperature range 400 K to 500 K, with three of the best methods.

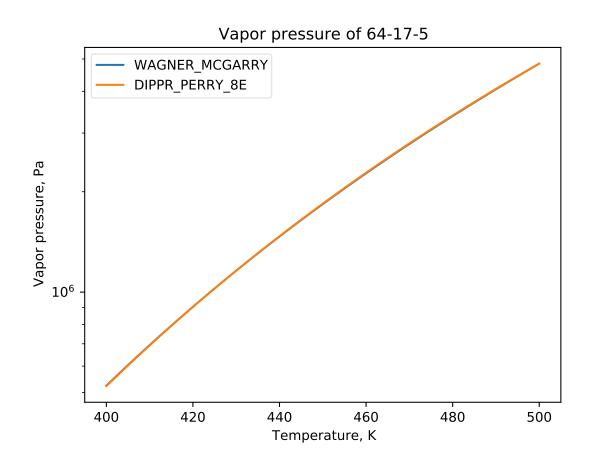
It is also possible to plot the nth derivative of the methods with the *order* parameter. The following plot shows the first derivative of vapor pressure of three estimation methods, a tabular source being interpolated, and 'DIPPR\_PERRY\_8E' as a reference method.

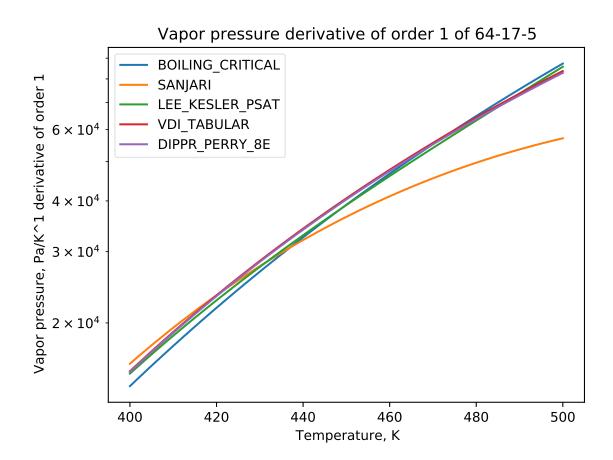
```
>>> ethanol_psat.plot_T_dependent_property(Tmin=400, Tmax=500, methods=['BOILING_CRITICAL

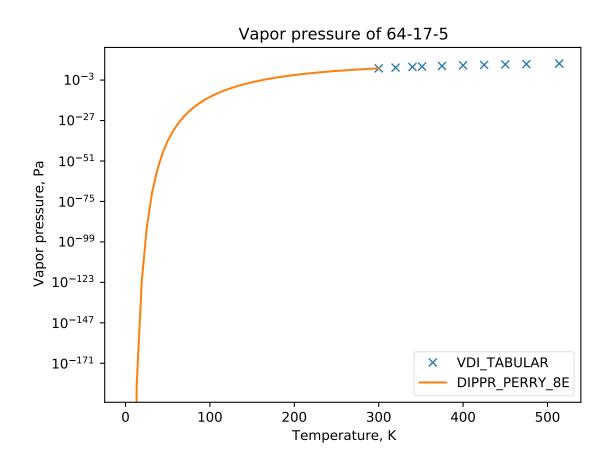
..., 'SANJARI', 'LEE_KESLER_PSAT', 'VDI_TABULAR', 'DIPPR_PERRY_8E'], pts=50, order=1)
```

Plots show how the extrapolation methods work. By default plots do not show extrapolated values from methods, but this can be forced by setting *only\_valid* to False. It is easy to see that extrapolation is designed to show the correct trend, but that individual methods will have very different extrapolations.

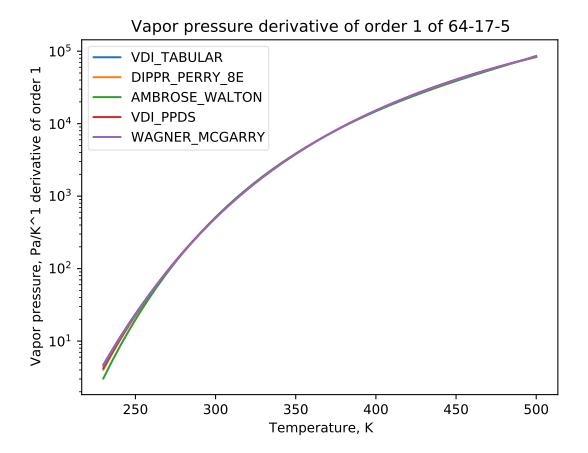
>>> ethanol\_psat.plot\_T\_dependent\_property(Tmin=1, Tmax=300, methods=['VDI\_TABULAR', \_\_\_'DIPPR\_PERRY\_8E', 'COOLPROP'], pts=50, only\_valid=False)







It may also be helpful to see the derivative with respect to temperature of methods. This can be done with the *order* keyword:



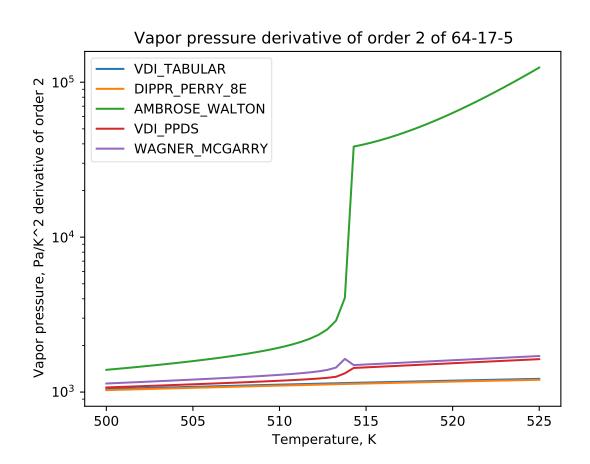
Higher order derivatives are also supported; most derivatives are numerically calculated, so there may be some noise. The derivative plot is particularly good at illustrating what happens at the critical point, when extrapolation takes over from the actual formulas.

### 3.1.6 Calculating Temperature From Properties

There is also functionality for reversing the calculation - finding out which temperature produces a specific property value. The method is *solve\_property*. For vapor pressure, we can use this technique to find out the normal boiling point as follows:

```
>>> ethanol_psat.solve_property(101325)
351.43136
```

The experimentally reported value is 351.39 K.



### 3.1.7 Property Derivatives

Functionality for calculating the derivative of the property is also implemented as *T\_dependent\_property\_derivative*:

```
>>> ethanol_psat.T_dependent_property_derivative(300)
498.882
```

The derivatives are numerical unless a special implementation has been added to the property's *calculate\_derivative* method.

Higher order derivatives are available as well with the *order* argument. All higher-order derivatives are numerical, and they tend to have reduced numerical precision due to floating point limitations.

```
>>> ethanol_psat.T_dependent_property_derivative(300.0, order=2)
24.74
>>> ethanol_psat.T_dependent_property_derivative(300.0, order=3)
2.75
```

### **3.1.8 Property Integrals**

Functionality for integrating over a property is implemented as T\_dependent\_property\_integral.

integral = 
$$\int_{T_1}^{T_2}$$
 property  $dT$ 

When the property is heat capacity, this calculation represents a change in enthalpy:

$$\Delta H = \int_{T_1}^{T_2} C_p \ dT$$

```
>>> CH4_Cp = HeatCapacityGas(CASRN='74-82-8')
>>> CH4_Cp.method = 'POLING_POLY'
>>> CH4_Cp.T_dependent_property_integral(300, 500)
8158.64
```

Besides enthalpy, a commonly used integral is that of the property divided by *T*:

integral = 
$$\int_{T_1}^{T_2} \frac{\text{property}}{T} dT$$

When the property is heat capacity, this calculation represents a change in entropy:

$$\Delta S = \int_{T_1}^{T_2} \frac{C_p}{T} \, dT$$

This integral, property over T, is implemented as *T\_dependent\_property\_integral\_over\_T* :

```
>>> CH4_Cp.T_dependent_property_integral_over_T(300, 500)
20.6088
```

Where speed has been important so far, these integrals have been implemented analytically in a property object's *calculate\_integral* and *calculate\_integral\_over\_T* method; otherwise the integration is performed numerically.

### 3.1.9 Using Tabular Data

A common scenario is that there are no correlations available for a compound, and that estimation methods are not applicable. However, there may be a few experimental data points available in the literature. In this case, the data can be specified and used directly with the *add\_tabular\_data* method. Extrapolation can often show the correct trends for these properties from even a few data points.

In the example below, we take 5 data points on the vapor pressure of water from 300 K to 350 K, and use them to extrapolate and estimate the triple temperature and critical temperature (assuming we know the triple and critical pressures).

The experimental values are 273.15 K and 647.14 K.

### 3.1.10 Adding New Methods

While a great many property methods have been implemented, there is always the case where a new one must be added. To support that, the method *add\_method* will add a user-specified method and switch the method selected to the newly added method.

As an example, we can compare the default vapor pressure formulation for n-hexane against a set of Antoine coefficients on the NIST WebBook.

```
>>> from chemicals import *
>>> from thermo import *
>>> obj = VaporPressure(CASRN= '110-54-3')
>>> obj(200)
20.742
>>> f = lambda T: Antoine(T=T, A=3.45604+5, B=1044.038, C=-53.893)
>>> obj.add_method(f=f, name='WebBook', Tmin=177.70, Tmax=264.93)
>>> obj.method
'WebBook'
>>> obj.extrapolation = 'AntoineAB'
>>> obj(200.0)
20.432
```

We can, again, extrapolate quite easily and estimate the triple temperature and critical temperature from these correlations (if we know the triple pressure and critical pressure).

```
>>> obj.solve_property(1.378), obj.solve_property(3025000.0)
(179.43, 508.04)
```

Optionally, some derivatives and integrals can be provided for new methods as well. This avoids having to compute derivatives or integrals numerically. SymPy may be helpful to find these analytical derivatives or integrals in many cases, as in the following example:

Note that adding methods like this breaks the ability to export as json and the repr of the object is no longer complete.

# 3.1.11 Adding New Correlation Coefficient Methods

While adding entirely new methods is useful, it is more common to want to use different coefficients in an existing equation. A number of different equations are recognized, and accept/require the parameters as per their function name in e.g. chemicals.vapor\_pressure.Antoine. More than one set of coefficients can be added for each model. After adding a new correlation the method is set to that method.

```
>>> obj = VaporPressure()
>>> obj.add_correlation(name='WebBook', model='Antoine', Tmin=177.70, Tmax=264.93, A=3.
...45604+5, B=1044.038, C=-53.893)
>>> obj(200)
20.43298036711
```

It is also possible to specify the parameters in the constructor of the object as well:

```
>>> obj = VaporPressure(Antoine_parameters={'WebBook': {'A': 8.45604, 'B': 1044.038, 'C':

→ -53.893, 'Tmin': 177.7, 'Tmax': 264.93}})
>>> obj(200)
20.43298036711
```

More than one set of parameters and more than one model may be specified this way; the model name is the same, with '\_parameters' appended to it.

For a full list of supported correlations (and their names), see add\_correlation.

# 3.1.12 Fitting Correlation Coefficients

Thermo contains functionality for performing regression to obtain equation coefficients from experimental data.

Data is obtained from the DDBST for the vapor pressure of acetone (http://www.ddbst.com/en/EED/PCP/VAP\_C4. php), and coefficients are regressed for several methods. There is data from five sources on that page, but no uncertainties are available; the fit will treat each data point equally.

```
>>> Ts = [203.65, 209.55, 212.45, 234.05, 237.04, 243.25, 249.35, 253.34, 257.25, 262.12,

→ 264.5, 267.05, 268.95, 269.74, 272.95, 273.46, 275.97, 276.61, 277.23, 282.03, 283.06,

→ 288.94, 291.49, 293.15, 293.15, 293.85, 294.25, 294.45, 294.6, 294.63, 294.85, 297.05,

→ 297.45, 298.15, 298.15, 298.15, 298.15, 298.15, 299.86, 300.75, 301.35, 303.15, 303.

→ 15, 304.35, 304.85, 305.45, 306.25, 308.15, 308.15, 308.15, 308.22, 308.35, 308.45,

→ 308.85, 309.05, 311.65, 311.85, 311.85, 311.95, 312.25, 314.68, 314.85, 349ntines of 10×1 80×2

→ 318.05, 318.15, 318.66, 320.35, 320.35, 320.45, 320.65, 322.55, 322.65, 322.85, 322.

→ 327.25, 327.25, 324.65, 324.75, 328.85, 333.73, 338.95]
```

(continued from previous page)

The fitting function returns the regressed coefficients, and optionally some statistics. The mean absolute relative error or "MAE" is often a good parameter for determining the goodness of fit; Antoine yielded an error of about 1%.

There are lots of methods available; Antoine was just used (the returned coefficients are in units of K and Pa with a base of 10), but for comparison several more are as well. Note that some require the critical temperature and/or pressure.

```
>>> Tc, Pc = 508.1, 4700000.0
>>> res, stats = TDependentProperty.fit_data_to_model(Ts=Ts, data=Psats, model='Yaws_Psat

→', do_statistics=True, multiple_tries=True)

>>> res, stats['MAE']
({'A': 1650.7, 'B': -32673., 'C': -728.7, 'D': 1.1, 'E': -0.000609}, 0.0178)
>>> res, stats = TDependentProperty.fit_data_to_model(Ts=Ts, data=Psats, model='DIPPR101

→', do_statistics=True, multiple_tries=3)

>>> stats['MAE']
0.0106
>>> res, stats = TDependentProperty.fit_data_to_model(Ts=Ts, data=Psats, model='Wagner',_
→do_statistics=True, multiple_tries=True, model_kwargs={'Tc': Tc, 'Pc': Pc})
>>> res, stats['MAE']
({'Tc': 508.1, 'Pc': 4700000.0, 'a': -15.7110, 'b': 23.63, 'c': -27.74, 'd': 25.152}, 0.
→0485)
>>> res, stats = TDependentProperty.fit_data_to_model(Ts=Ts, data=Psats, model='TRC_
→Antoine_extended', do_statistics=True, multiple_tries=True, model_kwargs={'Tc': Tc})
>>> res, stats['MAE']
({'Tc': 508.1, 'to': 67.0, 'A': 9.2515481, 'B': 1230.0976, 'C': -40.080954, 'n': 2.5, 'E
→': 333.0, 'F': -24950.0}, 0.01059)
```

A very common scenario is that some coefficients are desired to be fixed in the regression. This is supported with the *model\_kwargs* attribute. For example, in the above DIPPR101 case we can fix the *E* coefficient to 1 as follows:

Similarly, the feature is often used to set unneeded coefficients to zero In this case the TDE\_PVExpansion function has up to 8 parameters but only three are justified.

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Fitting coefficients is a complicated numerical problem. MINPACK's lmfit implements Levenberg-Marquardt with a number of tricks, and is used through SciPy in the fitting by default. Other minimization algorithms are supported, but generally don't do nearly as well. All minimization algorithms can only converge to a minima near points that they evaluate, and the choice of initial guesses is quite important. For many methods, there are several hardcoded guesses. By default, each of those guesses are evaluated and the minimization is initialized with the best guess. However, for maximum accuracy, *multiple\_tries* should be set to True, and *all* initial guesses are converged, and the best fit is returned.

Initial guesses for parameters can also be provided. In the below example, the initial parameters from http://ddbonline. ddbst.com/AntoineCalculation/AntoineCalculationCGI.exe for acetone are provided as initial guesses (converting them to a Pa and K basis, from mmHg and deg C).

In this case the initial guesses are good, but different parameters are still obtained by the fitting algorithm.

To speed up these calculations, an interface to numba is available. Simply set *use\_numba* to True. Note that the first regression per session may be slower as it has to compile the function.

# 3.1.13 Adding New Correlation Coefficient Methods From Data

In the following example, data for the molar volume of three phases of liquid oxygen are added, from Roder, H. M. "The Molar Volume (Density) of Solid Oxygen in Equilibrium with Vapor." Journal of Physical and Chemical Reference Data 7, no. 3 (1978): 949–58.

Each of the phases is treated as a different method. After fitting the data to linear and quadratic fits, the results are plotted.

```
>>> Ts_alpha = [4.2, 10.0, 18.5, 20, 21, 22, 23.880]
>>> Vms_alpha = [20.75e-6, 20.75e-6, 20.75e-6, 20.75e-6, 20.75e-6, 20.78e-6, 20.82e-6]
>>> Ts_beta = [23.880, 24, 26, 28, 30, 32, 34, 36, 38, 40, 42, 43.801]
>>> Vms_beta = [20.95e-6, 20.95e-6, 21.02e-6, 21.08e-6, 21.16e-6, 21.24e-6, 21.33e-6, 21.
\u03c42e-6, 21.52e-6, 21.63e-6, 21.75e-6, 21.87e-6]
>>> Ts_gamma = [42.801, 44.0, 46.0, 48.0, 50.0, 52.0, 54.0, 54.361]
>>> Vms_gamma = [23.05e-6, 23.06e-6, 23.18e-6, 23.30e-6, 23.43e-6, 23.55e-6, 23.67e-6, \u03c4
\u03c42e-6]
```

```
>>> obj = VolumeSolid(CASRN='7782-44-7')
>>> obj.fit_add_model(Ts=Ts_alpha, data=Vms_alpha, model='linear', name='alpha')
>>> obj.fit_add_model(Ts=Ts_beta, data=Vms_beta, model='quadratic', name='beta')
>>> obj.fit_add_model(Ts=Ts_gamma, data=Vms_gamma, model='quadratic', name='gamma')
>>> obj.plot_T_dependent_property(Tmin=4.2, Tmax=50)
```

# 3.2 Temperature and Pressure Dependent Properties

The pressure dependent objects work much like the temperature dependent ones; in fact, they subclass *TDependentProperty*. They have many new methods that require pressure as an input however. They work in two parts: a low-pressure correlation component, and a high-pressure correlation component. The high-pressure component usually but not always requires a low-pressure calculation to be performed first as its input.

# 3.2.1 Creating Objects

All arguments and information the property object requires must be provided in the constructor of the object. If a piece of information is not provided, whichever methods require it will not be available for that object. Many pressuredependent property correlations are actually dependent on other properties being calculated first. A mapping of those dependencies is as follows:

- Liquid molar volume: Depends on VaporPressure
- · Gas viscosity: Depends on VolumeGas
- Liquid viscosity: Depends on VaporPressure
- Gas thermal conductivity: Depends on VolumeGas, HeatCapacityGas, ViscosityGas

The required input objects should be created first, and provided as an input to the dependent object:

Various data files will be searched to see if information such as DIPPR expression coefficients are available for the compound during the initialization. This behavior can be avoided by setting the optional *load\_data* argument to False.

# 3.2.2 Pressure-dependent Methods

The pressure and temperature dependent object selects a low-pressure and a high-pressure method automatically during initialization. These method can be inspected with the *method* and *method\_P* properties. If no low-pressure methods are available, *method* will be None. If no high-pressure methods are available, *method\_P* will be None. If no high-pressure methods are available, *method\_P* will be None. *method* and *method\_P* are also valid parameters when constructing the object, but if either of the methods specified is not available an exception will be raised.

```
>>> water_mu.method, water_mu.method_P
('DIPPR_PERRY_8E', 'LUCAS')
```

All available low-pressure methods can be found by inspecting the all\_methods attribute:

```
>>> water_mu.all_methods
{'COOLPROP', 'DIPPR_PERRY_8E', 'VISWANATH_NATARAJAN_3', 'VDI_PPDS', 'LETSOU_STIEL'}
```

All available high-pressure methods can be found by inspecting the all\_methods\_P attribute:

```
>>> water_mu.all_methods_P
{'COOLPROP', 'LUCAS'}
```

Changing the low-pressure method or the high-pressure method is as easy as setting a new value to the attribute:

```
>>> water_mu.method = 'VDI_PPDS'
>>> water_mu.method
'VDI_PPDS'
>>> water_mu.method_P = 'COOLPROP'
>>> water_mu.method_P
'COOLPROP'
```

# 3.2.3 Calculating Properties

Calculation of the property at a specific temperature and pressure is as easy as calling the object which triggers the \_\_\_\_\_\_ method:

```
>>> water_mu.method = 'VDI_PPDS'
>>> water_mu.method_P = 'COOLPROP'
>>> water_mu(T=300.0, P=1e5)
0.000853742
```

This is actually a cached wrapper around the specific call, *TP\_dependent\_property*:

```
>>> water_mu.TP_dependent_property(300.0, P=1e5)
0.000853742
```

The caching of  $\_call\_$  is quite basic - the previously specified temperature and pressure are stored, and if the new *T* and *P* are the same as the previous *T* and *P* the previously calculated result is returned.

There is a lower-level interface for calculating properties with a specified method by name, calculate\_P. *TP\_dependent\_property* is a wrapper around calculate\_P that includes validation of the result.

```
>>> water_mu.calculate_P(T=300.0, P=1e5, method='COOLPROP')
0.000853742
>>> water_mu.calculate_P(T=300.0, P=1e5, method='LUCAS')
0.000865292
```

The above examples all show using calculating the property with a pressure specified. The same *TDependentProperty* methods are available too, so all the low-pressure calculation calls are also available.

```
>>> water_mu.calculate(T=300.0, method='VISWANATH_NATARAJAN_3')
0.000856467
>>> water_mu.T_dependent_property(T=400.0)
0.000217346
```

# 3.2.4 Limits and Extrapolation

The same temperature limits and low-pressure extrapolation methods are available as for *TDependentProperty*.

```
>>> water_mu.valid_methods(T=480)
['DIPPR_PERRY_8E', 'COOLPROP', 'VDI_PPDS', 'LETSOU_STIEL']
>>> water_mu.extrapolation
'linear'
```

To better understand what methods are available, the valid\_methods\_P method checks all available high-pressure correlations against their temperature and pressure limits.

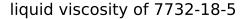
```
>>> water_mu.valid_methods_P(T=300, P=1e9)
['LUCAS', 'COOLPROP']
>>> water_mu.valid_methods_P(T=300, P=1e10)
['LUCAS']
>>> water_mu.valid_methods_P(T=900, P=1e6)
['LUCAS']
```

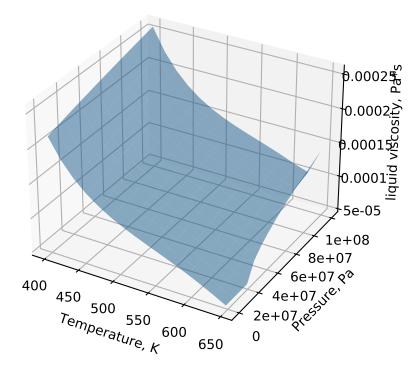
If the temperature and pressure are not provided, all available methods are returned; the returned value favors the methods by the ranking defined in thermo, with the currently selected method as the first item.

```
>>> water_mu.valid_methods_P()
['LUCAS', 'COOLPROP']
```

# 3.2.5 Plotting

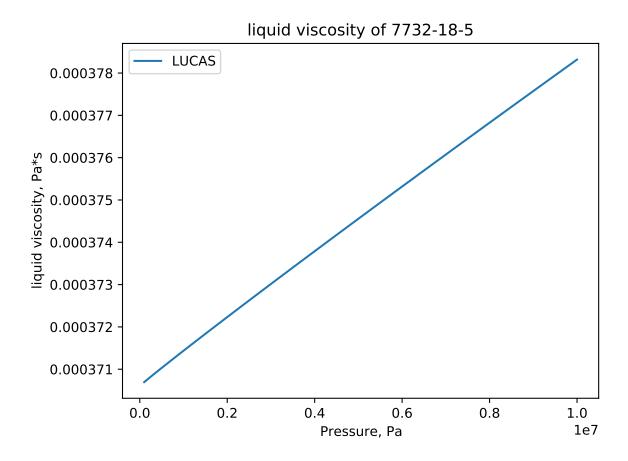
It is possible to compare the correlations graphically with the method *plot\_TP\_dependent\_property*.



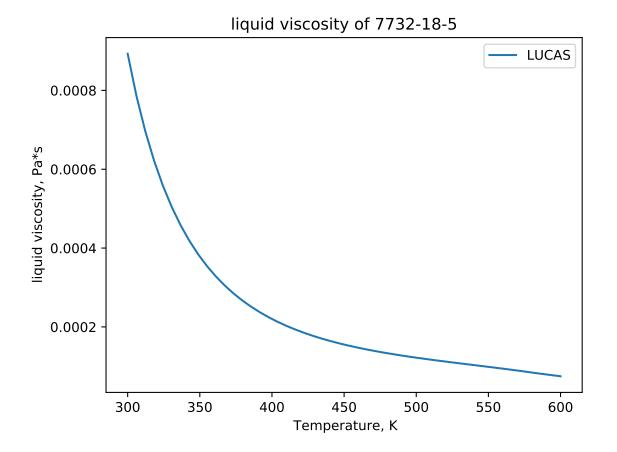


This can be a little confusing; but isotherms and isobars can be plotted as well, which are more straight forward. The respective methods are *plot\_isotherm* and *plot\_isobar*:

>>> water\_mu.plot\_isotherm(T=350, Pmin=1e5, Pmax=1e7, pts=50)



>>> water\_mu.plot\_isobar(P=1e7, Tmin=300, Tmax=600, pts=50)



## 3.2.6 Calculating Conditions From Properties

The method is *solve\_property* works only on the low-pressure correlations.

```
>>> water_mu.solve_property(1e-3)
294.0711641
```

# 3.2.7 Property Derivatives

Functionality for calculating the temperature derivative of the property is implemented twice; *T\_dependent\_property\_derivative* using the low-pressure correlations, and as as TP\_dependent\_property\_derivative\_T using the high-pressure correlations that require pressure as an input.

```
>>> water_mu.T_dependent_property_derivative(300)
-1.893961e-05
>>> water_mu.TP_dependent_property_derivative_T(300, P=1e7)
-1.927268e-05
```

The derivatives are numerical unless a special implementation has been added to the property's *calculate\_derivative\_T* and/or *calculate\_derivative* method.

Higher order derivatives are available as well with the order argument.

```
>>> water_mu.T_dependent_property_derivative(300.0, order=2)
5.923372e-07
>>> water_mu.TP_dependent_property_derivative_T(300.0, P=1e6, order=2)
-1.40946e-06
```

Functionality for calculating the pressure derivative of the property is also implemented as *TP\_dependent\_property\_derivative\_P*:

```
>>> water_mu.TP_dependent_property_derivative_P(P=5e7, T=400)
4.27782809e-13
```

The derivatives are numerical unless a special implementation has been added to the property's *calculate\_derivative\_P* method.

Higher order derivatives are available as well with the order argument.

```
>>> water_mu.TP_dependent_property_derivative_P(P=5e7, T=400, order=2)
-1.1858461e-15
```

## 3.2.8 Property Integrals

The same functionality for integrating over a property as in temperature-dependent objects is available, but only for integrating over temperature using low pressure correlations. No other use cases have been identified requiring integration over high-pressure conditions, or integration over the pressure domain.

```
>>> water_mu.T_dependent_property_integral(300, 400) # Integrating over viscosity has no_

→physical meaning

0.04243
```

## 3.2.9 Using Tabular Data

If there are experimentally available data for a property at high and low pressure, an interpolation table can be created and used as follows. The CoolProp method is used to generate a small table, and is then added as a new method in the example below.

```
>>> from thermo import *
>>> import numpy as np
>>> Ts = [300, 400, 500]
>>> Ps = [1e5, 1e6, 1e7]
>>> table = [[water_mu.calculate_P(T, P, "COOLPROP") for T in Ts] for P in Ps]
>>> water_mu.method_P
'LUCAS'
>>> water_mu.add_tabular_data_P(Ts, Ps, table)
>>> water_mu.method_P
'Tabular data series #0'
>>> water_mu(400, 1e7), water_mu.calculate_P(400, 1e7, "COOLPROP")
(0.000221166933349, 0.000221166933349)
>>> water_mu(450, 5e6), water_mu.calculate_P(450, 5e6, "COOLPROP")
(0.00011340, 0.00015423)
```

The more data points used, the closer a property will match.

# **3.3 Mixture Properties**

# 3.4 Notes

There is also the challenge that there is no clear criteria for distinguishing liquids from gases in supercritical mixtures. If the same method is not used for liquids and gases, there will be a sudden discontinuity which can cause numerical issues in modeling.

# CHAPTER

FOUR

# INTRODUCTION TO CHEMICALCONSTANTSPACKAGE AND PROPERTYCORRELATIONSPACKAGE

- ChemicalConstantsPackage Object
  - Creating ChemicalConstantsPackage Objects
  - Using ChemicalConstantsPackage Objects
  - Creating Smaller ChemicalConstantsPackage Objects
  - Adding or Replacing Constants
  - Creating ChemicalConstantsPackage Objects from chemicals
  - Storing and Loading ChemicalConstantsPackage Objects
- PropertyCorrelationsPackage

These two objects are designed to contain information needed by flash algorithms. In the first iteration of thermo, data was automatically looked up in databases and there was no way to replace that data. Thermo now keeps data and algorithms completely separate. This has also been very helpful to make unit tests that do not change their results.

There are five places to configure the flash and phase infrastructure:

- Constant data about chemicals, like melting point or boiling point or UNIFAC groups. This information needs to be put into an immutable *ChemicalConstantsPackage* object.
- Temperature-dependent data, like Antoine coefficients, Tait pressure-dependent volume parameters, or Laliberte electrolyte viscosity interaction parameters. These are stored in *TDependentProperty*, *TPDependentProperty*, and *MixtureProperty* objects. More information about configuring those to provide the desired properties can be found in property objects tutorial; this tutorial assumes you have already configured them as desired. These many objects are added to an *PropertyCorrelationsPackage* object before being provided to the flash algorithms.
- Phase-specific parameters that are not general and depend on a specific phase configuration for meaning; such as a volume translation coefficient or a binary interaction parameter. This information is provided when configuring each *Phase*.
- Information about bulk mixing rules or bulk property calculation methods; these don't have true thermodynamic definitions, and are configurable in the *BulkSettings* object.
- Settings of the *Flash* object; ideally no configuration would be required there. In some cases it might be useful to lower the tolerances or change an algorithm.

This tutorial covers the first two places, ChemicalConstantsPackage and PropertyCorrelationsPackage.

# 4.1 ChemicalConstantsPackage Object

# 4.1.1 Creating ChemicalConstantsPackage Objects

A *ChemicalConstantsPackage* can be created by specifying the known constant values of each chemical. All values are technically optional; the requirements of each *Flash* algorithm are different, but a minimum suggested amount is *names*, *CASs*, *MWs*, *Tcs*, *Pcs*, *omegas*, *Tbs*, and *atomss*. The list of all accepted properties can be found *here*.

# 4.1.2 Using ChemicalConstantsPackage Objects

Once created, all properties, even missing ones, can be accessed as attributes using the same names as required by the constructor:

```
>>> constants.MWs
[18.01528, 106.165, 106.165, 106.165]
>>> constants.Vml_STPs
[None, None, None, None]
```

It is the intention for these *ChemicalConstantsPackage* to be immutable. Python doesn't easily allow this to be enforced, but unexpected behavior will probably result if they are edited. If different properties are desired; create new *ChemicalConstantsPackage* objects.

The \_\_repr\_\_ of the *ChemicalConstantsPackage* object returns a representation of the object that can be used to reconstruct it:

```
>>> constants
ChemicalConstantsPackage(MWs=[18.01528, 106.165, 106.165, 106.165], names=['water', 'o-
→xylene', 'p-xylene', 'm-xylene'], omegas=[0.344, 0.3118, 0.324, 0.331], Pcs=[22048320.
→0, 3732000.0, 3511000.0, 3541000.0], Tcs=[647.14, 630.3, 616.2, 617.0])
>>> hash(eval(constants.__repr__())) == hash(constants)
True
```

# 4.1.3 Creating Smaller ChemicalConstantsPackage Objects

It is possible to create a new, smaller *ChemicalConstantsPackage* with fewer components by using the *subset* method, which accepts either indexes or slices and returns a new object:

(continued from previous page)

It is also possible to reduce the number of properties set with the *subset* methods:

```
>>> constants.subset([1, 3], properties=('names', 'MWs'))
ChemicalConstantsPackage(MWs=[106.165, 106.165], names=['o-xylene', 'm-xylene'])
```

# 4.1.4 Adding or Replacing Constants

It is possible to create a new *ChemicalConstantsPackage* with added properties and/or replacing the old properties, from an existing object. This is helpful if better values for select properties are known. The *with\_new\_constants* method does this.

```
>>> constants.with_new_constants(Tcs=[650.0, 630.0, 620.0, 620.0], Tms=[20.0, 100.0, 50.

→0, 12.3])
ChemicalConstantsPackage(MWs=[18.01528, 106.165, 106.165, 106.165], names=['water', 'o-

→xylene', 'p-xylene', 'm-xylene'], omegas=[0.344, 0.3118, 0.324, 0.331], Pcs=[22048320.

→0, 3732000.0, 3511000.0, 3541000.0], Tcs=[650.0, 630.0, 620.0, 620.0], Tms=[20.0, 100.

→0, 50.0, 12.3])
```

# 4.1.5 Creating ChemicalConstantsPackage Objects from chemicals

A convenience method exists to load these constants from a different data files exists. Some values for all properties are available; not all compounds have all properties.

When working with a fixed set of components, it may be a good idea to take this generated package, select only those properties being used, convert it to a string, and then embed that new object in a program. This will remove the need to load various data files, and if *chemicals* updates data files, different results won't be obtained from your constants package.

Once the object is printed, the generated text can be copy/pasted as valid Python into a program:

**Warning:** chemicals is a project with a focus on collecting data and correlations from various sources. In no way is it a project to critically evaluate these and provide recommendations. You are strongly encouraged to check values from it and modify them if you want different values. If you believe there is a value which has a typographical error please report it to the chemicals project. If data is missing or not as accurate as you would like, and you know of a better method or source, new methods and sources can be added to chemicals fairly easily once the data entry is complete. It is not feasible to add individual components, so please submit a complete table of data from the source.

# 4.1.6 Storing and Loading ChemicalConstantsPackage Objects

For larger applications with many components, it is not as feasible to convert the *ChemicalConstantsPackage* to a string and embed it in a program. For that application, the object can be converted back and forth from JSON:

```
>>> obj = ChemicalConstantsPackage(MWs=[106.165, 106.165], names=['o-xylene', 'm-xylene

__'])
>>> constants = ChemicalConstantsPackage(MWs=[18.01528, 106.165], names=['water', 'm-

__xylene'])
>>> string = constants.as_json()
>>> new_constants = ChemicalConstantsPackage.from_json(string)
>>> hash(new_constants) == hash(constants)
True
```

# 4.2 PropertyCorrelationsPackage

# CHAPTER

# INTRODUCTION TO PHASE AND FLASH CALCULATIONS

- Phase Objects
  - Available Phases
  - Serialization
  - Hashing
- Flashes with Pure Compounds
  - Vapor-Liquid Cubic Equation Of State Example
  - Vapor-Liquid Steam Example

The framework for performing phase and flash calculations is designed around the following principles:

- Immutability
- · Calculations are completely independent from any databases or lookups every input must be provided as input
- · Default to general-purpose algorithms that make no assumptions about specific systems
- · Inclusion of separate flashes algorithms wherever faster algorithms can be used for specific cases
- Allow options to restart a flash from a nearby previously calculated result, with options to skip checking the result for stability
- · Use very tight tolerances on all calculations
- Expose all constants used by algorithms

# 5.1 Phase Objects

A phase is designed to have a single state at any time, and contain all the information needed to compute phase-specific properties. Phases should always be initialized at a specific molar composition zs, T and P; and new phase objects at different conditions should be created from the existing ones with the *Phase.to* method (a little faster than creating them from scratch). That method also allows the new state to be set from any two of T, P, or V. When working in the T and P domain only, the *Phase.to\_TP\_zs* method is a little faster.

Phases are designed to be able to calculate every thermodynamic property. *T* and *P* are always attributes of the phase, but all other properties are functions that need to be called. Some examples of these properties are *V*, *H*, *S*, *Cp*,  $dP_dT$ ,  $d2P_dV2$ , fugacities, lnphis, dlnphis\_dT, and dlnphis\_dP.

If a system is already known to be single-phase, the phase framework can be used directly without performing flash calculations. This may offer a speed boost in some applications.

# 5.1.1 Available Phases

Although the underlying equations of state often don't distinguish between liquid or vapor phase, it was convenient to create separate phase objects designed to hold gas, liquid, and solid phases separately.

The following phases can represent both a liquid and a vapor state. Their class is not a true indication that their properties are liquid or gas.

- Cubic equations of state CEOSLiquid and CEOSGas
- IAPWS-95 Water and Steam IAPWS95Liquid and IAPWS95Gas
- Wrapper objects for CoolProp's Helmholtz EOSs CoolPropLiquid and CoolPropGas

The following phase objects can only represent a gas phase:

- Ideal-gas law IdealGas
- High-accuracy properties of dry air DryAirLemmon

The following phase objects can only represent a liquid phase:

• Ideal-liquid and/or activity coefficient models - GibbsExcessLiquid

# 5.1.2 Serialization

All phase models offer a *as\_json* method and a *from\_json* to serialize the object state for transport over a network, storing to disk, and passing data between processes.

```
>>> import json
>>> from scipy.constants import R
>>> from thermo import HeatCapacityGas, IdealGas, Phase
>>> HeatCapacityGases = [HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*-9.9e-13, R*1.57e-09,

\[imestrian] R*7e-08, R*-0.000261, R*3.539])), HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*1.79e-12,

\[imestrian] R*-6e-09, R*6.58e-06, R*-0.001794, R*3.63]))]
>>> phase = IdealGas(T=300, P=1e5, zs=[.79, .21], HeatCapacityGases=HeatCapacityGases)
>>> json_stuff = json.dumps(phase.as_json())
>>> new_phase = Phase.from_json(json.loads(json_stuff))
>>> assert new_phase == phase
```

Other json libraries can be used besides the standard json library by design.

Storing and recreating objects with Python's pickle.dumps library is also tested; this can be faster than using JSON at the cost of being binary data.

# 5.1.3 Hashing

All models have a <u>hash</u> method that can be used to compare different phases to see if they are absolutely identical (including which values have been calculated already).

They also have a *model\_hash* method that can be used to compare different phases to see if they have identical model parameters.

They also have a *state\_hash* method that can be used to compare different phases to see if they have identical temperature, composition, and model parameters.

# 5.2 Flashes with Pure Compounds

Pure components are really nice to work with because they have nice boundaries between each state, and the mole fraction is always 1; there is no composition dependence. There is a separate flash interfaces for pure components. These flashes are very mature and should be quite reliable.

# 5.2.1 Vapor-Liquid Cubic Equation Of State Example

The following example illustrates some of the types of flashes supported using the component methanol, the stated critical properties, a heat capacity correlation from Poling et. al., and the Peng-Robinson equation of state.

Obtain a heat capacity object, and select a source:

```
>>> from thermo.heat_capacity import POLING_POLY
>>> CpObj = HeatCapacityGas(CASRN='67-56-1')
>>> CpObj.method = POLING_POLY
>>> CpObj.POLING_coefs # Show the coefficients
[4.714, -0.006986, 4.211e-05, -4.443e-08, 1.535e-11]
>>> HeatCapacityGases = [CpObj]
```

Create a *ChemicalConstantsPackage* object which holds constant properties of the object, using a minimum of values:

Create a *PropertyCorrelationsPackage* object which holds temperature-dependent property objects, also setting *skip\_missing* to True so no database lookups are performed:

Create liquid and gas cubic phase objects using the Peng-Robinson equation of state:

Create the Flash object *FlashPureVLS* for pure components:

>>> flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])

Do a T-P flash:

```
>>> res = flasher.flash(T=300, P=1e5)
>>> res.phase, res.liquid0
('L', CEOSLiquid(eos_class=PRMIX, eos_kwargs={"Tcs": [512.5], "Pcs": [8084000.0], "omegas
__": [0.559]}, HeatCapacityGases=[HeatCapacityGas(CASRN="67-56-1", extrapolation="linear
__", method="POLING_POLY")], T=300.0, P=100000.0, zs=[1.0]))
```

Do a temperature and vapor-fraction flash:

>>> res = flasher.flash(T=300, VF=.3)

Do a pressure and vapor-fraction flash:

>>> res = flasher.flash(P=1e5, VF=.5)

Do a pressure and enthalpy flash:

>>> res = flasher.flash(P=1e5, H=100)

Do a pressure and entropy flash:

>>> res = flasher.flash(P=1e5, S=30)

Do a temperature and entropy flash:

>>> res = flasher.flash(T=400.0, S=30)

Do a temperature and enthalpy flash:

>>> res = flasher.flash(T=400.0, H=1000)

Do a volume and internal energy flash:

>>> res = flasher.flash(V=1e-4, U=1000)

As you can see, the interface is convenient and supports most types of flashes. In fact, the algorithms are generic; any of H, S, U, and can be combined with any combination of T, P, and V. Although most of the flashes shown above except TS and TH are usually well behaved, depending on the EOS combination there may be multiple solutions. No real guarantees can be made about which solution will be returned in those cases.

Flashes with two of H, S, and U are not implemented at present.

It is not necessary to use the same phase model for liquid and gas phases; the below example shows a flash switching the gas phase model to SRK.

Choosing to use an inconsistent model will slow down many calculations as more checks are required; and some flashes may have issues with discontinuities in some conditions, and simply a lack of solution in other conditions.

# 5.2.2 Vapor-Liquid Steam Example

The IAPWS-95 standard is implemented and available for easy use:

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(continued from previous page)

Not all flash calculations have been fully optimized, but the basic flashes are quite fast.

CHAPTER

SIX

# DETAILS OF GIBBSEXCESSLIQUID PHASE MODEL

There are lots of options that get called "ideal". The GibbsExcessLiquid object implements many of them, which means the configuration is complicated and the defaults may not act as expected.

# CHAPTER

# **API REFERENCE**

# 7.1 Activity Coefficients (thermo.activity)

This module contains a base class *GibbsExcess* for handling activity coefficient based models. The design is for a sub-class to provide the minimum possible number of derivatives of Gibbs energy, and for this base class to provide the rest of the methods. An ideal-liquid class with no excess Gibbs energy *IdealSolution* is also available.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Base Class
- Ideal Liquid Class
- Notes
  - References

# 7.1.1 Base Class

### class thermo.activity.GibbsExcess

Bases: object

Class for representing an activity coefficient model. While these are typically presented as tools to compute activity coefficients, in truth they are excess Gibbs energy models and activity coefficients are just one derived aspect of them.

This class does not implement any activity coefficient models itself; it must be subclassed by another model. All properties are derived with the CAS SymPy, not relying on any derivations previously published, and checked numerically for consistency.

Different subclasses have different parameter requirements for initialization; *IdealSolution* is available as a simplest model with activity coefficients of 1 to show what needs to be implemented in subclasses. It is also intended subclasses implement the method  $to_T xs$ , which creates a new object at the specified temperature and composition but with the same parameters.

These objects are intended to lazy-calculate properties as much as possible, and for the temperature and composition of an object to be immutable. Methods

CpE()	Calculate and return the first temperature derivative
HE()	of excess enthalpy of a liquid phase using an activity
	coefficient model.
	Calculate and return the excess entropy of a liquid
	phase using an activity coefficient model.
SE()	Calculates the excess entropy of a liquid phase using
	an activity coefficient model.
as_json()	Method to create a JSON-friendly representation of
	the Gibbs Excess model which can be stored, and
	reloaded later.
d2GE_dTdns()	Calculate and return the mole number derivative of
	the first temperature derivative of excess Gibbs en-
	ergy of a liquid phase using an activity coefficient
	model.
d2nGE_dTdns()	Calculate and return the partial mole number deriva-
	tive of the first temperature derivative of excess Gibbs
	energy of a liquid phase using an activity coefficient
	model.
d2nGE_dninjs()	Calculate and return the second partial mole number
	derivative of excess Gibbs energy of a liquid phase
	using an activity coefficient model.
dGE_dns()	Calculate and return the mole number derivative of
adl_ano()	excess Gibbs energy of a liquid phase using an activ-
	ity coefficient model.
dHE_dT()	Calculate and return the first temperature derivative
	of excess enthalpy of a liquid phase using an activity
	coefficient model.
dHE_dns()	Calculate and return the mole number derivative of
une_uns()	
	excess enthalpy of a liquid phase using an activity co- efficient model.
dur de c	Calculate and return the mole fraction derivative of
dHE_dxs()	
	excess enthalpy of a liquid phase using an activity co-
	efficient model.
dSE_dT() dSE_dns()	Calculate and return the first temperature derivative
	of excess entropy of a liquid phase using an activity
	coefficient model.
	Calculate and return the mole number derivative of
	excess entropy of a liquid phase using an activity co-
	efficient model.
dSE_dxs()	Calculate and return the mole fraction derivative of
	excess entropy of a liquid phase using an activity co-
	efficient model.
dgammas_dT()	Calculate and return the temperature derivatives of
	activity coefficients of a liquid phase using an activity
	coefficient model.
dgammas_dns()	Calculate and return the mole number derivative of
	activity coefficients of a liquid phase using an activity
	coefficient model.

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Table 1 – continue	ed from previous page
dnGE_dns()	Calculate and return the partial mole number deriva-
	tive of excess Gibbs energy of a liquid phase using an
	activity coefficient model.
dnHE_dns()	Calculate and return the partial mole number deriva-
	tive of excess enthalpy of a liquid phase using an ac-
	tivity coefficient model.
dnSE_dns()	Calculate and return the partial mole number deriva-
	tive of excess entropy of a liquid phase using an ac-
	tivity coefficient model.
<pre>from_j son(json_repr)</pre>	Method to create a Gibbs Excess model from a JSON-
	friendly serialization of another Gibbs Excess model.
gammas()	Calculate and return the activity coefficients of a liq-
	uid phase using an activity coefficient model.
<pre>gammas_infinite_dilution()</pre>	Calculate and return the infinite dilution activity co-
	efficients of each component.
<pre>model_hash()</pre>	Basic method to calculate a hash of the non-state
	parts of the model This is useful for comparing to
	models to determine if they are the same, i.e. in a
	VLL flash it is important to know if both liquids have
	the same model.
<pre>state_hash()</pre>	Basic method to calculate a hash of the state of the
	model and its model parameters.

## CpE()

Calculate and return the first temperature derivative of excess enthalpy of a liquid phase using an activity coefficient model.

$$\frac{\partial h^E}{\partial T} = -T \frac{\partial^2 g^E}{\partial T^2}$$

Returns

dHE\_dT [float] First temperature derivative of excess enthalpy of the liquid phase, [J/mol/K]

## HE()

Calculate and return the excess entropy of a liquid phase using an activity coefficient model.

$$h^E = -T\frac{\partial g^E}{\partial T} + g^E$$

#### Returns

**HE** [float] Excess enthalpy of the liquid phase, [J/mol]

SE()

Calculates the excess entropy of a liquid phase using an activity coefficient model.

$$s^E = \frac{h^E - g^E}{T}$$

#### Returns

SE [float] Excess entropy of the liquid phase, [J/mol/K]

#### Notes

Note also the relationship of the expressions for partial excess entropy:

$$S_i^E = -R\left(T\frac{\partial\ln\gamma_i}{\partial T} + \ln\gamma_i\right)$$

**\_\_\_eq\_\_**(*other*)

Return self==value.

\_\_hash\_\_()

Method to calculate and return a hash representing the exact state of the object. This includes *T*, *xs*, the model class, and which values have already been calculated.

#### Returns

hash [int] Hash of the object, [-]

## \_\_repr\_\_()

Method to create a string representation of the state of the model. Included is T, xs, and all constants necessary to create the model. This can be passed into exec to re-create the model. Note that parsing strings like this can be slow.

#### Returns

repr [str] String representation of the object, [-]

### **Examples**

```
>>> IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
```

#### as\_json()

Method to create a JSON-friendly representation of the Gibbs Excess model which can be stored, and reloaded later.

#### Returns

json\_repr [dict] JSON-friendly representation, [-]

## **Examples**

```
>>> import json
>>> model = IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
>>> json_view = model.as_json()
>>> json_str = json.dumps(json_view)
>>> assert type(json_str) is str
>>> model_copy = IdealSolution.from_json(json.loads(json_str))
>>> assert model_copy == model
```

## d2GE\_dTdns()

Calculate and return the mole number derivative of the first temperature derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

 $\frac{\partial^2 G^E}{\partial n_i \partial T}$ 

### Returns

**d2GE\_dTdns** [list[float]] First mole number derivative of the temperature derivative of excess Gibbs entropy of the liquid phase, [J/(mol^2\*K)]

## d2nGE\_dTdns()

Calculate and return the partial mole number derivative of the first temperature derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial^2 n G^E}{\partial n_i \partial T}$$

## Returns

**d2nGE\_dTdns** [list[float]] First partial mole number derivative of the temperature derivative of excess Gibbs entropy of the liquid phase, [J/(mol\*K)]

#### d2nGE\_dninjs()

Calculate and return the second partial mole number derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial^2 n G^E}{\partial n_i \partial n_i}$$

#### Returns

**d2nGE\_dninjs** [list[list[float]]] Second partial mole number derivative of excess Gibbs energy of a liquid phase, [J/(mol^2)]

### dGE\_dns()

Calculate and return the mole number derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial G^E}{\partial n_i}$$

#### Returns

**dGE\_dns** [list[float]] First mole number derivative of excess Gibbs entropy of the liquid phase, [J/(mol^2\*K)]

## dHE\_dT()

Calculate and return the first temperature derivative of excess enthalpy of a liquid phase using an activity coefficient model.

$$\frac{\partial h^E}{\partial T} = -T \frac{\partial^2 g^E}{\partial T^2}$$

### Returns

**dHE\_dT** [float] First temperature derivative of excess enthalpy of the liquid phase, [J/mol/K]

### dHE\_dns()

Calculate and return the mole number derivative of excess enthalpy of a liquid phase using an activity coefficient model.

$$\frac{\partial h^E}{\partial n_i}$$

#### Returns

**dHE\_dns** [list[float]] First mole number derivative of excess enthalpy of the liquid phase, [J/mol^2]

## dHE\_dxs()

Calculate and return the mole fraction derivative of excess enthalpy of a liquid phase using an activity coefficient model.

$$\frac{\partial h^E}{\partial x_i} = -T \frac{\partial^2 g^E}{\partial T \partial x_i} + \frac{\partial g^E}{\partial x_i}$$

Returns

**dHE\_dxs** [list[float]] First mole fraction derivative of excess enthalpy of the liquid phase, [J/mol]

#### dSE\_dT()

Calculate and return the first temperature derivative of excess entropy of a liquid phase using an activity coefficient model.

$$\frac{\partial s^E}{\partial T} = \frac{1}{T} \left( \frac{-\partial g^E}{\partial T} + \frac{\partial h^E}{\partial T} - \frac{(G+H)}{T} \right)$$

#### Returns

**dSE\_dT** [float] First temperature derivative of excess entropy of the liquid phase, [J/mol/K]

## dSE\_dns()

Calculate and return the mole number derivative of excess entropy of a liquid phase using an activity coefficient model.

$$\frac{\partial S^E}{\partial n_i}$$

#### Returns

**dSE\_dns** [list[float]] First mole number derivative of excess entropy of the liquid phase, [J/(mol^2\*K)]

#### dSE\_dxs()

Calculate and return the mole fraction derivative of excess entropy of a liquid phase using an activity coefficient model.

$$\frac{\partial S^E}{\partial x_i} = \frac{1}{T} \left( \frac{\partial h^E}{\partial x_i} - \frac{\partial g^E}{\partial x_i} \right) = -\frac{\partial^2 g^E}{\partial x_i \partial T}$$

#### Returns

**dSE\_dxs** [list[float]] First mole fraction derivative of excess entropy of the liquid phase, [J/(mol\*K)]

## dgammas\_dT()

Calculate and return the temperature derivatives of activity coefficients of a liquid phase using an activity coefficient model.

$$\frac{\partial \gamma_i}{\partial T} = \left(\frac{\frac{\partial^2 n G^E}{\partial T \partial n_i}}{RT} - \frac{\frac{\partial n_i G^E}{\partial n_i}}{RT^2}\right) \exp\left(\frac{\frac{\partial n_i G^E}{\partial n_i}}{RT}\right)$$

Returns

dgammas\_dT [list[float]] Temperature derivatives of activity coefficients, [1/K]

## dgammas\_dns()

Calculate and return the mole number derivative of activity coefficients of a liquid phase using an activity coefficient model.

$$\frac{\partial \gamma_i}{\partial n_i} = \gamma_i \left( \frac{\frac{\partial^2 G^E}{\partial x_i \partial x_j}}{RT} \right)$$

### Returns

dgammas\_dns [list[float]]] Mole number derivatives of activity coefficients, [1/mol]

#### dnGE\_dns()

Calculate and return the partial mole number derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial n G^E}{\partial n_i}$$

#### Returns

**dnGE\_dns** [list[float]] First partial mole number derivative of excess Gibbs entropy of the liquid phase, [J/(mol)]

## dnHE\_dns()

Calculate and return the partial mole number derivative of excess enthalpy of a liquid phase using an activity coefficient model.

$$\frac{\partial nh^E}{\partial n_i}$$

#### Returns

**dnHE\_dns** [list[float]] First partial mole number derivative of excess enthalpy of the liquid phase, [J/mol]

## dnSE\_dns()

Calculate and return the partial mole number derivative of excess entropy of a liquid phase using an activity coefficient model.

$$\frac{\partial nS^E}{\partial n_i}$$

### Returns

**dnSE\_dns** [list[float]] First partial mole number derivative of excess entropy of the liquid phase, [J/(mol\*K)]

### classmethod from\_json(json\_repr)

Method to create a Gibbs Excess model from a JSON-friendly serialization of another Gibbs Excess model.

#### **Parameters**

json\_repr [dict] JSON-friendly representation, [-]

#### Returns

model [GibbsExcess] Newly created object from the json serialization, [-]

## Notes

It is important that the input string be in the same format as that created by *GibbsExcess.as\_json*.

#### **Examples**

```
>>> model = IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
>>> json_view = model.as_json()
>>> new_model = IdealSolution.from_json(json_view)
>>> assert model == new_model
```

#### gammas()

Calculate and return the activity coefficients of a liquid phase using an activity coefficient model.

$$\gamma_i = \exp\left(\frac{\frac{\partial n_i G^E}{\partial n_i}}{RT}\right)$$

#### Returns

gammas [list[float]] Activity coefficients, [-]

#### gammas\_infinite\_dilution()

Calculate and return the infinite dilution activity coefficients of each component.

#### Returns

gammas\_infinite [list[float]] Infinite dilution activity coefficients, [-]

#### Notes

The algorithm is as follows. For each component, set its composition to zero. Normalize the remaining compositions to 1. Create a new object with that composition, and calculate the activity coefficient of the component whose concentration was set to zero.

## model\_hash()

Basic method to calculate a hash of the non-state parts of the model This is useful for comparing to models to determine if they are the same, i.e. in a VLL flash it is important to know if both liquids have the same model.

Note that the hashes should only be compared on the same system running in the same process!

## Returns

model\_hash [int] Hash of the object's model parameters, [-]

#### state\_hash()

Basic method to calculate a hash of the state of the model and its model parameters.

Note that the hashes should only be compared on the same system running in the same process!

## Returns

state\_hash [int] Hash of the object's model parameters and state, [-]

# 7.1.2 Ideal Liquid Class

```
class thermo.activity.IdealSolution(T=None, xs=None)
```

Bases: thermo.activity.GibbsExcess

Class for representing an ideal liquid, with no excess gibbs energy and thus activity coefficients of 1.

## Parameters

- T [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]

## **Examples**

```
>>> model = IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
>>> model.GE()
0.0
>>> model.gammas()
[1.0, 1.0, 1.0, 1.0]
>>> model.dgammas_dT()
[0.0, 0.0, 0.0, 0.0]
```

## Attributes

**T** [float] Temperature, [K]

**xs** [list[float]] Mole fractions, [-]

## Methods

GE()	Calculate and return the excess Gibbs energy of a liq-
	uid phase using an activity coefficient model.
d2GE_dT2()	Calculate and return the second temperature deriva-
	tive of excess Gibbs energy of a liquid phase using an
	activity coefficient model.
d2GE_dTdxs()	Calculate and return the temperature derivative of
	mole fraction derivatives of excess Gibbs energy of
	an ideal liquid.
d2GE_dxixjs()	Calculate and return the second mole fraction deriva-
	tives of excess Gibbs energy of an ideal liquid.
d3GE_dT3()	Calculate and return the third temperature derivative
	of excess Gibbs energy of a liquid phase using an ac-
	tivity coefficient model.
d3GE_dxixjxks()	Calculate and return the third mole fraction deriva-
	tives of excess Gibbs energy of an ideal liquid.
dGE_dT()	Calculate and return the temperature derivative of ex-
	cess Gibbs energy of a liquid phase using an activity
	coefficient model.
dGE_dxs()	Calculate and return the mole fraction derivatives of
	excess Gibbs energy of an ideal liquid.
	continues on next page

continues on next page

Table 2 – continued from	n previous page
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<i>to_T_xs</i> (T, xs)	Method to construct a new IdealSolution instance
	at temperature T, and mole fractions xs with the same
	parameters as the existing object.

## **GE**()

Calculate and return the excess Gibbs energy of a liquid phase using an activity coefficient model.

$$g^E = 0$$

#### Returns

GE [float] Excess Gibbs energy of an ideal liquid, [J/mol]

## d2GE\_dT2()

Calculate and return the second temperature derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial^2 g^E}{\partial T^2} = 0$$

### Returns

**d2GE\_dT2** [float] Second temperature derivative of excess Gibbs energy of an ideal liquid, [J/(mol\*K^2)]

## d2GE\_dTdxs()

Calculate and return the temperature derivative of mole fraction derivatives of excess Gibbs energy of an ideal liquid.

$$\frac{\partial^2 g^E}{\partial x_i \partial T} = 0$$

## Returns

**d2GE\_dTdxs** [list[float]] Temperature derivative of mole fraction derivatives of excess Gibbs energy of an ideal liquid, [J/(mol\*K)]

## d2GE\_dxixjs()

Calculate and return the second mole fraction derivatives of excess Gibbs energy of an ideal liquid.

$$\frac{\partial^2 g^E}{\partial x_i \partial x_j} = 0$$

#### Returns

**d2GE\_dxixjs** [list[list[float]]] Second mole fraction derivatives of excess Gibbs energy of an ideal liquid, [J/mol]

## d3GE\_dT3()

Calculate and return the third temperature derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial^3 g^E}{\partial T^3}=0$$

#### Returns

**d3GE\_dT3** [float] Third temperature derivative of excess Gibbs energy of an ideal liquid, [J/(mol\*K^3)]

## d3GE\_dxixjxks()

Calculate and return the third mole fraction derivatives of excess Gibbs energy of an ideal liquid.

$$\frac{\partial^3 g^E}{\partial x_i \partial x_j \partial x_k} = 0$$

### Returns

**d3GE\_dxixjxks** [list[list[list[float]]]] Third mole fraction derivatives of excess Gibbs energy of an ideal liquid, [J/mol]

### dGE\_dT()

Calculate and return the temperature derivative of excess Gibbs energy of a liquid phase using an activity coefficient model.

$$\frac{\partial g^E}{\partial T} = 0$$

#### Returns

**dGE\_dT** [float] First temperature derivative of excess Gibbs energy of an ideal liquid, [J/(mol\*K)]

## dGE\_dxs()

Calculate and return the mole fraction derivatives of excess Gibbs energy of an ideal liquid.

$$\frac{\partial g^E}{\partial x_i} = 0$$

#### Returns

**dGE\_dxs** [list[float]] Mole fraction derivatives of excess Gibbs energy of an ideal liquid, [J/mol]

## $to_T_xs(T, xs)$

Method to construct a new *IdealSolution* instance at temperature *T*, and mole fractions *xs* with the same parameters as the existing object.

## Parameters

T [float] Temperature, [K]

xs [list[float]] Mole fractions of each component, [-]

#### Returns

obj [IdealSolution] New IdealSolution object at the specified conditions [-]

#### **Examples**

```
>>> p = IdealSolution(T=300.0, xs=[.1, .2, .3, .4])
>>> p.to_T_xs(T=500.0, xs=[.25, .25, .25, .25])
IdealSolution(T=500.0, xs=[0.25, 0.25, 0.25, 0.25])
```

# 7.1.3 Notes

Excellent references for working with activity coefficient models are [1] and [2].

## References

# 7.2 Bulk Phases (thermo.bulk)

This module contains a phase wrapper for obtaining properties of a pseudo-phase made of multiple other phases. This is useful in the context of multiple liquid phases; or multiple solid phases; or looking at all the phases together.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Bulk Class
- Bulk Settings Class

# 7.2.1 Bulk Class

class thermo.bulk.Bulk(T, P, zs, phases, phase\_fractions, phase\_bulk=None)
Bases: thermo.phases.phase.Phase

Class to encapsulate multiple *Phase* objects and provide a unified interface for obtaining properties from a group of phases.

This class exists for three purposes:

- Providing a common interface for obtaining properties like Cp whether there is one phase or 100, calling Cp on the bulk will retrieve that value.
- Retrieving "bulk" properties that do make sense to be calculated for a combination of phases together.
- Allowing configurable estimations of non-bulk properties like isothermal compressibility or speed of sound for the group of phases together.

### Parameters

- T [float] Temperature of the bulk, [K]
- **P** [float] Pressure of the bulk, [Pa]
- zs [list[float]] Mole fractions of the bulk, [-]
- phases [list[Phase]] Phase objects, [-]
- phase\_fractions [list[float]] Molar fractions of each phase, [-]
- **phase\_bulk** [str, optional] None to represent a bulk of all present phases; 'l' to represent a bulk of only liquid phases; *s* to represent a bulk of only solid phases, [-]

# Notes

Please think carefully when retrieving a property of the bulk. If there are two liquid phases in a bulk, and a single viscosity value is retrieved, can that be used directly for a single phase pressure drop calculation? Not with any theoretical consistency, that's for sure.

# Attributes

beta Phase fraction of the bulk phase.

betas\_mass Method to calculate and return the mass fraction of all of the phases in the bulk.

**betas\_volume** Method to calculate and return the volume fraction of all of the phases in the bulk.

# Methods

<i>Cp(</i> )	Method to calculate and return the constant-
	temperature and constant phase-fraction heat
	capacity of the bulk phase.
Cp_ideal_gas()	Method to calculate and return the ideal-gas heat ca-
	pacity of the phase.
Н()	Method to calculate and return the constant-
	temperature and constant phase-fraction enthalpy of
	the bulk phase.
H_ideal_gas()	Method to calculate and return the ideal-gas enthalpy
	of the phase.
H_reactive()	Method to calculate and return the constant-
	temperature and constant phase-fraction reactive
	enthalpy of the bulk phase.
Joule_Thomson()	Method to calculate and return the Joule-Thomson
	coefficient of the bulk according to the selected cal-
	culation methodology.
MW()	Method to calculate and return the molecular weight
	of the bulk phase.
Pmc()	Method to calculate and return the mechanical criti-
	cal pressure of the phase.
S()	Method to calculate and return the constant-
	temperature and constant phase-fraction entropy of
	the bulk phase.
S_ideal_gas()	Method to calculate and return the ideal-gas entropy
	of the phase.
S_reactive()	Method to calculate and return the constant-
	temperature and constant phase-fraction reactive
	entropy of the bulk phase.
Tmc()	Method to calculate and return the mechanical criti-
	cal temperature of the phase.
V()	Method to calculate and return the molar volume of
	the bulk phase.
V_iter([force])	Method to calculate and return the molar volume of
	the bulk phase, with precision suitable for a $TV$ cal-
	culation to calculate a matching pressure.

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Vmc()	3 – continued from previous page Method to calculate and return the mechanical criti
Fine()	cal volume of the phase.
Zmc()	Method to calculate and return the mechanical criti
Zinc()	cal compressibility of the phase.
42D 4T2()	Method to calculate and return the second tempera
d2P_dT2()	
	ture derivative of pressure of the bulk according to the selected calculation methodology.
dop dro fragen()	Method to calculate and return the second constant
d2P_dT2_frozen()	
	volume derivative of pressure with respect to temper
	ature of the bulk phase, at constant phase fraction
	and phase compositions.
d2P_dTdV()	Method to calculate and return the second deriva
	tive of pressure with respect to temperature and vo
	ume of the bulk according to the selected calculatio
	methodology.
d2P_dTdV_frozen()	Method to calculate and return the second derivativ
	of pressure with respect to volume and temperature of
	the bulk phase, at constant phase fractions and phas
	compositions.
d2P_dV2()	Method to calculate and return the second volum
	derivative of pressure of the bulk according to the se
	lected calculation methodology.
d2P_dV2_frozen()	Method to calculate and return the constant
	temperature second derivative of pressure wit
	respect to volume of the bulk phase, at constar
	phase fractions and phase compositions.
$dA_dP()$	Method to calculate and return the constant
	temperature pressure derivative of Helmholt
	energy.
$dA_dT()$	Method to calculate and return the constant-pressur
	temperature derivative of Helmholtz energy.
dG_dP()	Method to calculate and return the constan
	temperature pressure derivative of Gibbs fre
	energy.
dG_dT()	Method to calculate and return the constant-pressur
	temperature derivative of Gibbs free energy.
$dP_dT()$	Method to calculate and return the first temperatur
	derivative of pressure of the bulk according to the se
	lected calculation methodology.
dP_dT_frozen()	Method to calculate and return the constant-volum
	derivative of pressure with respect to temperature of
	the bulk phase, at constant phase fractions and phas
	compositions.
$dP_dV()$	Method to calculate and return the first volum
	derivative of pressure of the bulk according to the se
	lected calculation methodology.
dP_dV_frozen()	Method to calculate and return the constant
	temperature derivative of pressure with respect t
	volume of the bulk phase, at constant phase fraction
	and phase compositions.
	continues on next pag

Table 3 – continued from previous page		
$dU_dP()$	Method to calculate and return the constant-	
	temperature pressure derivative of internal energy.	
dU_dT()	Method to calculate and return the constant-pressure	
	temperature derivative of internal energy.	
<pre>isobaric_expansion()</pre>	Method to calculate and return the isobatic expansion	
	coefficient of the bulk according to the selected cal-	
	culation methodology.	
k()	Calculate and return the thermal conductivity	
	of the bulk according to the selected thermal	
	conductivity settings in BulkSettings, the set-	
	tings in ThermalConductivityGasMixture	
	and <i>ThermalConductivityLiquidMixture</i> ,	
	and the configured pure-component set-	
	tings in <i>ThermalConductivityGas</i> and	
	ThermalConductivityLiquid.	
kappa()	Method to calculate and return the isothermal com-	
	pressibility of the bulk according to the selected cal-	
	culation methodology.	
mu()	Calculate and return the viscosity of the	
	bulk according to the selected viscos-	
	ity settings in BulkSettings, the set-	
	tings in ViscosityGasMixture and	
	ViscosityLiquidMixture, and the config-	
	ured pure-component settings in ViscosityGas	
ei mel	and ViscosityLiquid. Calculate and return the surface tension of the	
sigma()	bulk according to the selected surface ten-	
	sion settings in <i>BulkSettings</i> , the settings in	
	SurfaceTensionMixture and the configured	
	pure-component settings in SurfaceTension.	
<pre>speed_of_sound()</pre>	Method to calculate and return the molar speed of	
speca_or_sound()	sound of the bulk according to the selected calcula-	
	tion methodology.	
	uon memodology.	

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# **Cp**()

Method to calculate and return the constant-temperature and constant phase-fraction heat capacity of the bulk phase. This is a phase-fraction weighted calculation.

$$C_p = \sum_{i}^{p} C_{p,i} \beta_i$$

# Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

# Cp\_ideal\_gas()

Method to calculate and return the ideal-gas heat capacity of the phase.

$$C_p^{ig} = \sum_i z_i C_{p,i}^{ig}$$

Returns

**Cp** [float] Ideal gas heat capacity, [J/(mol\*K)]

**H**()

Method to calculate and return the constant-temperature and constant phase-fraction enthalpy of the bulk phase. This is a phase-fraction weighted calculation.

$$H = \sum_{i}^{p} H_{i}\beta_{i}$$

Returns

H [float] Molar enthalpy, [J/(mol)]

# H\_ideal\_gas()

Method to calculate and return the ideal-gas enthalpy of the phase.

$$H^{ig} = \sum_{i} z_i H_i^{ig}$$

# Returns

H [float] Ideal gas enthalpy, [J/(mol)]

### H\_reactive()

Method to calculate and return the constant-temperature and constant phase-fraction reactive enthalpy of the bulk phase. This is a phase-fraction weighted calculation.

$$H_{\text{reactive}} = \sum_{i}^{p} H_{\text{reactive},i} \beta_{i}$$

### Returns

**H** reactive [float] Reactive molar enthalpy, [J/(mol)]

### Joule\_Thomson()

Method to calculate and return the Joule-Thomson coefficient of the bulk according to the selected calculation methodology.

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_H$$

#### Returns

mu\_JT [float] Joule-Thomson coefficient [K/Pa]

MW()

Method to calculate and return the molecular weight of the bulk phase. This is a phase-fraction weighted calculation.

$$\mathbf{M}\mathbf{W} = \sum_{i}^{p} \mathbf{M}\mathbf{W}_{i}\beta_{i}$$

# Returns

MW [float] Molecular weight, [g/mol]

Pmc()

Method to calculate and return the mechanical critical pressure of the phase.

#### Returns

Pmc [float] Mechanical critical pressure, [Pa]

# **S**()

Method to calculate and return the constant-temperature and constant phase-fraction entropy of the bulk phase. This is a phase-fraction weighted calculation.

$$S = \sum_{i}^{p} S_{i} \beta_{i}$$

Returns

**S** [float] Molar entropy, [J/(mol\*K)]

# S\_ideal\_gas()

Method to calculate and return the ideal-gas entropy of the phase.

$$S^{ig} = \sum_{i} z_i S_i^{ig} - R \ln\left(\frac{P}{P_{ref}}\right) - R \sum_{i} z_i \ln(z_i)$$

Returns

**S** [float] Ideal gas molar entropy, [J/(mol\*K)]

# S\_reactive()

Method to calculate and return the constant-temperature and constant phase-fraction reactive entropy of the bulk phase. This is a phase-fraction weighted calculation.

$$S_{\text{reactive}} = \sum_{i}^{p} S_{\text{reactive},i} \beta_i$$

### Returns

**S\_reactive** [float] Reactive molar entropy, [J/(mol\*K)]

# Tmc()

Method to calculate and return the mechanical critical temperature of the phase.

### Returns

Tmc [float] Mechanical critical temperature, [K]

**V**()

Method to calculate and return the molar volume of the bulk phase. This is a phase-fraction weighted calculation.

$$V = \sum_{i}^{p} V_{i} \beta_{i}$$

# Returns

V [float] Molar volume, [m^3/mol]

V\_iter(force=False)

Method to calculate and return the molar volume of the bulk phase, with precision suitable for a *TV* calculation to calculate a matching pressure. This is a phase-fraction weighted calculation.

$$V = \sum_{i}^{p} V_{i}\beta_{i}$$

Returns

V [float or mpf] Molar volume, [m^3/mol]

### Vmc()

Method to calculate and return the mechanical critical volume of the phase.

# Returns

Vmc [float] Mechanical critical volume, [m^3/mol]

# Zmc()

Method to calculate and return the mechanical critical compressibility of the phase.

### Returns

**Zmc** [float] Mechanical critical compressibility, [-]

# property beta

Phase fraction of the bulk phase. Should always be 1 when representing all phases of a flash; but can be less than one if representing multiple solids or liquids as a single phase in a larger mixture.

#### Returns

beta [float] Phase fraction of bulk, [-]

# property betas\_mass

Method to calculate and return the mass fraction of all of the phases in the bulk.

### Returns

**betas\_mass** [list[float]] Mass phase fractions of all the phases in the bulk object, ordered vapor, liquid, then solid, [-]

# property betas\_volume

Method to calculate and return the volume fraction of all of the phases in the bulk.

# Returns

**betas\_volume** [list[float]] Volume phase fractions of all the phases in the bulk, ordered vapor, liquid, then solid, [-]

### d2P\_dT2()

Method to calculate and return the second temperature derivative of pressure of the bulk according to the selected calculation methodology.

#### Returns

d2P\_dT2 [float] Second temperature derivative of pressure, [Pa/K^2]

### d2P\_dT2\_frozen()

Method to calculate and return the second constant-volume derivative of pressure with respect to temperature of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial^2 P}{\partial T^2}\right)_{V,\beta,zs} = \sum_i^{\text{phases}} \beta_i \left(\frac{\partial^2 P}{\partial T^2}\right)_{i,V_i,\beta_i,zs_i}$$

#### Returns

**d2P\_dT2\_frozen** [float] Frozen constant-volume second derivative of pressure with respect to temperature of the bulk phase, [Pa/K^2]

# d2P\_dTdV()

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the bulk according to the selected calculation methodology.

### Returns

d2P\_dTdV [float] Second volume derivative of pressure, [mol\*Pa^2/(J\*K)]

# d2P\_dTdV\_frozen()

Method to calculate and return the second derivative of pressure with respect to volume and temperature of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial^2 P}{\partial V \partial T}\right)_{\beta, zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial^2 P}{\partial V \partial T}\right)_{i, \beta_i, zs_i}$$

#### Returns

**d2P\_dTdV\_frozen** [float] Frozen second derivative of pressure with respect to volume and temperature of the bulk phase, [Pa\*mol^2/m^6]

# d2P\_dV2()

Method to calculate and return the second volume derivative of pressure of the bulk according to the selected calculation methodology.

### Returns

d2P\_dV2 [float] Second volume derivative of pressure, [Pa\*mol^2/m^6]

# d2P\_dV2\_frozen()

Method to calculate and return the constant-temperature second derivative of pressure with respect to volume of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial^2 P}{\partial V^2}\right)_{T,\beta,zs} = \sum_i^{\text{phases}} \beta_i \left(\frac{\partial^2 P}{\partial V^2}\right)_{i,T,\beta_i,zs_i}$$

### Returns

**d2P\_dV2\_frozen** [float] Frozen constant-temperature second derivative of pressure with respect to volume of the bulk phase, [Pa\*mol^2/m^6]

 $dA_dP()$ 

Method to calculate and return the constant-temperature pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial U}{\partial P}\right)_T$$

Returns

dA\_dP [float] Constant-temperature pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

 $dA_dT()$ 

Method to calculate and return the constant-pressure temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial U}{\partial T}\right)_P$$

Returns

dA\_dT [float] Constant-pressure temperature derivative of Helmholtz energy, [J/(mol\*K)]

 $dG_dP()$ 

Method to calculate and return the constant-temperature pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial H}{\partial P}\right)_T$$

### Returns

**dG\_dP** [float] Constant-temperature pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

 $dG_dT()$ 

Method to calculate and return the constant-pressure temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

dG\_dT [float] Constant-pressure temperature derivative of Gibbs free energy, [J/(mol\*K)]

 $dP_dT()$ 

Method to calculate and return the first temperature derivative of pressure of the bulk according to the selected calculation methodology.

#### Returns

dP\_dT [float] First temperature derivative of pressure, [Pa/K]

# dP\_dT\_frozen()

Method to calculate and return the constant-volume derivative of pressure with respect to temperature of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial P}{\partial T}\right)_{V,\beta,zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial P}{\partial T}\right)_{i,V_i,\beta_i,zs_i}$$

### Returns

**dP\_dT\_frozen** [float] Frozen constant-volume derivative of pressure with respect to temperature of the bulk phase, [Pa/K]

# $dP_dV()$

Method to calculate and return the first volume derivative of pressure of the bulk according to the selected calculation methodology.

# Returns

dP\_dV [float] First volume derivative of pressure, [Pa\*mol/m^3]

# dP\_dV\_frozen()

Method to calculate and return the constant-temperature derivative of pressure with respect to volume of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial P}{\partial V}\right)_{T,\beta,zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial P}{\partial V}\right)_{i,T,\beta_i,zs_i}$$

### Returns

**dP\_dV\_frozen** [float] Frozen constant-temperature derivative of pressure with respect to volume of the bulk phase, [Pa\*mol/m^3]

 $dU_dP()$ 

Method to calculate and return the constant-temperature pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_T = -P\left(\frac{\partial V}{\partial P}\right)_T - V + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

**dU\_dP** [float] Constant-temperature pressure derivative of internal energy, [J/(mol\*Pa)]

dU\_dT()

Method to calculate and return the constant-pressure temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_P = -P\left(\frac{\partial V}{\partial T}\right)_P + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

**dU\_dT** [float] Constant-pressure temperature derivative of internal energy, [J/(mol\*K)]

#### isobaric\_expansion()

Method to calculate and return the isobatic expansion coefficient of the bulk according to the selected calculation methodology.

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

### Returns

beta [float] Isobaric coefficient of a thermal expansion, [1/K]

**k**()

Calculate and return the thermal conductivity of the bulk according to the selected thermal conductivity settings in *BulkSettings*, the settings in *ThermalConductivityGasMixture* and *ThermalConductivityLiquidMixture*, and the configured pure-component settings in *ThermalConductivityGas* and *ThermalConductivityLiquid*.

### Returns

k [float] Thermal Conductivity of bulk phase calculated with mixing rules, [Pa\*s]

kappa()

Method to calculate and return the isothermal compressibility of the bulk according to the selected calculation methodology.

$$\kappa = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

#### Returns

**kappa** [float] Isothermal coefficient of compressibility, [1/Pa]

# mu()

Calculate and return the viscosity of the bulk according to the selected viscosity settings in *BulkSettings*, the settings in *ViscosityGasMixture* and *ViscosityLiquidMixture*, and the configured pure-component settings in *ViscosityGas* and *ViscosityLiquid*.

#### Returns

mu [float] Viscosity of bulk phase calculated with mixing rules, [Pa\*s]

# sigma()

Calculate and return the surface tension of the bulk according to the selected surface tension settings in *BulkSettings*, the settings in *SurfaceTensionMixture* and the configured pure-component settings in *SurfaceTension*.

### Returns

sigma [float] Surface tension of bulk phase calculated with mixing rules, [N/m]

#### Notes

A value is only returned if all phases in the bulk are liquids; this property is for a liquid-ideal gas calculation, not the interfacial tension between two liquid phases.

### speed\_of\_sound()

Method to calculate and return the molar speed of sound of the bulk according to the selected calculation methodology.

$$w = \left[-V^2 \left(\frac{\partial P}{\partial V}\right)_T \frac{C_p}{C_v}\right]^{1/2}$$

A similar expression based on molar density is:

$$w = \left[ \left( \frac{\partial P}{\partial \rho} \right)_T \frac{C_p}{C_v} \right]^{1/2}$$

Returns

w [float] Speed of sound for a real gas, [m\*kg^0.5/(s\*mol^0.5)]

# 7.2.2 Bulk Settings Class

class thermo.bulk.BulkSettings(dP dT = 'MOLE WEIGHTED', dP dV = 'MOLE WEIGHTED', d2P dV2='MOLE WEIGHTED', d2P dT2='MOLE WEIGHTED', d2P\_dTdV='MOLE\_WEIGHTED', mu\_LL='LOG\_PROP\_MASS\_WEIGHTED', mu\_LL\_power\_exponent=0.4, mu\_VL='McAdams', mu\_VL\_power\_exponent=0.4, k LL='MASS WEIGHTED', k LL power exponent=0.4, k\_VL='MASS\_WEIGHTED', k\_VL\_power\_exponent=0.4, sigma\_LL='MASS\_WEIGHTED', sigma\_LL\_power\_exponent=0.4, T\_liquid\_volume\_ref=298.15, T\_normal=273.15, P\_normal=101325.0, T\_standard=288.15, P\_standard=101325.0, T\_gas\_ref=288.15, P gas ref=101325.0, speed of sound='MOLE WEIGHTED', kappa='MOLE WEIGHTED', isobaric expansion='MOLE WEIGHTED', Joule Thomson='MOLE WEIGHTED', VL ID='PIP', VL ID settings=None, S ID='d2P dVdT', S ID settings=None, solid\_sort\_method='prop', liquid\_sort\_method='prop', liquid\_sort\_cmps=[], solid\_sort\_cmps=[], liquid\_sort\_cmps\_neg=[], solid sort cmps neg=[], liquid sort prop='DENSITY MASS', solid\_sort\_prop='DENSITY\_MASS', phase\_sort\_higher\_first=True, *water\_sort='water not special', equilibrium\_perturbation=1e-07)* Bases: object

Class containing configuration methods for determining how properties of a *Bulk* phase made of different phases are handled. All parameters are also attributes.

### Parameters

- **dP\_dT** [str, optional] The method used to calculate the constant-volume temperature derivative of pressure of the bulk. One of *DP\_DT\_METHODS*, [-]
- **dP\_dV** [str, optional] The method used to calculate the constant-temperature volume derivative of pressure of the bulk. One of *DP\_DV\_METHODS*, [-]
- **d2P\_dV2** [str, optional] The method used to calculate the second constant-temperature volume derivative of pressure of the bulk. One of *D2P\_DV2\_METHODS*, [-]

- **d2P\_dT2** [str, optional] The method used to calculate the second constant-volume temperature derivative of pressure of the bulk. One of *D2P\_DT2\_METHODS*, [-]
- **d2P\_dTdV** [str, optional] The method used to calculate the temperature and volume derivative of pressure of the bulk. One of *D2P\_DTDV\_METHODS*, [-]
- **T\_gas\_ref** [float, optional] Reference temperature to use for the calculation of ideal-gas molar volume and flow rate, [K]
- **P\_gas\_ref** [float, optional] Reference pressure to use for the calculation of ideal-gas molar volume and flow rate, [Pa]
- **T\_normal** [float, optional] "Normal" gas reference temperature for the calculation of ideal-gas molar volume in the "normal" reference state; default 273.15 K (0 C) according to [1], [K]
- P\_normal [float, optional] "Normal" gas reference pressure for the calculation of ideal-gas molar volume in the "normal" reference state; default 101325 Pa (1 atm) according to [1], [Pa]
- T\_standard [float, optional] "Standard" gas reference temperature for the calculation of idealgas molar volume in the "standard" reference state; default 288.15 K (15° C) according to [2]; 288.7055555555555 is also often used (60° F), [K]
- P\_standard [float, optional] "Standard" gas reference pressure for the calculation of ideal-gas molar volume in the "standard" reference state; default 101325 Pa (1 atm) according to [2], [Pa]
- **mu\_LL** [str, optional] Mixing rule for multiple liquid phase liquid viscosity calculations; see *MU\_LL\_METHODS* for available options, [-]
- **mu\_LL\_power\_exponent** [float, optional] Liquid-liquid viscosity power-law mixing parameter, used only when a power law mixing rule is selected, [-]
- **mu\_VL** [str, optional] Mixing rule for vapor-liquid viscosity calculations; see *MU\_VL\_METHODS* for available options, [-]
- **mu\_VL\_power\_exponent** [float, optional] Vapor-liquid viscosity power-law mixing parameter, used only when a power law mixing rule is selected, [-]
- **k\_LL** [str, optional] Mixing rule for multiple liquid phase liquid thermal conductivity calculations; see *K\_LL\_METHODS* for available options, [-]
- **k\_LL\_power\_exponent** [float, optional] Liquid-liquid thermal conductivity power-law mixing parameter, used only when a power law mixing rule is selected, [-]
- **k\_VL** [str, optional] Mixing rule for vapor-liquid thermal conductivity calculations; see *K\_VL\_METHODS* for available options, [-]
- **k\_VL\_power\_exponent** [float, optional] Vapor-liquid thermal conductivity power-law mixing parameter, used only when a power law mixing rule is selected, [-]
- sigma\_LL [str, optional] Mixing rule for multiple liquid phase, air-liquid surface tension calculations; see SIGMA\_LL\_METHODS for available options, [-]
- **sigma\_LL\_power\_exponent** [float, optional] Air-liquid Liquid-liquid surface tension powerlaw mixing parameter, used only when a power law mixing rule is selected, [-]
- equilibrium\_perturbation [float, optional] The relative perturbation to use when calculating equilibrium derivatives numerically; for example if this is 1e-3 and T is the perturbation

variable and the statis is 500 K, the perturbation calculation temperature will be 500.5 K, [various]

- **isobaric\_expansion** [str, optional] Mixing rule for multiphase isobaric expansion calculations; see *BETA\_METHODS* for available options, [-]
- **speed\_of\_sound** [str, optional] Mixing rule for multiphase speed of sound calculations; see SPEED\_OF\_SOUND\_METHODS for available options, [-]
- **kappa** [str, optional] Mixing rule for multiphase *kappa* calculations; see *KAPPA\_METHODS* for available options, [-]
- **Joule\_Thomson** [str, optional] Mixing rule for multiphase *Joule-Thomson* calculations; see *JT\_METHODS* for available options, [-]

# Notes

The linear mixing rules "MOLE\_WEIGHTED", "MASS\_WEIGHTED", and "VOLUME\_WEIGHTED" have the following formula, with  $\beta$  representing molar, mass, or volume phase fraction:

bulk property = 
$$\left(\sum_{i}^{phases} \beta_i \text{property}\right)$$

The power mixing rules "POWER\_PROP\_MOLE\_WEIGHTED", "POWER\_PROP\_MASS\_WEIGHTED", and "POWER\_PROP\_VOLUME\_WEIGHTED" have the following formula, with  $\beta$  representing molar, mass, or volume phase fraction:

bulk property = 
$$\left(\sum_{i}^{phases} \beta_i \text{property exponent}\right)^{1/\text{exponent}}$$

The logarithmic mixing rules "LOG\_PROP\_MOLE\_WEIGHTED", "LOG\_PROP\_MASS\_WEIGHTED", and "LOG\_PROP\_VOLUME\_WEIGHTED" have the following formula, with  $\beta$  representing molar, mass, or volume phase fraction:

bulk property = 
$$\exp\left(\sum_{i}^{phases} \beta_i \ln(\text{property})\right)$$

The mixing rule "MINIMUM\_PHASE\_PROP" selects the lowest phase value of the property, always. The mixing rule "MAXIMUM\_PHASE\_PROP" selects the highest phase value of the property, always.

The mixing rule "AS\_ONE\_LIQUID" calculates a property using the bulk composition but applied to the liquid model only. The mixing rule "AS\_ONE\_GAS" calculates a property using the bulk composition but applied to the gas model only.

The mixing rule "FROM\_DERIVATIVE\_SETTINGS" is used to indicate that the property depends on other configurable properties; and when this is the specified option, those configurations will be used in the calculation of this property.

The mixing rule "EQUILIBRIUM\_DERIVATIVE" performs derivative calculations on flashes themselves. This is quite slow in comparison to other methods.

### References

[1], [2]

### **Methods**

```
as_json
```

as\_json()

```
thermo.bulk.DP_DT_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'EQUILIBRIUM_DERIVATIVE', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented calculation methods for the DP DT bulk setting
thermo.bulk.DP_DV_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'EQUILIBRIUM_DERIVATIVE', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented calculation methods for the DP DV bulk setting
thermo.bulk.D2P_DV2_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented calculation methods for the D2P DV2 bulk setting
thermo.bulk.D2P_DT2_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented calculation methods for the D2P DT2 bulk setting
thermo.bulk.D2P_DTDV_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented calculation methods for the D2P_DTDV bulk setting
thermo.bulk.MU_LL_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'AS_ONE_LIQUID', 'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED',
'LOG_PROP_VOLUME_WEIGHTED', 'POWER_PROP_MOLE_WEIGHTED', 'POWER_PROP_MASS_WEIGHTED',
'POWER_PROP_VOLUME_WEIGHTED', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented mixing rules for the MU LL setting
thermo.bulk.MU_VL_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'AS_ONE_LIQUID', 'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED',
'LOG_PROP_VOLUME_WEIGHTED', 'POWER_PROP_MOLE_WEIGHTED', 'POWER_PROP_MASS_WEIGHTED',
'POWER_PROP_VOLUME_WEIGHTED', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP', 'AS_ONE_GAS',
'Beattie Whalley', 'McAdams', 'Cicchitti', 'Lin Kwok', 'Fourar Bories', 'Duckler']
     List of all valid and implemented mixing rules for the MU VL setting
thermo.bulk.K_LL_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'AS_ONE_LIQUID', 'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED',
'LOG PROP VOLUME WEIGHTED'. 'POWER PROP MOLE WEIGHTED'. 'POWER PROP MASS WEIGHTED'.
'POWER_PROP_VOLUME_WEIGHTED', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
```

```
List of all valid and implemented mixing rules for the K_LL setting
```

```
thermo.bulk.K_VL_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'AS_ONE_LIQUID', 'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED',
'LOG_PROP_VOLUME_WEIGHTED', 'POWER_PROP_MOLE_WEIGHTED', 'POWER_PROP_MASS_WEIGHTED',
'POWER_PROP_VOLUME_WEIGHTED', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP', 'AS_ONE_GAS']
     List of all valid and implemented mixing rules for the K_VL setting
thermo.bulk.SIGMA_LL_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'AS_ONE_LIQUID', 'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED',
'LOG_PROP_VOLUME_WEIGHTED', 'POWER_PROP_MOLE_WEIGHTED', 'POWER_PROP_MASS_WEIGHTED',
'POWER_PROP_VOLUME_WEIGHTED', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP']
     List of all valid and implemented mixing rules for the SIGMA_LL setting
thermo.bulk.BETA_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP', 'EQUILIBRIUM_DERIVATIVE',
'FROM_DERIVATIVE_SETTINGS']
     List of all valid and implemented calculation methods for the isothermal compressibility bulk setting
thermo.bulk.SPEED_OF_SOUND_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED',
'VOLUME_WEIGHTED', 'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED',
'LOG_PROP_VOLUME_WEIGHTED', 'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP',
'FROM_DERIVATIVE_SETTINGS']
     List of all valid and implemented calculation methods for the speed_of_sound bulk setting
thermo.bulk.KAPPA_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP', 'EQUILIBRIUM_DERIVATIVE',
'FROM_DERIVATIVE_SETTINGS']
     List of all valid and implemented calculation methods for the kappa bulk setting
```

```
thermo.bulk.JT_METHODS = ['MOLE_WEIGHTED', 'MASS_WEIGHTED', 'VOLUME_WEIGHTED',
'LOG_PROP_MOLE_WEIGHTED', 'LOG_PROP_MASS_WEIGHTED', 'LOG_PROP_VOLUME_WEIGHTED',
'MINIMUM_PHASE_PROP', 'MAXIMUM_PHASE_PROP', 'EQUILIBRIUM_DERIVATIVE',
'FROM_DERIVATIVE_SETTINGS']
```

List of all valid and implemented calculation methods for the JT bulk setting

# 7.3 Legacy Chemicals (thermo.chemical)

class thermo.chemical.Chemical(ID, T=298.15, P=101325, autocalc=True)
Bases: object

Creates a Chemical object which contains basic information such as molecular weight and the structure of the species, as well as thermodynamic and transport properties as a function of temperature and pressure.

# Parameters

ID [str]

# One of the following [-]:

- Name, in IUPAC form or common form or a synonym registered in PubChem
- InChI name, prefixed by 'InChI=1S/' or 'InChI=1/'
- InChI key, prefixed by 'InChIKey='
- PubChem CID, prefixed by 'PubChem='
- SMILES (prefix with 'SMILES=' to ensure smiles parsing)

- CAS number
- T [float, optional] Temperature of the chemical (default 298.15 K), [K]
- P [float, optional] Pressure of the chemical (default 101325 Pa) [Pa]

# **Notes**

**Warning:** The Chemical class is not designed for high-performance or the ability to use different thermodynamic models. It is especially limited in its multiphase support and the ability to solve with specifications other than temperature and pressure. It is impossible to change constant properties such as a compound's critical temperature in this interface.

It is recommended to switch over to the *thermo.flash* interface which solves those problems and is better positioned to grow. That interface also requires users to be responsible for their chemical constants and pure component correlations; while default values can easily be loaded for most compounds, the user is ultimately responsible for them.

# Examples

Creating chemical objects:

```
>>> Chemical('hexane')
<Chemical [hexane], T=298.15 K, P=101325 Pa>
```

```
>>> Chemical('CCCCCCC', T=500, P=1E7)
<Chemical [octane], T=500.00 K, P=10000000 Pa>
```

>>> Chemical('7440-36-0', P=1000)
<Chemical [antimony], T=298.15 K, P=1000 Pa>

Getting basic properties:

```
>>> N2 = Chemical('Nitrogen')
>>> N2.Tm, N2.Tb, N2.Tc # melting, boiling, and critical points [K]
(63.15, 77.355, 126.2)
>>> N2.Pt, N2.Pc # sublimation and critical pressure [Pa]
(12526.9697368421, 3394387.5)
>>> N2.CAS, N2.formula, N2.InChI, N2.smiles, N2.atoms # CAS number, formula, InChI_
--string, smiles string, dictionary of atomic elements and their count
('7727-37-9', 'N2', 'N2/c1-2', 'N#N', {'N': 2})
```

Changing the T/P of the chemical, and gettign temperature-dependent properties:

```
>>> N2.Cp, N2.rho, N2.mu # Heat capacity [J/kg/K], density [kg/m<sup>3</sup>], viscosity_

→ [Pa*s]

(1039.4978324480921, 1.1452416223829405, 1.7804740647270688e-05)

>>> N2.calculate(T=65, P=1E6) # set it to a liquid at 65 K and 1 MPa

>>> N2.phase

'l'

>>> N2.Cp, N2.rho, N2.mu # properties are now of the liquid phase

(2002.8819854804037, 861.3539919443364, 0.0002857739143670701)
```

Molar units are also available for properties:

```
>>> N2.Cpm, N2.Vm, N2.Hvapm # heat capacity [J/mol/K], molar volume [m<sup>3</sup>/mol], 
→ enthalpy of vaporization [J/mol]
(56.10753421205674, 3.252251717875631e-05, 5982.710998291719)
```

A great deal of properties are available; for a complete list look at the attributes list.

```
>>> N2.alpha, N2.JT # thermal diffusivity [m^2/s], Joule-Thompson coefficient [K/Pa]
(9.874883993253272e-08, -4.0009932695519242e-07)
```

>>> N2.isentropic\_exponent, N2.isobaric\_expansion
(1.4000000000000001, 0.0047654228408661571)

For pure species, the phase is easily identified, allowing for properties to be obtained without needing to specify the phase. However, the properties are also available in the hypothetical gas phase (when under the boiling point) and in the hypothetical liquid phase (when above the boiling point) as these properties are needed to evaluate mixture properties. Specify the phase of a property to be retrieved by appending 'l' or 'g' or 's' to the property.

>>> tol = Chemical('toluene')

```
>>> tol.rhog, tol.Cpg, tol.kg, tol.mug
(4.241646701894199, 1126.5533755283168, 0.00941385692301755, 6.973325939594919e-06)
```

Temperature dependent properties are calculated by objects which provide many useful features related to the properties. To determine the temperature at which nitrogen has a saturation pressure of 1 MPa:

```
>>> N2.VaporPressure.solve_property(1E6)
103.73528598652341
```

To compute an integral of the ideal-gas heat capacity of nitrogen to determine the enthalpy required for a given change in temperature. Note the thermodynamic objects calculate values in molar units always.

>>> N2.HeatCapacityGas.T\_dependent\_property\_integral(100, 120) # J/mol/K
582.0121860897898

Derivatives of properties can be calculated as well, as may be needed by for example heat transfer calculations:

```
>>> N2.SurfaceTension.T_dependent_property_derivative(77)
-0.00022695346296730534
```

If a property is needed at multiple temperatures or pressures, it is faster to use the object directly to perform the calculation rather than setting the conditions for the chemical.

```
>>> [N2.VaporPressure(T) for T in range(80, 120, 10)]
[136979.4840843189, 360712.5746603142, 778846.276691705, 1466996.7208525643]
```

These objects are also how the methods by which the properties are calculated can be changed. To see the available methods for a property:

To specify the method which should be used for calculations of a property. In the example below, the Lee-kesler correlation for vapor pressure is specified.

```
>>> N2.calculate(80)
>>> N2.Psat
136979.4840843189
>>> N2.VaporPressure.method = 'LEE_KESLER_PSAT'
>>> N2.Psat
134987.76815364443
```

For memory reduction, these objects are shared by all chemicals which are the same; new instances will use the same specified methods.

```
>>> N2_2 = Chemical('nitrogen')
>>> N2_2.VaporPressure.user_methods
['LEE_KESLER_PSAT']
```

To disable this behavior, set thermo.chemical.caching to False.

```
>>> import thermo
>>> thermo.chemical.caching = False
>>> N2_3 = Chemical('nitrogen')
>>> N2_3.VaporPressure.user_methods
[]
```

Properties may also be plotted via these objects:

```
>>> N2.VaporPressure.plot_T_dependent_property()
>>> N2.VolumeLiquid.plot_isotherm(T=77, Pmin=1E5, Pmax=1E7)
>>> N2.VolumeLiquid.plot_isobar(P=1E6, Tmin=66, Tmax=120)
>>> N2.VolumeLiquid.plot_TP_dependent_property(Tmin=60, Tmax=100, Pmin=1E5, 
... Pmax=1E7)
```

# Attributes

T [float] Temperature of the chemical, [K]

**P** [float] Pressure of the chemical, [Pa]

**phase** [str] Phase of the chemical; one of 's', 'l', 'g', or 'l/g'.

ID [str] User specified string by which the chemical's CAS was looked up.

CAS [str] The CAS number of the chemical.

**PubChem** [int] PubChem Compound identifier (CID) of the chemical; all chemicals are sourced from their database. Chemicals can be looked at online at https://pubchem.ncbi.nlm.nih.gov.

MW [float] Molecular weight of the compound, [g/mol]

formula [str] Molecular formula of the compound.

**atoms** [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

similarity\_variable [float] Similarity variable, see chemicals.elements.
similarity\_variable for the definition, [mol/g]

smiles [str] Simplified molecular-input line-entry system representation of the compound.

InChI [str] IUPAC International Chemical Identifier of the compound.

InChI\_Key [str] 25-character hash of the compound's InChI.

**IUPAC\_name** [str] Preferred IUPAC name for a compound.

**synonyms** [list of strings] All synonyms for the compound found in PubChem, sorted by popularity.

**Tm** [float] Melting temperature [K]

Tb [float] Boiling temperature [K]

**Tc** [float] Critical temperature [K]

Pc [float] Critical pressure [Pa]

Vc [float] Critical volume [m^3/mol]

Zc [float] Critical compressibility [-]

rhoc [float] Critical density [kg/m^3]

rhocm [float] Critical molar density [mol/m^3]

omega [float] Acentric factor [-]

**StielPolar** [float] Stiel Polar factor, see chemicals.acentric.Stiel\_polar\_factor for the definition [-]

Tt [float] Triple temperature, [K]

**Pt** [float] Triple pressure, [Pa]

Hfus [float] Enthalpy of fusion [J/kg]

Hfusm [float] Molar enthalpy of fusion [J/mol]

Hsub [float] Enthalpy of sublimation [J/kg]

Hsubm [float] Molar enthalpy of sublimation [J/mol]

Hfm [float] Standard state molar enthalpy of formation, [J/mol]

Hf [float] Standard enthalpy of formation in a mass basis, [J/kg]

Hfgm [float] Ideal-gas molar enthalpy of formation, [J/mol]

Hfg [float] Ideal-gas enthalpy of formation in a mass basis, [J/kg]

Hcm [float] Molar higher heat of combustion [J/mol]

**Hc** [float] Higher Heat of combustion [J/kg]

Hcm\_lower [float] Molar lower heat of combustion [J/mol]

Hc\_lower [float] Lower Heat of combustion [J/kg]

S0m [float] Standard state absolute molar entropy of the chemical, [J/mol/K]

**S0** [float] Standard state absolute entropy of the chemical, [J/kg/K]

**S0gm** [float] Absolute molar entropy in an ideal gas state of the chemical, [J/mol/K]

S0g [float] Absolute mass entropy in an ideal gas state of the chemical, [J/kg/K]

Gfm [float] Standard state molar change of Gibbs energy of formation [J/mol]

Gf [float] Standard state change of Gibbs energy of formation [J/kg]

**Gfgm** [float] Ideal-gas molar change of Gibbs energy of formation [J/mol]

Gfg [float] Ideal-gas change of Gibbs energy of formation [J/kg]

Sfm [float] Standard state molar change of entropy of formation, [J/mol/K]

Sf [float] Standard state change of entropy of formation, [J/kg/K]

Sfgm [float] Ideal-gas molar change of entropy of formation, [J/mol/K]

Sfg [float] Ideal-gas change of entropy of formation, [J/kg/K]

**Hcgm** [float] Higher molar heat of combustion of the chemical in the ideal gas state, [J/mol]

Hcg [float] Higher heat of combustion of the chemical in the ideal gas state, [J/kg]

**Hcgm\_lower** [float] Lower molar heat of combustion of the chemical in the ideal gas state, [J/mol]

**Hcg\_lower** [float] Lower heat of combustion of the chemical in the ideal gas state, [J/kg]

Tflash [float] Flash point of the chemical, [K]

Tautoignition [float] Autoignition point of the chemical, [K]

LFL [float] Lower flammability limit of the gas in an atmosphere at STP, mole fraction [-]

**UFL** [float] Upper flammability limit of the gas in an atmosphere at STP, mole fraction [-]

- **TWA** [tuple[quantity, unit]] Time-Weighted Average limit on worker exposure to dangerous chemicals.
- **STEL** [tuple[quantity, unit]] Short-term Exposure limit on worker exposure to dangerous chemicals.

Ceiling [tuple[quantity, unit]] Ceiling limits on worker exposure to dangerous chemicals.

Skin [bool] Whether or not a chemical can be absorbed through the skin.

Carcinogen [str or dict] Carcinogen status information.

**dipole** [float] Dipole moment in debye, [3.33564095198e-30 ampere\*second^2]

Stockmayer [float] Lennard-Jones depth of potential-energy minimum over k, [K]

- molecular\_diameter [float] Lennard-Jones molecular diameter, [angstrom]
- **GWP** [float] Global warming potential (default 100-year outlook) (impact/mass chemical)/(impact/mass CO2), [-]
- ODP [float] Ozone Depletion potential (impact/mass chemical)/(impact/mass CFC-11), [-]

logP [float] Octanol-water partition coefficient, [-]

*legal\_status* [str or dict] Dictionary of legal status indicators for the chemical.

economic\_status [list] Dictionary of economic status indicators for the chemical.

**RI** [float] Refractive Index on the Na D line, [-]

RIT [float] Temperature at which refractive index reading was made

conductivity [float] Electrical conductivity of the fluid, [S/m]

conductivityT [float] Temperature at which conductivity measurement was made

**VaporPressure** [object] Instance of thermo.vapor\_pressure.VaporPressure, with data and methods loaded for the chemical; performs the actual calculations of vapor pressure of the chemical.

- **EnthalpyVaporization** [object] Instance of thermo.phase\_change. EnthalpyVaporization, with data and methods loaded for the chemical; performs the actual calculations of molar enthalpy of vaporization of the chemical.
- **VolumeSolid** [object] Instance of *thermo.volume.VolumeSolid*, with data and methods loaded for the chemical; performs the actual calculations of molar volume of the solid phase of the chemical.
- **VolumeLiquid** [object] Instance of *thermo.volume.VolumeLiquid*, with data and methods loaded for the chemical; performs the actual calculations of molar volume of the liquid phase of the chemical.
- **VolumeGas** [object] Instance of *thermo.volume.VolumeGas*, with data and methods loaded for the chemical; performs the actual calculations of molar volume of the gas phase of the chemical.
- **HeatCapacitySolid** [object] Instance of thermo.heat\_capacity.HeatCapacitySolid, with data and methods loaded for the chemical; performs the actual calculations of molar heat capacity of the solid phase of the chemical.
- **HeatCapacityLiquid** [object] Instance of thermo.heat\_capacity.HeatCapacityLiquid, with data and methods loaded for the chemical; performs the actual calculations of molar heat capacity of the liquid phase of the chemical.
- **HeatCapacityGas** [object] Instance of *thermo.heat\_capacity.HeatCapacityGas*, with data and methods loaded for the chemical; performs the actual calculations of molar heat capacity of the gas phase of the chemical.
- **ViscosityLiquid** [object] Instance of *thermo.viscosity.ViscosityLiquid*, with data and methods loaded for the chemical; performs the actual calculations of viscosity of the liquid phase of the chemical.
- **ViscosityGas** [object] Instance of *thermo.viscosity.ViscosityGas*, with data and methods loaded for the chemical; performs the actual calculations of viscosity of the gas phase of the chemical.
- **ThermalConductivityLiquid** [object] Instance of thermo.thermal\_conductivity. *ThermalConductivityLiquid*, with data and methods loaded for the chemical; performs the actual calculations of thermal conductivity of the liquid phase of the chemical.
- **ThermalConductivityGas** [object] Instance of thermo.thermal\_conductivity. *ThermalConductivityGas*, with data and methods loaded for the chemical; performs the actual calculations of thermal conductivity of the gas phase of the chemical.
- **SurfaceTension** [object] Instance of *thermo.interface.SurfaceTension*, with data and methods loaded for the chemical; performs the actual calculations of surface tension of the chemical.
- **Permittivity** [object] Instance of *thermo.permittivity.PermittivityLiquid*, with data and methods loaded for the chemical; performs the actual calculations of permittivity of the chemical.

Psat\_298 [float] Vapor pressure of the chemical at 298.15 K, [Pa]

phase\_STP [str] Phase of the chemical at 298.15 K and 101325 Pa; one of 's', 'l', 'g', or 'l/g'.

Vml\_Tb [float] Molar volume of liquid phase at the normal boiling point [m^3/mol]

Vml\_Tm [float] Molar volume of liquid phase at the melting point [m^3/mol]

Vml\_STP [float] Molar volume of liquid phase at 298.15 K and 101325 Pa [m^3/mol]

**rhoml\_STP** [float] Molar density of liquid phase at 298.15 K and 101325 Pa [mol/m^3]

- Vmg\_STP [float] Molar volume of gas phase at 298.15 K and 101325 Pa according to the ideal gas law, [m^3/mol]
- Vms\_Tm [float] Molar volume of solid phase at the melting point [m^3/mol]
- rhos\_Tm [float] Mass density of solid phase at the melting point [kg/m^3]
- **Hvap\_Tbm** [float] Molar enthalpy of vaporization at the normal boiling point [J/mol]
- Hvap\_Tb [float] Mass enthalpy of vaporization at the normal boiling point [J/kg]
- Hvapm\_298 [float] Molar enthalpy of vaporization at 298.15 K [J/mol]
- Hvap\_298 [float] Mass enthalpy of vaporization at 298.15 K [J/kg]
- **alpha** Thermal diffusivity of the chemical at its current temperature, pressure, and phase in units of [m<sup>2</sup>/s].
- **alphag** Thermal diffusivity of the gas phase of the chemical at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- **alphal** Thermal diffusivity of the liquid phase of the chemical at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- **API** API gravity of the liquid phase of the chemical, [degrees].
- *aromatic\_rings* Number of aromatic rings in a chemical, computed with RDKit from a chemical's SMILES.
- atom\_fractions Dictionary of atom: fractional occurence of the elements in a chemical.
- **Bvirial** Second virial coefficient of the gas phase of the chemical at its current temperature and pressure, in units of [mol/m^3].
- charge Charge of a chemical, computed with RDKit from a chemical's SMILES.
- **Cp** Mass heat capacity of the chemical at its current phase and temperature, in units of [J/kg/K].
- *Cpg* Gas-phase heat capacity of the chemical at its current temperature, in units of [J/kg/K].
- **Cpgm** Gas-phase ideal gas heat capacity of the chemical at its current temperature, in units of [J/mol/K].
- **Cp1** Liquid-phase heat capacity of the chemical at its current temperature, in units of [J/kg/K].
- **Cplm** Liquid-phase heat capacity of the chemical at its current temperature, in units of [J/mol/K].
- *Cpm* Molar heat capacity of the chemical at its current phase and temperature, in units of [J/mol/K].
- **Cps** Solid-phase heat capacity of the chemical at its current temperature, in units of [J/kg/K].
- **Cpsm** Solid-phase heat capacity of the chemical at its current temperature, in units of [J/mol/K].
- *Cvg* Gas-phase ideal-gas contant-volume heat capacity of the chemical at its current temperature, in units of [J/kg/K].
- *Cvgm* Gas-phase ideal-gas contant-volume heat capacity of the chemical at its current temperature, in units of [J/mol/K].
- *eos* Equation of state object held by the chemical; used to calculate excess thermodynamic quantities, and also provides a vapor pressure curve, enthalpy of vaporization curve, fugacity, thermodynamic partial derivatives, and more; see *thermo.eos* for a full listing.
- Hill formula of a compound.
- **Hvap** Enthalpy of vaporization of the chemical at its current temperature, in units of [J/kg].

**Hvapm** Enthalpy of vaporization of the chemical at its current temperature, in units of [J/mol].

- *isentropic\_exponent* Gas-phase ideal-gas isentropic exponent of the chemical at its current temperature, [dimensionless].
- *isobaric\_expansion* Isobaric (constant-pressure) expansion of the chemical at its current phase and temperature, in units of [1/K].
- *isobaric\_expansion\_g* Isobaric (constant-pressure) expansion of the gas phase of the chemical at its current temperature and pressure, in units of [1/K].
- *isobaric\_expansion\_1* Isobaric (constant-pressure) expansion of the liquid phase of the chemical at its current temperature and pressure, in units of [1/K].
- JT Joule Thomson coefficient of the chemical at its current phase and temperature, in units of [K/Pa].
- *JTg* Joule Thomson coefficient of the chemical in the gas phase at its current temperature and pressure, in units of [K/Pa].
- JT1 Joule Thomson coefficient of the chemical in the liquid phase at its current temperature and pressure, in units of [K/Pa].
- **k** Thermal conductivity of the chemical at its current phase, temperature, and pressure in units of [W/m/K].
- *kg* Thermal conductivity of the chemical in the gas phase at its current temperature and pressure, in units of [W/m/K].
- **k1** Thermal conductivity of the chemical in the liquid phase at its current temperature and pressure, in units of [W/m/K].
- mass\_fractions Dictionary of atom:mass-weighted fractional occurence of elements.
- mu Viscosity of the chemical at its current phase, temperature, and pressure in units of [Pa\*s].
- *mug* Viscosity of the chemical in the gas phase at its current temperature and pressure, in units of [Pa\*s].
- **mul** Viscosity of the chemical in the liquid phase at its current temperature and pressure, in units of [Pa\*s].
- *nu* Kinematic viscosity of the chemical at its current temperature, pressure, and phase in units of  $[m^2/s]$ .
- *nug* Kinematic viscosity of the gas phase of the chemical at its current temperature and pressure, in units of  $[m^2/s]$ .
- **nul** Kinematic viscosity of the liquid phase of the chemical at its current temperature and pressure, in units of [m^2/s].
- **Parachor** Parachor of the chemical at its current temperature and pressure, in units of [N^0.25\*m^2.75/mol].
- *permittivity* Relative permittivity (dielectric constant) of the chemical at its current temperature, [dimensionless].
- **Poynting** Poynting correction factor [dimensionless] for use in phase equilibria methods based on activity coefficients or other reference states.
- Pr Prandtl number of the chemical at its current temperature, pressure, and phase; [dimension-less].
- *Prg* Prandtl number of the gas phase of the chemical at its current temperature and pressure, [dimensionless].

- **Pr1** Prandtl number of the liquid phase of the chemical at its current temperature and pressure, [dimensionless].
- Psat Vapor pressure of the chemical at its current temperature, in units of [Pa].
- PSRK\_groups Dictionary of PSRK subgroup: count groups for the PSRK subgroups, as determined by DDBST's online service.
- rdkitmol RDKit object of the chemical, without hydrogen.
- rdkitmol\_Hs RDKit object of the chemical, with hydrogen.
- **rho** Mass density of the chemical at its current phase and temperature and pressure, in units of [kg/m^3].
- **rhog** Gas-phase mass density of the chemical at its current temperature and pressure, in units of [kg/m^3].
- **rhogm** Molar density of the chemical in the gas phase at the current temperature and pressure, in units of [mol/m^3].
- **rhol** Liquid-phase mass density of the chemical at its current temperature and pressure, in units of [kg/m<sup>3</sup>].
- **rholm** Molar density of the chemical in the liquid phase at the current temperature and pressure, in units of [mol/m<sup>3</sup>].
- **rhom** Molar density of the chemical at its current phase and temperature and pressure, in units of [mol/m^3].
- **rhos** Solid-phase mass density of the chemical at its current temperature, in units of [kg/m^3].
- *rhosm* Molar density of the chemical in the solid phase at the current temperature and pressure, in units of [mol/m^3].
- rings Number of rings in a chemical, computed with RDKit from a chemical's SMILES.
- **SG** Specific gravity of the chemical, [dimensionless].
- *SGg* Specific gravity of the gas phase of the chemical, [dimensionless].
- *SG1* Specific gravity of the liquid phase of the chemical at the specified temperature and pressure, [dimensionless].
- *SGs* Specific gravity of the solid phase of the chemical at the specified temperature and pressure, [dimensionless].
- sigma Surface tension of the chemical at its current temperature, in units of [N/m].
- **solubility\_parameter** Solubility parameter of the chemical at its current temperature and pressure, in units of [Pa^0.5].
- **UNIFAC\_Dortmund\_groups** Dictionary of Dortmund UNIFAC subgroup: count groups for the Dortmund UNIFAC subgroups, as determined by DDBST's online service.
- **UNIFAC\_groups** Dictionary of UNIFAC subgroup: count groups for the original UNIFAC subgroups, as determined by DDBST's online service.
- **UNIFAC\_R** UNIFAC R (normalized Van der Waals volume), dimensionless.
- UNIFAC\_Q UNIFAC Q (normalized Van der Waals area), dimensionless.

Van\_der\_Waals\_area Unnormalized Van der Waals area, in units of [m^2/mol].

Van\_der\_Waals\_volume Unnormalized Van der Waals volume, in units of [m^3/mol].

- Vm Molar volume of the chemical at its current phase and temperature and pressure, in units of [m^3/mol].
- *Vmg* Gas-phase molar volume of the chemical at its current temperature and pressure, in units of [m^3/mol].
- Vml Liquid-phase molar volume of the chemical at its current temperature and pressure, in units of [m^3/mol].
- Vms Solid-phase molar volume of the chemical at its current temperature, in units of [m^3/mol].
- *Z* Compressibility factor of the chemical at its current phase and temperature and pressure, [dimensionless].
- *Zg* Compressibility factor of the chemical in the gas phase at the current temperature and pressure, [dimensionless].
- **Z1** Compressibility factor of the chemical in the liquid phase at the current temperature and pressure, [dimensionless].
- **Zs** Compressibility factor of the chemical in the solid phase at the current temperature and pressure, [dimensionless].

# **Methods**

# Reynolds([V, D])

draw_2d([width, height, Hs])	Interface for drawing a 2D image of the molecule.
<i>draw_3d</i> ([width, height, style, Hs, atom_labels])	Interface for drawing an interactive 3D view of the
	molecule.

Bond	
Capillary	
Grashof	
Jakob	
Peclet heat	
Tsat	
Weber	
calc_H	
calc_H_excess	
calc_S	
calc_S_excess	
calculate	
calculate_PH	
calculate_PS	
calculate_TH	
calculate_TS	
set_TP_sources	
set_constant_sources	
set_constants	
set_eos	
set_ref	
set_thermo	

# property A

Helmholtz energy of the chemical at its current temperature and pressure, in units of [J/kg].

This property requires that thermo.chemical.set\_thermo ran successfully to be accurate. It also depends on the molar volume of the chemical at its current conditions.

# property API

API gravity of the liquid phase of the chemical, [degrees]. The reference condition is water at 15.6 °C (60 °F) and 1 atm (rho=999.016 kg/m^3, standardized).

# Examples

>>> Chemical('water').API
9.999752435378895

# property Am

Helmholtz energy of the chemical at its current temperature and pressure, in units of [J/mol].

This property requires that thermo.chemical.set\_thermo ran successfully to be accurate. It also depends on the molar volume of the chemical at its current conditions.

# Bond(L=None)

### property Bvirial

Second virial coefficient of the gas phase of the chemical at its current temperature and pressure, in units of [mol/m^3].

This property uses the object-oriented interface *thermo.volume.VolumeGas*, converting its result with thermo.utils.B\_from\_Z.

# **Examples**

```
>>> Chemical('water').Bvirial
-0.0009596286322838357
```

# Capillary(V=None)

# property Cp

Mass heat capacity of the chemical at its current phase and temperature, in units of [J/kg/K].

Utilizes the object oriented interfaces thermo.heat\_capacity.HeatCapacitySolid, thermo. heat\_capacity.HeatCapacityLiquid, and thermo.heat\_capacity.HeatCapacityGas to perform the actual calculation of each property. Note that those interfaces provide output in molar units (J/mol/K).

```
>>> w = Chemical('water')
>>> w.Cp, w.phase
(4180.597021827336, 'l')
>>> Chemical('palladium').Cp
234.26767209171211
```

### property Cpg

Gas-phase heat capacity of the chemical at its current temperature, in units of [J/kg/K]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity.HeatCapacityGas*; each Chemical instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

### **Examples**

```
>>> w = Chemical('water', T=520)
>>> w.Cpg
1967.6698314620658
```

#### property Cpgm

Gas-phase ideal gas heat capacity of the chemical at its current temperature, in units of [J/mol/K]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity.HeatCapacityGas*; each Chemical instance creates one to actually perform the calculations.

### Examples

```
>>> Chemical('water').Cpgm
33.583577868850675
>>> Chemical('water').HeatCapacityGas.T_dependent_property(320)
33.67865044005934
>>> Chemical('water').HeatCapacityGas.T_dependent_property_integral(300, 320)
672.6480417835064
```

# property Cpl

Liquid-phase heat capacity of the chemical at its current temperature, in units of [J/kg/K]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface thermo.heat\_capacity.HeatCapacityLiquid; each Chemical instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

# **Examples**

```
>>> Chemical('water', T=320).Cpl
4177.518996988284
```

Ideal entropy change of water from 280 K to 340 K, output converted back to mass-based units of J/kg/K.

# property Cplm

Liquid-phase heat capacity of the chemical at its current temperature, in units of [J/mol/K]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity.HeatCapacityLiquid*; each Chemical instance creates one to actually perform the calculations.

# Notes

Some methods give heat capacity along the saturation line, some at 1 atm but only up to the normal boiling point, and some give heat capacity at 1 atm up to the normal boiling point and then along the saturation line. Real-liquid heat capacity is pressure dependent, but this interface is not.

# **Examples**

```
>>> Chemical('water').Cplm
75.31462591538556
>>> Chemical('water').HeatCapacityLiquid.T_dependent_property(320)
75.2591744360631
>>> Chemical('water').HeatCapacityLiquid.T_dependent_property_integral(300, 320)
1505.0619005000553
```

# property Cpm

Molar heat capacity of the chemical at its current phase and temperature, in units of [J/mol/K].

Utilizes the object oriented interfaces thermo.heat\_capacity.HeatCapacitySolid, thermo. heat\_capacity.HeatCapacityLiquid, and thermo.heat\_capacity.HeatCapacityGas to perform the actual calculation of each property.

# **Examples**

```
>>> Chemical('cubane').Cpm
137.05489206785944
>>> Chemical('ethylbenzene', T=550, P=3E6).Cpm
294.18449553310046
```

#### property Cps

Solid-phase heat capacity of the chemical at its current temperature, in units of [J/kg/K]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity.HeatCapacitySolid*; each Chemical instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

# property Cpsm

Solid-phase heat capacity of the chemical at its current temperature, in units of [J/mol/K]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity.HeatCapacitySolid*; each Chemical instance creates one to actually perform the calculations.

# **Examples**

```
>>> Chemical('palladium').Cpsm
24.930765664000003
>>> Chemical('palladium').HeatCapacitySolid.T_dependent_property(320)
25.098979200000002
>>> Chemical('palladium').HeatCapacitySolid.all_methods
set(["PERRY151", 'CRCSTD', 'LASTOVKA_S'])
```

# property Cvg

Gas-phase ideal-gas contant-volume heat capacity of the chemical at its current temperature, in units of [J/kg/K]. Subtracts R from the ideal-gas heat capacity; does not include pressure-compensation from an equation of state.

# **Examples**

```
>>> w = Chemical('water', T=520)
>>> w.Cvg
1506.1471795798861
```

# property Cvgm

Gas-phase ideal-gas contant-volume heat capacity of the chemical at its current temperature, in units of [J/mol/K]. Subtracts R from the ideal-gas heat capacity; does not include pressure-compensation from an equation of state.

```
>>> w = Chemical('water', T=520)
>>> w.Cvgm
27.13366316134193
```

Grashof(Tw=None, L=None)

### property Hill

Hill formula of a compound. For a description of the Hill system, see chemicals.elements. atoms\_to\_Hill.

### **Examples**

```
>>> Chemical('furfuryl alcohol').Hill
'C5H602'
```

# property Hvap

Enthalpy of vaporization of the chemical at its current temperature, in units of [J/kg].

This property uses the object-oriented interface thermo.phase\_change.EnthalpyVaporization, but converts its results from molar to mass units.

# **Examples**

```
>>> Chemical('water', T=320).Hvap
2389540.219347256
```

#### property Hvapm

Enthalpy of vaporization of the chemical at its current temperature, in units of [J/mol]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.phase\_change.EnthalpyVaporization*; each Chemical instance creates one to actually perform the calculations.

# **Examples**

# property JT

Joule Thomson coefficient of the chemical at its current phase and temperature, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[T\left(\frac{\partial V}{\partial T}\right)_{P} - V\right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

```
>>> Chemical('water').JT
-2.2150394958666407e-07
```

# property JTg

Joule Thomson coefficient of the chemical in the gas phase at its current temperature and pressure, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[T\left(\frac{\partial V}{\partial T}\right)_{P} - V\right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

Utilizes the temperature-derivative method of thermo.volume.VolumeGas and the temperaturedependent heat capacity method thermo.heat\_capacity.HeatCapacityGas to obtain the properties required for the actual calculation.

#### **Examples**

```
>>> Chemical('dodecane', T=400, P=1000).JTg
5.4089897835384913e-05
```

# property JT1

Joule Thomson coefficient of the chemical in the liquid phase at its current temperature and pressure, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_H = \frac{1}{C_p} \left[T\left(\frac{\partial V}{\partial T}\right)_P - V\right] = \frac{V}{C_p} \left(\beta T - 1\right)$$

Utilizes the temperature-derivative method of thermo.volume.VolumeLiquid and the temperaturedependent heat capacity method thermo.heat\_capacity.HeatCapacityLiquid to obtain the properties required for the actual calculation.

# **Examples**

```
>>> Chemical('dodecane', T=400).JTl
-3.0827160465192742e-07
```

### Jakob(Tw=None)

#### property PSRK\_groups

Dictionary of PSRK subgroup: count groups for the PSRK subgroups, as determined by DDBST's online service.

# **Examples**

```
>>> Chemical('Cumene').PSRK_groups
{1: 2, 9: 5, 13: 1}
```

### property Parachor

Parachor of the chemical at its current temperature and pressure, in units of [N^0.25\*m^2.75/mol].

$$P = \frac{\sigma^{0.25} MW}{\rho_L - \rho_V}$$

Calculated based on surface tension, density of the liquid phase, and molecular weight. For uses of this property, see thermo.utils.Parachor.

The gas density is calculated using the ideal-gas law.

# **Examples**

>>> Chemical('octane').Parachor
6.2e-05

# Peclet\_heat(V=None, D=None)

# property Poynting

Poynting correction factor [dimensionless] for use in phase equilibria methods based on activity coefficients or other reference states. Performs the shortcut calculation assuming molar volume is independent of pressure.

$$\operatorname{Poy} = \exp\left[\frac{V_l(P - P^{sat})}{RT}\right]$$

The full calculation normally returns values very close to the approximate ones. This property is defined in terms of pure components only.

# **Notes**

The full equation shown below can be used as follows:

$$\operatorname{Poy} = \exp\left[\frac{\int_{P_i^{sat}}^{P} V_i^l dP}{RT}\right]$$

>>> from scipy.integrate import quad >>> c = Chemical('pentane', T=300, P=1E7) >>> exp(quad(lambda P : c.VolumeLiquid(c.T, P), c.Psat, c.P)[0]/R/c.T) 1.5821826990975127

# **Examples**

```
>>> Chemical('pentane', T=300, P=1E7).Poynting
1.5743051250679803
```

#### property Pr

Prandtl number of the chemical at its current temperature, pressure, and phase; [dimensionless].

$$Pr = \frac{C_p \mu}{k}$$

```
>>> Chemical('acetone').Pr
4.183039103542709
```

### property Prg

Prandtl number of the gas phase of the chemical at its current temperature and pressure, [dimensionless].

 $Pr = \frac{C_p \mu}{k}$ 

Utilizes the temperature and pressure dependent object oriented interfaces thermo.viscosity. *ViscosityGas*, thermo.thermal\_conductivity.ThermalConductivityGas, and thermo.heat\_capacity.HeatCapacityGas to calculate the actual properties.

### **Examples**

>>> Chemical('NH3').Prg
0.847263731933008

### property Prl

Prandtl number of the liquid phase of the chemical at its current temperature and pressure, [dimensionless].

$$Pr = \frac{C_p \mu}{k}$$

Utilizes the temperature and pressure dependent object oriented interfaces thermo.viscosity. ViscosityLiquid, thermo.thermal\_conductivity.ThermalConductivityLiquid, and thermo. heat\_capacity.HeatCapacityLiquid to calculate the actual properties.

### **Examples**

>>> Chemical('nitrogen', T=70).Prl
2.7828214501488886

### property Psat

Vapor pressure of the chemical at its current temperature, in units of [Pa]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.vapor\_pressure.VaporPressure*; each Chemical instance creates one to actually perform the calculations.

### **Examples**

# property R\_specific

Specific gas constant, in units of [J/kg/K].

```
>>> Chemical('water').R_specific
461.52265188218
```

**Reynolds**(V=None, D=None)

# property SG

Specific gravity of the chemical, [dimensionless].

For gas-phase conditions, this is calculated at 15.6  $^{\circ}$ C (60  $^{\circ}$ F) and 1 atm for the chemical and the reference fluid, air. For liquid and solid phase conditions, this is calculated based on a reference fluid of water at 4  $^{\circ}$ C at 1 atm, but the with the liquid or solid chemical's density at the currently specified conditions.

# **Examples**

```
>>> Chemical('MTBE').SG
0.7428160596603596
```

### property SGg

Specific gravity of the gas phase of the chemical, [dimensionless]. The reference condition is air at 15.6 °C (60 °F) and 1 atm (rho=1.223 kg/m^3). The definition for gases uses the compressibility factor of the reference gas and the chemical both at the reference conditions, not the conditions of the chemical.

### **Examples**

```
>>> Chemical('argon').SGg
1.3795835970877504
```

#### property SGl

Specific gravity of the liquid phase of the chemical at the specified temperature and pressure, [dimension-less]. The reference condition is water at 4 °C and 1 atm (rho=999.017 kg/m^3). For liquids, SG is defined that the reference chemical's T and P are fixed, but the chemical itself varies with the specified T and P.

### **Examples**

```
>>> Chemical('water', T=365).SGl
0.9650065522428539
```

### property SGs

Specific gravity of the solid phase of the chemical at the specified temperature and pressure, [dimension-less]. The reference condition is water at 4 °C and 1 atm (rho=999.017 kg/m^3). The SG varries with temperature and pressure but only very slightly.

```
>>> Chemical('iron').SGs
7.87774317235069
```

# Tsat(P)

# property U

Internal energy of the chemical at its current temperature and pressure, in units of [J/kg].

This property requires that thermo.chemical.set\_thermo ran successfully to be accurate. It also depends on the molar volume of the chemical at its current conditions.

# property UNIFAC\_Dortmund\_groups

Dictionary of Dortmund UNIFAC subgroup: count groups for the Dortmund UNIFAC subgroups, as determined by DDBST's online service.

# **Examples**

>>> Chemical('Cumene').UNIFAC\_Dortmund\_groups
{1: 2, 9: 5, 13: 1}

# property UNIFAC\_Q

UNIFAC Q (normalized Van der Waals area), dimensionless. Used in the UNIFAC model.

# **Examples**

```
>>> Chemical('decane').UNIFAC_Q
6.016
```

# property UNIFAC\_R

UNIFAC R (normalized Van der Waals volume), dimensionless. Used in the UNIFAC model.

# **Examples**

```
>>> Chemical('benzene').UNIFAC_R
3.1878
```

# property UNIFAC\_groups

Dictionary of UNIFAC subgroup: count groups for the original UNIFAC subgroups, as determined by DDBST's online service.

```
>>> Chemical('Cumene').UNIFAC_groups
{1: 2, 9: 5, 13: 1}
```

# property Um

Internal energy of the chemical at its current temperature and pressure, in units of [J/mol].

This property requires that thermo.chemical.set\_thermo ran successfully to be accurate. It also depends on the molar volume of the chemical at its current conditions.

# property Van\_der\_Waals\_area

Unnormalized Van der Waals area, in units of [m^2/mol].

# **Examples**

```
>>> Chemical('hexane').Van_der_Waals_area
964000.0
```

#### property Van\_der\_Waals\_volume

Unnormalized Van der Waals volume, in units of [m^3/mol].

### **Examples**

```
>>> Chemical('hexane').Van_der_Waals_volume
6.8261966e-05
```

# property Vm

Molar volume of the chemical at its current phase and temperature and pressure, in units of [m^3/mol].

Utilizes the object oriented interfaces thermo.volume.VolumeSolid, thermo.volume. VolumeLiquid, and thermo.volume.VolumeGas to perform the actual calculation of each property.

# **Examples**

```
>>> Chemical('ethylbenzene', T=550, P=3E6).Vm
0.00017758024401627633
```

# property Vmg

Gas-phase molar volume of the chemical at its current temperature and pressure, in units of [m^3/mol]. For calculation of this property at other temperatures or pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume.VolumeGas*; each Chemical instance creates one to actually perform the calculations.

Estimate the molar volume of the core of the sun, at 15 million K and 26.5 PetaPascals, assuming pure helium (actually 68% helium):

```
>>> Chemical('helium', T=15E6, P=26.5E15).Vmg
4.805464238181197e-07
```

### property Vmg\_ideal

Gas-phase molar volume of the chemical at its current temperature and pressure calculated with the idealgas law, in units of [m^3/mol].

# **Examples**

```
>>> Chemical('helium', T=300.0, P=1e5).Vmg_ideal
0.0249433878544
```

# property Vml

Liquid-phase molar volume of the chemical at its current temperature and pressure, in units of [m^3/mol]. For calculation of this property at other temperatures or pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume.VolumeLiquid*; each Chemical instance creates one to actually perform the calculations.

#### Examples

```
>>> Chemical('cyclobutane', T=225).Vml
7.42395423425395e-05
```

#### property Vms

Solid-phase molar volume of the chemical at its current temperature, in units of [m^3/mol]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume.VolumeSolid*; each Chemical instance creates one to actually perform the calculations.

### **Examples**

```
>>> Chemical('iron').Vms
7.09593392630242e-06
```

Weber(V=None, D=None)

# property Z

Compressibility factor of the chemical at its current phase and temperature and pressure, [dimensionless].

```
>>> Chemical('MTBE', T=900, P=1E-2).Z
0.9999999999079768
```

# property Zg

Compressibility factor of the chemical in the gas phase at the current temperature and pressure, [dimensionless].

Utilizes the object oriented interface and thermo.volume.VolumeGas to perform the actual calculation of molar volume.

# **Examples**

```
>>> Chemical('sulfur hexafluoride', T=700, P=1E9).Zg
11.140084184207813
```

# property Zl

Compressibility factor of the chemical in the liquid phase at the current temperature and pressure, [dimensionless].

Utilizes the object oriented interface and *thermo.volume.VolumeLiquid* to perform the actual calculation of molar volume.

# **Examples**

```
>>> Chemical('water').Zl
0.0007385375470263454
```

#### property Zs

Compressibility factor of the chemical in the solid phase at the current temperature and pressure, [dimensionless].

Utilizes the object oriented interface and thermo.volume.VolumeSolid to perform the actual calculation of molar volume.

# **Examples**

```
>>> Chemical('palladium').Z
0.00036248477437931853
```

# property absolute\_permittivity

Absolute permittivity of the chemical at its current temperature, in units of [farad/meter]. Those units are equivalent to ampere^2\*second^4/kg/m^3.

```
>>> Chemical('water', T=293.15).absolute_permittivity
7.096684821859018e-10
```

# property alpha

Thermal diffusivity of the chemical at its current temperature, pressure, and phase in units of  $[m^{2}/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

# **Examples**

```
>>> Chemical('furfural').alpha
8.696537158635412e-08
```

# property alphag

Thermal diffusivity of the gas phase of the chemical at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

Utilizes the temperature and pressure dependent object oriented interfaces thermo.volume.VolumeGas, thermo.thermal\_conductivity.ThermalConductivityGas, and thermo.heat\_capacity. HeatCapacityGas to calculate the actual properties.

### **Examples**

>>> Chemical('ammonia').alphag
1.6931865425158556e-05

### property alphal

Thermal diffusivity of the liquid phase of the chemical at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

Utilizes the temperature and pressure dependent object oriented interfaces thermo.volume. VolumeLiquid, thermo.thermal\_conductivity.ThermalConductivityLiquid, and thermo. heat\_capacity.HeatCapacityLiquid to calculate the actual properties.

# **Examples**

```
>>> Chemical('nitrogen', T=70).alphal
9.444949636299626e-08
```

# property aromatic\_rings

Number of aromatic rings in a chemical, computed with RDKit from a chemical's SMILES. If RDKit is not available, holds None.

```
>>> Chemical('Paclitaxel').aromatic_rings
3
```

## property atom\_fractions

Dictionary of atom: fractional occurence of the elements in a chemical. Useful when performing element balances. For mass-fraction occurences, see *mass\_fractions*.

## Examples

```
>>> Chemical('Ammonium aluminium sulfate').atom_fractions
{'H': 0.25, 'S': 0.125, 'Al': 0.0625, 'O': 0.5, 'N': 0.0625}
```

 $calc_H(T, P)$ 

calc\_H\_excess(T, P)

 $calc_S(T, P)$ 

calc\_S\_excess(T, P)

calculate(T=None, P=None)

calculate\_PH(P, H)

calculate\_PS(P, S)

calculate\_TH(T, H)

calculate\_TS(T, S)

#### property charge

Charge of a chemical, computed with RDKit from a chemical's SMILES. If RDKit is not available, holds None.

## Examples

>>> Chemical('sodium ion').charge
1

#### draw\_2d(width=300, height=300, Hs=False)

Interface for drawing a 2D image of the molecule. Requires an HTML5 browser, and the libraries RDKit and IPython. An exception is raised if either of these libraries is absent.

#### Parameters

width [int] Number of pixels wide for the view

height [int] Number of pixels tall for the view

Hs [bool] Whether or not to show hydrogen

## Examples

>>> Chemical('decane').draw\_2d()
<PIL.Image.Image image mode=RGBA size=300x300 at 0x...>

draw\_3d(width=300, height=500, style='stick', Hs=True, atom\_labels=True)

Interface for drawing an interactive 3D view of the molecule. Requires an HTML5 browser, and the libraries RDKit, pymol3D, and IPython. An exception is raised if all three of these libraries are not installed.

#### **Parameters**

width [int] Number of pixels wide for the view, [pixels]

height [int] Number of pixels tall for the view, [pixels]

style [str] One of 'stick', 'line', 'cross', or 'sphere', [-]

Hs [bool] Whether or not to show hydrogen, [-]

atom\_labels [bool] Whether or not to label the atoms, [-]

#### **Examples**

```
>>> Chemical('cubane').draw_3d()
<IPython.core.display.HTML object>
```

## property economic\_status

Dictionary of economic status indicators for the chemical.

#### **Examples**

```
>>> Chemical('benzene').economic_status
["US public: {'Manufactured': 6165232.1, 'Imported': 463146.474, 'Exported':_
→271908.252}",
u'1,000,000 - 10,000,000 tonnes per annum',
u'Intermediate Use Only',
'OECD HPV Chemicals']
```

## property eos

Equation of state object held by the chemical; used to calculate excess thermodynamic quantities, and also provides a vapor pressure curve, enthalpy of vaporization curve, fugacity, thermodynamic partial derivatives, and more; see *thermo.eos* for a full listing.

```
>>> Chemical('methane').eos.V_g
0.02441019502181826
```

## property isentropic\_exponent

Gas-phase ideal-gas isentropic exponent of the chemical at its current temperature, [dimensionless]. Does not include pressure-compensation from an equation of state.

## **Examples**

```
>>> Chemical('hydrogen').isentropic_exponent
1.405237786321222
```

## property isobaric\_expansion

Isobaric (constant-pressure) expansion of the chemical at its current phase and temperature, in units of [1/K].

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

#### **Examples**

Radical change in value just above and below the critical temperature of water:

```
>>> Chemical('water', T=647.1, P=22048320.0).isobaric_expansion
0.34074205839222449
```

```
>>> Chemical('water', T=647.2, P=22048320.0).isobaric_expansion
0.18143324022215077
```

#### property isobaric\_expansion\_g

Isobaric (constant-pressure) expansion of the gas phase of the chemical at its current temperature and pressure, in units of [1/K].

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_{F}$$

Utilizes the temperature-derivative method of thermo.VolumeGas to perform the actual calculation. The derivatives are all numerical.

## **Examples**

```
>>> Chemical('Hexachlorobenzene', T=900).isobaric_expansion_g
0.001151869741981048
```

#### property isobaric\_expansion\_l

Isobaric (constant-pressure) expansion of the liquid phase of the chemical at its current temperature and pressure, in units of [1/K].

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

Utilizes the temperature-derivative method of *thermo.volume.VolumeLiquid* to perform the actual calculation. The derivatives are all numerical.

### **Examples**

```
>>> Chemical('dodecane', T=400).isobaric_expansion_l
0.0011617555762469477
```

#### property k

Thermal conductivity of the chemical at its current phase, temperature, and pressure in units of [W/m/K].

Utilizes the object oriented interfaces thermo.thermal\_conductivity. ThermalConductivityLiquid and thermo.thermal\_conductivity.ThermalConductivityGas to perform the actual calculation of each property.

#### **Examples**

```
>>> Chemical('ethanol', T=300).kl
0.16313594741877802
>>> Chemical('ethanol', T=400).kg
0.026019924109310026
```

## property kg

Thermal conductivity of the chemical in the gas phase at its current temperature and pressure, in units of [W/m/K].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.thermal\_conductivity*. *ThermalConductivityGas*; each Chemical instance creates one to actually perform the calculations.

## **Examples**

```
>>> Chemical('water', T=320).kg
0.021273128263091207
```

#### property kl

Thermal conductivity of the chemical in the liquid phase at its current temperature and pressure, in units of [W/m/K].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.thermal\_conductivity*. *ThermalConductivityLiquid*; each Chemical instance creates one to actually perform the calculations.

```
>>> Chemical('water', T=320).kl
0.6369957248212118
```

## property legal\_status

Dictionary of legal status indicators for the chemical.

## **Examples**

```
>>> Chemical('benzene').legal_status
{'DSL': 'LISTED', 'EINECS': 'LISTED', 'NLP': 'UNLISTED', 'SPIN': 'LISTED', 'TSCA
__': 'LISTED'}
```

## property mass\_fractions

Dictionary of atom:mass-weighted fractional occurence of elements. Useful when performing mass balances. For atom-fraction occurences, see *atom\_fractions*.

## **Examples**

```
>>> Chemical('water').mass_fractions
{'H': 0.11189834407236524, '0': 0.8881016559276347}
```

#### property mu

Viscosity of the chemical at its current phase, temperature, and pressure in units of [Pa\*s].

Utilizes the object oriented interfaces *thermo.viscosity.ViscosityLiquid* and *thermo.viscosity.ViscosityGas* to perform the actual calculation of each property.

## **Examples**

```
>>> Chemical('ethanol', T=300).mu
0.001044526538460911
>>> Chemical('ethanol', T=400).mu
1.1853097849748217e-05
```

## property mug

Viscosity of the chemical in the gas phase at its current temperature and pressure, in units of [Pa\*s].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.viscosity.ViscosityGas*; each Chemical instance creates one to actually perform the calculations.

```
>>> Chemical('water', T=320, P=100).mug
1.0431450856297212e-05
```

#### property mul

Viscosity of the chemical in the liquid phase at its current temperature and pressure, in units of [Pa\*s].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.viscosity.ViscosityLiquid*; each Chemical instance creates one to actually perform the calculations.

## **Examples**

```
>>> Chemical('water', T=320).mul
0.0005767262693751547
```

#### property nu

Kinematic viscosity of the chemical at its current temperature, pressure, and phase in units of [m<sup>2</sup>/s].

 $\nu = \frac{\mu}{\rho}$ 

#### **Examples**

>>> Chemical('argon').nu
1.3846930410865003e-05

#### property nug

Kinematic viscosity of the gas phase of the chemical at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\nu = \frac{\mu}{\rho}$$

Utilizes the temperature and pressure dependent object oriented interfaces *thermo.volume.VolumeGas*, *thermo.viscosity.ViscosityGas* to calculate the actual properties.

## **Examples**

```
>>> Chemical('methane', T=115).nug
2.5056924327995865e-06
```

#### property nul

Kinematic viscosity of the liquid phase of the chemical at its current temperature and pressure, in units of  $[m^2/s]$ .

 $\nu = \frac{\mu}{\rho}$ 

Utilizes the temperature and pressure dependent object oriented interfaces thermo.volume. VolumeLiquid, thermo.viscosity.ViscosityLiquid to calculate the actual properties.

```
>>> Chemical('methane', T=110).nul
2.858088468937331e-07
```

## property permittivity

Relative permittivity (dielectric constant) of the chemical at its current temperature, [dimensionless].

For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.permittivity.PermittivityLiquid*; each Chemical instance creates one to actually perform the calculations.

## **Examples**

```
>>> Chemical('toluene', T=250).permittivity
2.49775625
```

#### property rdkitmol

RDKit object of the chemical, without hydrogen. If RDKit is not available, holds None.

For examples of what can be done with RDKit, see their website.

#### property rdkitmol\_Hs

RDKit object of the chemical, with hydrogen. If RDKit is not available, holds None.

For examples of what can be done with RDKit, see their website.

#### property rho

Mass density of the chemical at its current phase and temperature and pressure, in units of [kg/m^3].

Utilizes the object oriented interfaces thermo.volume.VolumeSolid, thermo.volume. VolumeLiquid, and thermo.volume.VolumeGas to perform the actual calculation of each property. Note that those interfaces provide output in units of m^3/mol.

## **Examples**

```
>>> Chemical('decane', T=550, P=2E6).rho
498.67008448640604
```

#### property rhog

Gas-phase mass density of the chemical at its current temperature and pressure, in units of [kg/m^3]. For calculation of this property at other temperatures or pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume.VolumeGas*; each Chemical instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

Estimate the density of the core of the sun, at 15 million K and 26.5 PetaPascals, assuming pure helium (actually 68% helium):

```
>>> Chemical('helium', T=15E6, P=26.5E15).rhog
8329.27226509739
```

Compared to a result on Wikipedia of 150000 kg/m^3, the fundamental equation of state performs poorly.

```
>>> He = Chemical('helium', T=15E6, P=26.5E15)
>>> He.VolumeGas.method_P = 'IDEAL'
>>> He.rhog
850477.8
```

The ideal-gas law performs somewhat better, but vastly overshoots the density prediction.

#### property rhogm

Molar density of the chemical in the gas phase at the current temperature and pressure, in units of [mol/m^3].

Utilizes the object oriented interface and *thermo.volume.VolumeGas* to perform the actual calculation of molar volume.

#### **Examples**

```
>>> Chemical('tungsten hexafluoride').rhogm
42.01349946063116
```

#### property rhol

Liquid-phase mass density of the chemical at its current temperature and pressure, in units of [kg/m^3]. For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume.VolumeLiquid*; each Chemical instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

## **Examples**

```
>>> Chemical('o-xylene', T=297).rhol
876.9946785618097
```

#### property rholm

Molar density of the chemical in the liquid phase at the current temperature and pressure, in units of [mol/m^3].

Utilizes the object oriented interface and *thermo.volume.VolumeLiquid* to perform the actual calculation of molar volume.

```
>>> Chemical('nitrogen', T=70).rholm
29937.20179186975
```

## property rhom

Molar density of the chemical at its current phase and temperature and pressure, in units of [mol/m^3].

Utilizes the object oriented interfaces thermo.volume.VolumeSolid, thermo.volume. VolumeLiquid, and thermo.volume.VolumeGas to perform the actual calculation of each property. Note that those interfaces provide output in units of m^3/mol.

## **Examples**

>>> Chemical('1-hexanol').rhom
7983.414573003429

#### property rhos

Solid-phase mass density of the chemical at its current temperature, in units of [kg/m^3]. For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume.VolumeSolid*; each Chemical instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

#### Examples

```
>>> Chemical('iron').rhos
7869.999999999994
```

#### property rhosm

Molar density of the chemical in the solid phase at the current temperature and pressure, in units of [mol/m^3].

Utilizes the object oriented interface and *thermo.volume.VolumeSolid* to perform the actual calculation of molar volume.

## **Examples**

```
>>> Chemical('palladium').rhosm
112760.75925577903
```

#### property rings

Number of rings in a chemical, computed with RDKit from a chemical's SMILES. If RDKit is not available, holds None.

```
>>> Chemical('Paclitaxel').rings
7
```

## set\_TP\_sources()

#### set\_constant\_sources()

#### set\_constants()

set\_eos(T, P, eos=<class 'thermo.eos.PR'>)

**set\_ref**(*T\_ref=298.15*, *P\_ref=101325*, *phase\_ref='calc'*, *H\_ref=0*, *S\_ref=0*)

#### set\_thermo()

#### property sigma

Surface tension of the chemical at its current temperature, in units of [N/m].

For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.interface.SurfaceTension*; each Chemical instance creates one to actually perform the calculations.

## **Examples**

```
>>> Chemical('water', T=320).sigma
0.06855002575793023
>>> Chemical('water', T=320).SurfaceTension.solve_property(0.05)
416.8307110842183
```

#### property solubility\_parameter

Solubility parameter of the chemical at its current temperature and pressure, in units of [Pa^0.5].

$$\delta = \sqrt{\frac{\Delta H_{vap} - RT}{V_m}}$$

Calculated based on enthalpy of vaporization and molar volume. Normally calculated at STP. For uses of this property, see thermo.solubility.solubility\_parameter.

## **Examples**

```
>>> Chemical('NH3').solubility_parameter
24766.329043856073
```

# 7.4 Chemical Constants and Correlations (thermo.chemical\_package)

This module contains classes for storing data and objects which are necessary for doing thermodynamic calculations. The intention for these classes is to serve as an in-memory storage layer between the disk and methods which do full thermodynamic calculations.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Chemical Constants Class
- Chemical Correlations Class
- Sample Constants and Correlations

# 7.4.1 Chemical Constants Class

<i>Tms=None</i> , <i>Tbs=None</i> , <i>Tcs=None</i> ,
Pcs=None, Vcs=None, omegas=None,
Zcs=None, rhocs=None, rhocs_mass=No
Hfus_Tms=None, Hfus_Tms_mass=None
Hvap_Tbs=None, Hvap_Tbs_mass=Non
Vml_STPs=None, rhol_STPs=None,
rhol_STPs_mass=None, Vml_60Fs=Non
rhol_60Fs=None, rhol_60Fs_mass=Non
Vmg_STPs=None, rhog_STPs=None,
rhog_STPs_mass=None, Hfgs=None,
Hfgs_mass=None, Gfgs=None,
Gfgs_mass=None, Sfgs=None,
Sfgs_mass=None, S0gs=None,
SOgs_mass=None, Hf_STPs=None,
Hf_STPs_mass=None, Tts=None, Pts=N
Hsub_Tts=None, Hsub_Tts_mass=None,
Hcs=None, Hcs_mass=None,
Hcs_lower=None, Hcs_lower_mass=Non
Tflashs=None, Tautoignitions=None,
LFLs=None, UFLs=None, TWAs=None,
STELs=None, Ceilings=None, Skins=No
Carcinogens=None, legal_statuses=Non
economic_statuses=None, GWPs=None,
ODPs=None, logPs=None,
Psat_298s=None, Hvap_298s=None,
Hvap_298s_mass=None, Vml_Tms=Non
rhos_Tms=None, Vms_Tms=None,
rhos_Tms_mass=None, sigma_STPs=No
sigma_Tbs=None, sigma_Tms=None,
RIs=None, RI_Ts=None,
conductivities=None, conductivity_Ts=N
charges=None, dipoles=None,
Stockmayers=None,
molecular_diameters=None,
Van_der_Waals_volumes=None,
Van_der_Waals_areas=None,
Parachors=None, StielPolars=None,
atomss=None, atom_fractions=None,
similarity_variables=None,
phase_STPs=None,
solubility_parameters=None,
PubChems=None, formulas=None,
smiless=None, InChIs=None,
InChI_Keys=None, UNIFAC_groups=No
UNIFAC_Dortmund_groups=None,
PSRK_groups=None, UNIFAC_Rs=None UNIFAC Os=None)

which a set of thermodynamic methods can access miscellaneous for purposes such as phase identification or initialization.

#### Parameters

- **N** [int] Number of components in the package, [-].
- cmps [range] Iterator over all components, [-].
- rhol\_60Fs [list[float]] Liquid molar densities for each component at 60 °F, [mol/m^3].
- **atom\_fractions** [list[dict]] Breakdown of each component into its elemental fractions, as a dict, [-].
- **atomss** [list[dict]] Breakdown of each component into its elements and their counts, as a dict, [-].
- Carcinogens [list[dict]] Status of each component in cancer causing registries, [-].
- CASs [list[str]] CAS registration numbers for each component, [-].
- **Ceilings** [list[tuple[(float, str)]]] Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].
- charges [list[float]] Charge number (valence) for each component, [-].
- conductivities [list[float]] Electrical conductivities for each component, [S/m].
- **conductivity\_Ts** [list[float]] Temperatures at which the electrical conductivities for each component were measured, [K].
- **dipoles** [list[float]] Dipole moments for each component, [debye].
- **economic\_statuses** [list[dict]] Status of each component in in relation to import and export from various regions, [-].
- formulas [list[str]] Formulas of each component, [-].
- **Gfgs** [list[float]] Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].
- **Gfgs\_mass** [list[float]] Ideal gas standard Gibbs free energy of formation for each component, [J/kg].
- **GWPs** [list[float]] Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].
- Hcs [list[float]] Higher standard molar heats of combustion for each component, [J/mol].
- Hcs\_mass [list[float]] Higher standard heats of combustion for each component, [J/kg].
- Hcs\_lower [list[float]] Lower standard molar heats of combustion for each component, [J/mol].
- **Hcs lower mass** [list[float]] Lower standard heats of combustion for each component, [J/kg].
- **Hfgs** [list[float]] Ideal gas standard molar enthalpies of formation for each component, [J/mol].
- **Hfgs\_mass** [list[float]] Ideal gas standard enthalpies of formation for each component, [J/kg].
- **Hfus\_Tms** [list[float]] Molar heats of fusion for each component at their respective melting points, [J/mol].
- **Hfus\_Tms\_mass** [list[float]] Heats of fusion for each component at their respective melting points, [J/kg].
- Hsub\_Tts [list[float]] Heats of sublimation for each component at their respective triple points, [J/mol].
- Hsub\_Tts\_mass [list[float]] Heats of sublimation for each component at their respective triple points, [J/kg].

- Hvap\_298s [list[float]] Molar heats of vaporization for each component at 298.15 K, [J/mol].
- Hvap\_298s\_mass [list[float]] Heats of vaporization for each component at 298.15 K, [J/kg].
- **Hvap\_Tbs** [list[float]] Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].
- Hvap\_Tbs\_mass [list[float]] Heats of vaporization for each component at their respective normal boiling points, [J/kg].
- InChI\_Keys [list[str]] InChI Keys for each component, [-].
- InChIs [list[str]] InChI strings for each component, [-].
- **legal\_statuses** [list[dict]] Status of each component in in relation to import and export rules from various regions, [-].
- LFLs [list[float]] Lower flammability limits for each component, [-].
- logPs [list[float]] Octanol-water partition coefficients for each component, [-].
- **molecular\_diameters** [list[float]] Lennard-Jones molecular diameters for each component, [angstrom].
- **MWs** [list[float]] Similativy variables for each component, [g/mol].
- names [list[str]] Names for each component, [-].
- **ODPs** [list[float]] Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

**omegas** [list[float]] Acentric factors for each component, [-].

Parachors [list[float]] Parachors for each component, [N^0.25\*m^2.75/mol].

Pcs [list[float]] Critical pressures for each component, [Pa].

phase\_STPs [list[str]] Standard states ('g', 'l', or 's') for each component, [-].

**Psat\_298s** [list[float]] Vapor pressures for each component at 298.15 K, [Pa].

PSRK\_groups [list[dict]] PSRK subgroup: count groups for each component, [-].

Pts [list[float]] Triple point pressures for each component, [Pa].

PubChems [list[int]] Pubchem IDs for each component, [-].

**rhocs** [list[float]] Molar densities at the critical point for each component, [mol/m^3].

rhocs\_mass [list[float]] Densities at the critical point for each component, [kg/m^3].

rhol\_STPs [list[float]] Molar liquid densities at STP for each component, [mol/m^3].

rhol\_STPs\_mass [list[float]] Liquid densities at STP for each component, [kg/m^3].

**RIs** [list[float]] Refractive indexes for each component, [-].

- **RI\_Ts** [list[float]] Temperatures at which the refractive indexes were reported for each component, [K].
- **S0gs** [list[float]] Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].
- **S0gs\_mass** [list[float]] Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].
- **Sfgs** [list[float]] Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

- **Sfgs\_mass** [list[float]] Ideal gas standard entropies of formation for each component, [J/(kg\*K)].
- solubility\_parameters [list[float]] Solubility parameters for each component at 298.15 K, [Pa^0.5].
- similarity\_variables [list[float]] Similarity variables for each component, [mol/g].
- Skins [list[bool]] Whether each compound can be absorbed through the skin or not, [-].
- smiless [list[str]] SMILES identifiers for each component, [-].
- **STELs** [list[tuple[(float, str)]]] Short term exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].
- StielPolars [list[float]] Stiel polar factors for each component, [-].
- **Stockmayers** [list[float]] Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].
- Tautoignitions [list[float]] Autoignition temperatures for each component, [K].
- **Tbs** [list[float]] Boiling temperatures for each component, [K].
- Tcs [list[float]] Critical temperatures for each component, [K].
- Tms [list[float]] Melting temperatures for each component, [K].
- Tflashs [list[float]] Flash point temperatures for each component, [K].
- Tts [list[float]] Triple point temperatures for each component, [K].
- **TWAs** [list[tuple[(float, str)]]] Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m^3), [various].
- UFLs [list[float]] Upper flammability limits for each component, [-].
- **UNIFAC\_Dortmund\_groups** [list[dict]] UNIFAC\_Dortmund\_group: count groups for each component, [-].
- UNIFAC\_groups [list[dict]] UNIFAC\_group: count groups for each component, [-].
- UNIFAC\_Rs [list[float]] UNIFAC R parameters for each component, [-].
- UNIFAC\_Qs [list[float]] UNIFAC Q parameters for each component, [-].
- Van\_der\_Waals\_areas [list[float]] Unnormalized Van der Waals areas for each component, [m^2/mol].
- Van\_der\_Waals\_volumes [list[float]] Unnormalized Van der Waals volumes for each component, [m^3/mol].
- Vcs [list[float]] Critical molar volumes for each component, [m^3/mol].
- **Vml\_STPs** [list[float]] Liquid molar volumes for each component at STP, [m^3/mol].
- Vml\_Tms [list[float]] Liquid molar volumes for each component at their respective melting points, [m^3/mol].
- Vms\_Tms [list[float]] Solid molar volumes for each component at their respective melting points, [m^3/mol].
- Vml\_60Fs [list[float]] Liquid molar volumes for each component at 60 °F, [m^3/mol].
- **rhos\_Tms** [list[float]] Solid molar densities for each component at their respective melting points, [mol/m^3].
- rhol\_60Fs\_mass [list[float]] Liquid mass densities for each component at 60 °F, [kg/m^3].

- **rhos\_Tms\_mass** [list[float]] Solid mass densities for each component at their melting point, [kg/m^3].
- Zcs [list[float]] Critical compressibilities for each component, [-].
- **n\_atoms** [int] Number of total atoms in a collection of 1 molecule of each species, [-].
- water\_index [int] Index of water in the package, [-].
- Vmg\_STPs [list[float]] Gas molar volumes for each component at STP; metastable if normally another state, [m<sup>3</sup>/mol].
- **rhog\_STPs** [list[float]] Molar gas densities at STP for each component; metastable if normally another state, [mol/m<sup>3</sup>].
- **rhog\_STPs\_mass** [list[float]] Gas densities at STP for each component; metastable if normally another state, [kg/m^3].
- **sigma\_STPs** [list[float]] Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].
- sigma\_Tms [list[float]] Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].
- sigma\_Tbs [list[float]] Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].
- Hf\_STPs [list[float]] Standard state molar enthalpies of formation for each component, [J/mol].
- **Hf\_STPs\_mass** [list[float]] Standard state mass enthalpies of formation for each component, [J/kg].

#### Notes

All parameters are also attributes.

#### **Examples**

Create a package with water and the xylenes, suitable for use with equations of state:

## Methods

as_json()	Method to create a JSON friendly serialization of the chemical constants package which can be stored, and reloaded later.
<pre>constants_from_IDs(IDs)</pre>	Method to construct a new <i>ChemicalConstantsPack-age</i> with loaded parameters from the chemicals library, using whatever default methods and values happen to be in that library.
correlations_from_IDs(IDs)	
	Method to construct a new <i>PropertyCorrelation-sPackage</i> with loaded parameters from the chemicals library, using whatever default methods and values happen to be in that library.
from_IDs(IDs)	
	Method to construct a new <i>ChemicalConstantsPackage</i> and <i>PropertyCorrelationsPackage</i> with loaded parameters from the chemicals library, using whatever default methods and values happen to be in that library.
<pre>from_j son(json_repr)</pre>	Method to create a ChemicalConstantsPackage from a JSON serialization of another ChemicalCon- stantsPackage.
<pre>subset([idxs, properties])</pre>	Method to construct a new ChemicalConstantsPack- age that removes all components not specified in the <i>idxs</i> argument.
<pre>with_new_constants(**kwargs)</pre>	Method to construct a new ChemicalConstantsPack- age that replaces or adds one or more properties for all components.

## \_\_add\_\_(b)

Method to create a new *ChemicalConstantsPackage* object from two other *ChemicalConstantsPackage* objects.

#### Returns

new [ChemicalConstantsPackage] New object, [-]

## **Examples**

```
>>> a = ChemicalConstantsPackage.constants_from_IDs(IDs=['water', 'hexane'])
>>> b = ChemicalConstantsPackage.constants_from_IDs(IDs=['toluene'])
>>> c = a + b
```

## as\_json()

Method to create a JSON friendly serialization of the chemical constants package which can be stored, and reloaded later.

#### Returns

json\_repr [dict] Json friendly representation, [-]

```
>>> import json
>>> constants = ChemicalConstantsPackage(MWs=[18.01528, 106.165], names=['water
..., 'm-xylene'])
>>> string = json.dumps(constants.as_json())
```

## static constants\_from\_IDs(IDs)

Method to construct a new *ChemicalConstantsPackage* with loaded parameters from the chemicals library, using whatever default methods and values happen to be in that library. Expect values to change over time.

#### Parameters

**IDs** [list[str]] Identifying strings for each compound; most identifiers are accepted and all inputs are documented in chemicals.identifiers.search\_chemical,[-]

#### Returns

**constants** [ChemicalConstantsPackage] New *ChemicalConstantsPackage* with loaded values, [-]

#### **Notes**

**Warning:** chemicals is a project with a focus on collecting data and correlations from various sources. In no way is it a project to critically evaluate these and provide recommendations. You are strongly encouraged to check values from it and modify them if you want different values. If you believe there is a value which has a typographical error please report it to the chemicals project. If data is missing or not as accuracte as you would like, and you know of a better method or source, new methods and sources can be added to chemicals fairly easily once the data entry is complete. It is not feasible to add individual components, so please submit a complete table of data from the source.

#### **Examples**

#### static correlations\_from\_IDs(IDs)

Method to construct a new *PropertyCorrelationsPackage* with loaded parameters from the chemicals library, using whatever default methods and values happen to be in that library. Expect values to change over time.

#### Parameters

**IDs** [list[str]] Identifying strings for each compound; most identifiers are accepted and all inputs are documented in chemicals.identifiers.search\_chemical, [-]

#### Returns

**correlations** [PropertyCorrelationsPackage] New *PropertyCorrelationsPackage* with loaded values, [-]

#### **Notes**

**Warning:** chemicals is a project with a focus on collecting data and correlations from various sources. In no way is it a project to critically evaluate these and provide recommendations. You are strongly encouraged to check values from it and modify them if you want different values. If you believe there is a value which has a typographical error please report it to the chemicals project. If data is missing or not as accuracte as you would like, and you know of a better method or source, new methods and sources can be added to chemicals fairly easily once the data entry is complete. It is not feasible to add individual components, so please submit a complete table of data from the source.

#### **Examples**

#### static from\_IDs(IDs)

Method to construct a new *ChemicalConstantsPackage* and *PropertyCorrelationsPackage* with loaded parameters from the chemicals library, using whatever default methods and values happen to be in that library. Expect values to change over time.

#### **Parameters**

**IDs** [list[str]] Identifying strings for each compound; most identifiers are accepted and all inputs are documented in chemicals.identifiers.search\_chemical, [-]

#### Returns

- **constants** [PropertyCorrelationsPackage] New *PropertyCorrelationsPackage* with loaded values, [-]
- **correlations** [PropertyCorrelationsPackage] New *PropertyCorrelationsPackage* with loaded values, [-]

### Notes

**Warning:** chemicals is a project with a focus on collecting data and correlations from various sources. In no way is it a project to critically evaluate these and provide recommendations. You are strongly encouraged to check values from it and modify them if you want different values. If you believe there is a value which has a typographical error please report it to the chemicals project. If data is missing or not as accuracte as you would like, and you know of a better method or source, new methods and sources can be added to chemicals fairly easily once the data entry is complete. It is not feasible to add individual components, so please submit a complete table of data from the source.

## **Examples**

#### classmethod from\_json(json\_repr)

Method to create a ChemicalConstantsPackage from a JSON serialization of another ChemicalConstantsPackage. Parameters

json\_repr [dict] Json representation, [-]

Returns

constants [ChemicalConstantsPackage] Newly created object from the json serialization, [-]

## Notes

It is important that the input be in the same format as that created by *ChemicalConstantsPackage*. *as\_json*.

## **Examples**

```
>>> import json
>>> constants = ChemicalConstantsPackage(MWs=[18.01528, 106.165], names=['water
..., 'm-xylene'])
>>> string = json.dumps(constants.as_json())
>>> new_constants = ChemicalConstantsPackage.from_json(json.loads(string))
>>> assert hash(new_constants) == hash(constants)
```

```
properties = ('atom_fractions', 'atomss', 'Carcinogens', 'CASs', 'Ceilings',
'charges', 'conductivities', 'dipoles', 'economic_statuses', 'formulas', 'Gfgs',
'Gfgs_mass', 'GWPs', 'Hcs', 'Hcs_lower', 'Hcs_lower_mass', 'Hcs_mass', 'Hfgs',
'Hfgs_mass', 'Hfus_Tms', 'Hfus_Tms_mass', 'Hsub_Tts', 'Hsub_Tts_mass', 'Hvap_298s',
'Hvap_298s_mass', 'Hvap_Tbs', 'Hvap_Tbs_mass', 'InChI_Keys', 'InChIs',
'legal_statuses', 'LFLs', 'logPs', 'molecular_diameters', 'MWs', 'names', 'ODPs',
'omegas', 'Parachors', 'Pcs', 'phase_STPs', 'Psat_298s', 'PSRK_groups', 'Pts',
'PubChems', 'rhocs', 'rhocs_mass', 'rhol_STPs', 'rhol_STPs_mass', 'RIs', 'S0gs',
'SOgs_mass', 'Sfgs', 'Sfgs_mass', 'similarity_variables', 'Skins', 'smiless',
'STELs', 'StielPolars', 'Stockmayers', 'Tautoignitions', 'Tbs', 'Tcs', 'Tflashs',
'Tms', 'Tts', 'TWAs', 'UFLs', 'UNIFAC_Dortmund_groups', 'UNIFAC_groups',
'Van_der_Waals_areas', 'Van_der_Waals_volumes', 'Vcs', 'Vml_STPs', 'Vml_Tms', 'Zcs',
'UNIFAC_Rs', 'UNIFAC_Qs', 'rhos_Tms', 'Vms_Tms', 'rhos_Tms_mass',
'solubility_parameters', 'Vml_60Fs', 'rhol_60Fs', 'rhol_60Fs_mass',
'conductivity_Ts', 'RI_Ts', 'Vmg_STPs', 'rhog_STPs', 'rhog_STPs_mass', 'sigma_STPs',
'sigma_Tms', 'sigma_Tbs', 'Hf_STPs', 'Hf_STPs_mass')
```

Tuple of all properties that can be held by this object.

subset(idxs=None, properties=None)

Method to construct a new ChemicalConstantsPackage that removes all components not specified in the *idxs* argument. Although this class has a great many attributes, it is often sufficient to work with a subset of those properties; and if a list of properties is provided, only those properties will be added to the new object as well.

#### Parameters

idxs [list[int] or Slice or None] Indexes of components that should be included; if None, all components will be included , [-]

**properties** [tuple[str] or None] List of properties to be included; all properties will be included if this is not specified

#### Returns

subset\_consts [ChemicalConstantsPackage] Object with reduced properties and or components, [-]

### Notes

It is not intended for properties to be edited in this object! One optimization is that all entirely empty properties use the same list-of-Nones.

All properties should have been specified before constructing the first ChemicalConstantsPackage.

## **Examples**

#### with\_new\_constants(\*\*kwargs)

Method to construct a new ChemicalConstantsPackage that replaces or adds one or more properties for all components.

#### Parameters

**kwargs** [dict[str: list[float]]] Properties specified by name [various]

Returns

**new\_constants** [ChemicalConstantsPackage] Object with new and/or replaced properties, [-]

## **Examples**

# 7.4.2 Chemical Correlations Class

class thermo.chemical\_package.PropertyCorrelationsPackage(constants, VaporPressures=None, SublimationPressures=None, VolumeGases=None, VolumeLiquids=None, VolumeSolids=None, *HeatCapacityGases=None*, *HeatCapacityLiquids=None*, *HeatCapacitySolids=None*, ViscosityGases=None, ViscosityLiquids=None, ThermalConductivityGases=None, ThermalConductivityLiquids=None, EnthalpyVaporizations=None, EnthalpySublimations=None, SurfaceTensions=None, PermittivityLiquids=None, VolumeGasMixtureObj=None, VolumeLiquidMixtureObj=None, VolumeSolidMixtureObj=None, *HeatCapacityGasMixtureObj=None*, *HeatCapacityLiquidMixtureObj=None*, *HeatCapacitySolidMixtureObj=None*, ViscosityGasMixtureObj=None, ViscosityLiquidMixtureObj=None, ThermalConductivityGasMixtureObj=None, ThermalConductivityLiquidMixture-Obj=None, SurfaceTensionMixtureObj=None, skip missing=False) Class for creating and storing T and P and zs dependent chemical property objects. All parameters are also attributes.

This object can be used either to hold already-created property objects; or to create new ones and hold them.

## Parameters

constants [ChemicalConstantsPackage] Object holding all constant properties, [-]

- **VaporPressures** [list[thermo.vapor\_pressure.VaporPressure], optional] Objects holding vapor pressure data and methods, [-]
- **SublimationPressures** [list[thermo.vapor\_pressure.SublimationPressure], optional] Objects holding sublimation pressure data and methods, [-]
- VolumeGases [list[thermo.volume.VolumeGas], optional] Objects holding gas volume data and methods, [-]
- **VolumeLiquids** [list[*thermo.volume.VolumeLiquid*], optional] Objects holding liquid volume data and methods, [-]
- **VolumeSolids** [list[*thermo.volume.VolumeSolid*], optional] Objects holding solid volume data and methods, [-]
- **HeatCapacityGases** [list[*thermo.heat\_capacity.HeatCapacityGas*], optional] Objects holding gas heat capacity data and methods, [-]

- **HeatCapacityLiquids** [list[thermo.heat\_capacity.HeatCapacityLiquid], optional]Objects holding liquid heat capacity data and methods, [-]
- **HeatCapacitySolids** [list[*thermo.heat\_capacity.HeatCapacitySolid*], optional] Objects holding solid heat capacity data and methods, [-]
- ViscosityGases [list[thermo.viscosity.ViscosityGas], optional] Objects holding gas viscosity data and methods, [-]
- **ViscosityLiquids** [list[thermo.viscosity.ViscosityLiquid], optional] Objects holding liquid viscosity data and methods, [-]
- **ThermalConductivityGases** [list[thermo.thermal\_conductivity. ThermalConductivityGas], optional] Objects holding gas thermal conductivity data and methods, [-]
- **ThermalConductivityLiquids** [list[thermo.thermal\_conductivity. ThermalConductivityLiquid], optional] Objects holding liquid thermal conductivity data and methods, [-]
- **EnthalpyVaporizations** [list[thermo.phase\_change.EnthalpyVaporization], optional] Objects holding enthalpy of vaporization data and methods, [-]
- **EnthalpySublimations** [list[thermo.phase\_change.EnthalpySublimation], optional] Objects holding enthalpy of sublimation data and methods, [-]
- **SurfaceTensions** [list[*thermo.interface.SurfaceTension*], optional] Objects holding surface tension data and methods, [-]
- **PermittivityLiquids** [list[*thermo.permittivity.PermittivityLiquid*], optional] Objects holding permittivity data and methods, [-]
- **skip\_missing** [bool, optional] If False, any properties not provided will have objects created; if True, no extra objects will be created.
- **VolumeSolidMixture** [*thermo.volume.VolumeSolidMixture*, optional] Predictor object for the volume of solid mixtures, [-]
- **VolumeLiquidMixture** [thermo.volume.VolumeLiquidMixture, optional] Predictor object for the volume of liquid mixtures, [-]
- **VolumeGasMixture** [thermo.volume.VolumeGasMixture, optional] Predictor object for the volume of gas mixtures, [-]
- **HeatCapacityLiquidMixture** [thermo.heat\_capacity.HeatCapacityLiquidMixture, optional] Predictor object for the heat capacity of liquid mixtures, [-]
- **HeatCapacityGasMixture** [thermo.heat\_capacity.HeatCapacityGasMixture, optional] Predictor object for the heat capacity of gas mixtures, [-]
- **HeatCapacitySolidMixture** [thermo.heat\_capacity.HeatCapacitySolidMixture, optional] Predictor object for the heat capacity of solid mixtures, [-]
- **ViscosityLiquidMixture** [thermo.viscosity.ViscosityLiquidMixture, optional] Predictor object for the viscosity of liquid mixtures, [-]
- ViscosityGasMixture [thermo.viscosity.ViscosityGasMixture, optional] Predictor object for the viscosity of gas mixtures, [-]

```
ThermalConductivityLiquidMixture [thermo.thermal_conductivity.
ThermalConductivityLiquidMixture, optional] Predictor object for the thermal conductivity of liquid mixtures, [-]
```

```
ThermalConductivityGasMixture [thermo.thermal_conductivity.
```

*ThermalConductivityGasMixture*, optional] Predictor object for the thermal conductivity of gas mixtures, [-]

**SurfaceTensionMixture** [thermo.interface.SurfaceTensionMixture, optional] Predictor object for the surface tension of liquid mixtures, [-]

## **Examples**

Create a package from CO2 and n-hexane, with ideal-gas heat capacities provided while excluding all other properties:

Create a package from various data files, creating all property objects:

#### Attributes

pure\_correlations [tuple(str)] List of all pure component property objects, [-]

### Methods

subset(idxs)	Method to construct a new PropertyCorrelation-
	sPackage that removes all components not specified
	in the <i>idxs</i> argument.

\_\_add\_\_(*b*)

Method to create a new *PropertyCorrelationsPackage* object from two other *PropertyCorrelationsPackage* objects.

#### Returns

new [PropertyCorrelationsPackage] New object, [-]

```
>>> a = ChemicalConstantsPackage.correlations_from_IDs(IDs=['water', 'hexane'])
>>> b = ChemicalConstantsPackage.correlations_from_IDs(IDs=['toluene'])
>>> c = a + b
```

subset(idxs)

Method to construct a new PropertyCorrelationsPackage that removes all components not specified in the *idxs* argument.

## Parameters

idxs [list[int] or Slice or None] Indexes of components that should be included; if None, all components will be included , [-]

#### Returns

subset\_correlations [PropertyCorrelationsPackage] Object with components, [-]

## 7.4.3 Sample Constants and Correlations

```
thermo.chemical_package.iapws_constants = ChemicalConstantsPackage(CASs=['7732-18-5'],
MWs=[18.015268], omegas=[0.344], Pcs=[22064000.0], Tcs=[647.096])
ChemicalConstantsPackage : Object intended to hold the IAPWS-95 water constants for use with the
thermo.phases.IAPWS95 phase object.
thermo.chemical_package.iapws_correlations =
```

```
thermo.chemical_package.lemmon2000_constants =
ChemicalConstantsPackage(CASs=['132259-10-0'], MWs=[28.9586], omegas=[0.0335],
Pcs=[3785020.0], Tcs=[132.6312])
```

*ChemicalConstantsPackage* : Object intended to hold the Lemmon (2000) air constants for use with the *thermo.phases.DryAirLemmon* phase object.

thermo.chemical\_package.lemmon2000\_correlations =
<thermo.chemical\_package.PropertyCorrelationsPackage object>
 PropertyCorrelationsPackage: Lemmon (2000) air correlations and properties, [-]

# 7.5 Creating Property Datasheets (thermo.datasheet)

thermo.datasheet.tabulate\_constants(chemical, full=False, vertical=False)

thermo.datasheet.tabulate\_gas(chemical, Tmin=None, Tmax=None, pts=10)

thermo.datasheet.tabulate\_liq(chemical, Tmin=None, Tmax=None, pts=10)

thermo.datasheet.tabulate\_solid(chemical, Tmin=None, Tmax=None, pts=10)

thermo.datasheet.tabulate\_streams(names=None, \*args, \*\*kwargs)

# 7.6 Electrochemistry (thermo.electrochem)

This module contains models for:

- Pure substance electrical conductivity lookups
- · Correlations for aqueous electrolyte heat capacity, density, and viscosity
- Aqueous electrolyte conductivity
- Water equilibrium constants
- · Balancing experimental ion analysis results so as to meet the electroneutrality condition

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Aqueous Electrolyte Density
- Aqueous Electrolyte Heat Capacity
- Aqueous Electrolyte Viscosity
- Aqueous Electrolyte Thermal Conductivity
- Aqueous Electrolyte Electrical Conductivity
- Pure Liquid Electrical Conductivity
- Water Dissociation Equilibrium
- Balancing Ions
- Fit Coefficients and Data

# 7.6.1 Aqueous Electrolyte Density

#### thermo.electrochem.Laliberte\_density(T, ws, CASRNs)

Calculate the density of an aqueous electrolyte mixture using the form proposed by [1]. Parameters are loaded by the function as needed. Units are Kelvin and Pa\*s.

$$\rho_m = \left(\frac{w_w}{\rho_w} + \sum_i \frac{w_i}{\rho_{app_i}}\right)^{-1}$$

#### **Parameters**

T [float] Temperature of fluid [K]

ws [array] Weight fractions of fluid components other than water

CASRNs [array] CAS numbers of the fluid components other than water

## Returns

rho [float] Solution density, [kg/m^3]

## Notes

Temperature range check is not used here.

#### References

[1]

## **Examples**

```
>>> Laliberte_density(273.15, [0.0037838838], ['7647-14-5'])
1002.62501201
```

## thermo.electrochem.Laliberte\_density\_mix(T, ws, c0s, c1s, c2s, c3s, c4s)

Calculate the density of an aqueous electrolyte mixture using the form proposed by [1]. All parameters must be provided to the function. Units are Kelvin and Pa\*s.

$$\rho_m = \left(\frac{w_w}{\rho_w} + \sum_i \frac{w_i}{\rho_{app_i}}\right)^{-1}$$

## Parameters

T [float] Temperature of fluid [K]

ws [array] Weight fractions of fluid components other than water

```
c0s [list[float]] Fit coefficient, [-]
```

- c1s [list[float]] Fit coefficient, [-]
- c2s [list[float]] Fit coefficient, [-]
- c3s [list[float]] Fit coefficient, [1/degC]
- c4s [list[float]] Fit coefficient, [degC]

#### Returns

rho [float] Solution density, [kg/m^3]

## References

[1]

## **Examples**

```
>>> Laliberte_density_mix(T=278.15, ws=[0.00581, 0.002], c0s=[-0.00324112223655149,_

→0.967814929691928], c1s=[0.0636354335906616, 5.540434135986], c2s=[1.

→01371399467365, 1.10374669742622], c3s=[0.0145951015210159, 0.0123340782160061],_

→c4s=[3317.34854426537, 2589.61875022366])

1005.6947727219
```

thermo.electrochem.Laliberte\_density\_i(T, w\_w, c0, c1, c2, c3, c4)

Calculate the density of a solute using the form proposed by Laliberte [1]. Parameters are needed, and a temperature, and water fraction. Units are Kelvin and Pa\*s.

$$\rho_{app,i} = \frac{(c_0[1-w_w]+c_1)\exp(10^{-6}[t+c_4]^2)}{(1-w_w)+c_2+c_3t}$$

#### **Parameters**

- T [float] Temperature of fluid [K]
- w\_w [float] Weight fraction of water in the solution, [-]
- c0 [float] Fit coefficient, [-]
- c1 [float] Fit coefficient, [-]
- c2 [float] Fit coefficient, [-]
- c3 [float] Fit coefficient, [1/degC]
- c4 [float] Fit coefficient, [degC]

#### Returns

rho\_i [float] Solute partial density, [kg/m^3]

#### Notes

Temperature range check is not used here.

#### References

[1]

## **Examples**

```
>>> params = [-0.00324112223655149, 0.0636354335906616, 1.01371399467365, 0.

→0145951015210159, 3317.34854426537]

>>> Laliberte_density_i(273.15+0, 1-0.0037838838, *params)

3761.8917585
```

## thermo.electrochem.Laliberte\_density\_w(T)

Calculate the density of water using the form proposed by [1]. No parameters are needed, just a temperature. Units are Kelvin and kg/m^3.

$$\rho_w = \frac{\left\{ \left( \left[ (-2.8054253 \times 10^{-10} \cdot t + 1.0556302 \times 10^{-7})t - 4.6170461 \times 10^{-5} \right]t - 0.0079870401 \right)t + 16.945176 \right\}t + 999.8370401}{1 + 0.01687985 \cdot t}$$

Parameters

T [float] Temperature of fluid [K]

Returns

rho\_w [float] Water density, [kg/m^3]

## Notes

Original source not cited No temperature range is used.

## References

[1]

## **Examples**

```
>>> Laliberte_density_w(298.15)
997.0448954179155
>>> Laliberte_density_w(273.15 + 50)
988.0362916114763
```

# 7.6.2 Aqueous Electrolyte Heat Capacity

## thermo.electrochem.Laliberte\_heat\_capacity(T, ws, CASRNs)

Calculate the heat capacity of an aqueous electrolyte mixture using the form proposed by [1]. Parameters are loaded by the function as needed.

$$Cp_m = w_w Cp_w + \sum w_i Cp_i$$

#### Parameters

T [float] Temperature of fluid [K]

ws [array] Weight fractions of fluid components other than water

CASRNs [array] CAS numbers of the fluid components other than water

## Returns

Cp [float] Solution heat capacity, [J/kg/K]

## Notes

A temperature range check is not included in this function. Units are Kelvin and J/kg/K.

#### References

[1]

```
>>> Laliberte_heat_capacity(273.15+1.5, [0.00398447], ['7647-14-5'])
4186.575407596064
```

thermo.electrochem.Laliberte\_heat\_capacity\_mix(T, ws, a1s, a2s, a3s, a4s, a5s, a6s)

Calculate the heat capacity of an aqueous electrolyte mixture using the form proposed by [1]. All parameters must be provided to this function.

$$Cp_m = w_w Cp_w + \sum w_i Cp_i$$

#### Parameters

T [float] Temperature of fluid [K]

ws [array] Weight fractions of fluid components other than water

CASRNs [array] CAS numbers of the fluid components other than water

#### Returns

Cp [float] Solution heat capacity, [J/kg/K]

## Notes

A temperature range check is not included in this function. Units are Kelvin and J/kg/K.

### References

[1]

## **Examples**

```
>>> Laliberte_heat_capacity_mix(T=278.15, ws=[0.00581, 0.002], a1s=[-0.

→0693559668993322, -0.103713247177424], a2s=[-0.0782134167486952, -0.

→0647453826944371], a3s=[3.84798479408635, 2.92191453087969], a4s=[-11.

→2762109247072, -5.48799065938436], a5s=[8.73187698542672, 2.41768600041476],

→a6s=[1.81245930472755, 1.32062411084408])

4154.788562680796
```

thermo.electrochem.Laliberte\_heat\_capacity\_i(T, w\_w, a1, a2, a3, a4, a5, a6)

Calculate the heat capacity of a solute using the form proposed by [1] Parameters are needed, and a temperature, and water fraction.

$$Cp_i = a_1 e^{\alpha} + a_5 (1 - w_w)^{a_6}$$

$$\alpha = a_2 t + a_3 \exp(0.01t) + a_4 (1 - w_w)$$

#### **Parameters**

T [float] Temperature of fluid [K]

w\_w [float] Weight fraction of water in the solution

a1-a6 [floats] Function fit parameters

#### Returns

**Cp\_i** [float] Solute partial heat capacity, [J/kg/K]

## Notes

Units are Kelvin and J/kg/K. Temperature range check is not used here.

## References

[1]

## **Examples**

```
>>> params = [-0.0693559668993322, -0.0782134167486952, 3.84798479408635, -11.

$\to 2762109247072, 8.73187698542672, 1.81245930472755]
>>> Laliberte_heat_capacity_i(1.5+273.15, 1-0.00398447, *params)
-2930.73539458
```

## thermo.electrochem.Laliberte\_heat\_capacity\_w(T)

Calculate the heat capacity of pure water in a fast but similar way as in [1]. [1] suggested the following interpolatative scheme, using points calculated from IAPWS-97 at a pressure of 0.1 MPa up to 95 °C and then at saturation pressure. The maximum temperature of [1] is 140 °C.

$$Cp_w = Cp_1 + (Cp_2 - Cp_1)\left(\frac{t - t_1}{t_2 - t_1}\right) + \frac{(Cp_3 - 2Cp_2 + Cp_1)}{2}\left(\frac{t - t_1}{t_2 - t_1}\right)\left(\frac{t - t_1}{t_2 - t_1} - 1\right)$$

In this implementation, the heat capacity of water is calculated from a chebyshev approximation of the scheme of [1] up to  $\sim$ 92 °C and then the heat capacity comes directly from IAPWS-95 at higher temperatures, also at the saturation pressure. There is no discontinuity between the methods.

## Parameters

T [float] Temperature of fluid [K]

## Returns

Cp\_w [float] Water heat capacity, [J/kg/K]

## **Notes**

Units are Kelvin and J/kg/K.

## References

[1]

## **Examples**

```
>>> Laliberte_heat_capacity_w(273.15+3.56)
4208.878727051538
```

## 7.6.3 Aqueous Electrolyte Viscosity

#### thermo.electrochem.Laliberte\_viscosity(T, ws, CASRNs)

Calculate the viscosity of an aqueous mixture using the form proposed by [1]. Parameters are loaded by the function as needed. Units are Kelvin and Pa\*s.

$$\mu_m = \mu_w^{w_w} \Pi \mu_i^{w_i}$$

#### **Parameters**

T [float] Temperature of fluid, [K]

ws [array] Weight fractions of fluid components other than water, [-]

CASRNs [array] CAS numbers of the fluid components other than water, [-]

## Returns

mu [float] Viscosity of aqueous mixture, [Pa\*s]

## Notes

Temperature range check is not used here. Check is performed using NaCl at 5 degC from the first value in [1]'s spreadsheet.

## References

## [1]

#### **Examples**

```
>>> Laliberte_viscosity(273.15+5, [0.005810], ['7647-14-5'])
0.0015285828581961414
```

thermo.electrochem.Laliberte\_viscosity\_mix(T, ws, v1s, v2s, v3s, v4s, v5s, v6s)

Calculate the viscosity of an aqueous mixture using the form proposed by [1]. All parameters must be provided in this implementation.

$$\mu_m = \mu_w^{w_w} \Pi \mu_i^{w_i}$$

#### **Parameters**

- T [float] Temperature of fluid, [K]
- ws [array] Weight fractions of fluid components other than water, [-]
- v1s [list[float]] Fit parameter, [-]
- v2s [list[float]] Fit parameter, [-]
- v3s [list[float]] Fit parameter, [-]
- v4s [list[float]] Fit parameter, [1/degC]
- v5s [list[float]] Fit parameter, [-]
- v6s [list[float]] Fit parameter, [-]

#### Returns

mu [float] Viscosity of aqueous mixture, [Pa\*s]

## References

[1]

#### **Examples**

```
>>> Laliberte_viscosity_mix(T=278.15, ws=[0.00581, 0.002], v1s=[16.221788633396, 69.

→5769240055845], v2s=[1.32293086770011, 4.17047793905946], v3s=[1.48485985010431,

→3.57817553622189], v4s=[0.00746912559657377, 0.0116677996754397], v5s=[30.

→7802007540575, 13897.6652650556], v6s=[2.05826852322558, 20.8027689840251])

0.0015377348091189648
```

#### thermo.electrochem.Laliberte\_viscosity\_i(T, w\_w, v1, v2, v3, v4, v5, v6)

Calculate the viscosity of a solute using the form proposed by [1] Parameters are needed, and a temperature. Units are Kelvin and Pa\*s.

$$\mu_i = \frac{\exp\left(\frac{v_1(1-w_w)^{v_2}+v_3}{v_4t+1}\right)}{v_5(1-w_w)^{v_6}+1}$$

## **Parameters**

T [float] Temperature of fluid, [K]

w\_w [float] Weight fraction of water in the solution, [-]

- v1 [float] Fit parameter, [-]
- v2 [float] Fit parameter, [-]
- v3 [float] Fit parameter, [-]
- v4 [float] Fit parameter, [1/degC]
- v5 [float] Fit parameter, [-]
- v6 [float] Fit parameter, [-]

#### Returns

mu\_i [float] Solute partial viscosity, [Pa\*s]

## Notes

Temperature range check is outside of this function. Check is performed using NaCl at 5 degC from the first value in [1]'s spreadsheet.

#### References

[1]

```
>>> params = [16.221788633396, 1.32293086770011, 1.48485985010431, 0.

→00746912559657377, 30.7802007540575, 2.05826852322558]

>>> Laliberte_viscosity_i(273.15+5, 1-0.005810, *params)

0.004254025533308794
```

## thermo.electrochem.Laliberte\_viscosity\_w(T)

Calculate the viscosity of a water using the form proposed by [1]. No parameters are needed, just a temperature. Units are Kelvin and Pa\*s. t is temperature in degrees Celcius.

$$\mu_w = \frac{t + 246}{(0.05594t + 5.2842)t + 137.37}$$

#### **Parameters**

T [float] Temperature of fluid, [K]

## Returns

mu\_w [float] Water viscosity, [Pa\*s]

## Notes

Original source or pure water viscosity is not cited. No temperature range is given for this equation.

## References

[1]

## **Examples**

>>> Laliberte\_viscosity\_w(298)
0.000893226448703328

# 7.6.4 Aqueous Electrolyte Thermal Conductivity

## thermo.electrochem.thermal\_conductivity\_Magomedov(T, P, ws, CASRNs, k\_w)

Calculate the thermal conductivity of an aqueous mixture of electrolytes using the form proposed by Magomedov

[1]. Parameters are loaded by the function as needed. Function will fail if an electrolyte is not in the database.

$$\lambda = \lambda_w \left[ 1 - \sum_{i=1}^n A_i (w_i + 2 \times 10^{-4} w_i^3) \right] - 2 \times 10^{-8} PT \sum_{i=1}^n w_i$$

## Parameters

T [float] Temperature of liquid [K]

**P** [float] Pressure of the liquid [Pa]

ws [array] Weight fractions of liquid components other than water

CASRNs [array] CAS numbers of the liquid components other than water

**k\_w** [float] Liquid thermal condiuctivity or pure water at T and P, [W/m/K]

## Returns

kl [float] Liquid thermal condiuctivity, [W/m/K]

## Notes

Range from 273 K to 473 K, P from 0.1 MPa to 100 MPa. C from 0 to 25 mass%. Internal untis are MPa for pressure and weight percent.

An example is sought for this function. It is not possible to reproduce the author's values consistently.

## References

[1]

## **Examples**

```
>>> thermal_conductivity_Magomedov(293., 1E6, [.25], ['7758-94-3'], k_w=0.59827)
0.548654049375
```

#### thermo.electrochem.Magomedov\_mix( $T, P, ws, Ais, k_w$ )

Calculate the thermal conductivity of an aqueous mixture of electrolytes using the correlation proposed by Magomedov [1]. All coefficients and the thermal conductivity of pure water must be provided.

$$\lambda = \lambda_w \left[ 1 - \sum_{i=1}^n A_i (w_i + 2 \times 10^{-4} w_i^3) \right] - 2 \times 10^{-8} PT \sum_{i=1}^n w_i$$

#### **Parameters**

T [float] Temperature of liquid [K]

**P** [float] Pressure of the liquid [Pa]

ws [list[float]] Weight fractions of liquid components other than water, [-]

Ais [list[float]] Ai coefficients which were regressed, [-]

k\_w [float] Liquid thermal condiuctivity or pure water at T and P, [W/m/K]

### Returns

kl [float] Liquid thermal condiuctivity, [W/m/K]

## Notes

Range from 273 K to 473 K, P from 0.1 MPa to 100 MPa. C from 0 to 25 mass%. Internal untis are MPa for pressure and weight percent.

## References

[1]

## **Examples**

```
>>> Magomedov_mix(293., 1E6, [.25], [0.00294], k_w=0.59827)
0.548654049375
```

# 7.6.5 Aqueous Electrolyte Electrical Conductivity

```
thermo.electrochem.dilute_ionic_conductivity(ionic_conductivities, zs, rhom)
```

This function handles the calculation of the electrical conductivity of a dilute electrolytic aqueous solution. Requires the mole fractions of each ion, the molar density of the whole mixture, and ionic conductivity coefficients for each ion.

$$\lambda = \sum_{i} \lambda_i^{\circ} z_i \rho_m$$

## Parameters

**ionic\_conductivities** [list[float]] Ionic conductivity coefficients of each ion in the mixture [m^2\*S/mol]

zs [list[float]] Mole fractions of each ion in the mixture, [-]

rhom [float] Overall molar density of the solution, [mol/m^3]

## Returns

kappa [float] Electrical conductivity of the fluid, [S/m]

## Notes

The ionic conductivity coefficients should not be *equivalent* coefficients; for example,  $0.0053 \text{ m}^2\text{*}$ S/mol is the equivalent conductivity coefficient of Mg+2, but this method expects twice its value - 0.0106. Both are reported commonly in literature.

Water can be included in this calculation by specifying a coefficient of 0. The conductivity of any electrolyte eclipses its own conductivity by many orders of magnitude. Any other solvents present will affect the conductivity extensively and there are few good methods to predict this effect.

## References

[1]

# **Examples**

Complex mixture of electrolytes ['Cl-', 'HCO3-', 'SO4-2', 'Na+', 'K+', 'Ca+2', 'Mg+2']:

```
>>> ionic_conductivities = [0.00764, 0.00445, 0.016, 0.00501, 0.00735, 0.0119, 0.

...01061]

>>> zs = [0.03104, 0.00039, 0.00022, 0.02413, 0.0009, 0.0024, 0.00103]

>>> dilute_ionic_conductivity(ionic_conductivities=ionic_conductivities, zs=zs,__

...rhom=53865.9)

22.05246783663
```

thermo.electrochem.conductivity\_McCleskey(*T*, *M*, *lambda\_coeffs*, *A\_coeffs*, *B*, *multiplier*, *rho=1000.0*) This function handles the calculation of the electrical conductivity of an electrolytic aqueous solution with one electrolyte in solution. It handles temperature dependency and concentrated solutions. Requires the temperature of the solution; its molality, and four sets of coefficients *lambda\_coeffs*, *A\_coeffs*, *B*, and *multiplier*.

$$\Lambda = \frac{\kappa}{C}$$
$$\Lambda = \Lambda^0(t) - A(t) \frac{m^{1/2}}{1 + Bm^{1/2}}$$
$$\Lambda^\circ(t) = c_1 t^2 + c_2 t + c_3$$
$$A(t) = d_1 t^2 + d_2 t + d_3$$

In the above equations, t is temperature in degrees Celcius; m is molality in mol/kg, and C is the concentration of the electrolytes in mol/m<sup>3</sup>, calculated as the product of density and molality.

## Parameters

- T [float] Temperature of the solution, [K]
- M [float] Molality of the solution with respect to one electrolyte (mol solute / kg solvent), [mol/kg]
- **lambda\_coeffs** [list[float]] List of coefficients for the polynomial used to calculate *lambda*; length-3 coefficients provided in [1], [-]
- **A\_coeffs** [list[float]] List of coefficients for the polynomial used to calculate *A*; length-3 coefficients provided in [1], [-]
- **B** [float] Empirical constant for an electrolyte, [-]
- **multiplier** [float] The multiplier to obtain the absolute conductivity from the equivalent conductivity; ex 2 for CaCl2, [-]
- rho [float, optional] The mass density of the aqueous mixture, [kg/m^3]

# Returns

**kappa** [float] Electrical conductivity of the solution at the specified molality and temperature [S/m]

# Notes

Coefficients provided in [1] result in conductivity being calculated in units of mS/cm; they are converted to S/m before returned.

# References

[1]

# **Examples**

A 0.5 wt% solution of CaCl2, conductivity calculated in mS/cm

```
>>> conductivity_McCleskey(T=293.15, M=0.045053, A_coeffs=[.03918, 3.905,
... 137.7], lambda_coeffs=[0.01124, 2.224, 72.36], B=3.8, multiplier=2)
0.8482584585108555
```

## thermo.electrochem.ionic\_strength(mis, zis)

Calculate the ionic strength of a solution in one of two ways, depending on the inputs only. For Pitzer and Bromley models, *mis* should be molalities of each component. For eNRTL models, *mis* should be mole fractions of each electrolyte in the solution. This will sum to be much less than 1.

$$I = \frac{1}{2} \sum M_i z_i^2$$
$$I = \frac{1}{2} \sum x_i z_i^2$$

# Parameters

mis [list] Molalities of each ion, or mole fractions of each ion [mol/kg or -]

zis [list] Charges of each ion [-]

# Returns

I [float] ionic strength, [?]

# References

# [1], [2]

# **Examples**

```
>>> ionic_strength([0.1393, 0.1393], [1, -1])
0.1393
```

# 7.6.6 Pure Liquid Electrical Conductivity

## thermo.electrochem.conductivity(CASRN, method=None)

This function handles the retrieval of a chemical's conductivity. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 100 chemicals.

# Parameters

```
CASRN [string] CASRN [-]
```

#### Returns

kappa [float] Electrical conductivity of the fluid, [S/m]

T [float or None] Temperature at which conductivity measurement was made or None if not available, [K]

#### **Other Parameters**

**method** [string, optional] A string for the method name to use, as defined by constants in conductivity\_methods

#### Notes

Only one source is available in this function. It is:

• 'LANGE\_COND' which is from Lange's Handbook, Table 8.34 Electrical Conductivity of Various Pure Liquids', a compillation of data in [1]. The individual datapoints in this source are not cited at all.

#### References

[1]

# **Examples**

```
>>> conductivity('7732-18-5')
(4e-06, 291.15)
```

## thermo.electrochem.conductivity\_methods(CASRN)

Return all methods available to obtain electrical conductivity for the specified chemical.

# Parameters

```
CASRN [str] CASRN, [-]
```

## Returns

**methods** [list[str]] Methods which can be used to obtain electrical conductivity with the given inputs.

See also:

#### conductivity

thermo.electrochem.conductivity\_all\_methods = ['LANGE\_COND']
Built-in mutable sequence.

If no argument is given, the constructor creates a new empty list. The argument must be an iterable if specified.

# 7.6.7 Water Dissociation Equilibrium

# thermo.electrochem.Kweq\_Arcis\_Tremaine\_Bandura\_Lvov(T, rho\_w)

Calculates equilibrium constant for OH- and H+ in water, according to [1].

$$Q = \rho \exp(\alpha_0 + \alpha_1 T^{-1} + \alpha_2 T^{-2} \rho^{2/3})$$

$$-\log_{10} K_w = -2n \left[ \log_{10}(1+Q) - \frac{Q}{Q+1}\rho(\beta_0 + \beta_1 T^{-1} + \beta_2 \rho) \right] - \log_{10} K_w^G + 2\log_{10} \frac{18.015268}{1000}$$

**Parameters** 

T [float] Temperature of water [K]

rho\_w [float] Density of water at temperature and pressure [kg/m^3]

## Returns

Kweq [float] Ionization constant of water, [-]

#### Notes

Formulation is in terms of density in g/cm^3; density is converted internally.

n = 6; alpha0 = -0.864671; alpha1 = 8659.19; alpha2 = -22786.2; beta0 = 0.642044; beta1 = -56.8534; beta2 = -0.375754

#### References

[1]

# **Examples**

```
>>> -1*log10(Kweq_Arcis_Tremaine_Bandura_Lvov(600, 700))
11.138236348
```

# thermo.electrochem.Kweq\_IAPWS(T, rho\_w)

Calculates equilibrium constant for OH- and H+ in water, according to [1]. This is the most recent formulation available.

$$Q = \rho \exp(\alpha_0 + \alpha_1 T^{-1} + \alpha_2 T^{-2} \rho^{2/3})$$

$$-\log_{10} K_w = -2n \left[ \log_{10}(1+Q) - \frac{Q}{Q+1}\rho(\beta_0 + \beta_1 T^{-1} + \beta_2 \rho) \right] - \log_{10} K_w^G + 2\log_{10} \frac{18.015268}{1000}$$

Parameters

T [float] Temperature of water [K]

rho\_w [float] Density of water at temperature and pressure [kg/m^3]

#### Returns

Kweq [float] Ionization constant of water, [-]

# Notes

Formulation is in terms of density in g/cm^3; density is converted internally.

n = 6; alpha0 = -0.864671; alpha1 = 8659.19; alpha2 = -22786.2; beta0 = 0.642044; beta1 = -56.8534; beta2 = -0.375754

# References

[1]

# **Examples**

Example from IAPWS check:

```
>>> -1*log10(Kweq_IAPWS(600, 700))
11.203153057603775
```

# thermo.electrochem.Kweq\_IAPWS\_gas(T)

Calculates equilibrium constant for OH- and H+ in water vapor, according to [1]. This is the most recent formulation available.

$$-log_{10}K_w^G = \gamma_0 + \gamma_1 T^{-1} + \gamma_2 T^{-2} + \gamma_3 T^{-3}$$

# **Parameters**

T [float] Temperature of H2O [K]

Returns

 $K_w_G$  [float]

## Notes

gamma0 = 6.141500E-1; gamma1 = 4.825133E4; gamma2 = -6.770793E4; gamma3 = 1.010210E7

## References

[1]

## **Examples**

```
>>> Kweq_IAPWS_gas(800)
1.4379721554798815e-61
```

#### thermo.electrochem.Kweq\_1981(T, rho\_w)

Calculates equilibrium constant for OH- and H+ in water, according to [1]. Second most recent formulation.

$$\log_{10} K_w = A + B/T + C/T^2 + D/T^3 + (E + F/T + G/T^2) \log_{10} \rho_w$$

#### Parameters

T [float] Temperature of fluid [K]

**rho\_w** [float] Density of water, [kg/m^3]

# Returns

Kweq [float] Ionization constant of water, [-]

#### Notes

Density is internally converted to units of g/cm^3.

A = -4.098; B = -3245.2; C = 2.2362E5; D = -3.984E7; E = 13.957; F = -1262.3; G = 8.5641E5

#### References

[1]

#### **Examples**

```
>>> -1*log10(Kweq_1981(600, 700))
11.274522047
```

# 7.6.8 Balancing lons

Performs an ion balance to adjust measured experimental ion compositions to electroneutrality. Can accept either the actual mole fractions of the ions, or their concentrations in units of [mg/L] as well for convinience.

The default method will locate the most prevalent ion in the type of ion not in excess - and increase it until the two ion types balance.

## Parameters

- **anions** [list(ChemicalMetadata)] List of all negatively charged ions measured as being in the solution; ChemicalMetadata instances or simply objects with the attributes *MW* and *charge*, [-]
- **cations** [list(ChemicalMetadata)] List of all positively charged ions measured as being in the solution; ChemicalMetadata instances or simply objects with the attributes *MW* and *charge*, [-]
- anion\_zs [list, optional] Mole fractions of each anion as measured in the aqueous solution, [-]
- cation\_zs [list, optional] Mole fractions of each cation as measured in the aqueous solution, [-]
- **anion\_concs** [list, optional] Concentrations of each anion in the aqueous solution in the units often reported (for convinience only) [mg/L]
- **cation\_concs** [list, optional] Concentrations of each cation in the aqueous solution in the units often reported (for convinience only) [mg/L]
- **rho\_w** [float, optional] Density of the aqueous solutionr at the temperature and pressure the anion and cation concentrations were measured (if specified), [kg/m^3]

- **method** [str, optional] The method to use to balance the ionimbalance; one of 'dominant', 'decrease dominant', 'increase dominant', 'proportional insufficient ions increase', 'proportional excess ions decrease', 'proportional cation adjustment', 'proportional anion adjustment', 'Na or Cl increase', 'Na or Cl decrease', 'adjust', 'increase', 'decrease', 'makeup'].
- **selected\_ion** [ChemicalMetadata, optional] Some methods adjust only one user-specified ion; this is that input. For the case of the 'makeup' method, this is a tuple of (anion, cation) ChemicalMetadata instances and only the ion type not in excess will be used.

## Returns

- **anions** [list[ChemicalMetadata]] List of all negatively charged ions measured as being in the solution; ChemicalMetadata instances after potentially adding in an ion which was not present but specified by the user, [-]
- **cations** [list[ChemicalMetadata]] List of all positively charged ions measured as being in the solution; ChemicalMetadata instances after potentially adding in an ion which was not present but specified by the user, [-]
- **anion\_zs** [list[float],] Mole fractions of each anion in the aqueous solution after the charge balance, [-]
- **cation\_zs** [list[float]] Mole fractions of each cation in the aqueous solution after the charge balance, [-]

z\_water [float[float]] Mole fraction of the water in the solution, [-]

## Notes

The methods perform the charge balance as follows:

- 'dominant' : The ion with the largest mole fraction in solution has its concentration adjusted up or down as necessary to balance the solution.
- 'decrease dominant' : The ion with the largest mole fraction in the type of ion with *excess* charge has its own mole fraction decreased to balance the solution.
- 'increase dominant' : The ion with the largest mole fraction in the type of ion with *insufficient* charge has its own mole fraction decreased to balance the solution.
- 'proportional insufficient ions increase' : The ion charge type which is present insufficiently has each of the ions mole fractions *increased* proportionally until the solution is balanced.
- 'proportional excess ions decrease' : The ion charge type which is present in excess has each of the ions mole fractions *decreased* proportionally until the solution is balanced.
- 'proportional cation adjustment' : All *cations* have their mole fractions increased or decreased proportionally as necessary to balance the solution.
- 'proportional anion adjustment' : All *anions* have their mole fractions increased or decreased proportionally as necessary to balance the solution.
- 'Na or Cl increase' : Either Na+ or Cl- is *added* to the solution until the solution is balanced; the species will be added if they were not present initially as well.
- 'Na or Cl decrease' : Either Na+ or Cl- is *removed* from the solution until the solution is balanced; the species will be added if they were not present initially as well.
- 'adjust' : An ion specified with the parameter *selected\_ion* has its mole fraction *increased or decreased* as necessary to balance the solution. An exception is raised if the specified ion alone cannot balance the solution.

- 'increase' : An ion specified with the parameter *selected\_ion* has its mole fraction *increased* as necessary to balance the solution. An exception is raised if the specified ion alone cannot balance the solution.
- 'decrease' : An ion specified with the parameter *selected\_ion* has its mole fraction *decreased* as necessary to balance the solution. An exception is raised if the specified ion alone cannot balance the solution.
- 'makeup' : Two ions ase specified as a tuple with the parameter *selected\_ion*. Whichever ion type is present in the solution insufficiently is added; i.e. if the ions were Mg+2 and Cl-, and there was too much negative charge in the solution, Mg+2 would be added until the solution was balanced.

# **Examples**

```
>>> anions_n = ['Cl-', 'HCO3-', 'SO4-2']
>>> cations_n = ['Na+', 'K+', 'Ca+2', 'Mg+2']
>>> cations = [identifiers.pubchem_db.search_name(i) for i in cations_n]
>>> anions = [identifiers.pubchem_db.search_name(i) for i in anions_n]
>>> an_res, cat_res, an_zs, cat_zs, z_water = balance_ions(anions, cations,
... anion_zs=[0.02557, 0.00039, 0.00026], cation_zs=[0.0233, 0.00075,
... 0.00262, 0.00119], method='proportional excess ions decrease')
>>> an_zs
[0.02557, 0.00039, 0.00026]
>>> cat_zs
[0.01948165456267761, 0.0006270918850647299, 0.0021906409851594564, 0.
...0009949857909693717]
>>> z_water
0.9504856267761288
```

# 7.6.9 Fit Coefficients and Data

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.

```
In [1]: from thermo.electrochem import Magomedovk_thermal_cond, cond_data_McCleskey, CRC_
→aqueous_thermodynamics, electrolyte_dissociation_reactions, Laliberte_data
In [2]: Magomedovk_thermal_cond
Out[2]:
              Formula
                                    Chemical
                                                   Ai
CASRN
497-19-8
               Na2CO3
                           Sodium carbonate -0.00050
584-08-7
                K2C03
                        Potassium carbonate
                                              0.00160
7447-39-4
                CuC12
                           Cuprous chloride
                                              0.00360
7488-54-2
               Rb2SO4
                           Rubidium sulfate
                                              0.00134
                         Sodium perchlorate
7601-89-0
               NaClO4
                                              0.00250
7646-79-9
                CoCl2
                         Cobaltous chloride
                                              0.00320
7664-93-9
                H2SO4
                               Acid sulfate
                                              0.00305
                               Zinc bromide
7699-45-8
                ZnBr2
                                              0.00410
7718-54-9
                NiCl2
                         Nickelous chloride
                                              0.00330
7758-94-3
                FeCl2
                           Ferrous chloride
                                              0.00294
                             Silver nitrate
7761-88-8
                AgN03
                                              0.00190
7775-09-9
               NaClO3
                            Sodium chlorate
                                              0.00240
7778-50-9
              K2Cr2O7 Potassium dichromate
                                              0.00188
                          Nickelous sulfate
7786-81-4
                NiSO4
                                              0.00140
```

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7789-00-6	K2CrO4	Potass	ium chr	omate	0.00130	0		
7789-23-3	KF	Potassium fluoride			0.00180	0		
7789-38-0	NaBrO3	Sodium bromate			0.00170	0		
7789-39-1	RbBr	Rubi	dium br	omide	0.00305	5		
7789-42-6	CdBr2	Cadmium bromide			0.00274	1		
7789-46-0	FeBr2	Fer	rous br	omide	0.00375	5		
7790-29-6	RbI	Rub	idium i	odide	0.00322	2		
7790-80-9	CdI2	Ca	dmium i	odide	0.00302	2		
7791-11-9	RbCl	Rubid	ium chl	oride	0.00238	3		
10042-76-9	Sr(NO3)2	Stron	tium ni	trate	0.00153	3		
10043-01-3	Al2(SO4)3	Alum	inum su	lfate	0.00335	5		
10099-74-8	Pb(NO3)2		Lead ni	trate	0.00138	3		
10102-68-8	CaI2	Ca	lcium i	odide	0.00340	0		
10139-47-6	ZnI2		Zinc i	odide	0.00410	0		
10325-94-7	Cd(NO3)2	Cad	mium ni	trate	0.00155	5		
10377-51-2	LiI	Li	thium i	odide	0.00435	5		
10377-58-9	MgI2	Magn	esium i	odide	0.00417	7		
10476-81-0	SrBr2	Stron	tium br	omide	0.00290	0		
10476-85-4	SrCl2	Stront	ium chl	oride	0.00170	0		
10476-86-5	SrI2	Stro	ntium i	odide	0.00311	1		
12027-06-4	NH4I	Amm	onium i	odide	0.00480	0		
13126-12-0	RbN03	Rubi	dium ni	trate	0.00214	1		
13462-88-9	NiBr2	Nicke	lous br	omide	0.00396	5		
13462-90-3	NiI2	Nick	elous i	odide	0.00393			
15238-00-3	CoI2	Coba	ltous i	odide	0.00384			
<pre>In [3]: con Out[3]:</pre>		leskey						
	formula	c1	c2		d3	В	multiplier	
CASRN								
7447-40-7	KCl	0.009385	2.533		44.11	1.70	1	
7647-14-5	NaCl	0.008967	2.196		44.55	1.30	1	
7647-01-0		-0.006766	6.614		48.53	0.01	1	
7447-41-8	LiCl	0.008784	1.996		42.79	1.00	1	
7647-17-8	CsCl	0.010080	2.479		41.29	1.40	1	
12125-02-9	NH4Cl	0.006575	2.684		30.00	0.70	1	
10043-52-4	CaCl2	0.011240	2.224		137.70	3.80	2	
7786-30-3	MgCl2	0.009534	2.247		129.80	3.10	2	
10361-37-2	BaCl2	0.010380	2.346		111.80	2.40	2	
10476-85-4	SrCl2	0.009597	2.279		60.18	0.80	2	
7664-93-9	H2SO4 -	-0.019850	7.421		1869.00	11.50	2	
7757-82-6	Na2SO4	0.009501	2.317		135.50	2.20	2	
7778-80-5	K2SO4	0.008819	2.872		247.10	5.30	2	
10294-54-9	Cs2SO4	0.012730	2.457		187.40	3.30	2	
7778-18-9	CaSO4	0.011920	2.564		644.40	9.60	2	
7646-93-7	KHSO4 -	-0.003092	9.759		1776.00	8.20	1	
298-14-6	KHCO3	0.007807	2.040		38.58	0.90	1	
584-08-7	K2CO3	0.011450	2.726		81.12	2.10	2	
144-55-8	NaHCO3	0.012600	1.543		52.94	1.10	1	
497-19-8	Na2CO3	0.022960	5.211		455.80	4.80	2	
1310-73-2	NaOH	0.006936	3.872		56.76	0.20	1	
7681-49-4	NaF	0.007346	2.032		69.99	2.30	1	
								(continues on next page)

(continued from previous page) 7789-23-3 KF 0.007451 2.294 39.40 0.90 1 . . . 7758-02-3 0.007076 2.612 29.49 0.60 KBr 1 . . . 7757-79-1 KNO3 0.009117 2.309 . . . 49.12 0.70 1 2 7779-88-6 Zn(NO3)2 0.015260 4.519 ... 302.90 4.00 [26 rows x 9 columns] In [4]: CRC\_aqueous\_thermodynamics Out[4]: Formula Name  $\ldots$  S(aq) Cp(aq) CAS . . . 57-12-5 CN-Cyanide ion . . . 94.1 NaN 71-47-6 CH00-Formate ion 92.0 -87.9 . . . 71-50-1 CH3C00-Acetate ion 86.6 -6.3 Bicarbonate ion ... 71-52-3 HCO3-91.2 NaN 302-04-5 Thiocyanate ion ... 144.3 SCN--40.2. . . . . . . . . . . . . . . . . . 117412-24-5 Be02-2 Beryllium dioxide ion ... -159.0 NaN Yttrium hydroxide ion 127622-32-6 Y(OH)+2 NaN . . . NaN Te(OH)3+ Tellurium(IV) trihydroxide ion ... 111.7 129466-35-9 NaN Indium hydroxide ion -88.0 NaN 186449-38-7 InOH+2 . . . 2099995000-00-0 Y2(OH)2+4 Yttrium dihydroxide ion . . . NaN NaN [173 rows x 7 columns] In [5]: electrolyte\_dissociation\_reactions Out[5]: Electrolyte name Electrolyte CAS ... Cation charge Cation count 0 Diammonium Hydrogen phosphate 7783-28-0 1 2 . . . Ammonium Sulfate 1 2 1 7783-20-2 . . . 2 2 ammonium sulfite 10196-04-0 1 . . . 3 3 Ammonium phosphate 1 10361-65-6 . . . 4 Ammonium siliconhexafluoride 16919-19-0 1 2 . 259 Zinc selenite 13597-46-1 2 1 . . . Zinc selenate 260 13597-54-1 2 1 . . . Zinc Nitrate 2 261 7779-88-6 1 . . . Zinc Chloride 2 262 7646-85-7 1 . . . 263 Zinc Sulfate 7733-02-0 2 1 . . . [264 rows x 11 columns] In [6]: Laliberte\_data Out[6]: Name Max w.2 No of points in corr.2 Formula . . . CASRN . . . 7783-20-2 Ammonium Sulfate (NH4)2SO4 NaN NaN . . . 10043-01-3 Aluminum Sulfate Al2(SO4)3 NaN NaN . . . Aluminum Chloride 7446-70-0 AlCl3 NaN NaN . . . 10022-31-8 Barium Nitrate Ba(NO3)2 ... 0.047274 96.0 10361-37-2 Barium Chloride BaC12 . . . 0.248237 16.0 . . . . . . . . . . . . . . . . . .

.. 10

					(continued from previous page)
57-50-1	Sucrose	Sucrose		NaN	NaN
13825-74-6	Titanyl Sulfate	TiOSO4		NaN	NaN
7779-88-6	Zinc Nitrate	Zn(NO3)2		0.077132	144.0
7646-85-7	Zinc Chloride	ZnC12		NaN	NaN
7733-02-0	Zinc Sulfate	ZnS04		NaN	NaN
[109 rows x 32 columns]					

# 7.7 Cubic Equations of State (thermo.eos)

This module contains implementations of most cubic equations of state for pure components. This includes Peng-Robinson, SRK, Van der Waals, PRSV, TWU and many other variants.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

```
• Base Class
```

- Standard Peng-Robinson Family EOSs
  - Standard Peng Robinson
  - Peng Robinson (1978)
  - Peng Robinson Stryjek-Vera
  - Peng Robinson Stryjek-Vera 2
  - Peng Robinson Twu (1995)
  - Peng Robinson Polynomial alpha Function
- Volume Translated Peng-Robinson Family EOSs
  - Peng Robinson Translated
  - Peng Robinson Translated Twu (1991)
  - Peng Robinson Translated-Consistent
  - Peng Robinson Translated (Pina-Martinez, Privat, and Jaubert Variant)
- Soave-Redlich-Kwong Family EOSs
  - Standard SRK
  - Twu SRK (1995)
  - API SRK
  - SRK Translated
  - SRK Translated-Consistent
  - SRK Translated (Pina-Martinez, Privat, and Jaubert Variant)
  - MSRK Translated
- Van der Waals Equations of State
- Redlich-Kwong Equations of State

- Ideal Gas Equation of State
- Lists of Equations of State
- Demonstrations of Concepts
  - Maximum Pressure at Constant Volume
  - Debug Plots to Understand EOSs

# 7.7.1 Base Class

#### class thermo.eos.GCEOS

Bases: object

Class for solving a generic Pressure-explicit three-parameter cubic equation of state. Does not implement any parameters itself; must be subclassed by an equation of state class which uses it. Works for mixtures or pure species for all properties except fugacity. All properties are derived with the CAS SymPy, not relying on any derivations previously published.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V^2 + \delta V + \epsilon}$$

The main methods (in order they are called) are GCEOS.solve, GCEOS.set\_from\_PT, GCEOS. volume\_solutions, and GCEOS.set\_properties\_from\_solution.

*GCEOS.solve* calls *GCEOS.check\_sufficient\_inputs*, which checks if two of *T*, *P*, and *V* were set. It then solves for the remaining variable. If *T* is missing, method *GCEOS.solve\_T* is used; it is parameter specific, and so must be implemented in each specific EOS. If *P* is missing, it is directly calculated. If *V* is missing, it is calculated with the method *GCEOS.volume\_solutions*. At this point, either three possible volumes or one user specified volume are known. The value of *a\_alpha*, and its first and second temperature derivative are calculated with the EOS-specific method *GCEOS.a\_alpha\_and\_derivatives*.

If V is not provided, *GCEOS*. *volume\_solutions* calculates the three possible molar volumes which are solutions to the EOS; in the single-phase region, only one solution is real and correct. In the two-phase region, all volumes are real, but only the largest and smallest solution are physically meaningful, with the largest being that of the gas and the smallest that of the liquid.

*GCEOS.set\_from\_PT* is called to sort out the possible molar volumes. For the case of a user-specified V, the possibility of there existing another solution is ignored for speed. If there is only one real volume, the method *GCEOS.set\_properties\_from\_solution* is called with it. If there are two real volumes, *GCEOS.set\_properties\_from\_solution* is called once with each volume. The phase is returned by *GCEOS.set\_properties\_from\_solution*, and the volumes is set to either GCEOS.V\_1 or GCEOS.V\_g as appropriate.

*GCEOS.set\_properties\_from\_solution* is a large function which calculates all relevant partial derivatives and properties of the EOS. 17 derivatives and excess enthalpy and entropy are calculated first. Finally, it sets all these properties as attibutes for either the liquid or gas phase with the convention of adding on  $_l$  or  $_g$  to the variable names, respectively.

## Attributes

- T [float] Temperature of cubic EOS state, [K]
- **P** [float] Pressure of cubic EOS state, [Pa]
- a [float] a parameter of cubic EOS; formulas vary with the EOS, [Pa\*m^6/mol^2]
- **b** [float] *b* parameter of cubic EOS; formulas vary with the EOS, [m<sup>3</sup>/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

- epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]
- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- **da\_alpha\_dT** [float] Temperature derivative of  $a\alpha$  calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of *a*α calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]
- Zc [float] Critical compressibility of cubic EOS state, [-]
- **phase** [str] One of 'l', 'g', or 'l/g' to represent whether or not there is a liquid-like solution, vapor-like solution, or both available, [-]
- **raw\_volumes** [list[(float, complex), 3]] Calculated molar volumes from the volume solver; depending on the state and selected volume solver, imaginary volumes may be represented by 0 or -1j to save the time of actually calculating them, [m^3/mol]
- V\_l [float] Liquid phase molar volume, [m^3/mol]
- **V\_g** [float] Vapor phase molar volume, [m^3/mol]
- V [float or None] Molar volume specified as input; otherwise None, [m^3/mol]
- Z\_l [float] Liquid phase compressibility, [-]

**Z\_g** [float] Vapor phase compressibility, [-]

- PIP\_1 [float] Liquid phase phase identification parameter, [-]
- **PIP\_g** [float] Vapor phase phase identification parameter, [-]
- dP\_dT\_l [float] Liquid phase temperature derivative of pressure at constant volume, [Pa/K].

$$\left(\frac{\partial P}{\partial T}\right)_V = \frac{R}{V-b} - \frac{a\frac{d\alpha(T)}{dT}}{V^2 + V\delta + \epsilon}$$

**dP\_dT\_g** [float] Vapor phase temperature derivative of pressure at constant volume, [Pa/K].

$$\left(\frac{\partial P}{\partial T}\right)_V = \frac{R}{V-b} - \frac{a\frac{d\alpha(T)}{dT}}{V^2 + V\delta + \epsilon}$$

**dP\_dV\_l** [float] Liquid phase volume derivative of pressure at constant temperature, [Pa\*mol/m^3].

$$\left(\frac{\partial P}{\partial V}\right)_{T} = -\frac{RT}{\left(V-b\right)^{2}} - \frac{a\left(-2V-\delta\right)\alpha(T)}{\left(V^{2}+V\delta+\epsilon\right)^{2}}$$

**dP\_dV\_g** [float] Gas phase volume derivative of pressure at constant temperature, [Pa\*mol/m^3].

$$\left(\frac{\partial P}{\partial V}\right)_T = -\frac{RT}{\left(V-b\right)^2} - \frac{a\left(-2V-\delta\right)\alpha(T)}{\left(V^2+V\delta+\epsilon\right)^2}$$

**dV\_dT\_l** [float] Liquid phase temperature derivative of volume at constant pressure, [m^3/(mol\*K)].

$$\left(\frac{\partial V}{\partial T}\right)_P = -\frac{\left(\frac{\partial P}{\partial T}\right)_V}{\left(\frac{\partial P}{\partial V}\right)_T}$$

**dV\_dT\_g** [float] Gas phase temperature derivative of volume at constant pressure, [m^3/(mol\*K)].

$$\left(\frac{\partial V}{\partial T}\right)_P = -\frac{\left(\frac{\partial P}{\partial T}\right)_V}{\left(\frac{\partial P}{\partial V}\right)_T}$$

**dV\_dP\_l** [float] Liquid phase pressure derivative of volume at constant temperature, [m^3/(mol\*Pa)].

$$\left(\frac{\partial V}{\partial P}\right)_T = -\frac{\left(\frac{\partial V}{\partial T}\right)_P}{\left(\frac{\partial P}{\partial T}\right)_V}$$

**dV\_dP\_g** [float] Gas phase pressure derivative of volume at constant temperature, [m^3/(mol\*Pa)].

$$\left(\frac{\partial V}{\partial P}\right)_T = -\frac{\left(\frac{\partial V}{\partial T}\right)_P}{\left(\frac{\partial P}{\partial T}\right)_V}$$

**dT\_dV\_l** [float] Liquid phase volume derivative of temperature at constant pressure, [K\*mol/m^3].

$$\left(\frac{\partial T}{\partial V}\right)_P = \frac{1}{\left(\frac{\partial V}{\partial T}\right)_P}$$

- **dT\_dV\_g** [float] Gas phase volume derivative of temperature at constant pressure, [K\*mol/m^3]. See GCEOS.set\_properties\_from\_solution for the formula.
- **dT\_dP\_l** [float] Liquid phase pressure derivative of temperature at constant volume, [K/Pa].

$$\left(\frac{\partial T}{\partial P}\right)_V = \frac{1}{\left(\frac{\partial P}{\partial T}\right)_V}$$

dT\_dP\_g [float] Gas phase pressure derivative of temperature at constant volume, [K/Pa].

$$\left(\frac{\partial T}{\partial P}\right)_V = \frac{1}{\left(\frac{\partial P}{\partial T}\right)_V}$$

**d2P\_dT2\_l** [float] Liquid phase second derivative of pressure with respect to temperature at constant volume, [Pa/K^2].

$$\left(\frac{\partial^2 P}{\partial T^2}\right)_V = -\frac{a\frac{d^2\alpha(T)}{dT^2}}{V^2 + V\delta + \epsilon}$$

d2P\_dT2\_g [float] Gas phase second derivative of pressure with respect to temperature at constant volume, [Pa/K^2].

$$\left(\frac{\partial^2 P}{\partial T^2}\right)_V = -\frac{a\frac{d^2\alpha(T)}{dT^2}}{V^2+V\delta+\epsilon}$$

**d2P\_dV2\_l** [float] Liquid phase second derivative of pressure with respect to volume at constant temperature, [Pa\*mol^2/m^6].

$$\left(\frac{\partial^2 P}{\partial V^2}\right)_T = 2\left(\frac{RT}{\left(V-b\right)^3} - \frac{a\left(2V+\delta\right)^2\alpha(T)}{\left(V^2+V\delta+\epsilon\right)^3} + \frac{a\alpha(T)}{\left(V^2+V\delta+\epsilon\right)^2}\right)$$

**d2P\_dTdV\_l** [float] Liquid phase second derivative of pressure with respect to volume and then temperature, [Pa\*mol/(K\*m^3)].

$$\left(\frac{\partial^2 P}{\partial T \partial V}\right) = -\frac{R}{\left(V-b\right)^2} + \frac{a\left(2V+\delta\right)\frac{d\alpha(T)}{dT}}{\left(V^2+V\delta+\epsilon\right)^2}$$

**d2P\_dTdV\_g** [float] Gas phase second derivative of pressure with respect to volume and then temperature, [Pa\*mol/(K\*m^3)].

$$\left(\frac{\partial^2 P}{\partial T \partial V}\right) = -\frac{R}{\left(V-b\right)^2} + \frac{a\left(2V+\delta\right)\frac{d\alpha(T)}{dT}}{\left(V^2+V\delta+\epsilon\right)^2}$$

- **H\_dep\_l** [float] Liquid phase departure enthalpy, [J/mol]. See GCEOS. set\_properties\_from\_solution for the formula.
- **H\_dep\_g** [float] Gas phase departure enthalpy, [J/mol]. See GCEOS. set\_properties\_from\_solution for the formula.
- **S\_dep\_l** [float] Liquid phase departure entropy, [J/(mol\*K)]. See GCEOS. set\_properties\_from\_solution for the formula.
- **S\_dep\_g** [float] Gas phase departure entropy, [J/(mol\*K)]. See GCEOS. set\_properties\_from\_solution for the formula.
- G\_dep\_l [float] Liquid phase departure Gibbs energy, [J/mol].

$$G_{dep} = H_{dep} - TS_{dep}$$

**G\_dep\_g** [float] Gas phase departure Gibbs energy, [J/mol].

$$G_{dep} = H_{dep} - TS_{dep}$$

**Cp\_dep\_l** [float] Liquid phase departure heat capacity, [J/(mol\*K)]

$$C_{p,dep} = (C_p - C_v)_{\text{from EOS}} + C_{v,dep} - R$$

**Cp\_dep\_g** [float] Gas phase departure heat capacity, [J/(mol\*K)]

$$C_{p,dep} = (C_p - C_v)_{\text{from EOS}} + C_{v,dep} - R$$

- **Cv\_dep\_l** [float] Liquid phase departure constant volume heat capacity, [J/(mol\*K)]. See *GCEOS.set\_properties\_from\_solution* for the formula.
- **Cv\_dep\_g** [float] Gas phase departure constant volume heat capacity, [J/(mol\*K)]. See GCEOS. set\_properties\_from\_solution for the formula.
- c1 [float] Full value of the constant in the *a* parameter, set in some EOSs, [-]
- c2 [float] Full value of the constant in the *b* parameter, set in some EOSs, [-]
- **A\_dep\_g** Departure molar Helmholtz energy from ideal gas behavior for the gas phase, [J/mol].
- A\_dep\_1 Departure molar Helmholtz energy from ideal gas behavior for the liquid phase, [J/mol].

**beta\_g** Isobaric (constant-pressure) expansion coefficient for the gas phase, [1/K].

beta\_1 Isobaric (constant-pressure) expansion coefficient for the liquid phase, [1/K].

- *Cp\_minus\_Cv\_g* Cp Cv for the gas phase, [J/mol/K].
- *Cp\_minus\_Cv\_1* Cp Cv for the liquid phase, [J/mol/K].
- **d2a\_alpha\_dTdP\_g\_V** Derivative of the temperature derivative of *a\_alpha* with respect to pressure at constant volume (varying T) for the gas phase, [J^2/mol^2/Pa^2/K].
- *d2a\_alpha\_dTdP\_1\_V* Derivative of the temperature derivative of *a\_alpha* with respect to pressure at constant volume (varying T) for the liquid phase, [J^2/mol^2/Pa^2/K].
- d2H\_dep\_dT2\_g Second temperature derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K^2].
- d2H\_dep\_dT2\_g\_P Second temperature derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K^2].
- *d2H\_dep\_dT2\_g\_V* Second temperature derivative of departure enthalpy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^2].
- d2H\_dep\_dT2\_1 Second temperature derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K^2].
- d2H\_dep\_dT2\_1\_P Second temperature derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K^2].
- *d2H\_dep\_dT2\_1\_V* Second temperature derivative of departure enthalpy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^2].
- *d2H\_dep\_dTdP\_g* Temperature and pressure derivative of departure enthalpy at constant pressure then temperature for the gas phase, [(J/mol)/K/Pa].
- d2H\_dep\_dTdP\_1 Temperature and pressure derivative of departure enthalpy at constant pressure then temperature for the liquid phase, [(J/mol)/K/Pa].
- *d2P\_drho2\_g* Second derivative of pressure with respect to molar density for the gas phase, [Pa/(mol/m^3)^2].
- d2P\_drho2\_1 Second derivative of pressure with respect to molar density for the liquid phase, [Pa/(mol/m^3)^2].
- *d2P\_dT2\_PV\_g* Second derivative of pressure with respect to temperature twice, but with pressure held constant the first time and volume held constant the second time for the gas phase, [Pa/K^2].
- d2P\_dT2\_PV\_1 Second derivative of pressure with respect to temperature twice, but with pressure held constant the first time and volume held constant the second time for the liquid phase, [Pa/K^2].
- *d2P\_dTdP\_g* Second derivative of pressure with respect to temperature and, then pressure; and with volume held constant at first, then temperature, for the gas phase, [1/K].
- *d2P\_dTdP\_1* Second derivative of pressure with respect to temperature and, then pressure; and with volume held constant at first, then temperature, for the liquid phase, [1/K].
- *d2P\_dTdrho\_g* Derivative of pressure with respect to molar density, and temperature for the gas phase, [Pa/(K\*mol/m^3)].
- d2P\_dTdrho\_1 Derivative of pressure with respect to molar density, and temperature for the liquid phase, [Pa/(K\*mol/m^3)].
- *d2P\_dVdP\_g* Second derivative of pressure with respect to molar volume and then pressure for the gas phase, [mol/m^3].

- d2P\_dVdP\_1 Second derivative of pressure with respect to molar volume and then pressure for the liquid phase, [mol/m^3].
- d2P\_dVdT\_g Alias of GCEOS.d2P\_dTdV\_g
- d2P\_dVdT\_1 Alias of GCEOS.d2P\_dTdV\_1
- *d2P\_dVdT\_TP\_g* Second derivative of pressure with respect to molar volume and then temperature at constant temperature then pressure for the gas phase, [Pa\*mol/m^3/K].
- *d2P\_dVdT\_TP\_1* Second derivative of pressure with respect to molar volume and then temperature at constant temperature then pressure for the liquid phase, [Pa\*mol/m^3/K].
- *d2rho\_dP2\_g* Second derivative of molar density with respect to pressure for the gas phase, [(mol/m^3)/Pa^2].
- d2rho\_dP2\_1 Second derivative of molar density with respect to pressure for the liquid phase, [(mol/m^3)/Pa^2].
- d2rho\_dPdT\_g Second derivative of molar density with respect to pressure and temperature for the gas phase, [(mol/m^3)/(K\*Pa)].
- d2rho\_dPdT\_1 Second derivative of molar density with respect to pressure and temperature for the liquid phase, [(mol/m^3)/(K\*Pa)].
- *d2rho\_dT2\_g* Second derivative of molar density with respect to temperature for the gas phase, [(mol/m^3)/K^2].
- d2rho\_dT2\_1 Second derivative of molar density with respect to temperature for the liquid phase, [(mol/m^3)/K^2].
- d2S\_dep\_dT2\_g Second temperature derivative of departure entropy with respect to temperature for the gas phase, [(J/mol)/K^3].
- *d2S\_dep\_dT2\_g\_V* Second temperature derivative of departure entropy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^3].
- d2S\_dep\_dT2\_1 Second temperature derivative of departure entropy with respect to temperature for the liquid phase, [(J/mol)/K^3].
- *d2S\_dep\_dT2\_1\_V* Second temperature derivative of departure entropy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^3].
- *d2S\_dep\_dTdP\_g* Temperature and pressure derivative of departure entropy at constant pressure then temperature for the gas phase, [(J/mol)/K^2/Pa].
- d2S\_dep\_dTdP\_1 Temperature and pressure derivative of departure entropy at constant pressure then temperature for the liquid phase, [(J/mol)/K^2/Pa].
- *d2T\_dP2\_g* Second partial derivative of temperature with respect to pressure (constant volume) for the gas phase, [K/Pa^2].
- d2T\_dP2\_1 Second partial derivative of temperature with respect to pressure (constant temperature) for the liquid phase, [K/Pa^2].
- d2T\_dPdrho\_g Derivative of temperature with respect to molar density, and pressure for the gas phase, [K/(Pa\*mol/m^3)].
- d2T\_dPdrho\_1 Derivative of temperature with respect to molar density, and pressure for the liquid phase, [K/(Pa\*mol/m^3)].
- *d2T\_dPdV\_g* Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the gas phase, [K\*mol/(Pa\*m^3)].

- d2T\_dPdV\_1 Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the liquid phase, [K\*mol/(Pa\*m^3)].
- d2T\_drho2\_g Second derivative of temperature with respect to molar density for the gas phase, [K/(mol/m^3)^2].
- d2T\_drho2\_1 Second derivative of temperature with respect to molar density for the liquid phase, [K/(mol/m^3)^2].
- *d2T\_dV2\_g* Second partial derivative of temperature with respect to volume (constant pressure) for the gas phase, [K\*mol^2/m^6].
- **d2T\_dV2\_1** Second partial derivative of temperature with respect to volume (constant pressure) for the liquid phase, [K\*mol^2/m^6].
- *d2T\_dVdP\_g* Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the gas phase, [K\*mol/(Pa\*m^3)].
- *d2T\_dVdP\_1* Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the liquid phase, [K\*mol/(Pa\*m^3)].
- *d2V\_dP2\_g* Second partial derivative of volume with respect to pressure (constant temperature) for the gas phase, [m^3/(Pa^2\*mol)].
- *d2V\_dP2\_1* Second partial derivative of volume with respect to pressure (constant temperature) for the liquid phase, [m^3/(Pa^2\*mol)].
- *d2V\_dPdT\_g* Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the gas phase, [m^3/(K\*Pa\*mol)].
- *d2V\_dPdT\_1* Second partial derivative of volume with respect to pressure (constant temperature) and then presssure (constant temperature) for the liquid phase, [m^3/(K\*Pa\*mol)].
- *d2V\_dT2\_g* Second partial derivative of volume with respect to temperature (constant pressure) for the gas phase, [m^3/(mol\*K^2)].
- d2V\_dT2\_1 Second partial derivative of volume with respect to temperature (constant pressure) for the liquid phase, [m^3/(mol\*K^2)].
- *d2V\_dTdP\_g* Second partial derivative of volume with respect to pressure (constant temperature) and then presssure (constant temperature) for the gas phase, [m^3/(K\*Pa\*mol)].
- *d2V\_dTdP\_1* Second partial derivative of volume with respect to pressure (constant temperature) and then presssure (constant temperature) for the liquid phase, [m^3/(K\*Pa\*mol)].
- **d3a\_alpha\_dT3** Method to calculate the third temperature derivative of  $a\alpha$ , [J^2/mol^2/Pa/K^3].
- **da\_alpha\_dP\_g\_V** Derivative of the *a\_alpha* with respect to pressure at constant volume (varying T) for the gas phase, [J^2/mol^2/Pa^2].
- **da\_alpha\_dP\_1\_V** Derivative of the *a\_alpha* with respect to pressure at constant volume (varying T) for the liquid phase, [J^2/mol^2/Pa^2].
- dbeta\_dP\_g Derivative of isobaric expansion coefficient with respect to pressure for the gas phase, [1/(Pa\*K)].
- dbeta\_dP\_1 Derivative of isobaric expansion coefficient with respect to pressure for the liquid phase, [1/(Pa\*K)].
- dbeta\_dT\_g Derivative of isobaric expansion coefficient with respect to temperature for the gas phase, [1/K^2].

- *dbeta\_dT\_1* Derivative of isobaric expansion coefficient with respect to temperature for the liquid phase, [1/K^2].
- *dfugacity\_dP\_g* Derivative of fugacity with respect to pressure for the gas phase, [-].
- dfugacity\_dP\_1 Derivative of fugacity with respect to pressure for the liquid phase, [-].
- **dfugacity\_dT\_g** Derivative of fugacity with respect to temperature for the gas phase, [Pa/K].
- dfugacity\_dT\_1 Derivative of fugacity with respect to temperature for the liquid phase, [Pa/K].
- *dH\_dep\_dP\_g* Derivative of departure enthalpy with respect to pressure for the gas phase, [(J/mol)/Pa].
- *dH\_dep\_dP\_g\_V* Derivative of departure enthalpy with respect to pressure at constant volume for the liquid phase, [(J/mol)/Pa].
- *dH\_dep\_dP\_1* Derivative of departure enthalpy with respect to pressure for the liquid phase, [(J/mol)/Pa].
- *dH\_dep\_dP\_1\_V* Derivative of departure enthalpy with respect to pressure at constant volume for the gas phase, [(J/mol)/Pa].
- *dH\_dep\_dT\_g* Derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K].
- *dH\_dep\_dT\_g\_V* Derivative of departure enthalpy with respect to temperature at constant volume for the gas phase, [(J/mol)/K].
- dH\_dep\_dT\_1 Derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K].
- *dH\_dep\_dT\_1\_V* Derivative of departure enthalpy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K].
- *dH\_dep\_dV\_g\_P* Derivative of departure enthalpy with respect to volume at constant pressure for the gas phase, [J/m^3].
- *dH\_dep\_dV\_g\_T* Derivative of departure enthalpy with respect to volume at constant temperature for the gas phase, [J/m^3].
- *dH\_dep\_dV\_1\_P* Derivative of departure enthalpy with respect to volume at constant pressure for the liquid phase, [J/m^3].
- $dH_dep_dV_1_T$  Derivative of departure enthalpy with respect to volume at constant temperature for the gas phase, [J/m^3].
- *dP\_drho\_g* Derivative of pressure with respect to molar density for the gas phase, [Pa/(mol/m^3)].
- dP\_drho\_1 Derivative of pressure with respect to molar density for the liquid phase, [Pa/(mol/m^3)].
- *dphi\_dP\_g* Derivative of fugacity coefficient with respect to pressure for the gas phase, [1/Pa].
- *dphi\_dP\_1* Derivative of fugacity coefficient with respect to pressure for the liquid phase, [1/Pa].
- *dphi\_dT\_g* Derivative of fugacity coefficient with respect to temperature for the gas phase, [1/K].
- dphi\_dT\_1 Derivative of fugacity coefficient with respect to temperature for the liquid phase,
  [1/K].

- *drho\_dP\_g* Derivative of molar density with respect to pressure for the gas phase, [(mol/m^3)/Pa].
- *drho\_dP\_1* Derivative of molar density with respect to pressure for the liquid phase, [(mol/m^3)/Pa].
- **drho\_dT\_g** Derivative of molar density with respect to temperature for the gas phase, [(mol/m^3)/K].
- drho\_dT\_1 Derivative of molar density with respect to temperature for the liquid phase, [(mol/m^3)/K].
- dS\_dep\_dP\_g Derivative of departure entropy with respect to pressure for the gas phase, [(J/mol)/K/Pa].
- *dS\_dep\_dP\_g\_V* Derivative of departure entropy with respect to pressure at constant volume for the gas phase, [(J/mol)/K/Pa].
- dS\_dep\_dP\_1 Derivative of departure entropy with respect to pressure for the liquid phase, [(J/mol)/K/Pa].
- *dS\_dep\_dP\_1\_V* Derivative of departure entropy with respect to pressure at constant volume for the liquid phase, [(J/mol)/K/Pa].
- *dS\_dep\_dT\_g* Derivative of departure entropy with respect to temperature for the gas phase, [(J/mol)/K^2].
- *dS\_dep\_dT\_g\_V* Derivative of departure entropy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^2].
- **dS\_dep\_dT\_1** Derivative of departure entropy with respect to temperature for the liquid phase, [(J/mol)/K^2].
- *dS\_dep\_dT\_1\_V* Derivative of departure entropy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^2].
- *dS\_dep\_dV\_g\_P* Derivative of departure entropy with respect to volume at constant pressure for the gas phase, [J/K/m^3].
- *dS\_dep\_dV\_g\_T* Derivative of departure entropy with respect to volume at constant temperature for the gas phase, [J/K/m^3].
- *dS\_dep\_dV\_1\_P* Derivative of departure entropy with respect to volume at constant pressure for the liquid phase, [J/K/m^3].
- *dS\_dep\_dV\_1\_T* Derivative of departure entropy with respect to volume at constant temperature for the gas phase, [J/K/m^3].
- *dT\_drho\_g* Derivative of temperature with respect to molar density for the gas phase, [K/(mol/m^3)].
- *dT\_drho\_1* Derivative of temperature with respect to molar density for the liquid phase, [K/(mol/m^3)].
- *dZ\_dP\_g* Derivative of compressibility factor with respect to pressure for the gas phase, [1/Pa].
- dZ\_dP\_1 Derivative of compressibility factor with respect to pressure for the liquid phase, [1/Pa].
- *dZ\_dT\_g* Derivative of compressibility factor with respect to temperature for the gas phase, [1/K].
- dZ\_dT\_1 Derivative of compressibility factor with respect to temperature for the liquid phase, [1/K].

fugacity\_g Fugacity for the gas phase, [Pa].

*fugacity\_1* Fugacity for the liquid phase, [Pa].

- *kappa\_g* Isothermal (constant-temperature) expansion coefficient for the gas phase, [1/Pa].
- *kappa\_1* Isothermal (constant-temperature) expansion coefficient for the liquid phase, [1/Pa].
- *Inphi\_g* The natural logarithm of the fugacity coefficient for the gas phase, [-].
- **Inphi\_1** The natural logarithm of the fugacity coefficient for the liquid phase, [-].
- *more\_stable\_phase* Checks the Gibbs energy of each possible phase, and returns 'l' if the liquid-like phase is more stable, and 'g' if the vapor-like phase is more stable.
- mpmath\_volume\_ratios Method to compare, as ratios, the volumes of the implemented cubic solver versus those calculated using mpmath.
- *mpmath\_volumes* Method to calculate to a high precision the exact roots to the cubic equation, using *mpmath*.
- *mpmath\_volumes\_float* Method to calculate real roots of a cubic equation, using *mpmath*, but returned as floats.
- **phi\_g** Fugacity coefficient for the gas phase, [Pa].
- phi\_1 Fugacity coefficient for the liquid phase, [Pa].
- *rho\_g* Gas molar density, [mol/m^3].
- *rho\_1* Liquid molar density, [mol/m<sup>3</sup>].
- sorted\_volumes List of lexicographically-sorted molar volumes available from the root finding algorithm used to solve the PT point.
- **state\_specs** Convenience method to return the two specified state specs (T, P, or V) as a dictionary.
- **U\_dep\_g** Departure molar internal energy from ideal gas behavior for the gas phase, [J/mol].
- **U\_dep\_1** Departure molar internal energy from ideal gas behavior for the liquid phase, [J/mol].
- Vc Critical volume, [m^3/mol].
- *V\_dep\_g* Departure molar volume from ideal gas behavior for the gas phase, [m^3/mol].
- **V\_dep\_1** Departure molar volume from ideal gas behavior for the liquid phase, [m^3/mol].
- V\_g\_mpmath The molar volume of the gas phase calculated with mpmath to a higher precision, [m^3/mol].
- V\_1\_mpmath The molar volume of the liquid phase calculated with mpmath to a higher precision, [m^3/mol].

# **Methods**

Hvap(T)	Method to calculate enthalpy of vaporization for a
	pure fluid from an equation of state, without iteration.
PT_surface_special([Tmin, Tmax, Pmin, Pmax,	Method to create a plot of the special curves of a fluid
])	- vapor pressure, determinant zeros, pseudo critical
	point, and mechanical critical point.

Table 7 – continued from previous page			
<i>P_PIP_transition</i> (T[, low_P_limit])	Method to calculate the pressure which makes the		
	phase identification parameter exactly 1.		
P_discriminant_zero_g()	Method to calculate the pressure which zero the dis-		
	criminant function of the general cubic eos, and is		
	likely to sit on a boundary between not having a		
	vapor-like volume; and having a vapor-like volume.		
P_discriminant_zero_1()	Method to calculate the pressure which zero the dis-		
	criminant function of the general cubic eos, and is		
	likely to sit on a boundary between not having a		
	liquid-like volume; and having a liquid-like volume.		
P_discriminant_zeros()	Method to calculate the pressures which zero the dis-		
1_discriminant_zeros()	criminant function of the general cubic eos, at the cur-		
	-		
D discriminant source and lutites 1/T h date	rent temperature.		
<i>P_discriminant_zeros_analytical</i> (T, b, delta,	Method to calculate the pressures which zero the dis-		
	criminant function of the general cubic eos.		
P_max_at_V(V)	Dummy method.		
<pre>Psat(T[, polish, guess])</pre>	Generic method to calculate vapor pressure for a		
	specified T.		
<pre>Psat_errors([Tmin, Tmax, pts, plot, show,])</pre>	Method to create a plot of vapor pressure and the rel-		
	ative error of its calculation vs.		
<i>T_discriminant_zero_g</i> ([T_guess])	Method to calculate the temperature which zeros the		
	discriminant function of the general cubic eos, and		
	is likely to sit on a boundary between not having a		
	vapor-like volume; and having a vapor-like volume.		
T_discriminant_zero_1([T_guess])	Method to calculate the temperature which zeros the		
	discriminant function of the general cubic eos, and		
	is likely to sit on a boundary between not having a		
	liquid-like volume; and having a liquid-like volume.		
T_max_at_V(V[, Pmax])	Method to calculate the maximum temperature the		
	EOS can create at a constant volume, if one exists;		
	returns None otherwise.		
<i>T_min_at_V</i> (V[, Pmin])	Returns the minimum temperature for the EOS to		
	have the volume as specified.		
Tsat(P[, polish])	Generic method to calculate the temperature for a		
	specified vapor pressure of the pure fluid.		
$V = cct(\mathbf{T})$			
$V_g_sat(T)$	Method to calculate molar volume of the vapor phase		
	along the saturation line.		
<i>V_1_sat(</i> <b>T</b> )	Method to calculate molar volume of the liquid phase		
	along the saturation line.		
Vs_mpmath()	Method to calculate real roots of a cubic equation,		
	using <i>mpmath</i> .		
<pre>a_alpha_and_derivatives(T[, full, quick,])</pre>	Method to calculate $a\alpha$ and its first and second		
	derivatives.		
a_alpha_and_derivatives_pure(T)	Dummy method to calculate $a\alpha$ and its first and sec-		
	ond derivatives.		
a_alpha_for_Psat(T, Psat[, a_alpha_guess])	Method to calculate which value of $a\alpha$ is required for		
	a given T, Psat pair.		
a_alpha_for_V(T, P, V)	Method to calculate which value of $a\alpha$ is required for		
	a given T, P pair to match a specified V.		
a_alpha_plot([Tmin, Tmax, pts, plot, show])	Method to create a plot of the $a\alpha$ parameter and its		
	first two derivatives.		
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Table	7 - continued from	n previous page
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Table 7 – continued	d from previous page
as_json()	Method to create a JSON-friendly serialization of the
	eos which can be stored, and reloaded later.
<pre>check_sufficient_inputs()</pre>	Method to an exception if none of the pairs (T, P), (T,
* V	V), or (P, V) are given.
d2phi_sat_dT2(T[, polish])	Method to calculate the second temperature deriva-
	tive of saturation fugacity coefficient of the com-
	pound.
<i>dH_dep_dT_sat_g</i> (T[, polish])	Method to calculate and return the temperature
un_uep_ur_sac_g(r[, ponsil])	derivative of saturation vapor excess enthalpy.
di don dT cot l(T[ polich])	Method to calculate and return the temperature
<i>dH_dep_dT_sat_1</i> (T[, polish])	-
	derivative of saturation liquid excess enthalpy.
dPsat_dT(T[, polish, also_Psat])	Generic method to calculate the temperature deriva-
	tive of vapor pressure for a specified <i>T</i> .
<i>dS_dep_dT_sat_g</i> (T[, polish])	Method to calculate and return the temperature
	derivative of saturation vapor excess entropy.
dS_dep_dT_sat_1(T[, polish])	Method to calculate and return the temperature
	derivative of saturation liquid excess entropy.
discriminant([T, P])	Method to compute the discriminant of the cubic vol-
	ume solution with the current EOS parameters, op-
	tionally at the same (assumed) T, and P or at different
	ones, if values are specified.
<pre>dphi_sat_dT(T[, polish])</pre>	Method to calculate the temperature derivative of sat-
	uration fugacity coefficient of the compound.
<pre>from_json(json_repr)</pre>	Method to create a eos from a JSON serialization of
	another eos.
<pre>model_hash()</pre>	Basic method to calculate a hash of the non-state
model_mash()	parts of the model This is useful for comparing to
	models to determine if they are the same, i.e. in a
	VLL flash it is important to know if both liquids have the same model.
whi est(T[ welich])	
<pre>phi_sat(T[, polish])</pre>	Method to calculate the saturation fugacity coeffi-
	cient of the compound.
resolve_full_alphas()	Generic method to resolve the eos with fully calcu-
	lated alpha derviatives.
<pre>saturation_prop_plot(prop[, Tmin, Tmax,])</pre>	Method to create a plot of a specified property of the
	EOS along the (pure component) saturation line.
<pre>set_from_PT(Vs[, only_l, only_g])</pre>	Counts the number of real volumes in Vs, and deter-
	mines what to do.
<pre>set_properties_from_solution(T, P, V, b,)</pre>	Sets all interesting properties which can be calculated
	from an EOS alone.
<i>solve</i> ([pure_a_alphas, only_l, only_g,])	First EOS-generic method; should be called by all
	specific EOSs.
<pre>solve_T(P, V[, solution])</pre>	Generic method to calculate $T$ from a specified $P$ and
	V.
<pre>solve_missing_volumes()</pre>	Generic method to ensure both volumes, if solutions
	are physical, have calculated properties.
<pre>state_hash()</pre>	Basic method to calculate a hash of the state of the
State_Hash()	model and its model parameters.
to([T, P, V])	Method to construct a new EOS object at two of $T, P$
	or V.
	continues on next page

Table 7 – continued from previous page

Table 7 – continued from previous page			
to_PV(P, V)	Method to construct a new EOS object at the spcified		
	P and V.		
$to_TP(T, P)$	Method to construct a new EOS object at the spcified		
	T and $P$ .		
$to_TV(T, V)$	Method to construct a new EOS object at the spcified		
	T and $V$ .		
volume_error()	Method to calculate the relative absolute error in the		
	calculated molar volumes.		
volume_errors([Tmin, Tmax, Pmin, Pmax, pts,	Method to create a plot of the relative absolute error		
])	in the cubic volume solution as compared to a higher-		
	precision calculation.		
volume_solutions(T, P, b, delta, epsilon,)	Halley's method based solver for cubic EOS volumes		
	based on the idea of initializing from a single liquid-		
	like guess which is solved precisely, deflating the cu-		
	bic analytically, solving the quadratic equation for the		
	next two volumes, and then performing two halley		
	steps on each of them to obtain the final solutions.		
volume_solutions_full(T, P, b, delta,[,])	Newton-Raphson based solver for cubic EOS vol-		
	umes based on the idea of initializing from an ana-		
	lytical solver.		
volume_solutions_mp(T, P, b, delta, epsilon,)	Solution of this form of the cubic EOS in terms of vol-		
	umes, using the <i>mpmath</i> arbitrary precision library.		

#### property A\_dep\_g

Departure molar Helmholtz energy from ideal gas behavior for the gas phase, [J/mol].

$$A_{dep} = U_{dep} - TS_{dep}$$

#### property A\_dep\_1

Departure molar Helmholtz energy from ideal gas behavior for the liquid phase, [J/mol].

$$A_{dep} = U_{dep} - TS_{dep}$$

# property Cp\_minus\_Cv\_g

Cp - Cv for the gas phase, [J/mol/K].

$$C_p - C_v = -T \left(\frac{\partial P}{\partial T}\right)_V^2 / \left(\frac{\partial P}{\partial V}\right)_T$$

# property Cp\_minus\_Cv\_1

Cp - Cv for the liquid phase, [J/mol/K].

$$C_p - C_v = -T \left(\frac{\partial P}{\partial T}\right)_V^2 / \left(\frac{\partial P}{\partial V}\right)_T$$

Hvap(T)

Method to calculate enthalpy of vaporization for a pure fluid from an equation of state, without iteration.

$$\frac{dP^{sat}}{dT} = \frac{\Delta H_{vap}}{T(V_g - V_l)}$$

Results above the critical temperature are meaningless. A first-order polynomial is used to extrapolate under 0.32 Tc; however, there is normally not a volume solution to the EOS which can produce that low of a pressure.

# **Parameters**

T [float] Temperature, [K]

# Returns

**Hvap** [float] Increase in enthalpy needed for vaporization of liquid phase along the saturation line, [J/mol]

# Notes

Calculates vapor pressure and its derivative with Psat and  $dPsat_dT$  as well as molar volumes of the saturation liquid and vapor phase in the process.

Very near the critical point this provides unrealistic results due to *Psat*'s polynomials being insufficiently accurate.

# References

[1]

```
N = 1
```

The number of components in the EOS

PT\_surface\_special(*Tmin=0.0001*, *Tmax=100000.0*, *Pmin=0.01*, *Pmax=1000000000.0*, *pts=50*, show=False, color\_map=None, mechanical=True, pseudo\_critical=True, Psat=True,

 $determinant\_zeros=True, phase\_ID\_transition=True, base\_property='V', \\$ 

base\_min=None, base\_max=None, base\_selection='Gmin')

Method to create a plot of the special curves of a fluid - vapor pressure, determinant zeros, pseudo critical point, and mechanical critical point.

The color background is a plot of the molar volume (by default) which has the minimum Gibbs energy (by default). If shown with a sufficient number of points, the curve between vapor and liquid should be shown smoothly.

## Parameters

Tmin [float, optional] Minimum temperature of calculation, [K]

Tmax [float, optional] Maximum temperature of calculation, [K]

Pmin [float, optional] Minimum pressure of calculation, [Pa]

**Pmax** [float, optional] Maximum pressure of calculation, [Pa]

pts [int, optional] The number of points to include in both the x and y axis [-]

**show** [bool, optional] Whether or not the plot should be rendered and shown; a handle to it is returned if *plot* is True for other purposes such as saving the plot to a file, [-]

color\_map [matplotlib.cm.ListedColormap, optional] Matplotlib colormap object, [-]

**mechanical** [bool, optional] Whether or not to include the mechanical critical point; this is the same as the critical point for a pure compound but not for a mixture, [-]

**pseudo\_critical** [bool, optional] Whether or not to include the pseudo critical point; this is the same as the critical point for a pure compound but not for a mixture, [-]

**Psat** [bool, optional] Whether or not to include the vapor pressure curve; for mixtures this is neither the bubble nor dew curve, but rather a hypothetical one which uses the same equation as the pure components, [-]

- **determinant\_zeros** [bool, optional] Whether or not to include a curve showing when the EOS's determinant hits zero, [-]
- **phase\_ID\_transition** [bool, optional] Whether or not to show a curve of where the PIP hits 1 exactly, [-]
- **base\_property** [str, optional] The property which should be plotted; '\_l' and '\_g' are added automatically according to the selected phase, [-]
- **base\_min** [float, optional] If specified, the *base* property will values will be limited to this value at the minimum, [-]
- **base\_max** [float, optional] If specified, the *base* property will values will be limited to this value at the maximum, [-]
- **base\_selection** [str, optional] For the base property, there are often two possible phases and but only one value can be plotted; use '1' to pefer liquid-like values, 'g' to prefer gas-like values, and 'Gmin' to prefer values of the phase with the lowest Gibbs energy, [-]

#### Returns

fig [matplotlib.figure.Figure] Plotted figure, only returned if plot is True, [-]

## **P\_PIP\_transition**(*T*, *low\_P\_limit=0.0*)

Method to calculate the pressure which makes the phase identification parameter exactly 1. There are three regions for this calculation:

- subcritical PIP = 1 for the gas-like phase at P = 0
- initially supercritical PIP = 1 on a curve starting at the critical point, increasing for a while, decreasing for a while, and then curving sharply back to a zero pressure.
- later supercritical PIP = 1 for the liquid-like phase at P = 0

#### Parameters

**T** [float] Temperature for the calculation, [K]

low\_P\_limit [float] What value to return for the subcritical and later region, [Pa]

## Returns

**P** [float] Pressure which makes the PIP = 1, [Pa]

## Notes

The transition between the region where this function returns values and the high temperature region that doesn't is the Joule-Thomson inversion point at a pressure of zero and can be directly solved for.

#### Examples

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=299.,_
...,P=1E6)
>>> eos.P_PIP_transition(100)
0.0
>>> low_T = eos.to(T=100.0, P=eos.P_PIP_transition(100, low_P_limit=1e-5))
>>> low_T.PIP_l, low_T.PIP_g
(45.778088191, 0.9999999997903)
>>> initial_super = eos.to(T=600.0, P=eos.P_PIP_transition(600))
```

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```
>>> initial_super.P, initial_super.PIP_g
(6456282.17132, 0.999999999999)
>>> high_T = eos.to(T=900.0, P=eos.P_PIP_transition(900, low_P_limit=1e-5))
>>> high_T.P, high_T.PIP_g
(12536704.763, 0.9999999999)
```

# P\_discriminant\_zero\_g()

Method to calculate the pressure which zero the discriminant function of the general cubic eos, and is likely to sit on a boundary between not having a vapor-like volume; and having a vapor-like volume.

#### Returns

**P\_discriminant\_zero\_g** [float] Pressure which make the discriminants zero at the right condition, [Pa]

# **Examples**

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=299.,
→P=1E6)
>>> P_trans = eos.P_discriminant_zero_g()
>>> P_trans
149960391.7
```

In this case, the discriminant transition does not reveal a transition to two roots being available, only negative roots becoming negative and imaginary.

```
>>> eos.to(T=eos.T, P=P_trans*.99999999).mpmath_volumes_float
((-0.0001037013146195082-1.5043987866732543e-08j), (-0.0001037013146195082+1.

->5043987866732543e-08j), (0.00011799201928619508+0j))
>>> eos.to(T=eos.T, P=P_trans*1.0000001).mpmath_volumes_float
((-0.00010374888853182635+0j), (-0.00010365374200380354+0j), (0.

->00011799201875924273+0j))
```

## P\_discriminant\_zero\_1()

Method to calculate the pressure which zero the discriminant function of the general cubic eos, and is likely to sit on a boundary between not having a liquid-like volume; and having a liquid-like volume.

# Returns

P\_discriminant\_zero\_l [float] Pressure which make the discriminants zero at the right condition, [Pa]

## **Examples**

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=299.,_
...,P=1E6)
>>> P_trans = eos.P_discriminant_zero_1()
>>> P_trans
478346.37289
```

In this case, the discriminant transition shows the change in roots:

```
>>> eos.to(T=eos.T, P=P_trans*.99999999).mpmath_volumes_float
((0.00013117994140177062+0j), (0.002479717165903531+0j), (0.
→002480236178570793+0j))
>>> eos.to(T=eos.T, P=P_trans*1.0000001).mpmath_volumes_float
((0.0001311799413872173+0j), (0.002479976386402769-8.206310112063695e-07j), (0.
→002479976386402769+8.206310112063695e-07j))
```

# P\_discriminant\_zeros()

Method to calculate the pressures which zero the discriminant function of the general cubic eos, at the current temperature.

#### Returns

P\_discriminant\_zeros [list[float]] Pressures which make the discriminants zero, [Pa]

## **Examples**

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=299.,

→P=1E6)
>>> eos.P_discriminant_zeros()
[478346.3, 149960391.7]
```

static P\_discriminant\_zeros\_analytical(T, b, delta, epsilon, a\_alpha, valid=False)

Method to calculate the pressures which zero the discriminant function of the general cubic eos. This is a quartic function solved analytically.

#### **Parameters**

T [float] Temperature, [K]

**b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**valid** [bool] Whether to filter the calculated pressures so that they are all real, and positive only, [-]

## Returns

P\_discriminant\_zeros [float] Pressures which make the discriminants zero, [Pa]

## Notes

Calculated analytically. Derived as follows.

(continued from previous page)

# $P_max_at_V(V)$

Dummy method. The idea behind this method, which is implemented by some subclasses, is to calculate the maximum pressure the EOS can create at a constant volume, if one exists; returns None otherwise. This method, as a dummy method, always returns None.

#### Parameters

V [float] Constant molar volume, [m^3/mol]

Returns

**P** [float] Maximum possible isochoric pressure, [Pa]

# $P_{zero_g_{cheb_{limits}} = (0.0, 0.0)$

#### P\_zero\_l\_cheb\_limits = (0.0, 0.0)

#### **Psat**(*T*, *polish=False*, *guess=None*)

Generic method to calculate vapor pressure for a specified T.

From Tc to 0.32Tc, uses a 10th order polynomial of the following form:

$$\ln \frac{P_r}{T_r} = \sum_{k=0}^{10} C_k \left(\frac{\alpha}{T_r} - 1\right)^k$$

If *polish* is True, SciPy's *newton* solver is launched with the calculated vapor pressure as an initial guess in an attempt to get more accuracy. This may not converge however.

Results above the critical temperature are meaningless. A first-order polynomial is used to extrapolate under 0.32 Tc; however, there is normally not a volume solution to the EOS which can produce that low of a pressure.

## **Parameters**

T [float] Temperature, [K]

**polish** [bool, optional] Whether to attempt to use a numerical solver to make the solution more precise or not

# Returns

Psat [float] Vapor pressure, [Pa]

#### Notes

EOSs sharing the same b, delta, and epsilon have the same coefficient sets.

Form for the regression is inspired from [1].

No volume solution is needed when *polish=False*; the only external call is for the value of *a\_alpha*.

#### References

[1]

# $Psat_cheb_range = (0.0, 0.0)$

**Psat\_errors**(*Tmin=None*, *Tmax=None*, *pts=50*, *plot=False*, *show=False*, *trunc\_err\_low=1e-18*, *trunc\_err\_high=1.0*, *Pmin=1e-100*)

Method to create a plot of vapor pressure and the relative error of its calculation vs. the iterative *polish* approach.

#### **Parameters**

- **Tmin** [float] Minimum temperature of calculation; if this is too low the saturation routines will stop converging, [K]
- **Tmax** [float] Maximum temperature of calculation; cannot be above the critical temperature, [K]

pts [int, optional] The number of temperature points to include [-]

plot [bool] If False, the solution is returned without plotting the data, [-]

**show** [bool] Whether or not the plot should be rendered and shown; a handle to it is returned if *plot* is True for other purposes such as saving the plot to a file, [-]

trunc\_err\_low [float] Minimum plotted error; values under this are rounded to 0, [-]

trunc\_err\_high [float] Maximum plotted error; values above this are rounded to 1, [-]

**Pmin** [float] Minimum pressure for the solution to work on, [Pa]

#### Returns

errors [list[float]] Absolute relative errors, [-]

Psats\_num [list[float]] Vapor pressures calculated to full precision, [Pa]

Psats\_fit [list[float]] Vapor pressures calculated with the fast solution, [Pa]

fig [matplotlib.figure.Figure] Plotted figure, only returned if plot is True, [-]

# T\_discriminant\_zero\_g(T\_guess=None)

Method to calculate the temperature which zeros the discriminant function of the general cubic eos, and is likely to sit on a boundary between not having a vapor-like volume; and having a vapor-like volume.

#### Parameters

T\_guess [float, optional] Temperature guess, [K]

Returns

**T\_discriminant\_zero\_g** [float] Temperature which make the discriminants zero at the right condition, [K]

#### Notes

Significant numerical issues remain in improving this method.

## **Examples**

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=299.,_
__P=1E6)
>>> T_trans = eos.T_discriminant_zero_g()
>>> T_trans
644.3023307
```

In this case, the discriminant transition does not reveal a transition to two roots being available, only to there being a double (imaginary) root.

```
>>> eos.to(P=eos.P, T=T_trans).mpmath_volumes_float
((9.309597822372529e-05-0.00015876248805149625j), (9.309597822372529e-05+0.
→00015876248805149625j), (0.005064847204219234+0j))
```

#### **T\_discriminant\_zero\_l**(*T\_guess=None*)

Method to calculate the temperature which zeros the discriminant function of the general cubic eos, and is likely to sit on a boundary between not having a liquid-like volume; and having a liquid-like volume.

#### **Parameters**

T\_guess [float, optional] Temperature guess, [K]

Returns

T\_discriminant\_zero\_l [float] Temperature which make the discriminants zero at the right condition, [K]

#### Notes

Significant numerical issues remain in improving this method.

# **Examples**

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=299.,_
→P=1E6)
>>> T_trans = eos.T_discriminant_zero_1()
>>> T_trans
644.3023307
```

In this case, the discriminant transition does not reveal a transition to two roots being available, only to there being a double (imaginary) root.

```
>>> eos.to(P=eos.P, T=T_trans).mpmath_volumes_float
((9.309597822372529e-05-0.00015876248805149625j), (9.309597822372529e-05+0.
→00015876248805149625j), (0.005064847204219234+0j))
```

#### T\_max\_at\_V(V, Pmax=None)

Method to calculate the maximum temperature the EOS can create at a constant volume, if one exists; returns None otherwise.

#### Parameters

V [float] Constant molar volume, [m^3/mol]

Pmax [float] Maximum possible isochoric pressure, if already known [Pa]

# Returns

T [float] Maximum possible temperature, [K]

# **Examples**

>>> e = PR(P=1e5, V=0.0001437, Tc=512.5, Pc=8084000.0, omega=0.559)
>>> e.T\_max\_at\_V(e.V)
431155.5

# $T_min_at_V(V, Pmin=1e-15)$

Returns the minimum temperature for the EOS to have the volume as specified. Under this temperature, the pressure will go negative (and the EOS will not solve).

#### **Tsat**(*P*, *polish=False*)

Generic method to calculate the temperature for a specified vapor pressure of the pure fluid. This is simply a bounded solver running between 0.2Tc and Tc on the *Psat* method.

#### **Parameters**

**P** [float] Vapor pressure, [Pa]

**polish** [bool, optional] Whether to attempt to use a numerical solver to make the solution more precise or not

# Returns

Tsat [float] Temperature of saturation, [K]

# Notes

It is recommended not to run with *polish=True*, as that will make the calculation much slower.

# property U\_dep\_g

Departure molar internal energy from ideal gas behavior for the gas phase, [J/mol].

$$U_{dep} = H_{dep} - PV_{dep}$$

## property U\_dep\_1

Departure molar internal energy from ideal gas behavior for the liquid phase, [J/mol].

$$U_{dep} = H_{dep} - PV_{dep}$$

# property V\_dep\_g

Departure molar volume from ideal gas behavior for the gas phase, [m<sup>3</sup>/mol].

$$V_{dep} = V - \frac{RT}{P}$$

## property V\_dep\_l

Departure molar volume from ideal gas behavior for the liquid phase, [m^3/mol].

$$V_{dep} = V - \frac{RT}{P}$$

#### property V\_g\_mpmath

The molar volume of the gas phase calculated with *mpmath* to a higher precision,  $[m^3/mol]$ . This is useful for validating the cubic root solver(s). It is not quite a true arbitrary solution to the EOS, because the constants *b*, epsilon, *delta* and *a\_alpha* as well as the input arguments *T* and *P* are not calculated with arbitrary precision. This is a feature when comparing the volume solution algorithms however as they work with the same finite-precision variables.

#### $V_g_sat(T)$

Method to calculate molar volume of the vapor phase along the saturation line.

#### **Parameters**

T [float] Temperature, [K]

#### Returns

V\_g\_sat [float] Gas molar volume along the saturation line, [m^3/mol]

#### Notes

Computes *Psat*, and then uses *volume\_solutions* to obtain the three possible molar volumes. The highest value is returned.

# property V\_1\_mpmath

The molar volume of the liquid phase calculated with *mpmath* to a higher precision,  $[m^3/mol]$ . This is useful for validating the cubic root solver(s). It is not quite a true arbitrary solution to the EOS, because the constants *b*, epsilon, *delta* and *a\_alpha* as well as the input arguments *T* and *P* are not calculated with arbitrary precision. This is a feature when comparing the volume solution algorithms however as they work with the same finite-precision variables.

## $V_1_sat(T)$

Method to calculate molar volume of the liquid phase along the saturation line.

#### **Parameters**

T [float] Temperature, [K]

#### Returns

V\_l\_sat [float] Liquid molar volume along the saturation line, [m^3/mol]

#### Notes

Computes *Psat*, and then uses *volume\_solutions* to obtain the three possible molar volumes. The lowest value is returned.

#### property Vc

Critical volume, [m^3/mol].

$$V_c = \frac{Z_c R T_c}{P_c}$$

#### Vs\_mpmath()

Method to calculate real roots of a cubic equation, using mpmath.

#### Returns

Vs [list[mpf]] Either 1 or 3 real volumes as calculated by mpmath, [m^3/mol]

#### **Examples**

# \_\_repr\_\_()

Create a string representation of the EOS - by default, include all parameters so as to make it easy to construct new instances from states. Includes the two specified state variables, *Tc*, *Pc*, *omega* and any *kwargs*.

#### Returns

**recreation** [str] String which is valid Python and recreates the current state of the object if ran, [-]

# **Examples**

```
>>> eos = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=400.0, P=1e6)
>>> eos
PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=400.0, P=1000000.0)
```

**a\_alpha\_and\_derivatives**(T, full=True, quick=True, pure\_a\_alphas=True) Method to calculate  $a\alpha$  and its first and second derivatives.

#### Parameters

**T** [float] Temperature, [K]

full [bool, optional] If False, calculates and returns only a\_alpha, [-]

quick [bool, optional] Legary parameter being phased out [-]

**pure\_a\_alphas** [bool, optional] Whether or not to recalculate the a\_alpha terms of pure components (for the case of mixtures only) which stay the same as the composition changes (i.e in a PT flash); does nothing in the case of pure EOSs [-]

# Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

## a\_alpha\_and\_derivatives\_pure(T)

Dummy method to calculate  $a\alpha$  and its first and second derivatives. Should be implemented with the same function signature in each EOS variant; this only raises a NotImplemented Exception. Should return 'a\_alpha', 'da\_alpha\_dT', and 'd2a\_alpha\_dT2'.

# Parameters

T [float] Temperature, [K]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

#### a\_alpha\_for\_Psat(T, Psat, a\_alpha\_guess=None)

Method to calculate which value of  $a\alpha$  is required for a given *T*, *Psat* pair. This is a numerical solution, but not a very complicated one.

#### Parameters

T [float] Temperature, [K]

Psat [float] Vapor pressure specified, [Pa]

a\_alpha\_guess [float] Optionally, an initial guess for the solver [J^2/mol^2/Pa]

## Returns

**a\_alpha** [float] Value calculated to match specified volume for the current EOS, [J^2/mol^2/Pa]

# Notes

The implementation of this function is a direct calculation of departure gibbs energy, which is equal in both phases at saturation.

# **Examples**

```
>>> eos = PR(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6)
>>> eos.a_alpha_for_Psat(T=400, Psat=5e5)
3.1565798926
```

# $a_alpha_for_V(T, P, V)$

Method to calculate which value of  $a\alpha$  is required for a given T, P pair to match a specified V. This is a straightforward analytical equation.

## Parameters

- T [float] Temperature, [K]
- **P** [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]

#### Returns

**a\_alpha** [float] Value calculated to match specified volume for the current EOS, [J^2/mol^2/Pa]

#### Notes

The derivation of the solution is as follows:

a\_alpha\_plot(Tmin=0.0001, Tmax=None, pts=1000, plot=True, show=True)

Method to create a plot of the  $a\alpha$  parameter and its first two derivatives. This easily allows identification of EOSs which are displaying inconsistent behavior.

#### **Parameters**

Tmin [float] Minimum temperature of calculation, [K]

Tmax [float] Maximum temperature of calculation, [K]

pts [int, optional] The number of temperature points to include [-]

**plot** [bool] If False, the calculated values and temperatures are returned without plotting the data, [-]

**show** [bool] Whether or not the plot should be rendered and shown; a handle to it is returned if *plot* is True for other purposes such as saving the plot to a file, [-]

# Returns

Ts [list[float]] Logarithmically spaced temperatures in specified range, [K]

a\_alpha [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]
- fig [matplotlib.figure.Figure] Plotted figure, only returned if *plot* is True, [-]

#### as\_json()

Method to create a JSON-friendly serialization of the eos which can be stored, and reloaded later.

#### Returns

json\_repr [dict] JSON-friendly representation, [-]

# **Examples**

# property beta\_g

Isobaric (constant-pressure) expansion coefficient for the gas phase, [1/K].

$$\beta = \frac{1}{V} \frac{\partial V}{\partial T}$$

# property beta\_1

Isobaric (constant-pressure) expansion coefficient for the liquid phase, [1/K].

$$\beta = \frac{1}{V} \frac{\partial V}{\partial T}$$

# c1 = None

Parameter used by some equations of state in the *a* calculation

# c2 = None

Parameter used by some equations of state in the b calculation

# check\_sufficient\_inputs()

Method to an exception if none of the pairs (T, P), (T, V), or (P, V) are given.

# property d2H\_dep\_dT2\_g

Second temperature derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K^2].

$$\frac{\partial^2 H_{dep,g}}{\partial T^2} = P \frac{d^2}{dT^2} V(T) - \frac{8T \frac{d}{dT} V(T) \frac{d^2}{dT^2} \operatorname{a\alpha}(T)}{\left(\delta^2 - 4\epsilon\right) \left(\frac{\left(\delta + 2V(T)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{2T \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^3}{dT^3} \operatorname{a\alpha}(T)}{\sqrt{\delta^2 - 4\epsilon}} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) - \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) - \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\delta^2 - 4$$

# property d2H\_dep\_dT2\_g\_P

Second temperature derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K^2].

$$\frac{\partial^2 H_{dep,g}}{\partial T^2} = P \frac{d^2}{dT^2} V(T) - \frac{8T \frac{d}{dT} V(T) \frac{d^2}{dT^2} \operatorname{a\alpha}(T)}{\left(\delta^2 - 4\epsilon\right) \left(\frac{\left(\delta + 2V(T)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{2T \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^3}{dT^3} \operatorname{a\alpha}(T)}{\sqrt{\delta^2 - 4\epsilon}} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) - \frac{1}{\delta^2}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) - \frac{1}{\delta^2}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\sqrt{\delta^2 - 4\epsilon}}\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta^2 - 4\epsilon\right) \left(\delta^2 - 4\epsilon\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\delta^2}{\sqrt{\delta^2 - 4\epsilon}}\right)} + \frac{16 \left(\delta^2 - 4\epsilon\right) \left(\delta^2 - 4\epsilon\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\delta^2 - 4\epsilon\right)^2$$

# property d2H\_dep\_dT2\_g\_V

Second temperature derivative of departure enthalpy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^2].

$$\left(\frac{\partial^2 H_{dep,g}}{\partial T^2}\right)_V = \frac{2T \operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^3}{dT^3} \operatorname{a}\alpha\left(T\right)}{\sqrt{\delta^2 - 4\epsilon}} + V \frac{\partial^2}{\partial T^2} P(V,T) + \frac{2 \operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^2}{dT^2} \operatorname{a}\alpha\left(T\right)}{\sqrt{\delta^2 - 4\epsilon}}$$

#### property d2H\_dep\_dT2\_1

Second temperature derivative of departure enthalpy with respect to temperature for the liquid phase,  $[(J/mol)/K^{2}]$ .

$$\frac{\partial^2 H_{dep,l}}{\partial T^2} = P \frac{d^2}{dT^2} V(T) - \frac{8T \frac{d}{dT} V(T) \frac{d^2}{dT^2} a\alpha\left(T\right)}{\left(\delta^2 - 4\epsilon\right) \left(\frac{\left(\delta + 2V(T)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{2T \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^3}{dT^3} a\alpha\left(T\right)}{\sqrt{\delta^2 - 4\epsilon}} + \frac{16\left(\delta + 2V(T)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) + \frac{16\left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \alpha\left(T\right) + \frac{16\left(\delta$$

# property d2H\_dep\_dT2\_1\_P

Second temperature derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K^2].

$$\frac{\partial^2 H_{dep,l}}{\partial T^2} = P \frac{d^2}{dT^2} V(T) - \frac{8T \frac{d}{dT} V(T) \frac{d^2}{dT^2} \operatorname{ac}(T)}{(\delta^2 - 4\epsilon) \left(\frac{(\delta + 2V(T))^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{2T \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^3}{dT^3} \operatorname{ac}(T)}{\sqrt{\delta^2 - 4\epsilon}} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}(T) + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{dT} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} \operatorname{ac}(T)\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)}{(\delta^2 - 4\epsilon)^2 \left(\frac{\delta^2}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)}{(\delta^2 - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)}{(\delta^2 - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)}{(\delta^2 - \frac{1}{2}\right)} + \frac{16 \left(\delta + 2V(T)\right) \left(T \frac{d}{\delta^2} - \frac{1}{2}\right)}{(\delta^2 - \frac{1}{2}\right)} + \frac{16 \left(\delta^2 - \frac{1}{2}\right)}{(\delta^2 - \frac{1}{2}\right)} + \frac{16 \left(\delta^2 - \frac{1}{2}\right)}{(\delta^2 - \frac{1}{2}\right)} + \frac{16 \left(\delta^2 - \frac{1}{2}\right)}{(\delta^2 - \frac$$

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# property d2H\_dep\_dT2\_1\_V

Second temperature derivative of departure enthalpy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^2].

$$\left(\frac{\partial^2 H_{dep,l}}{\partial T^2}\right)_V = \frac{2T \operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^3}{dT^3} \operatorname{a}\alpha\left(T\right)}{\sqrt{\delta^2 - 4\epsilon}} + V \frac{\partial^2}{\partial T^2} P(V,T) + \frac{2 \operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^2}{dT^2} \operatorname{a}\alpha\left(T\right)}{\sqrt{\delta^2 - 4\epsilon}}$$

# property d2H\_dep\_dTdP\_g

Temperature and pressure derivative of departure enthalpy at constant pressure then temperature for the gas phase, [(J/mol)/K/Pa].

$$\left(\frac{\partial^2 H_{dep,g}}{\partial T \partial P}\right)_{T,P} = P \frac{\partial^2}{\partial T \partial P} V(T,P) - \frac{4T \frac{\partial}{\partial P} V(T,P) \frac{d^2}{dT^2} \operatorname{a\alpha}\left(T\right)}{\left(\delta^2 - 4\epsilon\right) \left(\frac{\left(\delta + 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta + 2V(T,P)\right) \left(T \frac{d}{dT} \operatorname{a\alpha}\left(T\right) - \operatorname{a\alpha}\left(T\right)\right) \frac{\partial}{\partial P} \left(\frac{\partial}{\partial T} \left(\frac{\delta + 2V(T,P)}{\delta^2 - 4\epsilon} - 1\right)\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta + 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)}$$

#### property d2H\_dep\_dTdP\_l

Temperature and pressure derivative of departure enthalpy at constant pressure then temperature for the liquid phase, [(J/mol)/K/Pa].

$$\left(\frac{\partial^2 H_{dep,l}}{\partial T \partial P}\right)_V = P \frac{\partial^2}{\partial T \partial P} V(T,P) - \frac{4T \frac{\partial}{\partial P} V(T,P) \frac{d^2}{dT^2} a\alpha\left(T\right)}{\left(\delta^2 - 4\epsilon\right) \left(\frac{\left(\delta + 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta + 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta + 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} a\alpha\left(T\right) - a\alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} \alpha\left(T\right) - \alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} \alpha\left(T\right) - \alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)^2}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} \alpha\left(T\right) - \alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} \alpha\left(T\right) - \alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \left(T \frac{d}{dT} \alpha\left(T\right) - \alpha\left(T\right)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta - 2V(T,P)\right) \frac{\partial}{\partial P} V(T,P)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)}} + \frac{16\left(\delta^2 - 2V(T,P)\right)}{\left(\delta^2 - 4\epsilon\right)^2 \left(\frac{\left(\delta - 2V(T,P)\right)}{\delta^2 - 4\epsilon} - 1\right)$$

#### property d2P\_dT2\_PV\_g

Second derivative of pressure with respect to temperature twice, but with pressure held constant the first time and volume held constant the second time for the gas phase, [Pa/K^2].

$$\left(\frac{\partial^2 P}{\partial T \partial T}\right)_{P,V} = -\frac{R\frac{d}{dT}V(T)}{\left(-b+V(T)\right)^2} - \frac{\left(-\delta\frac{d}{dT}V(T) - 2V(T)\frac{d}{dT}V(T)\right)\frac{d}{dT}\operatorname{a}\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^2} - \frac{\frac{d^2}{dT^2}\operatorname{a}\alpha\left(T\right)}{\delta V(T) + \epsilon + V^2(T)}$$

## property d2P\_dT2\_PV\_1

Second derivative of pressure with respect to temperature twice, but with pressure held constant the first time and volume held constant the second time for the liquid phase, [Pa/K^2].

$$\left(\frac{\partial^2 P}{\partial T \partial T}\right)_{P,V} = -\frac{R\frac{d}{dT}V(T)}{\left(-b+V(T)\right)^2} - \frac{\left(-\delta\frac{d}{dT}V(T) - 2V(T)\frac{d}{dT}V(T)\right)\frac{d}{dT}\operatorname{a}\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^2} - \frac{\frac{d^2}{dT^2}\operatorname{a}\alpha\left(T\right)}{\delta V(T) + \epsilon + V^2(T)}$$

#### property d2P\_dTdP\_g

Second derivative of pressure with respect to temperature and, then pressure; and with volume held constant at first, then temperature, for the gas phase, [1/K].

$$\left(\frac{\partial^2 P}{\partial T \partial P}\right)_{V,T} = -\frac{R\frac{d}{dP}V(P)}{\left(-b+V(P)\right)^2} - \frac{\left(-\delta\frac{d}{dP}V(P) - 2V(P)\frac{d}{dP}V(P)\right)\frac{d}{dT}\operatorname{a}\alpha\left(T\right)}{\left(\delta V(P) + \epsilon + V^2(P)\right)^2}$$

## property d2P\_dTdP\_1

Second derivative of pressure with respect to temperature and, then pressure; and with volume held constant at first, then temperature, for the liquid phase, [1/K].

$$\left(\frac{\partial^2 P}{\partial T \partial P}\right)_{V,T} = -\frac{R\frac{d}{dP}V(P)}{\left(-b+V(P)\right)^2} - \frac{\left(-\delta\frac{d}{dP}V(P) - 2V(P)\frac{d}{dP}V(P)\right)\frac{d}{dT}\operatorname{a}\alpha\left(T\right)}{\left(\delta V(P) + \epsilon + V^2(P)\right)^2}$$

# property d2P\_dTdrho\_g

Derivative of pressure with respect to molar density, and temperature for the gas phase, [Pa/(K\*mol/m^3)].

$$\frac{\partial^2 P}{\partial \rho \partial T} = -V^2 \frac{\partial^2 P}{\partial T \partial V}$$

# property d2P\_dTdrho\_l

Derivative of pressure with respect to molar density, and temperature for the liquid phase, [Pa/(K\*mol/m^3)].

$$\frac{\partial^2 P}{\partial \rho \partial T} = -V^2 \frac{\partial^2 P}{\partial T \partial V}$$

#### property d2P\_dVdP\_g

Second derivative of pressure with respect to molar volume and then pressure for the gas phase, [mol/m^3].

$$\frac{\partial^2 P}{\partial V \partial P} = \frac{2RT\frac{d}{dP}V(P)}{\left(-b+V(P)\right)^3} - \frac{\left(-\delta - 2V(P)\right)\left(-2\delta\frac{d}{dP}V(P) - 4V(P)\frac{d}{dP}V(P)\right)a\alpha\left(T\right)}{\left(\delta V(P) + \epsilon + V^2(P)\right)^3} + \frac{2a\alpha\left(T\right)\frac{d}{dP}V(P)}{\left(\delta V(P) + \epsilon + V^2(P)\right)^2}$$

#### property d2P\_dVdP\_1

Second derivative of pressure with respect to molar volume and then pressure for the liquid phase, [mol/m^3].

$$\frac{\partial^2 P}{\partial V \partial P} = \frac{2RT\frac{d}{dP}V(P)}{\left(-b+V(P)\right)^3} - \frac{\left(-\delta - 2V(P)\right)\left(-2\delta\frac{d}{dP}V(P) - 4V(P)\frac{d}{dP}V(P)\right)a\alpha\left(T\right)}{\left(\delta V(P) + \epsilon + V^2(P)\right)^3} + \frac{2a\alpha\left(T\right)\frac{d}{dP}V(P)}{\left(\delta V(P) + \epsilon + V^2(P)\right)^2}$$

# property d2P\_dVdT\_TP\_g

Second derivative of pressure with respect to molar volume and then temperature at constant temperature then pressure for the gas phase, [Pa\*mol/m^3/K].

$$\left(\frac{\partial^2 P}{\partial V \partial T}\right)_{T,P} = \frac{2RT\frac{d}{dT}V(T)}{\left(-b+V(T)\right)^3} - \frac{R}{\left(-b+V(T)\right)^2} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T)\right)\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + E^2(T)\right)^3} - \frac{\left$$

#### property d2P\_dVdT\_TP\_1

Second derivative of pressure with respect to molar volume and then temperature at constant temperature then pressure for the liquid phase, [Pa\*mol/m^3/K].

$$\left(\frac{\partial^2 P}{\partial V \partial T}\right)_{T,P} = \frac{2RT\frac{d}{dT}V(T)}{\left(-b+V(T)\right)^3} - \frac{R}{\left(-b+V(T)\right)^2} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T) - 4V(T)\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)\left(-2\delta\frac{d}{dT}V(T)\right)a\alpha\left(T\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + \epsilon + V^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + E^2(T)\right)^3} - \frac{\left(-\delta - 2V(T)\right)}{\left(\delta V(T) + E^2$$

property d2P\_dVdT\_g
Alias of GCEOS.d2P\_dTdV\_g

#### property d2P\_dVdT\_1

Alias of GCEOS.d2P\_dTdV\_1

# property d2P\_drho2\_g

Second derivative of pressure with respect to molar density for the gas phase, [Pa/(mol/m^3)^2].

$$\frac{\partial^2 P}{\partial \rho^2} = -V^2 \left( -V^2 \frac{\partial^2 P}{\partial V^2} - 2V \frac{\partial P}{\partial V} \right)$$

## property d2P\_drho2\_1

Second derivative of pressure with respect to molar density for the liquid phase, [Pa/(mol/m^3)^2].

$$\frac{\partial^2 P}{\partial \rho^2} = -V^2 \left( -V^2 \frac{\partial^2 P}{\partial V^2} - 2V \frac{\partial P}{\partial V} \right)$$

# property d2S\_dep\_dT2\_g

Second temperature derivative of departure entropy with respect to temperature for the gas phase, [(J/mol)/K^3].

$$\frac{\partial^2 S_{dep,g}}{\partial T^2} = -\frac{R\left(\frac{d}{dT}V(T) - \frac{V(T)}{T}\right)\frac{d}{dT}V(T)}{V^2(T)} + \frac{R\left(\frac{d^2}{dT^2}V(T) - \frac{2\frac{d}{dT}V(T)}{T} + \frac{2V(T)}{T^2}\right)}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V^2(T)} - \frac{2R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V^2(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)}$$

# property d2S\_dep\_dT2\_g\_V

Second temperature derivative of departure entropy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^3].

$$\left(\frac{\partial^2 S_{dep,g}}{\partial T^2}\right)_V = -\frac{R\left(\frac{\partial}{\partial T}P(V,T) - \frac{P(V,T)}{T}\right)\frac{\partial}{\partial T}P(V,T)}{P^2(V,T)} + \frac{R\left(\frac{\partial^2}{\partial T^2}P(V,T) - \frac{2\frac{\partial}{\partial T}P(V,T)}{T} + \frac{2P(V,T)}{T^2}\right)}{P(V,T)} + \frac{R\left(\frac{\partial}{\partial T}P(V,T) - \frac{2P(V,T)}{T}\right)}{P(V,T)} + \frac{2P(V,T)}{T}$$

# property d2S\_dep\_dT2\_1

Second temperature derivative of departure entropy with respect to temperature for the liquid phase, [(J/mol)/K^3].

$$\frac{\partial^2 S_{dep,l}}{\partial T^2} = -\frac{R\left(\frac{d}{dT}V(T) - \frac{V(T)}{T}\right)\frac{d}{dT}V(T)}{V^2(T)} + \frac{R\left(\frac{d^2}{dT^2}V(T) - \frac{2\frac{d}{dT}V(T)}{T} + \frac{2V(T)}{T^2}\right)}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} + \frac{R\left(\frac{d}{dT}V(T)\right)^2}{V^2(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} - \frac{R\frac{d^2}{dT^2}V(T)}{V(T)} - \frac{R\frac{d}{dT}V(T)}{V(T)} - \frac{R\frac{d^2}{dT}V(T)}{V(T)} - \frac{R\frac{d^2}{dT}V(T)}{V(T)} - \frac{R\frac{d}{dT}V(T)}{V(T)} - \frac{R\frac{d^2}{dT}V(T)}{V(T)} - \frac{R\frac{d^2}{dT}V(T)}{V(T)} - \frac{R\frac{d}{dT}V(T)}{V(T)} - \frac{R\frac{d}{dT}V(T)}{V$$

# property d2S\_dep\_dT2\_1\_V

Second temperature derivative of departure entropy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^3].

$$\left(\frac{\partial^2 S_{dep,l}}{\partial T^2}\right)_V = -\frac{R\left(\frac{\partial}{\partial T}P(V,T) - \frac{P(V,T)}{T}\right)\frac{\partial}{\partial T}P(V,T)}{P^2(V,T)} + \frac{R\left(\frac{\partial^2}{\partial T^2}P(V,T) - \frac{2\frac{\partial}{\partial T}P(V,T)}{T} + \frac{2P(V,T)}{T^2}\right)}{P(V,T)} + \frac{R\left(\frac{\partial}{\partial T}P(V,T) - \frac{2P(V,T)}{T}\right)}{P(V,T)} + \frac{2P(V,T)}{T}$$

#### property d2S\_dep\_dTdP\_g

Temperature and pressure derivative of departure entropy at constant pressure then temperature for the gas phase, [(J/mol)/K^2/Pa].

$$\left(\frac{\partial^2 S_{dep,g}}{\partial T \partial P}\right)_{T,P} = -\frac{R\frac{\partial^2}{\partial T \partial P}V(T,P)}{V(T,P)} + \frac{R\frac{\partial}{\partial P}V(T,P)\frac{\partial}{\partial T}V(T,P)}{V^2(T,P)} - \frac{R\frac{\partial^2}{\partial T \partial P}V(T,P)}{b - V(T,P)} - \frac{R\frac{\partial}{\partial P}V(T,P)\frac{\partial}{\partial T}V(T,P)}{(b - V(T,P))^2} + \frac{16}{2}\frac{1}{2}\frac$$

#### property d2S\_dep\_dTdP\_1

Temperature and pressure derivative of departure entropy at constant pressure then temperature for the liquid phase, [(J/mol)/K^2/Pa].

$$\left(\frac{\partial^2 S_{dep,l}}{\partial T \partial P}\right)_{T,P} = -\frac{R\frac{\partial^2}{\partial T \partial P}V(T,P)}{V(T,P)} + \frac{R\frac{\partial}{\partial P}V(T,P)\frac{\partial}{\partial T}V(T,P)}{V^2(T,P)} - \frac{R\frac{\partial^2}{\partial T \partial P}V(T,P)}{b - V(T,P)} - \frac{R\frac{\partial}{\partial P}V(T,P)\frac{\partial}{\partial T}V(T,P)}{(b - V(T,P))^2} + \frac{1}{2}\left(\frac{1}{2}\right)^2 \left(\frac{1}{2}\right)^2 \left($$

# property d2T\_dP2\_g

Second partial derivative of temperature with respect to pressure (constant volume) for the gas phase, [K/Pa^2].

$$\left(\frac{\partial^2 T}{\partial P^2}\right)_V = -\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

# property d2T\_dP2\_1

Second partial derivative of temperature with respect to pressure (constant temperature) for the liquid phase, [K/Pa^2].

$$\left(\frac{\partial^2 T}{\partial P^2}\right)_V = -\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

# property d2T\_dPdV\_g

Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the gas phase, [K\*mol/(Pa\*m^3)].

$$\left(\frac{\partial^2 T}{\partial P \partial V}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V\right] \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

## property d2T\_dPdV\_1

Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the liquid phase, [K\*mol/(Pa\*m^3)].

$$\left(\frac{\partial^2 T}{\partial P \partial V}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V\right] \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

#### property d2T\_dPdrho\_g

Derivative of temperature with respect to molar density, and pressure for the gas phase, [K/(Pa\*mol/m^3)].

$$\frac{\partial^2 T}{\partial \rho \partial P} = -V^2 \frac{\partial^2 T}{\partial P \partial V}$$

#### property d2T\_dPdrho\_1

Derivative of temperature with respect to molar density, and pressure for the liquid phase,  $[K/(Pa*mol/m^3)]$ .

$$\frac{\partial^2 T}{\partial \rho \partial P} = -V^2 \frac{\partial^2 T}{\partial P \partial V}$$

#### property d2T\_dV2\_g

Second partial derivative of temperature with respect to volume (constant pressure) for the gas phase, [K\*mol^2/m^6].

$$\left(\frac{\partial^2 T}{\partial V^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial V^2}\right)_T \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T \partial V}\right)\right] \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T \partial V}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right]$$

## property d2T\_dV2\_1

Second partial derivative of temperature with respect to volume (constant pressure) for the liquid phase, [K\*mol^2/m^6].

$$\left(\frac{\partial^2 T}{\partial V^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial V^2}\right)_T \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T \partial V}\right)\right] \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left(\frac{\partial^2 P}{\partial T \partial V}\right)_V^{-2} + \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left(\frac{\partial^2 P}{\partial T$$

## property d2T\_dVdP\_g

Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the gas phase, [K\*mol/(Pa\*m^3)].

$$\left(\frac{\partial^2 T}{\partial P \partial V}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V\right] \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

# property d2T\_dVdP\_1

Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the liquid phase, [K\*mol/(Pa\*m^3)].

$$\left(\frac{\partial^2 T}{\partial P \partial V}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V\right] \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

# property d2T\_drho2\_g

Second derivative of temperature with respect to molar density for the gas phase, [K/(mol/m^3)^2].

$$\frac{\partial^2 T}{\partial \rho^2} = -V^2 (-V^2 \frac{\partial^2 T}{\partial V^2} - 2V \frac{\partial T}{\partial V})$$

# property d2T\_drho2\_1

Second derivative of temperature with respect to molar density for the liquid phase,  $[K/(mol/m^3)^2]$ .

$$\frac{\partial^2 T}{\partial \rho^2} = -V^2 \left(-V^2 \frac{\partial^2 T}{\partial V^2} - 2V \frac{\partial T}{\partial V}\right)$$

# property d2V\_dP2\_g

Second partial derivative of volume with respect to pressure (constant temperature) for the gas phase,  $[m^3/(Pa^2*mol)]$ .

$$\left(\frac{\partial^2 V}{\partial P^2}\right)_T = -\left(\frac{\partial^2 P}{\partial V^2}\right)_T \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

# property d2V\_dP2\_1

Second partial derivative of volume with respect to pressure (constant temperature) for the liquid phase,  $[m^3/(Pa^2*mol)]$ .

$$\left(\frac{\partial^2 V}{\partial P^2}\right)_T = -\left(\frac{\partial^2 P}{\partial V^2}\right)_T \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

# property d2V\_dPdT\_g

Second partial derivative of volume with respect to pressure (constant temperature) and then presssure (constant temperature) for the gas phase,  $[m^3/(K^*Pa^*mol)]$ .

$$\left(\frac{\partial^2 V}{\partial T \partial P}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right] \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

## property d2V\_dPdT\_1

Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the liquid phase, [m^3/(K\*Pa\*mol)].

$$\left(\frac{\partial^2 V}{\partial T \partial P}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right] \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

## property d2V\_dT2\_g

Second partial derivative of volume with respect to temperature (constant pressure) for the gas phase,  $[m^3/(mol^*K^2)].$ 

$$\left(\frac{\partial^2 V}{\partial T^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial T \partial V}\right)\right] \left(\frac{\partial P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right] \left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T^{-2} - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right]$$

# property d2V\_dT2\_1

Second partial derivative of volume with respect to temperature (constant pressure) for the liquid phase, [m^3/(mol\*K^2)].

$$\left(\frac{\partial^2 V}{\partial T^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial T\partial V}\right)\right] \left(\frac{\partial P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T\partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right] \left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T\partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T^{-2} - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right]$$

## property d2V\_dTdP\_g

Second partial derivative of volume with respect to pressure (constant temperature) and then presssure (constant temperature) for the gas phase, [m^3/(K\*Pa\*mol)].

$$\left(\frac{\partial^2 V}{\partial T \partial P}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right] \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

# property d2V\_dTdP\_1

Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the liquid phase, [m^3/(K\*Pa\*mol)].

$$\left(\frac{\partial^2 V}{\partial T \partial P}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right] \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

#### property d2a\_alpha\_dTdP\_g\_V

Derivative of the temperature derivative of  $a_{alpha}$  with respect to pressure at constant volume (varying T) for the gas phase,  $[J^2/mol^2/Pa^2/K]$ .

$$\left(\frac{\partial \left(\frac{\partial a\alpha}{\partial T}\right)_P}{\partial P}\right)_V = \left(\frac{\partial^2 a\alpha}{\partial T^2}\right)_P \cdot \left(\frac{\partial T}{\partial P}\right)_V$$

,

#### property d2a\_alpha\_dTdP\_1\_V

Derivative of the temperature derivative of *a\_alpha* with respect to pressure at constant volume (varying T) for the liquid phase,  $[J^2/mol^2/Pa^2/K]$ .

$$\left(\frac{\partial \left(\frac{\partial a\alpha}{\partial T}\right)_P}{\partial P}\right)_V = \left(\frac{\partial^2 a\alpha}{\partial T^2}\right)_P \cdot \left(\frac{\partial T}{\partial P}\right)_V$$

# d2phi\_sat\_dT2(T, polish=True)

Method to calculate the second temperature derivative of saturation fugacity coefficient of the compound. This does require solving the EOS itself.

#### Parameters

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

# Returns

**d2phi\_sat\_dT2** [float] Second temperature derivative of fugacity coefficient along the liquid-vapor saturation line, [1/K^2]

#### Notes

This is presently a numerical calculation.

# property d2rho\_dP2\_g

Second derivative of molar density with respect to pressure for the gas phase, [(mol/m^3)/Pa^2].

$$\frac{\partial^2 \rho}{\partial P^2} = -\frac{\partial^2 V}{\partial P^2} \frac{1}{V^2} + 2\left(\frac{\partial V}{\partial P}\right)^2 \frac{1}{V^3}$$

# property d2rho\_dP2\_1

Second derivative of molar density with respect to pressure for the liquid phase, [(mol/m^3)/Pa^2].

$$\frac{\partial^2 \rho}{\partial P^2} = -\frac{\partial^2 V}{\partial P^2} \frac{1}{V^2} + 2\left(\frac{\partial V}{\partial P}\right)^2 \frac{1}{V^3}$$

# property d2rho\_dPdT\_g

Second derivative of molar density with respect to pressure and temperature for the gas phase, [(mol/m^3)/(K\*Pa)].

$$\frac{\partial^2 \rho}{\partial T \partial P} = -\frac{\partial^2 V}{\partial T \partial P} \frac{1}{V^2} + 2\left(\frac{\partial V}{\partial T}\right) \left(\frac{\partial V}{\partial P}\right) \frac{1}{V^3}$$

#### property d2rho\_dPdT\_1

Second derivative of molar density with respect to pressure and temperature for the liquid phase,  $[(mol/m^3)/(K^*Pa)]$ .

$$\frac{\partial^2 \rho}{\partial T \partial P} = -\frac{\partial^2 V}{\partial T \partial P} \frac{1}{V^2} + 2\left(\frac{\partial V}{\partial T}\right) \left(\frac{\partial V}{\partial P}\right) \frac{1}{V^3}$$

# property d2rho\_dT2\_g

Second derivative of molar density with respect to temperature for the gas phase, [(mol/m^3)/K^2].

$$\frac{\partial^2 \rho}{\partial T^2} = -\frac{\partial^2 V}{\partial T^2} \frac{1}{V^2} + 2\left(\frac{\partial V}{\partial T}\right)^2 \frac{1}{V^3}$$

# property d2rho\_dT2\_1

Second derivative of molar density with respect to temperature for the liquid phase, [(mol/m^3)/K^2].

$$\frac{\partial^2 \rho}{\partial T^2} = -\frac{\partial^2 V}{\partial T^2} \frac{1}{V^2} + 2 \left(\frac{\partial V}{\partial T}\right)^2 \frac{1}{V^3}$$

#### property d3a\_alpha\_dT3

Method to calculate the third temperature derivative of  $a\alpha$ , [J<sup>2</sup>/mol<sup>2</sup>/Pa/K<sup>3</sup>]. This parameter is needed for some higher derivatives that are needed in some flash calculations.

#### Returns

**d3a\_alpha\_dT3** [float] Third temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^3]

## property dH\_dep\_dP\_g

Derivative of departure enthalpy with respect to pressure for the gas phase, [(J/mol)/Pa].

$$\frac{\partial H_{dep,g}}{\partial P} = P \frac{d}{dP} V(P) + V(P) + \frac{4 \left(T \frac{d}{dT} a\alpha \left(T\right) - a\alpha \left(T\right)\right) \frac{d}{dP} V(P)}{\left(\delta^2 - 4\epsilon\right) \left(-\frac{\left(\delta + 2V(P)\right)^2}{\delta^2 - 4\epsilon} + 1\right)}$$

# property dH\_dep\_dP\_g\_V

Derivative of departure enthalpy with respect to pressure at constant volume for the liquid phase, [(J/mol)/Pa].

$$\left(\frac{\partial H_{dep,g}}{\partial P}\right)_{V} = -R\left(\frac{\partial T}{\partial P}\right)_{V} + V + \frac{2\left(T\left(\frac{\partial\left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V} + \left(\frac{\partial a\alpha}{\partial T}\right)_{P}\left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial a\alpha}{\partial P}\right)_{V}\right)\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)_{V} + \frac{2\left(T\left(\frac{\partial\left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V} + \left(\frac{\partial a\alpha}{\partial T}\right)_{P}\left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial a\alpha}{\partial P}\right)_{V}\right)\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)_{V} + \frac{2\left(T\left(\frac{\partial\left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V} + \left(\frac{\partial a\alpha}{\partial T}\right)_{P}\left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial a\alpha}{\partial P}\right)_{V}\right)\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)_{V} + \frac{2\left(T\left(\frac{\partial\left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V} + \left(\frac{\partial a\alpha}{\partial T}\right)_{P}\left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial a\alpha}{\partial P}\right)_{V}\right)\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)_{V} + \frac{2\left(T\left(\frac{\partial\left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V} + \left(\frac{\partial a\alpha}{\partial T}\right)_{P}\left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial a\alpha}{\partial P}\right)_{V}\right)\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)_{V} + \frac{2\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \left(\frac{\partial T}{\partial P}\right)_{V} + \left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2\left(T\left(\frac{\partial T}{\partial P}\right)_{P}\right)_{V} + \left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\right)_{V} + \frac{2}{2}\left(T\left(\frac{\partial T}{\partial P}\right)_{V} + \frac{2}{2}\left(T\left(\frac$$

## property dH\_dep\_dP\_1

Derivative of departure enthalpy with respect to pressure for the liquid phase, [(J/mol)/Pa].

$$\frac{\partial H_{dep,l}}{\partial P} = P \frac{d}{dP} V(P) + V(P) + \frac{4 \left(T \frac{d}{dT} a\alpha \left(T\right) - a\alpha \left(T\right)\right) \frac{d}{dP} V(P)}{\left(\delta^2 - 4\epsilon\right) \left(-\frac{\left(\delta + 2V(P)\right)^2}{\delta^2 - 4\epsilon} + 1\right)}$$

# property dH\_dep\_dP\_1\_V

Derivative of departure enthalpy with respect to pressure at constant volume for the gas phase, [(J/mol)/Pa].

$$\left(\frac{\partial H_{dep,g}}{\partial P}\right)_{V} = -R\left(\frac{\partial T}{\partial P}\right)_{V} + V + \frac{2\left(T\left(\frac{\partial\left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V} + \left(\frac{\partial a\alpha}{\partial T}\right)_{P}\left(\frac{\partial T}{\partial P}\right)_{V} - \left(\frac{\partial a\alpha}{\partial P}\right)_{V}\right)\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)}{\sqrt{\delta^{2}-4\epsilon}}$$

# property dH\_dep\_dT\_g

Derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K].

$$\frac{\partial H_{dep,g}}{\partial T} = P \frac{d}{dT} V(T) - R + \frac{2T}{\sqrt{\delta^2 - 4\epsilon}} \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^2}{dT^2} \operatorname{a\alpha}\left(T\right) + \frac{4\left(T \frac{d}{dT} \operatorname{a\alpha}\left(T\right) - \operatorname{a\alpha}\left(T\right)\right) \frac{d}{dT} V(T)}{\left(\delta^2 - 4\epsilon\right) \left(-\frac{\left(\delta + 2V(T)\right)^2}{\delta^2 - 4\epsilon} + 1\right)}$$

# property dH\_dep\_dT\_g\_V

Derivative of departure enthalpy with respect to temperature at constant volume for the gas phase, [(J/mol)/K].

$$\left(\frac{\partial H_{dep,g}}{\partial T}\right)_{V} = -R + \frac{2T \operatorname{atanh}\left(\frac{2V_{g}+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right) \frac{d^{2}}{dT^{2}} \mathbf{a}_{\alpha}\left(T\right)}{\sqrt{\delta^{2}-4\epsilon}} + V_{g} \frac{\partial}{\partial T} P(T,V)$$

# property dH\_dep\_dT\_l

Derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K].

$$\frac{\partial H_{dep,l}}{\partial T} = P \frac{d}{dT} V(T) - R + \frac{2T}{\sqrt{\delta^2 - 4\epsilon}} \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) \frac{d^2}{dT^2} \operatorname{a\alpha}\left(T\right) + \frac{4\left(T \frac{d}{dT} \operatorname{a\alpha}\left(T\right) - \operatorname{a\alpha}\left(T\right)\right) \frac{d}{dT} V(T)}{\left(\delta^2 - 4\epsilon\right) \left(-\frac{\left(\delta + 2V(T)\right)^2}{\delta^2 - 4\epsilon} + 1\right)}$$

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## property dH\_dep\_dT\_1\_V

Derivative of departure enthalpy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K].

$$\left(\frac{\partial H_{dep,l}}{\partial T}\right)_{V} = -R + \frac{2T \operatorname{atanh}\left(\frac{2V_{l}+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)\frac{d^{2}}{dT^{2}} \mathbf{a}_{\alpha}\left(T\right)}{\sqrt{\delta^{2}-4\epsilon}} + V_{l}\frac{\partial}{\partial T}P(T,V)$$

# dH\_dep\_dT\_sat\_g(T, polish=False)

Method to calculate and return the temperature derivative of saturation vapor excess enthalpy.

## Parameters

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

# Returns

**dH\_dep\_dT\_sat\_g** [float] Vapor phase temperature derivative of excess enthalpy along the liquid-vapor saturation line, [J/mol/K]

# dH\_dep\_dT\_sat\_1(T, polish=False)

Method to calculate and return the temperature derivative of saturation liquid excess enthalpy.

#### **Parameters**

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

# Returns

**dH\_dep\_dT\_sat\_l** [float] Liquid phase temperature derivative of excess enthalpy along the liquid-vapor saturation line, [J/mol/K]

# property dH\_dep\_dV\_g\_P

Derivative of departure enthalpy with respect to volume at constant pressure for the gas phase, [J/m^3].

$$\left(\frac{\partial H_{dep,g}}{\partial V}\right)_P = \left(\frac{\partial H_{dep,g}}{\partial T}\right)_P \cdot \left(\frac{\partial T}{\partial V}\right)_P$$

# property dH\_dep\_dV\_g\_T

Derivative of departure enthalpy with respect to volume at constant temperature for the gas phase, [J/m^3].

$$\left(\frac{\partial H_{dep,g}}{\partial V}\right)_T = \left(\frac{\partial H_{dep,g}}{\partial P}\right)_T \cdot \left(\frac{\partial P}{\partial V}\right)_T$$

## property dH\_dep\_dV\_1\_P

Derivative of departure enthalpy with respect to volume at constant pressure for the liquid phase, [J/m^3].

$$\left(\frac{\partial H_{dep,l}}{\partial V}\right)_{P} = \left(\frac{\partial H_{dep,l}}{\partial T}\right)_{P} \cdot \left(\frac{\partial T}{\partial V}\right)_{P}$$

# property dH\_dep\_dV\_l\_T

Derivative of departure enthalpy with respect to volume at constant temperature for the gas phase, [J/m^3].

$$\left(\frac{\partial H_{dep,l}}{\partial V}\right)_T = \left(\frac{\partial H_{dep,l}}{\partial P}\right)_T \cdot \left(\frac{\partial P}{\partial V}\right)_T$$

#### property dP\_drho\_g

Derivative of pressure with respect to molar density for the gas phase, [Pa/(mol/m^3)].

$$\frac{\partial P}{\partial \rho} = -V^2 \frac{\partial P}{\partial V}$$

#### property dP\_drho\_1

Derivative of pressure with respect to molar density for the liquid phase, [Pa/(mol/m^3)].

$$\frac{\partial P}{\partial \rho} = -V^2 \frac{\partial P}{\partial V}$$

## **dPsat\_dT**(*T*, *polish=False*, *also\_Psat=False*)

Generic method to calculate the temperature derivative of vapor pressure for a specified *T*. Implements the analytical derivative of the three polynomials described in *Psat*.

As with *Psat*, results above the critical temperature are meaningless. The first-order polynomial which is used to calculate it under 0.32 Tc may not be physicall meaningful, due to there normally not being a volume solution to the EOS which can produce that low of a pressure.

#### **Parameters**

- T [float] Temperature, [K]
- **polish** [bool, optional] Whether to attempt to use a numerical solver to make the solution more precise or not
- **also\_Psat** [bool, optional] Calculating *dPsat\_dT* necessarily involves calculating *Psat*; when this is set to True, a second return value is added, whic is the actual *Psat* value.

#### Returns

**dPsat\_dT** [float] Derivative of vapor pressure with respect to temperature, [Pa/K]

**Psat** [float, returned if *also\_Psat* is *True*] Vapor pressure, [Pa]

# Notes

There is a small step change at 0.32 Tc for all EOS due to the two switch between polynomials at that point.

Useful for calculating enthalpy of vaporization with the Clausius Clapeyron Equation. Derived with SymPy's diff and cse.

## property dS\_dep\_dP\_g

Derivative of departure entropy with respect to pressure for the gas phase, [(J/mol)/K/Pa].

$$\frac{\partial S_{dep,g}}{\partial P} = -\frac{R\frac{d}{dP}V(P)}{V(P)} + \frac{R\frac{d}{dP}V(P)}{-b+V(P)} + \frac{4\frac{d}{dP}V(P)\frac{d}{dT}a\alpha(T)}{\left(\delta^2 - 4\epsilon\right)\left(-\frac{\left(\delta + 2V(P)\right)^2}{\delta^2 - 4\epsilon} + 1\right)} + \frac{R^2T}{PV(P)}\left(\frac{P}{RT}\frac{d}{dP}V(P) + \frac{V(P)}{RT}\right)$$

# property dS\_dep\_dP\_g\_V

Derivative of departure entropy with respect to pressure at constant volume for the gas phase, [(J/mol)/K/Pa].

$$\left(\frac{\partial S_{dep,g}}{\partial P}\right)_{V} = \frac{2\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)\left(\frac{\partial \left(\frac{\partial aT}{\partial T}\right)_{P}}{\partial P}\right)_{V}}{\sqrt{\delta^{2}-4\epsilon}} + \frac{R^{2}\left(-\frac{PV\frac{d}{dP}T(P)}{RT^{2}(P)} + \frac{V}{RT(P)}\right)T(P)}{PV}$$

## property dS\_dep\_dP\_1

Derivative of departure entropy with respect to pressure for the liquid phase, [(J/mol)/K/Pa].

$$\frac{\partial S_{dep,l}}{\partial P} = -\frac{R\frac{d}{dP}V(P)}{V(P)} + \frac{R\frac{d}{dP}V(P)}{-b + V(P)} + \frac{4\frac{d}{dP}V(P)\frac{d}{dT}\alpha\alpha(T)}{\left(\delta^2 - 4\epsilon\right)\left(-\frac{(\delta + 2V(P))^2}{\delta^2 - 4\epsilon} + 1\right)} + \frac{R^2T}{PV(P)}\left(\frac{P}{RT}\frac{d}{dP}V(P) + \frac{V(P)}{RT}\right)$$

# property dS\_dep\_dP\_1\_V

Derivative of departure entropy with respect to pressure at constant volume for the liquid phase, [(J/mol)/K/Pa].

$$\left(\frac{\partial S_{dep,l}}{\partial P}\right)_{V} = \frac{2 \operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right) \left(\frac{\partial \left(\frac{\partial a\alpha}{\partial T}\right)_{P}}{\partial P}\right)_{V}}{\sqrt{\delta^{2}-4\epsilon}} + \frac{R^{2} \left(-\frac{PV \frac{d}{dP}T(P)}{RT^{2}(P)} + \frac{V}{RT(P)}\right) T(P)}{PV}$$

# property dS\_dep\_dT\_g

Derivative of departure entropy with respect to temperature for the gas phase, [(J/mol)/K^2].

$$\frac{\partial S_{dep,g}}{\partial T} = -\frac{R\frac{d}{dT}V(T)}{V(T)} + \frac{R\frac{d}{dT}V(T)}{-b + V(T)} + \frac{4\frac{d}{dT}V(T)\frac{d}{dT}a\alpha(T)}{\left(\delta^2 - 4\epsilon\right)\left(-\frac{(\delta + 2V(T))^2}{\delta^2 - 4\epsilon} + 1\right)} + \frac{2\frac{d^2}{dT^2}a\alpha(T)}{\sqrt{\delta^2 - 4\epsilon}} \operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) + \frac{R^2T}{PV(T)} + \frac{2R^2T}{\sqrt{\delta^2 - 4\epsilon}} + \frac{2R^2T}{\sqrt{\delta^2 -$$

# property dS\_dep\_dT\_g\_V

Derivative of departure entropy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^2].

$$\left(\frac{\partial S_{dep,g}}{\partial T}\right)_{V} = \frac{R^{2}T\left(\frac{V\frac{\partial}{\partial T}P(T,V)}{RT} - \frac{VP(T,V)}{RT^{2}}\right)}{VP(T,V)} + \frac{2\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2} - 4\epsilon}}\right)\frac{d^{2}}{dT^{2}}\operatorname{a}\alpha\left(T\right)}{\sqrt{\delta^{2} - 4\epsilon}}$$

## property dS\_dep\_dT\_1

Derivative of departure entropy with respect to temperature for the liquid phase, [(J/mol)/K^2].

$$\frac{\partial S_{dep,l}}{\partial T} = -\frac{R\frac{d}{dT}V(T)}{V(T)} + \frac{R\frac{d}{dT}V(T)}{-b + V(T)} + \frac{4\frac{d}{dT}V(T)\frac{d}{dT}\alpha\alpha(T)}{\left(\delta^2 - 4\epsilon\right)\left(-\frac{(\delta + 2V(T))^2}{\delta^2 - 4\epsilon} + 1\right)} + \frac{2\frac{d^2}{dT^2}\alpha\alpha(T)}{\sqrt{\delta^2 - 4\epsilon}}\operatorname{atanh}\left(\frac{\delta + 2V(T)}{\sqrt{\delta^2 - 4\epsilon}}\right) + \frac{R^2T}{PV(T)}$$

## property dS\_dep\_dT\_1\_V

Derivative of departure entropy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^2].

$$\left(\frac{\partial S_{dep,l}}{\partial T}\right)_{V} = \frac{R^{2}T\left(\frac{V\frac{\partial}{\partial T}P(T,V)}{RT} - \frac{VP(T,V)}{RT^{2}}\right)}{VP(T,V)} + \frac{2\operatorname{atanh}\left(\frac{2V+\delta}{\sqrt{\delta^{2}-4\epsilon}}\right)\frac{d^{2}}{dT^{2}}\operatorname{a}\alpha\left(T\right)}{\sqrt{\delta^{2}-4\epsilon}}$$

# dS\_dep\_dT\_sat\_g(T, polish=False)

Method to calculate and return the temperature derivative of saturation vapor excess entropy.

#### **Parameters**

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

#### Returns

**dS\_dep\_dT\_sat\_g** [float] Vapor phase temperature derivative of excess entropy along the liquid-vapor saturation line, [J/mol/K^2]

# dS\_dep\_dT\_sat\_1(T, polish=False)

Method to calculate and return the temperature derivative of saturation liquid excess entropy.

#### **Parameters**

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

## Returns

**dS\_dep\_dT\_sat\_l** [float] Liquid phase temperature derivative of excess entropy along the liquid-vapor saturation line, [J/mol/K^2]

# property dS\_dep\_dV\_g\_P

Derivative of departure entropy with respect to volume at constant pressure for the gas phase, [J/K/m^3].

$$\left(\frac{\partial S_{dep,g}}{\partial V}\right)_P = \left(\frac{\partial S_{dep,g}}{\partial T}\right)_P \cdot \left(\frac{\partial T}{\partial V}\right)_P$$

## property dS\_dep\_dV\_g\_T

Derivative of departure entropy with respect to volume at constant temperature for the gas phase, [J/K/m^3].

$$\left(\frac{\partial S_{dep,g}}{\partial V}\right)_T = \left(\frac{\partial S_{dep,g}}{\partial P}\right)_T \cdot \left(\frac{\partial P}{\partial V}\right)_T$$

## property dS\_dep\_dV\_1\_P

Derivative of departure entropy with respect to volume at constant pressure for the liquid phase, [J/K/m^3].

$$\left(\frac{\partial S_{dep,l}}{\partial V}\right)_P = \left(\frac{\partial S_{dep,l}}{\partial T}\right)_P \cdot \left(\frac{\partial T}{\partial V}\right)_P$$

# property dS\_dep\_dV\_1\_T

Derivative of departure entropy with respect to volume at constant temperature for the gas phase, [J/K/m^3].

$$\left(\frac{\partial S_{dep,l}}{\partial V}\right)_T = \left(\frac{\partial S_{dep,l}}{\partial P}\right)_T \cdot \left(\frac{\partial P}{\partial V}\right)_T$$

#### property dT\_drho\_g

Derivative of temperature with respect to molar density for the gas phase, [K/(mol/m^3)].

$$\frac{\partial T}{\partial \rho} = V^2 \frac{\partial T}{\partial V}$$

#### property dT\_drho\_l

Derivative of temperature with respect to molar density for the liquid phase, [K/(mol/m^3)].

$$\frac{\partial T}{\partial \rho} = V^2 \frac{\partial T}{\partial V}$$

## property dZ\_dP\_g

Derivative of compressibility factor with respect to pressure for the gas phase, [1/Pa].

$$\frac{\partial Z}{\partial P} = \frac{1}{RT} \left( V - \frac{\partial V}{\partial P} \right)$$

## property dZ\_dP\_1

Derivative of compressibility factor with respect to pressure for the liquid phase, [1/Pa].

$$\frac{\partial Z}{\partial P} = \frac{1}{RT} \left( V - \frac{\partial V}{\partial P} \right)$$

# property dZ\_dT\_g

Derivative of compressibility factor with respect to temperature for the gas phase, [1/K].

$$\frac{\partial Z}{\partial T} = \frac{P}{RT} \left( \frac{\partial V}{\partial T} - \frac{V}{T} \right)$$

# property dZ\_dT\_1

Derivative of compressibility factor with respect to temperature for the liquid phase, [1/K].

$$\frac{\partial Z}{\partial T} = \frac{P}{RT} \left( \frac{\partial V}{\partial T} - \frac{V}{T} \right)$$

# property da\_alpha\_dP\_g\_V

Derivative of the  $a_alpha$  with respect to pressure at constant volume (varying T) for the gas phase,  $[J^2/mol^2/Pa^2]$ .

$$\left(\frac{\partial a\alpha}{\partial P}\right)_V = \left(\frac{\partial a\alpha}{\partial T}\right)_P \cdot \left(\frac{\partial T}{\partial P}\right)_V$$

#### property da\_alpha\_dP\_l\_V

Derivative of the  $a_alpha$  with respect to pressure at constant volume (varying T) for the liquid phase,  $[J^2/mol^2/Pa^2]$ .

$$\left(\frac{\partial a\alpha}{\partial P}\right)_V = \left(\frac{\partial a\alpha}{\partial T}\right)_P \cdot \left(\frac{\partial T}{\partial P}\right)_V$$

# property dbeta\_dP\_g

Derivative of isobaric expansion coefficient with respect to pressure for the gas phase, [1/(Pa\*K)].

$$\frac{\partial \beta_g}{\partial P} = \frac{\frac{\partial^2}{\partial T \partial P} V(T, P)_g}{V(T, P)_g} - \frac{\frac{\partial}{\partial P} V(T, P)_g \frac{\partial}{\partial T} V(T, P)_g}{V^2(T, P)_g}$$

#### property dbeta\_dP\_1

Derivative of isobaric expansion coefficient with respect to pressure for the liquid phase, [1/(Pa\*K)].

. .

$$\frac{\partial \beta_g}{\partial P} = \frac{\frac{\partial^2}{\partial T \partial P} V(T, P)_l}{V(T, P)_l} - \frac{\frac{\partial}{\partial P} V(T, P)_l \frac{\partial}{\partial T} V(T, P)_l}{V^2(T, P)_l}$$

# property dbeta\_dT\_g

Derivative of isobaric expansion coefficient with respect to temperature for the gas phase, [1/K^2].

$$\frac{\partial \beta_g}{\partial T} = \frac{\frac{\partial^2}{\partial T^2} V(T, P)_g}{V(T, P)_g} - \frac{\left(\frac{\partial}{\partial T} V(T, P)_g\right)^2}{V^2(T, P)_g}$$

# property dbeta\_dT\_1

Derivative of isobaric expansion coefficient with respect to temperature for the liquid phase, [1/K^2].

$$\frac{\partial \beta_l}{\partial T} = \frac{\frac{\partial^2}{\partial T^2} V(T, P)_l}{V(T, P)_l} - \frac{\left(\frac{\partial}{\partial T} V(T, P)_l\right)^2}{V^2(T, P)_l}$$

# property dfugacity\_dP\_g

Derivative of fugacity with respect to pressure for the gas phase, [-].

$$\frac{\partial (\text{fugacity})_g}{\partial P} = \frac{P}{RT} \left( -T \frac{\partial}{\partial P} \operatorname{S}_{\text{dep}} \left( T, P \right) + \frac{\partial}{\partial P} \operatorname{H}_{\text{dep}} \left( T, P \right) \right) e^{\frac{1}{RT} \left( -T \operatorname{S}_{\text{dep}} \left( T, P \right) + \operatorname{H}_{\text{dep}} \left( T, P \right) \right)} + e^{\frac{1}{RT} \left( -T \operatorname{S}_{\text{dep}} \left( T, P \right) + \operatorname{H}_{\text{dep}} \left( T, P \right) \right)}$$

# property dfugacity\_dP\_1

Derivative of fugacity with respect to pressure for the liquid phase, [-].

$$\frac{\partial (\text{fugacity})_l}{\partial P} = \frac{P}{RT} \left( -T \frac{\partial}{\partial P} \operatorname{S}_{\text{dep}}\left(T, P\right) + \frac{\partial}{\partial P} \operatorname{H}_{\text{dep}}\left(T, P\right) \right) e^{\frac{1}{RT}\left(-T \operatorname{S}_{\text{dep}}\left(T, P\right) + \operatorname{H}_{\text{dep}}\left(T, P\right)\right)} + e^{\frac{1}{RT}\left(-T \operatorname{S}_{\text{dep}}\left(T, P\right) + \operatorname{H}_{\text{dep}}\left(T, P\right)\right)}$$

# property dfugacity\_dT\_g

Derivative of fugacity with respect to temperature for the gas phase, [Pa/K].

$$\frac{\partial (\text{fugacity})_g}{\partial T} = P\left(\frac{1}{RT}\left(-T\frac{\partial}{\partial T}S_{\text{dep}}\left(T,P\right) - S_{\text{dep}}\left(T,P\right) + \frac{\partial}{\partial T}H_{\text{dep}}\left(T,P\right)\right) - \frac{1}{RT^2}\left(-TS_{\text{dep}}\left(T,P\right) + H_{\text{dep}}\left(T,P\right) + H_{\text{dep}}\left(T,P\right) + H_{\text{dep}}\left(T,P\right)\right)\right)$$

# property dfugacity\_dT\_l

Derivative of fugacity with respect to temperature for the liquid phase, [Pa/K].

$$\frac{\partial (\text{fugacity})_{l}}{\partial T} = P\left(\frac{1}{RT}\left(-T\frac{\partial}{\partial T}\operatorname{S}_{\text{dep}}\left(T,P\right) - \operatorname{S}_{\text{dep}}\left(T,P\right) + \frac{\partial}{\partial T}\operatorname{H}_{\text{dep}}\left(T,P\right)\right) - \frac{1}{RT^{2}}\left(-T\operatorname{S}_{\text{dep}}\left(T,P\right) + \operatorname{H}_{\text{dep}}\left(T,P\right)\right)\right)$$

#### discriminant(T=None, P=None)

Method to compute the discriminant of the cubic volume solution with the current EOS parameters, optionally at the same (assumed) T, and P or at different ones, if values are specified.

## **Parameters**

- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]

# Returns

discriminant [float] Discriminant, [-]

# Notes

This call is quite quick; only  $a\alpha$  is needed and if T is the same as the current object than it has already been computed.

The formula is as follows:

$$\text{discriminant} = -\left(-\frac{27P^{2}\epsilon\left(\frac{Pb}{RT}+1\right)}{R^{2}T^{2}} - \frac{27P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{3}T^{3}}\right)\left(-\frac{P^{2}\epsilon\left(\frac{Pb}{RT}+1\right)}{R^{2}T^{2}} - \frac{P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{3}T^{3}}\right) + \left(-\frac{P^{2}\epsilon\left(\frac{Pb}{RT}+1\right)}{R^{2}T^{2}} - \frac{P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{2}T^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}b\,\mathrm{a}\alpha\left(T\right)}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}c}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}c}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}} - \frac{P^{2}c}{R^{2}}\right) + \left(-\frac{P^{2}c}{R^{2}}$$

The formula is derived as follows:

```
>>> from sympy import *
>>> P, T, R, b = symbols('P, T, R, b')
>>> a_alpha = symbols(r'a\ \alpha', cls=Function)
>>> delta, epsilon = symbols('delta, epsilon')
>>> eta = b
>>> B = b*P/(R*T)
>>> deltas = delta*P/(R*T)
>>> thetas = a_alpha(T)*P/(R*T)**2
>>> epsilons = epsilon*(P/(R*T))**2
>>> etas = eta*P/(R*T)
>>> a = 1
>>> b = (deltas - B - 1)
>>> c = (thetas + epsilons - deltas*(B+1))
>>> d = -(epsilons*(B+1) + thetas*etas)
>>> disc = b*b*c*c - 4*a*c*c*c - 4*b*b*b*d - 27*a*a*d*d + 18*a*b*c*d
```

## **Examples**

>>> base = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=500.0, P=1E6)
>>> base.discriminant()
-0.001026390999
>>> base.discriminant(T=400)
0.0010458828
>>> base.discriminant(T=400, P=1e9)
12584660355.4

# property dphi\_dP\_g

Derivative of fugacity coefficient with respect to pressure for the gas phase, [1/Pa].

$$\frac{\partial \phi}{\partial P} = \frac{\left(-T\frac{\partial}{\partial P} \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \frac{\partial}{\partial P} \operatorname{H}_{\operatorname{dep}}\left(T,P\right)\right) e^{\frac{-T \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT}}}{RT}$$

# property dphi\_dP\_l

Derivative of fugacity coefficient with respect to pressure for the liquid phase, [1/Pa].

$$\frac{\partial \phi}{\partial P} = \frac{\left(-T\frac{\partial}{\partial P} \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \frac{\partial}{\partial P} \operatorname{H}_{\operatorname{dep}}\left(T,P\right)\right) e^{\frac{-T \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT}}}{RT}$$

## property dphi\_dT\_g

Derivative of fugacity coefficient with respect to temperature for the gas phase, [1/K].

$$\frac{\partial \phi}{\partial T} = \left(\frac{-T\frac{\partial}{\partial T} \operatorname{S}_{\operatorname{dep}}\left(T,P\right) - \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \frac{\partial}{\partial T} \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT} - \frac{-T \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT^{2}}\right) e^{\frac{-T \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT}}\right)$$

## property dphi\_dT\_1

Derivative of fugacity coefficient with respect to temperature for the liquid phase, [1/K].

$$\frac{\partial \phi}{\partial T} = \left(\frac{-T\frac{\partial}{\partial T} \operatorname{S}_{\operatorname{dep}}\left(T,P\right) - \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \frac{\partial}{\partial T} \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT} - \frac{-T \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT^{2}}\right) e^{\frac{-T \operatorname{S}_{\operatorname{dep}}\left(T,P\right) + \operatorname{H}_{\operatorname{dep}}\left(T,P\right)}{RT}}\right)$$

# dphi\_sat\_dT(T, polish=True)

Method to calculate the temperature derivative of saturation fugacity coefficient of the compound. This does require solving the EOS itself.

# Parameters

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

## Returns

**dphi\_sat\_dT** [float] First temperature derivative of fugacity coefficient along the liquid-vapor saturation line, [1/K]

# property drho\_dP\_g

Derivative of molar density with respect to pressure for the gas phase, [(mol/m^3)/Pa].

$$\frac{\partial \rho}{\partial P} = \frac{-1}{V^2} \frac{\partial V}{\partial P}$$

# property drho\_dP\_1

Derivative of molar density with respect to pressure for the liquid phase, [(mol/m^3)/Pa].

$$\frac{\partial \rho}{\partial P} = \frac{-1}{V^2} \frac{\partial V}{\partial P}$$

# property drho\_dT\_g

Derivative of molar density with respect to temperature for the gas phase, [(mol/m^3)/K].

$$\frac{\partial \rho}{\partial T} = -\frac{1}{V^2} \frac{\partial V}{\partial T}$$

# property drho\_dT\_1

Derivative of molar density with respect to temperature for the liquid phase, [(mol/m^3)/K].

$$\frac{\partial \rho}{\partial T} = -\frac{1}{V^2} \frac{\partial V}{\partial T}$$

# classmethod from\_json(json\_repr)

Method to create a eos from a JSON serialization of another eos.

#### **Parameters**

json\_repr [dict] JSON-friendly representation, [-]

#### Returns

eos [GCEOS] Newly created object from the json serialization, [-]

# Notes

It is important that the input string be in the same format as that created by GCEOS.as\_json.

## **Examples**

## property fugacity\_g

Fugacity for the gas phase, [Pa].

fugacity = 
$$P \exp\left(\frac{G_{dep}}{RT}\right)$$

# property fugacity\_l

Fugacity for the liquid phase, [Pa].

fugacity = 
$$P \exp\left(\frac{G_{dep}}{RT}\right)$$

## property kappa\_g

Isothermal (constant-temperature) expansion coefficient for the gas phase, [1/Pa].

$$\kappa = \frac{-1}{V} \frac{\partial V}{\partial P}$$

## property kappa\_1

Isothermal (constant-temperature) expansion coefficient for the liquid phase, [1/Pa].

$$\kappa = \frac{-1}{V} \frac{\partial V}{\partial P}$$

# kwargs = {}

Dictionary which holds input parameters to an EOS which are non-standard; this excludes *T*, *P*, *V*, *omega*, *Tc*, *Pc*, *Vc* but includes EOS specific parameters like *S1* and *alpha\_coeffs*.

# kwargs\_keys = () property lnphi\_g

The natural logarithm of the fugacity coefficient for the gas phase, [-].

#### property lnphi\_l

The natural logarithm of the fugacity coefficient for the liquid phase, [-].

#### model\_hash()

Basic method to calculate a hash of the non-state parts of the model This is useful for comparing to models to determine if they are the same, i.e. in a VLL flash it is important to know if both liquids have the same model.

Note that the hashes should only be compared on the same system running in the same process!

Returns

model\_hash [int] Hash of the object's model parameters, [-]

## property more\_stable\_phase

Checks the Gibbs energy of each possible phase, and returns 'l' if the liquid-like phase is more stable, and 'g' if the vapor-like phase is more stable.

# **Examples**

```
>>> PR(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6).more_stable_phase
'1'
```

# property mpmath\_volume\_ratios

Method to compare, as ratios, the volumes of the implemented cubic solver versus those calculated using *mpmath*.

#### Returns

ratios [list[mpc]] Either 1 or 3 volume ratios as calculated by mpmath, [-]

## **Examples**

```
>>> eos = PRTranslatedTwu(T=300, P=1e5, Tc=512.5, Pc=8084000.0, omega=0.559,_

alpha_coeffs=(0.694911, 0.9199, 1.7), c=-1e-6)

>>> eos.mpmath_volume_ratios
(mpc(real='0.999999999999999995', imag='0.0'), mpc(real='0.9999999999999999999995',_

imag='0.0'), mpc(real='1.000000000000000005', imag='0.0'))
```

## property mpmath\_volumes

Method to calculate to a high precision the exact roots to the cubic equation, using mpmath.

## Returns

Vs [tuple[mpf]] 3 Real or not real volumes as calculated by *mpmath*, [m^3/mol]

## **Examples**

# property mpmath\_volumes\_float

Method to calculate real roots of a cubic equation, using *mpmath*, but returned as floats.

## Returns

Vs [list[float]] All volumes calculated by *mpmath*, [m^3/mol]

# **Examples**

```
>>> eos = PRTranslatedTwu(T=300, P=1e5, Tc=512.5, Pc=8084000.0, omega=0.559,

alpha_coeffs=(0.694911, 0.9199, 1.7), c=-1e-6)

>>> eos.mpmath_volumes_float
((4.892617053202614e-05+0j), (0.0005415081544513214+0j), (0.

a024314946394269742+0j))
```

#### multicomponent = False

Whether or not the EOS is multicomponent or not

nonstate\_constants = ('Tc', 'Pc', 'omega', 'kwargs', 'a', 'b', 'delta', 'epsilon')

#### property phi\_g

Fugacity coefficient for the gas phase, [Pa].

$$\phi = \frac{\text{fugacity}}{P}$$

## property phi\_l

Fugacity coefficient for the liquid phase, [Pa].

$$\phi = \frac{\text{fugacity}}{P}$$

# phi\_sat(T, polish=True)

Method to calculate the saturation fugacity coefficient of the compound. This does not require solving the EOS itself.

#### **Parameters**

T [float] Temperature, [K]

**polish** [bool, optional] Whether to perform a rigorous calculation or to use a polynomial fit, [-]

## Returns

phi\_sat [float] Fugacity coefficient along the liquid-vapor saturation line, [-]

## **Notes**

Accuracy is generally around 1e-7. If Tr is under 0.32, the rigorous method is always used, but a solution may not exist if both phases cannot coexist. If Tr is above 1, likewise a solution does not exist.

# resolve\_full\_alphas()

Generic method to resolve the eos with fully calculated alpha derviatives. Re-calculates properties with the new alpha derivatives for any previously solved roots.

# property rho\_g

Gas molar density, [mol/m^3].

$$\rho_g = \frac{1}{V_g}$$

# property rho\_l

Liquid molar density, [mol/m^3].

$$\rho_l = \frac{1}{V_l}$$

**saturation\_prop\_plot**(*prop*, *Tmin=None*, *Tmax=None*, *pts=100*, *plot=False*, *show=False*, *both=False*) Method to create a plot of a specified property of the EOS along the (pure component) saturation line.

#### **Parameters**

prop [str] Property to be used; such as 'H\_dep\_l' ( when both is False) or 'H\_dep' (when both is True), [-]

**Tmin** [float] Minimum temperature of calculation; if this is too low the saturation routines will stop converging, [K]

- **Tmax** [float] Maximum temperature of calculation; cannot be above the critical temperature, [K]
- pts [int, optional] The number of temperature points to include [-]
- **plot** [bool] If False, the calculated values and temperatures are returned without plotting the data, [-]
- **show** [bool] Whether or not the plot should be rendered and shown; a handle to it is returned if *plot* is True for other purposes such as saving the plot to a file, [-]
- **both** [bool] When true, append '\_l' and '\_g' and draw both the liquid and vapor property specified and return two different sets of values.

#### Returns

Ts [list[float]] Logarithmically spaced temperatures in specified range, [K]

**props** [list[float]] The property specified if *both* is False; otherwise, the liquid properties, [various]

props\_g [list[float]] The gas properties, only returned if *both* is True, [various]

fig [matplotlib.figure.Figure] Plotted figure, only returned if *plot* is True, [-]

# scalar = True

## set\_from\_PT(Vs, only\_l=False, only\_g=False)

Counts the number of real volumes in Vs, and determines what to do. If there is only one real volume, the method *set\_properties\_from\_solution* is called with it. If there are two real volumes, *set\_properties\_from\_solution* is called once with each volume. The phase is returned by *set\_properties\_from\_solution*, and the volumes is set to either  $V_l$  or  $V_g$  as appropriate.

# Parameters

Vs [list[float]] Three possible molar volumes, [m^3/mol]

- **only\_l** [bool] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set.
- **only\_g** [bool] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set.

# **Notes**

An optimization attempt was made to remove min() and max() from this function; that is indeed possible, but the check for handling if there are two or three roots makes it not worth it.

Sets all interesting properties which can be calculated from an EOS alone. Determines which phase the fluid is on its own; for details, see *phase identification parameter*.

The list of properties set is as follows, with all properties suffixed with '\_l' or '\_g'.

dP\_dT, dP\_dV, dV\_dT, dV\_dP, dT\_dV, dT\_dP, d2P\_dT2, d2P\_dV2, d2V\_dT2, d2V\_dP2, d2T\_dV2, d2T\_dP2, d2V\_dPdT, d2P\_dTdV, d2T\_dPdV, H\_dep, S\_dep, G\_dep and PIP.

#### Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]

- V [float] Molar volume, [m<sup>3</sup>/mol]
- **b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]
- **quick** [bool, optional] Whether to use a SymPy cse-derived expression (3x faster) or individual formulas

## Returns

phase [str] Either 'l' or 'g'

# Notes

The individual formulas for the derivatives and excess properties are as follows. For definitions of *beta*, see *isobaric\_expansion*; for *kappa*, see isothermal\_compressibility; for *Cp\_minus\_Cv*, see *Cp\_minus\_Cv*; for *phase\_identification\_parameter*, see *phase\_identification\_parameter*.

First derivatives; in part using the Triple Product Rule [2], [3]:

$$\begin{split} \left(\frac{\partial P}{\partial T}\right)_{V} &= \frac{R}{V-b} - \frac{a\frac{d\alpha(T)}{dT}}{V^{2}+V\delta+\epsilon} \\ \left(\frac{\partial P}{\partial V}\right)_{T} &= -\frac{RT}{(V-b)^{2}} - \frac{a\left(-2V-\delta\right)\alpha(T)}{(V^{2}+V\delta+\epsilon)^{2}} \\ &\left(\frac{\partial V}{\partial T}\right)_{P} = -\frac{\left(\frac{\partial P}{\partial T}\right)_{V}}{\left(\frac{\partial P}{\partial V}\right)_{T}} \\ &\left(\frac{\partial V}{\partial P}\right)_{T} = -\frac{\left(\frac{\partial V}{\partial T}\right)_{P}}{\left(\frac{\partial P}{\partial T}\right)_{V}} \\ &\left(\frac{\partial T}{\partial V}\right)_{P} = \frac{1}{\left(\frac{\partial V}{\partial T}\right)_{P}} \\ &\left(\frac{\partial T}{\partial P}\right)_{V} = \frac{1}{\left(\frac{\partial P}{\partial T}\right)_{V}} \end{split}$$

Second derivatives with respect to one variable; those of T and V use identities shown in [1] and verified numerically:

$$\begin{pmatrix} \frac{\partial^2 P}{\partial T^2} \end{pmatrix}_V = -\frac{a \frac{d^2 \alpha(T)}{dT^2}}{V^2 + V\delta + \epsilon} \\ \left( \frac{\partial^2 P}{\partial V^2} \right)_T = 2 \left( \frac{RT}{\left(V - b\right)^3} - \frac{a \left(2V + \delta\right)^2 \alpha(T)}{\left(V^2 + V\delta + \epsilon\right)^3} + \frac{a \alpha(T)}{\left(V^2 + V\delta + \epsilon\right)^2} \right)$$

Second derivatives with respect to the other two variables; those of T and V use identities shown in [1] and verified numerically:

$$\left(\frac{\partial^2 P}{\partial T \partial V}\right) = -\frac{R}{\left(V-b\right)^2} + \frac{a\left(2V+\delta\right)\frac{d\alpha(T)}{dT}}{\left(V^2+V\delta+\epsilon\right)^2}$$

Excess properties

$$\begin{aligned} H_{dep} &= \int_{\infty}^{V} \left[ T \frac{\partial P}{\partial T_{V}} - P \right] dV + PV - RT = PV - RT + \frac{2}{\sqrt{\delta^{2} - 4\epsilon}} \left( Ta \frac{d\alpha(T)}{dT} - a\alpha(T) \right) \operatorname{atanh} \left( \frac{2V + \delta}{\sqrt{\delta^{2} - 4\epsilon}} \right) \\ S_{dep} &= \int_{\infty}^{V} \left[ \frac{\partial P}{\partial T} - \frac{R}{V} \right] dV + R \ln \frac{PV}{RT} = -R \ln(V) + R \ln \left( \frac{PV}{RT} \right) + R \ln(V - b) + \frac{2a \frac{d\alpha(T)}{dT}}{\sqrt{\delta^{2} - 4\epsilon}} \operatorname{atanh} \left( \frac{2V + \delta}{\sqrt{\delta^{2} - 4\epsilon}} \right) \\ G_{dep} &= H_{dep} - TS_{dep} \end{aligned}$$
$$C_{v,dep} &= T \int_{\infty}^{V} \left( \frac{\partial^{2} P}{\partial T^{2}} \right) dV = -Ta \left( \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} \ln \left( V - \frac{\delta^{2}}{2} \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} + \frac{\delta}{2} + 2\epsilon \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} \right) - \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} \ln \left( V + \frac{\delta^{2}}{2} \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} + \frac{\delta}{2} + 2\epsilon \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} \right) + \frac{\delta^{2}}{\delta^{2} - 4\epsilon} \ln \left( V + \frac{\delta^{2}}{2} \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} + \frac{\delta}{2} + 2\epsilon \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} \right) + \frac{\delta^{2}}{\delta^{2} - 4\epsilon} \ln \left( V + \frac{\delta^{2}}{2} \sqrt{\frac{1}{\delta^{2} - 4\epsilon}} + \frac{\delta^{2}}{\delta^{2} - 4\epsilon} + \frac{$$

$$C_{p,dep} = (C_p - C_v)_{\text{from EOS}} + C_{v,dep} - R$$

## References

#### [1], [2], [3]

**solve**(*pure\_a\_alphas=True, only\_l=False, only\_g=False, full\_alphas=True*)

First EOS-generic method; should be called by all specific EOSs. For solving for *T*, the EOS must provide the method *solve\_T*. For all cases, the EOS must provide *a\_alpha\_and\_derivatives*. Calls *set\_from\_PT* once done.

#### solve\_T(P, V, solution=None)

Generic method to calculate T from a specified P and V. Provides SciPy's *newton* solver, and iterates to solve the general equation for P, recalculating  $a\_alpha$  as a function of temperature using  $a\_alpha\_and\_derivatives$  each iteration.

## Parameters

**P** [float] Pressure, [Pa]

V [float] Molar volume, [m^3/mol]

**solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

# Returns

T [float] Temperature, [K]

# solve\_missing\_volumes()

Generic method to ensure both volumes, if solutions are physical, have calculated properties. This effectively un-does the optimization of the  $only_l$  and  $only_g$  keywords.

# property sorted\_volumes

List of lexicographically-sorted molar volumes available from the root finding algorithm used to solve the PT point. The convention of sorting lexicographically comes from numpy's handling of complex numbers, which python does not define. This method was added to facilitate testing, as the volume solution method changes over time and the ordering does as well.

## **Examples**

```
>>> PR(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6).sorted_volumes
((0.000130222125139+0j), (0.00112363131346-0.00129269672343j), (0.
→00112363131346+0.00129269672343j))
```

# state\_hash()

Basic method to calculate a hash of the state of the model and its model parameters.

Note that the hashes should only be compared on the same system running in the same process!

## Returns

state\_hash [int] Hash of the object's model parameters and state, [-]

# property state\_specs

Convenience method to return the two specified state specs (T, P, or V) as a dictionary.

#### **Examples**

```
>>> PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=500.0, V=1.0).state_specs
{'T': 500.0, 'V': 1.0}
```

# to(T=None, P=None, V=None)

Method to construct a new EOS object at two of T, P or V. In the event the specs match those of the current object, it will be returned unchanged.

#### **Parameters**

- T [float or None, optional] Temperature, [K]
- P [float or None, optional] Pressure, [Pa]
- V [float or None, optional] Molar volume, [m^3/mol]

# Returns

obj [EOS] Pure component EOS at the two specified specs, [-]

#### Notes

Constructs the object with parameters Tc, Pc, omega, and kwargs.

# **Examples**

```
>>> base = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=500.0, P=1E6)
>>> base.to(T=300.0, P=1e9).state_specs
{'T': 300.0, 'P': 1000000000.0}
>>> base.to(T=300.0, V=1.0).state_specs
{'T': 300.0, 'V': 1.0}
>>> base.to(P=1e5, V=1.0).state_specs
{'P': 1000000.0, 'V': 1.0}
```

# $to_PV(P, V)$

Method to construct a new EOS object at the spcified P and V. In the event the P and V match the current object's P and V, it will be returned unchanged.

# Parameters

**P** [float] Pressure, [Pa]

V [float] Molar volume, [m^3/mol]

# Returns

**obj** [EOS] Pure component EOS at specified *P* and *V*, [-]

# Notes

Constructs the object with parameters Tc, Pc, omega, and kwargs.

# **Examples**

```
>>> base = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=500.0, P=1E6)
>>> new = base.to_PV(P=1000.0, V=1.0)
>>> base.state_specs, new.state_specs
({'T': 500.0, 'P': 1000000.0}, {'P': 1000.0, 'V': 1.0})
```

# $to_TP(T, P)$

Method to construct a new EOS object at the specified T and P. In the event the T and P match the current object's T and P, it will be returned unchanged.

# Parameters

T [float] Temperature, [K]

P [float] Pressure, [Pa]

# Returns

obj [EOS] Pure component EOS at specified T and P, [-]

# Notes

Constructs the object with parameters Tc, Pc, omega, and kwargs.

# **Examples**

```
>>> base = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=500.0, P=1E6)
>>> new = base.to_TP(T=1.0, P=2.0)
>>> base.state_specs, new.state_specs
({'T': 500.0, 'P': 1000000.0}, {'T': 1.0, 'P': 2.0})
```

# $\texttt{to\_TV}(T, V)$

Method to construct a new EOS object at the specified T and V. In the event the T and V match the current object's T and V, it will be returned unchanged.

# **Parameters**

- **T** [float] Temperature, [K]
- V [float] Molar volume, [m^3/mol]

# Returns

**obj** [EOS] Pure component EOS at specified *T* and *V*, [-]

# Notes

Constructs the object with parameters Tc, Pc, omega, and kwargs.

## **Examples**

```
>>> base = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=500.0, P=1E6)
>>> new = base.to_TV(T=1000000.0, V=1.0)
>>> base.state_specs, new.state_specs
({'T': 500.0, 'P': 1000000.0}, {'T': 1000000.0, 'V': 1.0})
```

#### volume\_error()

Method to calculate the relative absolute error in the calculated molar volumes. This is computed with *mpmath*. If the number of real roots is different between mpmath and the implemented solver, an error of 1 is returned.

#### **Parameters**

T [float] Temperature, [K]

# Returns

error [float] relative absolute error in molar volumes, [-]

## **Examples**

```
>>> eos = PRTranslatedTwu(T=300, P=1e5, Tc=512.5, Pc=8084000.0, omega=0.559, 
→alpha_coeffs=(0.694911, 0.9199, 1.7), c=-1e-6)
>>> eos.volume_error()
5.2192e-17
```

volume\_errors(Tmin=0.0001, Tmax=10000.0, Pmin=0.01, Pmax=1000000000.0, pts=50, plot=False,

*show=False, trunc\_err\_low=1e-18, trunc\_err\_high=1.0, color\_map=None, timing=False)* Method to create a plot of the relative absolute error in the cubic volume solution as compared to a higherprecision calculation. This method is incredible valuable for the development of more reliable floating-point based cubic solutions.

#### Parameters

Tmin [float] Minimum temperature of calculation, [K]

Tmax [float] Maximum temperature of calculation, [K]

Pmin [float] Minimum pressure of calculation, [Pa]

Pmax [float] Maximum pressure of calculation, [Pa]

**pts** [int, optional] The number of points to include in both the *x* and *y* axis; the validation calculation is slow, so increasing this too much is not advisable, [-]

plot [bool] If False, the calculated errors are returned without plotting the data, [-]

**show** [bool] Whether or not the plot should be rendered and shown; a handle to it is returned if *plot* is True for other purposes such as saving the plot to a file, [-]

trunc\_err\_low [float] Minimum plotted error; values under this are rounded to 0, [-]

- trunc\_err\_high [float] Maximum plotted error; values above this are rounded to 1, [-]
- color\_map [matplotlib.cm.ListedColormap] Matplotlib colormap object, [-]
- **timing** [bool] If True, plots the time taken by the volume root calculations themselves; this can reveal whether the solvers are taking fast or slow paths quickly, [-]

# Returns

**errors** [list[list[float]]] Relative absolute errors in the volume calculation (or timings in seconds if *timing* is True), [-]

fig [matplotlib.figure.Figure] Plotted figure, only returned if *plot* is True, [-]

# static volume\_solutions(T, P, b, delta, epsilon, a\_alpha)

Halley's method based solver for cubic EOS volumes based on the idea of initializing from a single liquidlike guess which is solved precisely, deflating the cubic analytically, solving the quadratic equation for the next two volumes, and then performing two halley steps on each of them to obtain the final solutions. This method does not calculate imaginary roots - they are set to zero on detection. This method has been rigorously tested over a wide range of conditions.

The method uses the standard combination of bisection to provide high and low boundaries as well, to keep the iteration always moving forward.

#### **Parameters**

- T [float] Temperature, [K]
- **P** [float] Pressure, [Pa]

**b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### Returns

Vs [tuple[float]] Three possible molar volumes, [m^3/mol]

## Notes

A sample region where this method works perfectly is shown below:

#### static volume\_solutions\_full(T, P, b, delta, epsilon, a\_alpha, tries=0)

Newton-Raphson based solver for cubic EOS volumes based on the idea of initializing from an analytical solver. This algorithm can only be described as a monstrous mess. It is fairly fast for most cases, but about 3x slower than volume\_solutions\_halley. In the worst case this will fall back to *mpmath*.

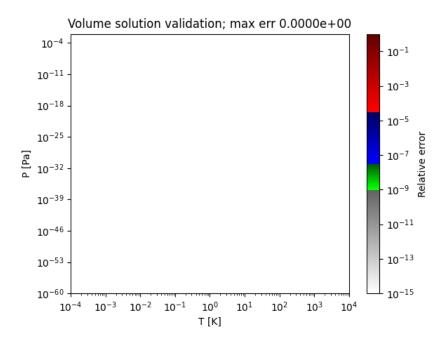
#### Parameters

- **T** [float] Temperature, [K]
- **P** [float] Pressure, [Pa]
- **b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]



**tries** [int, optional] Internal parameter as this function will call itself if it needs to; number of previous solve attempts, [-]

# Returns

**Vs** [tuple[complex]] Three possible molar volumes, [m^3/mol]

## **Notes**

Sample regions where this method works perfectly are shown below:

static volume\_solutions\_mp(T, P, b, delta, epsilon, a\_alpha, dps=50)

Solution of this form of the cubic EOS in terms of volumes, using the *mpmath* arbitrary precision library. The number of decimal places returned is controlled by the *dps* parameter.

This function is the reference implementation which provides exactly correct solutions; other algorithms are compared against this one.

# Parameters

- **T** [float] Temperature, [K]
- **P** [float] Pressure, [Pa]

**b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

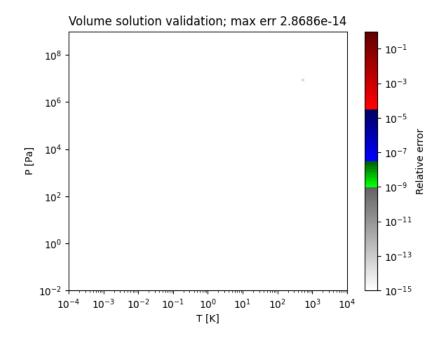
epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

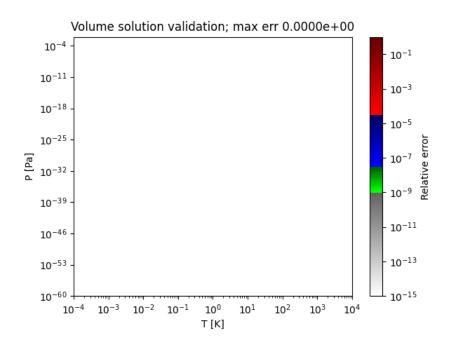
a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

dps [int] Number of decimal places in the result by mpmath, [-]

## Returns

Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]





#### Notes

Although *mpmath* has a cubic solver, it has been found to fail to solve in some cases. Accordingly, the algorithm is as follows:

Working precision is dps plus 40 digits; and if P < 1e-10 Pa, it is dps plus 400 digits. The input parameters are converted exactly to mpf objects on input.

*polyroots* from mpmath is used with *maxsteps=2000*, and extra precision of 15 digits. If the solution does not converge, 20 extra digits are added up to 8 times. If no solution is found, mpmath's *findroot* is called on the pressure error function using three initial guesses from another solver.

Needless to say, this function is quite slow.

# References

[1]

# **Examples**

Test case which presented issues for PR EOS (three roots were not being returned):

```
>>> volume_solutions_mpmath(0.01, 1e-05, 2.5405184201558786e-05, 5.

→081036840311757e-05, -6.454233843151321e-10, 0.3872747173781095)

(mpf('0.0000254054613415548712260258773060137'), mpf('4.

→66038025602155259976574392093252'), mpf('8309.80218708657190094424659859346'))
```

# 7.7.2 Standard Peng-Robinson Family EOSs

# **Standard Peng Robinson**

class thermo.eos.PR(Tc, Pc, omega, T=None, P=None, V=None) Bases: thermo.eos.GCEOS

Class for solving the Peng-Robinson [1] [2] cubic equation of state for a pure compound. Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

The main methods here are *PR.a\_alpha\_and\_derivatives\_pure*, which calculates  $a\alpha$  and its first and second derivatives, and *PR.solve\_T*, which from a specified *P* and *V* obtains *T*.

Two of (T, P, V) are needed to solve the EOS.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$
  

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
  

$$b = 0.07780 \frac{RT_c}{P_c}$$
  

$$\alpha(T) = [1 + \kappa(1 - \sqrt{T_r})]^2$$
  

$$\kappa = 0.37464 + 1.54226\omega - 0.26992\omega^2$$

**Parameters** 

- Tc [float] Critical temperature, [K]
- **Pc** [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

# Notes

The constants in the expressions for a and b are given to full precision in the actual code, as derived in [3]. The full expression for critical compressibility is:

$$Z_c = \frac{1}{32} \left( \sqrt[3]{16\sqrt{2} - 13} - \frac{7}{\sqrt[3]{16\sqrt{2} - 13}} + 11 \right)$$

# References

[1], [2], [3]

# **Examples**

T-P initialization, and exploring each phase's properties:

```
>>> eos = PR(Tc=507.6, Pc=3025000.0, omega=0.2975, T=400., P=1E6)
>>> eos.V_1, eos.V_g
(0.000156073184785, 0.0021418768167)
>>> eos.phase
'l/g'
>>> eos.H_dep_l, eos.H_dep_g
(-26111.8775716, -3549.30057795)
>>> eos.S_dep_1, eos.S_dep_g
(-58.098447843, -6.4394518931)
>>> eos.U_dep_1, eos.U_dep_g
(-22942.1657091, -2365.3923474)
>>> eos.G_dep_1, eos.G_dep_g
(-2872.49843435, -973.51982071)
>>> eos.A_dep_1, eos.A_dep_g
(297.21342811, 210.38840980)
>>> eos.beta_l, eos.beta_g
(0.00269337091778, 0.0101232239111)
>>> eos.kappa_1, eos.kappa_g
(9.3357215438e-09, 1.97106698097e-06)
>>> eos.Cp_minus_Cv_l, eos.Cp_minus_Cv_g
(48.510162249, 44.544161128)
>>> eos.Cv_dep_1, eos.Cp_dep_1
(18.8921126734, 59.0878123050)
```

P-T initialization, liquid phase, and round robin trip:

```
>>> eos = PR(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.000130222125139, -31134.75084, -72.47561931)
```

T-V initialization, liquid phase:

```
>>> eos2 = PR(Tc=507.6, Pc=3025000, omega=0.2975, T=299., V=eos.V_1)
>>> eos2.P, eos2.phase
(1000000.00, '1')
```

P-V initialization at same state:

```
>>> eos3 = PR(Tc=507.6, Pc=3025000, omega=0.2975, V=eos.V_1, P=1E6)
>>> eos3.T, eos3.phase
(299.0000000000, '1')
```

# **Methods**

P_max_at_V(V)	Method to calculate the maximum pressure the EOS can create at a constant volume, if one exists; returns
	None otherwise.
a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for this EOS.
d3a_alpha_dT3_pure(T)	Method to calculate the third temperature derivative
	of <i>a_alpha</i> .
<pre>solve_T(P, V[, solution])</pre>	Method to calculate T from a specified P and V for
	the PR EOS.

# $P_max_at_V(V)$

Method to calculate the maximum pressure the EOS can create at a constant volume, if one exists; returns None otherwise.

# Parameters

V [float] Constant molar volume, [m^3/mol]

# Returns

P [float] Maximum possible isochoric pressure, [Pa]

# Notes

The analytical determination of this formula involved some part of the discriminant, and much black magic.

# **Examples**

```
>>> e = PR(P=1e5, V=0.0001437, Tc=512.5, Pc=8084000.0, omega=0.559)
>>> e.P_max_at_V(e.V)
2247886208.7
```

## Zc = 0.30740130869870386

Mechanical compressibility of Peng-Robinson EOS

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Uses the set values of *Tc*, *kappa*, and *a*.

$$a\alpha = a\left(\kappa\left(-\frac{T^{0.5}}{Tc^{0.5}}+1\right)+1\right)^2$$
$$\frac{da\alpha}{dT} = -\frac{1.0a\kappa}{T^{0.5}Tc^{0.5}}\left(\kappa\left(-\frac{T^{0.5}}{Tc^{0.5}}+1\right)+1\right)$$
$$\frac{d^2a\alpha}{dT^2} = 0.5a\kappa\left(-\frac{1}{T^{1.5}Tc^{0.5}}\left(\kappa\left(\frac{T^{0.5}}{Tc^{0.5}}-1\right)-1\right)+\frac{\kappa}{T^{1.0}Tc^{1.0}}\right)$$

#### **Parameters**

T [float] Temperature at which to calculate the values, [-]

# Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

# Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

# **Examples**

Dodecane at 250 K:

```
>>> eos = PR(Tc=658.0, Pc=1820000.0, omega=0.562, T=500., P=1e5)
>>> eos.a_alpha_and_derivatives_pure(250.0)
(15.66839156301, -0.03094091246957, 9.243186769880e-05)
```

# a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for this EOS. Uses the set values of *Tc*, *kappa*, and *a*.

$$a\alpha = a\left(\kappa\left(-\frac{T^{0.5}}{Tc^{0.5}}+1\right)+1\right)^2$$

## **Parameters**

T [float] Temperature at which to calculate the value, [-]

## Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

# Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

# **Examples**

Dodecane at 250 K:

```
>>> eos = PR(Tc=658.0, Pc=1820000.0, omega=0.562, T=500., P=1e5)
>>> eos.a_alpha_pure(250.0)
15.66839156301
```

# c1 = 0.4572355289213822

Full value of the constant in the *a* parameter

# c2 = 0.07779607390388846

Full value of the constant in the *b* parameter

# d3a\_alpha\_dT3\_pure(T)

Method to calculate the third temperature derivative of *a\_alpha*. Uses the set values of *Tc*, *kappa*, and *a*. This property is not normally needed.

$$\frac{d^3 a \alpha}{dT^3} = \frac{3a \kappa \left(-\frac{\kappa}{T_c} + \frac{\sqrt{\frac{T}{T_c}} \left(\kappa \left(\sqrt{\frac{T}{T_c}} - 1\right) - 1\right)}{T}\right)}{4T^2}$$

**Parameters** 

T [float] Temperature at which to calculate the derivative, [-]

# Returns

**d3a\_alpha\_dT3** [float] Third temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^3]

#### Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

#### **Examples**

Dodecane at 500 K:

```
>>> eos = PR(Tc=658.0, Pc=1820000.0, omega=0.562, T=500., P=1e5)
>>> eos.d3a_alpha_dT3_pure(500.0)
-9.8038800671e-08
```

# solve\_T(P, V, solution=None)

Method to calculate *T* from a specified *P* and *V* for the PR EOS. Uses *Tc*, *a*, *b*, and *kappa* as well, obtained from the class's namespace.

## **Parameters**

- **P** [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]
- **solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

## Returns

T [float] Temperature, [K]

## **Notes**

The exact solution can be derived as follows, and is excluded for breviety.

```
>>> from sympy import *
>>> P, T, V = symbols('P, T, V')
>>> Tc, Pc, omega = symbols('Tc, Pc, omega')
>>> R, a, b, kappa = symbols('R, a, b, kappa')
>>> a_alpha = a*(1 + kappa*(1-sqrt(T/Tc)))**2
>>> PR_formula = R*T/(V-b) - a_alpha/(V*(V+b)+b*(V-b)) - P
>>> #solve(PR_formula, T)
```

After careful evaluation of the results of the analytical formula, it was discovered, that numerical precision issues required several NR refinement iterations; at at times, when the analytical value is extremely erroneous, a call to a full numerical solver not using the analytical solution at all is required.

# **Examples**

```
>>> eos = PR(Tc=658.0, Pc=1820000.0, omega=0.562, T=500., P=1e5)
>>> eos.solve_T(P=eos.P, V=eos.V_g)
500.0000000
```

# Peng Robinson (1978)

**class** thermo.eos.**PR78**(*Tc*, *Pc*, *omega*, *T=None*, *P=None*, *V=None*) Bases: thermo.eos.PR

Class for solving the Peng-Robinson cubic equation of state for a pure compound according to the 1978 variant [1] [2]. Subclasses *PR*, which provides everything except the variable *kappa*. Solves the EOS on initialization. See *PR* for further documentation.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$
  

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
  

$$b = 0.07780 \frac{RT_c}{P_c}$$
  

$$\alpha(T) = [1 + \kappa(1 - \sqrt{T_r})]^2$$
  

$$\kappa_i = 0.37464 + 1.54226\omega_i - 0.26992\omega_i^2 \text{ if } \omega_i \le 0.491$$

 $\kappa_i = 0.379642 + 1.48503\omega_i - 0.164423\omega_i^2 + 0.0166666\omega_i^3$  if  $\omega_i > 0.491$ 

Parameters

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

T [float, optional] Temperature, [K]

- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

# Notes

This variant is recommended over the original.

# References

[1], [2]

### **Examples**

P-T initialization (furfuryl alcohol), liquid phase:

```
>>> eos = PR78(Tc=632, Pc=5350000, omega=0.734, T=299., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 8.3519628969e-05, -63764.671093, -130.737153225)
```

high\_omega\_constants = (0.379642, 1.48503, -0.164423, 0.016666) Constants for the *kappa* formula for the high-omega region.

**low\_omega\_constants = (0.37464, 1.54226, -0.26992)** Constants for the *kappa* formula for the low-omega region.

## Peng Robinson Stryjek-Vera

**class** thermo.eos.**PRSV**(*Tc*, *Pc*, *omega*, *T*=*None*, *P*=*None*, *V*=*None*, *kappa1*=*None*) Bases: thermo.eos.PR

Class for solving the Peng-Robinson-Stryjek-Vera equations of state for a pure compound as given in [1]. The same as the Peng-Robinson EOS, except with a different *kappa* formula and with an optional fit parameter. Subclasses *PR*, which provides only several constants. See *PR* for further documentation and examples.

$$P = \frac{RT}{v - b} - \frac{a\alpha(T)}{v(v + b) + b(v - b)}$$
  

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
  

$$b = 0.07780 \frac{RT_c}{P_c}$$
  

$$\alpha(T) = [1 + \kappa(1 - \sqrt{T_r})]^2$$
  

$$\kappa = \kappa_0 + \kappa_1(1 + T_r^{0.5})(0.7 - T_r)$$

 $\kappa_0 = 0.378893 + 1.4897153\omega - 0.17131848\omega^2 + 0.0196554\omega^3$ 

#### Parameters

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

T [float, optional] Temperature, [K]

P [float, optional] Pressure, [Pa]

V [float, optional] Molar volume, [m^3/mol]

kappa1 [float, optional] Fit parameter; available in [1] for over 90 compounds, [-]

[1] recommends that kappal be set to 0 for Tr > 0.7. This is not done by default; the class boolean  $kappal_Tr_limit$  may be set to True and the problem re-solved with that specified if desired.  $kappal_Tr_limit$  is not supported for P-V inputs.

Solutions for P-V solve for T with SciPy's newton solver, as there is no analytical solution for T

[2] and [3] are two more resources documenting the PRSV EOS. [4] lists *kappa* values for 69 additional compounds. See also *PRSV2*. Note that tabulated *kappa* values should be used with the critical parameters used in their fits. Both [1] and [4] only considered vapor pressure in fitting the parameter.

## References

[1], [2], [3], [4]

# **Examples**

P-T initialization (hexane, with fit parameter in [1]), liquid phase:

```
>>> eos = PRSV(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6, kappa1=0.05104)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.000130126913554, -31698.926746, -74.16751538)
```

## Methods

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for this EOS.
<pre>solve_T(P, V[, solution])</pre>	Method to calculate $T$ from a specified $P$ and $V$ for
	the PRSV EOS.

### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Uses the set values of *Tc*, *kappa0*, *kappa1*, and *a*.

The *a\_alpha* function is shown below; the first and second derivatives are not shown for brevity.

$$a\alpha = a\left(\left(\kappa_0 + \kappa_1\left(\sqrt{\frac{T}{T_c}} + 1\right)\left(-\frac{T}{T_c} + \frac{7}{10}\right)\right)\left(-\sqrt{\frac{T}{T_c}} + 1\right) + 1\right)^2$$

### Parameters

T [float] Temperature at which to calculate the values, [-]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

This method does not alter the object's state and the temperature provided can be a different than that of the object.

The expressions can be derived as follows:

```
>>> from sympy import *
>>> P, T, V = symbols('P, T, V')
>>> Tc, Pc, omega = symbols('Tc, Pc, omega')
>>> R, a, b, kappa0, kappa1 = symbols('R, a, b, kappa0, kappa1')
>>> kappa = kappa0 + kappa1*(1 + sqrt(T/Tc))*(Rational(7, 10)-T/Tc)
>>> a_alpha = a*(1 + kappa*(1-sqrt(T/Tc)))**2
>>> # diff(a_alpha, T)
>>> # diff(a_alpha, T, 2)
```

#### **Examples**

### a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for this EOS. Uses the set values of *Tc*, *kappa0*, *kappa1*, and *a*.

$$a\alpha = a\left(\left(\kappa_0 + \kappa_1\left(\sqrt{\frac{T}{T_c}} + 1\right)\left(-\frac{T}{T_c} + \frac{7}{10}\right)\right)\left(-\sqrt{\frac{T}{T_c}} + 1\right) + 1\right)^2$$

#### **Parameters**

T [float] Temperature at which to calculate the value, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

### **Examples**

```
>>> eos = PRSV(Tc=507.6, Pc=3025000, omega=0.2975, T=406.08, P=1E6, kappa1=0.

→05104)
>>> eos.a_alpha_pure(185.0)
4.7686547259
```

## solve\_T(P, V, solution=None)

Method to calculate T from a specified P and V for the PRSV EOS. Uses Tc, a, b, kappa0 and kappa as well, obtained from the class's namespace.

#### Parameters

- **P** [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]
- **solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

#### Returns

T [float] Temperature, [K]

#### Notes

Not guaranteed to produce a solution. There are actually two solution, one much higher than normally desired; it is possible the solver could converge on this.

### Peng Robinson Stryjek-Vera 2

class thermo.eos.PRSV2(Tc, Pc, omega, T=None, P=None, V=None, kappa1=0, kappa2=0, kappa3=0)
Bases: thermo.eos.PR

Class for solving the Peng-Robinson-Stryjek-Vera 2 equations of state for a pure compound as given in [1]. The same as the Peng-Robinson EOS, except with a different *kappa* formula and with three fit parameters. Subclasses *PR*, which provides only several constants. See *PR* for further documentation and examples.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$
  

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
  

$$b = 0.07780 \frac{RT_c}{P_c}$$
  

$$\alpha(T) = [1 + \kappa(1 - \sqrt{T_r})]^2$$
  

$$= \kappa_0 + [\kappa_1 + \kappa_2(\kappa_3 - T_r)(1 - T_r^{0.5})](1 + T_r^{0.5})(0.7 - T_r)$$
  

$$= 0.378893 + 1.4897153\omega - 0.17131848\omega^2 + 0.0196554\omega^3$$

### **Parameters**

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]

к

 $\kappa_0$ 

- omega [float] Acentric factor, [-]
- **T** [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

kappa1 [float, optional] Fit parameter; available in [1] for over 90 compounds, [-]

kappa2 [float, optional] Fit parameter; available in [1] for over 90 compounds, [-]

kappa [float, optional] Fit parameter; available in [1] for over 90 compounds, [-]

Note that tabulated *kappa* values should be used with the critical parameters used in their fits. [1] considered only vapor pressure in fitting the parameter.

## References

[1]

# **Examples**

P-T initialization (hexane, with fit parameter in [1]), liquid phase:

# Methods

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for this EOS.
<pre>solve_T(P, V[, solution])</pre>	Method to calculate $T$ from a specified $P$ and $V$ for
	the PRSV2 EOS.

### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Uses the set values of *Tc*, *kappa0*, *kappa1*, *kappa2*, *kappa3*, and *a*.

$$\alpha(T) = [1 + \kappa (1 - \sqrt{T_r})]^2$$
$$\kappa = \kappa_0 + [\kappa_1 + \kappa_2(\kappa_3 - T_r)(1 - T_r^{0.5})](1 + T_r^{0.5})(0.7 - T_r)$$

### **Parameters**

T [float] Temperature at which to calculate the values, [-]

# Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

The first and second derivatives of *a\_alpha* are available through the following SymPy expression.

### **Examples**

#### a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for this EOS. Uses the set values of *Tc*, *kappa0*, *kappa1*, *kappa2*, *kappa3*, and *a*.

$$\alpha(T) = [1 + \kappa(1 - \sqrt{T_r})]^2$$

$$\kappa = \kappa_0 + [\kappa_1 + \kappa_2(\kappa_3 - T_r)(1 - T_r^{0.5})](1 + T_r^{0.5})(0.7 - T_r)$$

#### **Parameters**

ŀ

T [float] Temperature at which to calculate the values, [-]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### **Examples**

```
>>> eos = PRSV2(Tc=507.6, Pc=3025000, omega=0.2975, T=400., P=1E6, kappa1=0.

.05104, kappa2=0.8634, kappa3=0.460)
>>> eos.a_alpha_pure(1276.0)
33.321674050
```

# solve\_T(P, V, solution=None)

Method to calculate *T* from a specified *P* and *V* for the PRSV2 EOS. Uses *Tc*, *a*, *b*, *kappa0*, *kappa1*, *kappa2*, and *kappa3* as well, obtained from the class's namespace.

#### **Parameters**

- P [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]

**solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

#### Returns

T [float] Temperature, [K]

## Notes

Not guaranteed to produce a solution. There are actually 8 solutions, six with an imaginary component at a tested point. The two temperature solutions are quite far apart, with one much higher than the other; it is possible the solver could converge on the higher solution, so use T inputs with care. This extra solution is a perfectly valid one however. The secant method is implemented at present.

#### **Examples**

#### Peng Robinson Twu (1995)

**class** thermo.eos.**TWUPR**(*Tc*, *Pc*, *omega*, *T=None*, *P=None*, *V=None*) Bases: thermo.eos\_alpha\_functions.TwuPR95\_a\_alpha, thermo.eos.PR

Class for solving the Twu (1995) [1] variant of the Peng-Robinson cubic equation of state for a pure compound. Subclasses *PR*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

The main implemented method here is  $a\_alpha\_and\_derivatives\_pure$ , which sets  $a\alpha$  and its first and second derivatives.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{v - b} - \frac{a\alpha(T)}{v(v + b) + b(v - b)}$$
  

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
  

$$b = 0.07780 \frac{RT_c}{P_c}$$
  

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$
  

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.125283, 0.911807, 1.948150;

L1, M1, N1 = 0.511614, 0.784054, 2.812520

For supercritical conditions:

L0, M0, N0 = 0.401219, 4.963070, -0.2;

L1, M1, N1 = 0.024955, 1.248089, -8.

## Parameters

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

## Notes

Claimed to be more accurate than the PR, PR78 and PRSV equations.

There is no analytical solution for T. There are multiple possible solutions for T under certain conditions; no guaranteed are provided regarding which solution is obtained.

### References

[1]

## **Examples**

```
>>> eos = TWUPR(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6)
>>> eos.V_l, eos.H_dep_l, eos.S_dep_l
(0.00013017554170, -31652.73712, -74.112850429)
```

### **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for the Twu alpha function.
a_alpha_pure(T)	Method to calculate $a\alpha$ for the Twu alpha function.

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for the Twu alpha function. Uses the set values of *Tc*, *omega* and *a*.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.125283, 0.911807, 1.948150;

L1, M1, N1 = 0.511614, 0.784054, 2.812520

For supercritical conditions:

L0, M0, N0 = 0.401219, 4.963070, -0.2;

L1, M1, N1 = 0.024955, 1.248089, -8.

#### **Parameters**

**T** [float] Temperature at which to calculate the values, [-]

## Returns

- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

#### Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

The derivatives are somewhat long and are not described here for brevity; they are obtainable from the following SymPy expression.

### a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for the Twu alpha function. Uses the set values of Tc, omega and a.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$
$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.125283, 0.911807, 1.948150;

L1, M1, N1 = 0.511614, 0.784054, 2.812520

For supercritical conditions:

L0, M0, N0 = 0.401219, 4.963070, -0.2;

L1, M1, N1 = 0.024955, 1.248089, -8.

#### **Parameters**

T [float] Temperature at which to calculate the value, [-]

### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

This method does not alter the object's state and the temperature provided can be a different than that of the object.

### Peng Robinson Polynomial alpha Function

**class** thermo.eos.**PRTranslatedPoly**(*Tc*, *Pc*, *omega*, *alpha\_coeffs=None*, *c=0.0*, *T=None*, *P=None*, *V=None*) Bases: thermo.eos\_alpha\_functions.Poly\_a\_alpha, thermo.eos.PRTranslated

Class for solving the volume translated Peng-Robinson equation of state with a polynomial alpha function. With the right coefficients, this model can reproduce any property incredibly well. Subclasses *PRTranslated*. Solves the EOS on initialization. This is intended as a base class for all translated variants of the Peng-Robinson EOS.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$
$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
$$b = 0.07780 \frac{RT_c}{P_c}$$
$$\alpha(T) = f(T)$$

#### $\kappa = 0.37464 + 1.54226\omega - 0.26992\omega^2$

#### **Parameters**

**Tc** [float] Critical temperature, [K]

- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- **alpha\_coeffs** [tuple or None] Coefficients which may be specified by subclasses; set to None to use the original Peng-Robinson alpha function, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

#### **Examples**

Methanol, with alpha functions reproducing CoolProp's implementation of its vapor pressure (up to 13 coefficients)

```
>>> alpha_coeffs_exact = [9.645280470011588e-32, -4.362226651748652e-28, 9.

...034194757823037e-25, -1.1343330204981244e-21, 9.632898335494218e-19, -5.

...841502902171077e-16, 2.601801729901228e-13, -8.615431349241052e-11, 2.

...1202999753932622e-08, -3.829144045293198e-06, 0.0004930777289075716, -0.

...04285337965522619, 2.2473964123842705, -51.13852710672087]

>>> kwargs = dict(Tc=512.5, Pc=8084000.0, omega=0.559, alpha_coeffs=alpha_coeffs_

...exact, c=1.557458e-05)

>>> eos = PRTranslatedPoly(T=300, P=1e5, **kwargs)
```

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```
>>> eos.Psat(500)/PropsSI("P", 'T', 500.0, 'Q', 0, 'methanol')
1.0000112765
```

## **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second derivatives given that there is a polynomial equation
a_alpha_pure(T)	for $\alpha$ . Method to calculate <i>a_alpha</i> given that there is a polynomial equation for $\alpha$ .

### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives given that there is a polynomial equation for  $\alpha$ .

$$a\alpha = a \cdot \operatorname{poly}(T)$$

#### Parameters

T [float] Temperature, [K]

#### Returns

**a\_alphas** [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

### a\_alpha\_pure(T)

Method to calculate  $a\_alpha$  given that there is a polynomial equation for  $\alpha$ .

$$a\alpha = a \cdot \operatorname{poly}(T)$$

#### **Parameters**

**T** [float] Temperature, [K]

### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

# 7.7.3 Volume Translated Peng-Robinson Family EOSs

## **Peng Robinson Translated**

class thermo.eos.PRTranslated(Tc, Pc, omega, alpha\_coeffs=None, c=0.0, T=None, P=None, V=None)
Bases: thermo.eos.PR

Class for solving the volume translated Peng-Robinson equation of state. Subclasses *PR*. Solves the EOS on initialization. This is intended as a base class for all translated variants of the Peng-Robinson EOS.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
  

$$b = 0.07780 \frac{RT_c}{P_c}$$
  

$$\alpha(T) = [1 + \kappa (1 - \sqrt{T_r})]^2$$
  

$$\kappa = 0.37464 + 1.54226\omega - 0.26992\omega^2$$

### Parameters

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- **alpha\_coeffs** [tuple or None] Coefficients which may be specified by subclasses; set to None to use the original Peng-Robinson alpha function, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

#### References

[1]

# **Examples**

P-T initialization:

```
>>> eos = PRTranslated(T=305, P=1.1e5, Tc=512.5, Pc=8084000.0, omega=0.559, c=-1e-6)
>>> eos.phase, eos.V_1, eos.V_g
('1/g', 4.90798083711e-05, 0.0224350982488)
```

## Peng Robinson Translated Twu (1991)

class thermo.eos.PRTranslatedTwu(Tc, Pc, omega, alpha\_coeffs=None, c=0.0, T=None, P=None, V=None)
Bases: thermo.eos\_alpha\_functions.Twu91\_a\_alpha, thermo.eos.PRTranslated

Class for solving the volume translated Peng-Robinson equation of state with the Twu (1991) [1] alpha function. Subclasses *thermo.eos\_alpha\_functions.Twu91\_a\_alpha* and *PRTranslated*. Solves the EOS on initialization.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$
$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$
$$b = 0.07780 \frac{RT_c}{P_c}$$
$$\alpha = \left(\frac{T}{T_c}\right)^{c_3(c_2-1)} e^{c_1\left(-\left(\frac{T}{T_c}\right)^{c_2c_3}+1\right)}$$

## Parameters

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- alpha\_coeffs [tuple(float[3])] Coefficients L, M, N (also called C1, C2, C3) of TWU 1991 form,
  [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

## Notes

This variant offers substantial improvements to the PR-type EOSs - likely getting about as accurate as this form of cubic equation can get.

### References

[1]

# **Examples**

P-T initialization:

```
>>> alpha_coeffs = (0.694911381318495, 0.919907783415812, 1.70412689631515)
>>> kwargs = dict(Tc=512.5, Pc=8084000.0, omega=0.559, alpha_coeffs=alpha_coeffs,_

..., c=-1e-6)
>>> eos = PRTranslatedTwu(T=300, P=1e5, **kwargs)
>>> eos.phase, eos.V_l, eos.V_g
('1/g', 4.8918748906e-05, 0.024314406330)
```

# Peng Robinson Translated-Consistent

# class thermo.eos.PRTranslatedConsistent(Tc, Pc, omega, alpha\_coeffs=None, c=None, T=None, P=None, V=None)

Bases: thermo.eos.PRTranslatedTwu

Class for solving the volume translated Le Guennec, Privat, and Jaubert revision of the Peng-Robinson equation of state for a pure compound according to [1]. Subclasses *PRTranslatedTwu*, which provides everything except the estimation of c and the alpha coefficients. This model's *alpha* is based on the TWU 1991 model; when estimating, N is set to 2. Solves the EOS on initialization. See *PRTranslated* for further documentation.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$
$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$

$$b = 0.07780 \frac{RT_c}{P_c}$$
$$\alpha = \left(\frac{T}{T_c}\right)^{c_3(c_2-1)} e^{c_1\left(-\left(\frac{T}{T_c}\right)^{c_2c_3}+1\right)}$$

If *c* is not provided, it is estimated as:

$$c = \frac{RT_c}{P_c} (0.0198\omega - 0.0065)$$

If *alpha\_coeffs* is not provided, the parameters L and M are estimated from the acentric factor as follows:

$$L = 0.1290\omega^2 + 0.6039\omega + 0.0877$$

$$M = 0.1760\omega^2 - 0.2600\omega + 0.8884$$

**Parameters** 

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- **alpha\_coeffs** [tuple(float[3]), optional] Coefficients L, M, N (also called C1, C2, C3) of TWU 1991 form, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

## **Notes**

This variant offers substantial improvements to the PR-type EOSs - likely getting about as accurate as this form of cubic equation can get.

# References

[1]

#### **Examples**

P-T initialization (methanol), liquid phase:

```
>>> eos = PRTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=250., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.000124374813374486, -34155.16119794619, -83.34913258614345)
```

### Peng Robinson Translated (Pina-Martinez, Privat, and Jaubert Variant)

class thermo.eos.PRTranslatedPPJP(Tc, Pc, omega, c=0.0, T=None, P=None, V=None)

Bases: thermo.eos.PRTranslated

Class for solving the volume translated Pina-Martinez, Privat, Jaubert, and Peng revision of the Peng-Robinson equation of state for a pure compound according to [1]. Subclasses *PRTranslated*, which provides everything except the variable *kappa*. Solves the EOS on initialization. See *PRTranslated* for further documentation.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$

$$a = 0.45724 \frac{R^2 T_c^2}{P_c}$$

$$b = 0.07780 \frac{RT_c}{P_c}$$

$$\alpha(T) = [1 + \kappa(1 - \sqrt{T_r})]^2$$

$$\kappa = 0.3919 + 1.4996\omega - 0.2721\omega^2 + 0.1063\omega^3$$

# Parameters

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

### Notes

This variant offers incremental improvements in accuracy only, but those can be fairly substantial for some substances.

#### References

[1]

# **Examples**

P-T initialization (methanol), liquid phase:

```
>>> eos = PRTranslatedPPJP(Tc=507.6, Pc=3025000, omega=0.2975, c=0.6390E-6, T=250.,_
→P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('l', 0.0001229231238092, -33466.2428296, -80.75610242427)
```

# 7.7.4 Soave-Redlich-Kwong Family EOSs

# Standard SRK

class thermo.eos.SRK(*Tc*, *Pc*, *omega*, *T=None*, *P=None*, *V=None*)

Bases: thermo.eos.GCEOS

Class for solving the Soave-Redlich-Kwong [1] [2] [3] cubic equation of state for a pure compound. Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V - b} - \frac{a\alpha(T)}{V(V + b)}$$

$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2} - 1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$

$$b = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right) \frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$

$$\alpha(T) = \left[1 + m\left(1 - \sqrt{\frac{T}{T_c}}\right)\right]^2$$

$$m = 0.480 + 1.574\omega - 0.176\omega^2$$

**Parameters** 

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

T [float, optional] Temperature, [K]

**P** [float, optional] Pressure, [Pa]

V [float, optional] Molar volume, [m^3/mol]

# References

# [1], [2], [3]

# **Examples**

```
>>> eos = SRK(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.000146821077354, -31754.663859, -74.373272044)
```

# **Methods**

P_max_at_V(V)	Method to calculate the maximum pressure the EOS
	can create at a constant volume, if one exists; returns
	None otherwise.
a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for this EOS.
<i>solve_T</i> (P, V[, solution])	Method to calculate $T$ from a specified $P$ and $V$ for
	the SRK EOS.

### $P_max_at_V(V)$

Method to calculate the maximum pressure the EOS can create at a constant volume, if one exists; returns None otherwise.

#### Parameters

V [float] Constant molar volume, [m^3/mol]

# Returns

**P** [float] Maximum possible isochoric pressure, [Pa]

# Notes

The analytical determination of this formula involved some part of the discriminant, and much black magic.

## **Examples**

>>> e = SRK(P=1e5, V=0.0001437, Tc=512.5, Pc=8084000.0, omega=0.559)
>>> e.P\_max\_at\_V(e.V)
490523786.2

# Zc = 0.3333333333333333333

Mechanical compressibility of SRK EOS

### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Uses the set values of Tc, m, and a.

$$a\alpha = a\left(m\left(-\sqrt{\frac{T}{T_c}}+1\right)+1\right)^2$$
$$\frac{da\alpha}{dT} = \frac{am}{T}\sqrt{\frac{T}{T_c}}\left(m\left(\sqrt{\frac{T}{T_c}}-1\right)-1\right)$$
$$\frac{d^2a\alpha}{dT^2} = \frac{am\sqrt{\frac{T}{T_c}}}{2T^2}\left(m+1\right)$$

Parameters

T [float] Temperature at which to calculate the values, [-]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

## a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for this EOS. Uses the set values of *Tc*, *m*, and *a*.

$$a\alpha = a\left(m\left(-\sqrt{\frac{T}{T_c}}+1\right)+1\right)^2$$

### **Parameters**

**T** [float] Temperature at which to calculate the values, [-]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## c1 = 0.4274802335403414

Full value of the constant in the *a* parameter

#### c2 = 0.08664034996495772

Full value of the constant in the *b* parameter

# epsilon = 0.0

epsilon is always zero for the SRK EOS

#### solve\_T(P, V, solution=None)

Method to calculate T from a specified P and V for the SRK EOS. Uses a, b, and Tc obtained from the class's namespace.

## Parameters

P [float] Pressure, [Pa]

V [float] Molar volume, [m^3/mol]

**solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

## Returns

T [float] Temperature, [K]

## Notes

The exact solution can be derived as follows; it is excluded for breviety.

```
>>> from sympy import *
>>> P, T, V, R, a, b, m = symbols('P, T, V, R, a, b, m')
>>> Tc, Pc, omega = symbols('Tc, Pc, omega')
>>> a_alpha = a*(1 + m*(1-sqrt(T/Tc)))**2
>>> SRK = R*T/(V-b) - a_alpha/(V*(V+b)) - P
>>> solve(SRK, T)
```

### Twu SRK (1995)

**class** thermo.eos.**TWUSRK**(*Tc*, *Pc*, *omega*, *T=None*, *P=None*, *V=None*)

 $Bases:\ thermo. eos\_alpha\_functions. Twu SRK95\_a\_alpha,\ thermo. eos. SRK$ 

Class for solving the Soave-Redlich-Kwong cubic equation of state for a pure compound. Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

The main implemented method here is  $a\_alpha\_and\_derivatives\_pure$ , which sets  $a\alpha$  and its first and second derivatives.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V - b} - \frac{a\alpha(T)}{V(V + b)}$$

$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2} - 1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$

$$b = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right) \frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.141599, 0.919422, 2.496441

L1, M1, N1 = 0.500315, 0.799457, 3.291790

For supercritical conditions:

L0, M0, N0 = 0.441411, 6.500018, -0.20

L1, M1, N1 = 0.032580, 1.289098, -8.0

#### Parameters

**Tc** [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

# Notes

There is no analytical solution for T. There are multiple possible solutions for T under certain conditions; no guaranteed are provided regarding which solution is obtained.

## References

[1]

# **Examples**

```
>>> eos = TWUSRK(Tc=507.6, Pc=3025000, omega=0.2975, T=299., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.000146892222966, -31612.6025870, -74.022966093)
```

# Methods

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for the Twu alpha function.
a_alpha_pure(T)	Method to calculate $a\alpha$ for the Twu alpha function.

# a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for the Twu alpha function. Uses the set values of *Tc*, *omega* and *a*.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.141599, 0.919422, 2.496441

L1, M1, N1 = 0.500315, 0.799457, 3.291790

For supercritical conditions:

L0, M0, N0 = 0.441411, 6.500018, -0.20

L1, M1, N1 = 0.032580, 1.289098, -8.0

# Parameters

T [float] Temperature at which to calculate the values, [-]

# Returns

- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

This method does not alter the object's state and the temperature provided can be a different than that of the object.

The derivatives are somewhat long and are not described here for brevity; they are obtainable from the following SymPy expression.

## a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for the Twu alpha function. Uses the set values of Tc, omega and a.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.141599, 0.919422, 2.496441

L1, M1, N1 = 0.500315, 0.799457, 3.291790

For supercritical conditions:

L0, M0, N0 = 0.441411, 6.500018, -0.20

L1, M1, N1 = 0.032580, 1.289098, -8.0

## Parameters

T [float] Temperature at which to calculate the value, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

## **API SRK**

class thermo.eos.APISRK(Tc, Pc, omega=None, T=None, P=None, V=None, S1=None, S2=0)
Bases: thermo.eos.SRK

Class for solving the Refinery Soave-Redlich-Kwong cubic equation of state for a pure compound shown in the API Databook [1]. Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

Implemented methods here are  $a\_alpha\_and\_derivatives$ , which sets  $a\alpha$  and its first and second derivatives, and solve\_T, which from a specified P and V obtains T. Two fit constants are used in this expression, with an estimation scheme for the first if unavailable and the second may be set to zero.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V(V+b)}$$
$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2}-1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$
$$b = \left(\frac{(\sqrt[3]{2}-1)}{3}\right)\frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$
$$\alpha(T) = \left[1 + S_1\left(1 - \sqrt{T_r}\right) + S_2\frac{1 - \sqrt{T_r}}{\sqrt{T_r}}\right]^2$$

 $S_1 = 0.48508 + 1.55171\omega - 0.15613\omega^2$  if S1 is not tabulated

Parameters

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float, optional] Acentric factor, [-]

- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- S1 [float, optional] Fit constant or estimated from acentric factor if not provided [-]
- S2 [float, optional] Fit constant or 0 if not provided [-]

## References

[1]

# Examples

```
>>> eos = APISRK(Tc=514.0, Pc=6137000.0, S1=1.678665, S2=-0.216396, P=1E6, T=299)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 7.0456950702e-05, -42826.286146, -103.626979037)
```

# Methods

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for this EOS.
<pre>solve_T(P, V[, solution])</pre>	Method to calculate $T$ from a specified $P$ and $V$ for
	the API SRK EOS.

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Uses the set values of *Tc, a, S1*, and *S2*.

$$a\alpha(T) = a \left[ 1 + S_1 \left( 1 - \sqrt{T_r} \right) + S_2 \frac{1 - \sqrt{T_r}}{\sqrt{T_r}} \right]^2$$

$$\frac{da\alpha}{dT} = a \frac{T_c}{T^2} \left( -S_2 \left( \sqrt{\frac{T}{T_c}} - 1 \right) + \sqrt{\frac{T}{T_c}} \left( S_1 \sqrt{\frac{T}{T_c}} + S_2 \right) \right) \left( S_2 \left( \sqrt{\frac{T}{T_c}} - 1 \right) + \sqrt{\frac{T}{T_c}} \left( S_1 \left( \sqrt{\frac{T}{T_c}} - 1 \right) - 1 \right) \right)$$

$$\frac{d^2 a\alpha}{dT^2} = a \frac{1}{2T^3} \left( S_1^2 T \sqrt{\frac{T}{T_c}} - S_1 S_2 T \sqrt{\frac{T}{T_c}} + 3S_1 S_2 T c \sqrt{\frac{T}{T_c}} + S_1 T \sqrt{\frac{T}{T_c}} - 3S_2^2 T c \sqrt{\frac{T}{T_c}} + 4S_2^2 T c + 3S_2 T c \sqrt{\frac{T}{T_c}} \right)$$

# a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for this EOS. Uses the set values of *Tc*, *m*, and *a*.

$$a\alpha = a\left(m\left(-\sqrt{\frac{T}{T_c}}+1\right)+1\right)^2$$

## Parameters

T [float] Temperature at which to calculate the values, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## solve\_T(P, V, solution=None)

Method to calculate *T* from a specified *P* and *V* for the API SRK EOS. Uses *a*, *b*, and *Tc* obtained from the class's namespace.

# **Parameters**

- P [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]

**solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

## Returns

T [float] Temperature, [K]

If S2 is set to 0, the solution is the same as in the SRK EOS, and that is used. Otherwise, newton's method must be used to solve for *T*. There are 8 roots of T in that case, six of them real. No guarantee can be made regarding which root will be obtained.

### **SRK Translated**

class thermo.eos.SRKTranslated(Tc, Pc, omega, alpha\_coeffs=None, c=0.0, T=None, P=None, V=None)
Bases: thermo.eos.SRK

Class for solving the volume translated Peng-Robinson equation of state. Subclasses *SRK*. Solves the EOS on initialization. This is intended as a base class for all translated variants of the SRK EOS.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$
$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2}-1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$
$$b = \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$
$$\alpha(T) = \left[1 + m\left(1 - \sqrt{\frac{T}{T_c}}\right)\right]^2$$
$$m = 0.480 + 1.574\omega - 0.176\omega^2$$

## Parameters

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

- **alpha\_coeffs** [tuple or None] Coefficients which may be specified by subclasses; set to None to use the original Peng-Robinson alpha function, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

## References

[1]

### **Examples**

P-T initialization:

```
>>> eos = SRKTranslated(T=305, P=1.1e5, Tc=512.5, Pc=8084000.0, omega=0.559, c=-1e-

→6)
>>> eos.phase, eos.V_l, eos.V_g
('1/g', 5.5131657318e-05, 0.022447661363)
```

# SRK Translated-Consistent

**class** thermo.eos.**SRKTranslatedConsistent**(*Tc*, *Pc*, *omega*, *alpha\_coeffs=None*, *c=None*, *T=None*, P=None, V=None)

Bases: thermo.eos\_alpha\_functions.Twu91\_a\_alpha, thermo.eos.SRKTranslated

Class for solving the volume translated Le Guennec, Privat, and Jaubert revision of the SRK equation of state for a pure compound according to [1].

This model's *alpha* is based on the TWU 1991 model; when estimating, N is set to 2. Solves the EOS on initialization. See *SRK* for further documentation.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$
$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2}-1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$
$$b = \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$
$$\alpha = \left(\frac{T}{T_c}\right)^{c_3(c_2-1)} e^{c_1\left(-\left(\frac{T}{T_c}\right)^{c_2c_3}+1\right)}$$

If *c* is not provided, it is estimated as:

$$c = \frac{RT_c}{P_c} (0.0172\omega - 0.0096)$$

If *alpha\_coeffs* is not provided, the parameters L and M are estimated from the acentric factor as follows:

$$L = 0.0947\omega^2 + 0.6871\omega + 0.1508$$
$$M = 0.1615\omega^2 - 0.2349\omega + 0.8876$$

#### **Parameters**

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

- **alpha\_coeffs** [tuple(float[3]), optional] Coefficients L, M, N (also called C1, C2, C3) of TWU 1991 form, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- **T** [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

This variant offers substantial improvements to the SRK-type EOSs - likely getting about as accurate as this form of cubic equation can get.

#### References

[1]

### **Examples**

P-T initialization (methanol), liquid phase:

```
>>> eos = SRKTranslatedConsistent(Tc=507.6, Pc=3025000, omega=0.2975, T=250., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.00011846802568940222, -34324.05211005662, -83.83861726864234)
```

## SRK Translated (Pina-Martinez, Privat, and Jaubert Variant)

### class thermo.eos.SRKTranslatedPPJP(*Tc*, *Pc*, *omega*, *c*=0.0, *T*=None, *P*=None, *V*=None) Bases: thermo.eos.SRK

Class for solving the volume translated Pina-Martinez, Privat, Jaubert, and Peng revision of the Soave-Redlich-Kwong equation of state for a pure compound according to [1]. Subclasses *SRK*, which provides everything except the variable *kappa*. Solves the EOS on initialization. See *SRK* for further documentation.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$
$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2}-1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$
$$b = \left(\frac{(\sqrt[3]{2}-1)}{3}\right)\frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$
$$\alpha(T) = \left[1 + m\left(1 - \sqrt{\frac{T}{T_c}}\right)\right]^2$$
$$m = 0.4810 + 1.5963\omega - 0.2963\omega^2 + 0.1223\omega^3$$

#### **Parameters**

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- c [float, optional] Volume translation parameter, [m^3/mol]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

This variant offers incremental improvements in accuracy only, but those can be fairly substantial for some substances.

#### References

[1]

### **Examples**

P-T initialization (hexane), liquid phase:

```
>>> eos = SRKTranslatedPPJP(Tc=507.6, Pc=3025000, omega=0.2975, c=22.3098E-6, T=250.

..., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('1', 0.00011666322408111662, -34158.934132722185, -83.06507748137201)
```

## **MSRK Translated**

**class** thermo.eos.**MSRKTranslated**(*Tc*, *Pc*, *omega*, *M*=*None*, *N*=*None*, *alpha\_coeffs*=*None*, *c*=0.0, *T*=*None*, P=*None*, *V*=*None*)

Bases: thermo.eos\_alpha\_functions.Soave\_1979\_a\_alpha, thermo.eos.SRKTranslated

Class for solving the volume translated Soave (1980) alpha function, revision of the Soave-Redlich-Kwong equation of state for a pure compound according to [1]. Uses two fitting parameters *N* and *M* to more accurately fit the vapor pressure of pure species. Subclasses *SRKTranslated*. Solves the EOS on initialization. See *SRKTranslated* for further documentation.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$
$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2}-1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^2}{P_c}$$
$$b = \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$
$$\alpha(T) = 1 + (1 - T_r)(M + \frac{N}{T_r})$$

## **Parameters**

Tc [float] Critical temperature, [K]

- Pc [float] Critical pressure, [Pa]
- omega [float] Acentric factor, [-]
- **c** [float, optional] Volume translation parameter, [m^3/mol]

alpha\_coeffs [tuple(float[3]), optional] Coefficients M, N of this EOS's alpha function, [-]

- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

This is an older correlation that offers lower accuracy on many properties which were sacrificed to obtain the vapor pressure accuracy. The alpha function of this EOS does not meet any of the consistency requriements for alpha functions.

Coefficients can be found in [2], or estimated with the method in [3]. The estimation method in [3] works as follows, using the acentric factor and true critical compressibility:

$$M = 0.4745 + 2.7349(\omega Z_c) + 6.0984(\omega Z_c)^2$$

 $N = 0.0674 + 2.1031(\omega Z_c) + 3.9512(\omega Z_c)^2$ 

An alternate estimation scheme is provided in [1], which provides analytical solutions to calculate the parameters M and N from two points on the vapor pressure curve, suggested as 10 mmHg and 1 atm. This is used as an estimation method here if the parameters are not provided, and the two vapor pressure points are obtained from the original SRK equation of state.

## References

## [1], [2], [3]

# **Examples**

P-T initialization (hexane), liquid phase:

```
>>> eos = MSRKTranslated(Tc=507.6, Pc=3025000, omega=0.2975, c=22.0561E-6, M=0.7446,

→ N=0.2476, T=250., P=1E6)

>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l

('1', 0.0001169276461322, -34571.6862673, -84.757900348)
```

# Methods

<pre>estimate_MN(Tc, Pc, omega[, c])</pre>	Calculate the alpha values for the MSRK equation to
	match two pressure points, and solve analytically for
	the M, N required to match exactly that.

static estimate\_MN(Tc, Pc, omega, c=0.0)

Calculate the alpha values for the MSRK equation to match two pressure points, and solve analytically for the M, N required to match exactly that. Since no experimental data is available, make it up with the original SRK EOS.

### Parameters

Tc [float] Critical temperature, [K]

Pc [float] Critical pressure, [Pa]

omega [float] Acentric factor, [-]

c [float, optional] Volume translation parameter, [m^3/mol]

# Returns

M [float] M parameter, [-]

N [float] N parameter, [-]

## **Examples**

```
>>> from sympy import *
>>> Tc, m, n = symbols('Tc, m, n')
>>> T0, T1 = symbols('T_10, T_760')
>>> alpha0, alpha1 = symbols('alpha_10, alpha_760')
>>> Eqs = [Eq(alpha0, 1 + (1 - T0/Tc)*(m + n/(T0/Tc))), Eq(alpha1, 1 + (1 - T1/
_Tc)*(m + n/(T1/Tc)))]
>>> solve(Eqs, [n, m])
```

# 7.7.5 Van der Waals Equations of State

```
class thermo.eos.VDW(Tc, Pc, T=None, P=None, V=None, omega=None)
```

Bases: thermo.eos.GCEOS

Class for solving the Van der Waals [1] [2] cubic equation of state for a pure compound. Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V-b} - \frac{a}{V^2}$$
$$a = \frac{27}{64} \frac{(RT_c)^2}{P_c}$$
$$b = \frac{RT_c}{8P_c}$$

## Parameters

- Tc [float] Critical temperature, [K]
- Pc [float] Critical pressure, [Pa]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

omega [float, optional] Acentric factor - not used in equation of state!, [-]

## **Notes**

omega is allowed as an input for compatibility with the other EOS forms, but is not used.

## References

[1], [2]

## **Examples**

```
>>> eos = VDW(Tc=507.6, Pc=3025000, T=299., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('l', 0.000223329856081, -13385.7273746, -32.65923125)
```

## Attributes

omega

## **Methods**

P_discriminant_zeros_analytical(T, b, delta,	Method to calculate the pressures which zero the dis-
)	criminant function of the VDW eos.
T_discriminant_zeros_analytical([valid])	Method to calculate the temperatures which zero the
	discriminant function of the VDW eos.
a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ .
<pre>solve_T(P, V[, solution])</pre>	Method to calculate $T$ from a specified $P$ and $V$ for
	the VDW EOS.

# **static P\_discriminant\_zeros\_analytical**(*T*, *b*, *delta*, *epsilon*, *a\_alpha*, *valid=False*) Method to calculate the pressures which zero the discriminant function of the VDW eos. This is an cubic

function solved analytically.

## Parameters

- **T** [float] Temperature, [K]
- **b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]
- delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]
- epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]
- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- **valid** [bool] Whether to filter the calculated pressures so that they are all real, and positive only, [-]

## Returns

P\_discriminant\_zeros [tuple[float]] Pressures which make the discriminant zero, [Pa]

Calculated analytically. Derived as follows. Has multiple solutions.

```
>>> from sympy import *
>>> P, T, V, R, b, a = symbols('P, T, V, R, b, a')
>>> P_vdw = R^*T/(V-b) - a/(V^*V)
>>> delta, epsilon = 0, 0
>>> eta = b
>>> B = b^*P/(R^*T)
>>> deltas = delta*P/(R*T)
>>> thetas = a*P/(R*T)**2
>>> epsilons = epsilon*(P/(R*T))**2
>>> etas = eta*P/(R*T)
>>> a_coeff = 1
>>> b_coeff = (deltas - B - 1)
>>> c = (thetas + epsilons - deltas*(B+1))
>>> d = -(epsilons*(B+1) + thetas*etas)
>>> disc = b_coeff*b_coeff*c*c - 4*a_coeff*c*c*c - 4*b_coeff*b_coeff*b_coeff*d -
→ 27*a_coeff*a_coeff*d*d + 18*a_coeff*b_coeff*c*d
>>> base = -(expand(disc/P**2*R**3*T**3/a))
>>> collect(base, P) args
```

# T\_discriminant\_zeros\_analytical(valid=False)

Method to calculate the temperatures which zero the discriminant function of the *VDW* eos. This is an analytical cubic function solved analytically.

#### Parameters

**valid** [bool] Whether to filter the calculated temperatures so that they are all real, and positive only, [-]

#### Returns

T\_discriminant\_zeros [list[float]] Temperatures which make the discriminant zero, [K]

## Notes

Calculated analytically. Derived as follows. Has multiple solutions.

```
>>> from sympy import *
>>> P, T, V, R, b, a = symbols('P, T, V, R, b, a')
>>> delta, epsilon = 0, 0
>>> eta = b
>>> B = b*P/(R*T)
>>> deltas = delta*P/(R*T)
>>> thetas = a*P/(R*T)**2
>>> epsilons = epsilon*(P/(R*T))**2
>>> etas = eta*P/(R*T)
>>> a_coeff = 1
>>> b_coeff = (deltas - B - 1)
>>> c = (thetas + epsilons - deltas*(B+1))
>>> d = -(epsilons*(B+1) + thetas*etas)
>>> disc = b_coeff*b_coeff*c*c - 4*a_coeff*c*c*c - 4*b_coeff*b_coeff*b_coeff*d -
-> 27*a_coeff*a_coeff*d*d + 18*a_coeff*b_coeff*c*d
```

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```
>>> base = -(expand(disc/P**2*R**3*T**3/a))
>>> base_T = simplify(base*T**3)
>>> sln = collect(expand(base_T), T).args
```

### Zc = 0.375

Mechanical compressibility of VDW EOS

### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Uses the set values of a.

 $\begin{aligned} a\alpha &= a \\ \frac{da\alpha}{dT} &= 0 \\ \frac{d^2a\alpha}{dT^2} &= 0 \end{aligned}$ 

#### **Parameters**

T [float] Temperature at which to calculate the values, [-]

### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

### a\_alpha\_pure(T)

Method to calculate  $a\alpha$ . Uses the set values of a.

$$a\alpha = a$$

#### **Parameters**

**T** [float] Temperature at which to calculate the values, [-]

## Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

### delta = 0.0

delta is always zero for the VDW EOS

## epsilon = 0.0

epsilon is always zero for the VDW EOS

### omega = None

omega has no impact on the VDW EOS

#### solve\_T(P, V, solution=None)

Method to calculate T from a specified P and V for the VDW EOS. Uses a, and b, obtained from the class's namespace.

$$T = \frac{1}{RV^2} \left( PV^2 \left( V - b \right) + Va - ab \right)$$

**Parameters** 

- **P** [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]

**solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

# Returns

T [float] Temperature, [K]

# 7.7.6 Redlich-Kwong Equations of State

class thermo.eos.RK(Tc, Pc, T=None, P=None, V=None, omega=None)

Bases: thermo.eos.GCEOS

Class for solving the Redlich-Kwong [1] [2] [3] cubic equation of state for a pure compound. Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V - b} - \frac{a}{V\sqrt{\frac{T}{T_c}}(V + b)}$$
$$a = \left(\frac{R^2(T_c)^2}{9(\sqrt[3]{2} - 1)P_c}\right) = \frac{0.42748 \cdot R^2(T_c)^{2.5}}{P_c}$$
$$b = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right)\frac{RT_c}{P_c} = \frac{0.08664 \cdot RT_c}{P_c}$$

### Parameters

Tc [float] Critical temperature, [K]

- Pc [float] Critical pressure, [Pa]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

## **Notes**

omega is allowed as an input for compatibility with the other EOS forms, but is not used.

## References

[1], [2], [3]

## **Examples**

```
>>> eos = RK(Tc=507.6, Pc=3025000, T=299., P=1E6)
>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l
('l', 0.000151893468781, -26160.8424877, -63.013137852)
```

#### Attributes

omega

## **Methods**

T_discriminant_zeros_analytical([valid])	Method to calculate the temperatures which zero the
	discriminant function of the RK eos.
a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for this EOS.
<pre>solve_T(P, V[, solution])</pre>	Method to calculate $T$ from a specified $P$ and $V$ for
	the RK EOS.

## T\_discriminant\_zeros\_analytical(valid=False)

Method to calculate the temperatures which zero the discriminant function of the *RK* eos. This is an analytical function with an 11-coefficient polynomial which is solved with *numpy*.

#### **Parameters**

**valid** [bool] Whether to filter the calculated temperatures so that they are all real, and positive only, [-]

#### Returns

T\_discriminant\_zeros [float] Temperatures which make the discriminant zero, [K]

#### Notes

Calculated analytically. Derived as follows. Has multiple solutions.

```
>>> from sympy import *
>>> P, T, V, R, b, a, Troot = symbols('P, T, V, R, b, a, Troot')
>>> a_alpha = a/sqrt(T)
>>> delta, epsilon = b, 0
>>> eta = b
>>> B = b*P/(R*T)
>>> deltas = delta*P/(R*T)
>>> thetas = a_alpha^P/(R^T)^{*2}
>>> epsilons = epsilon*(P/(R*T))**2
>>> etas = eta*P/(R*T)
>>> a_coeff = 1
>>> b_coeff = (deltas - B - 1)
>>> c = (thetas + epsilons - deltas*(B+1))
>>> d = -(epsilons*(B+1) + thetas*etas)
>>> disc = b_coeff*b_coeff*c*c - 4*a_coeff*c*c*c - 4*b_coeff*b_coeff*b_coeff*d -
→ 27*a_coeff*a_coeff*d*d + 18*a_coeff*b_coeff*c*d
```

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```
>>> new_disc = disc.subs(sqrt(T), Troot)
>>> new_T_base = expand(expand(new_disc)*Troot**15)
>>> ans = collect(new_T_base, Troot).args
```

#### Zc = 0.3333333333333333333

Mechanical compressibility of RK EOS

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. Uses the set values of a.

$$a\alpha = \frac{a}{\sqrt{\frac{T}{T_c}}}$$
$$\frac{da\alpha}{dT} = -\frac{a}{2T\sqrt{\frac{T}{T_c}}}$$
$$\frac{d^2a\alpha}{dT^2} = \frac{3a}{4T^2\sqrt{\frac{T}{T_c}}}$$

#### **Parameters**

T [float] Temperature at which to calculate the values, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

#### a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for this EOS. Uses the set values of a.

$$a\alpha = \frac{a}{\sqrt{\frac{T}{T_c}}}$$

#### **Parameters**

T [float] Temperature at which to calculate the values, [-]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

### c1 = 0.4274802335403414

Full value of the constant in the *a* parameter

#### c2 = 0.08664034996495772

Full value of the constant in the *b* parameter

#### epsilon = 0.0

epsilon is always zero for the RK EOS

## omega = None

omega has no impact on the RK EOS

#### solve\_T(P, V, solution=None)

Method to calculate T from a specified P and V for the RK EOS. Uses a, and b, obtained from the class's namespace.

### Parameters

- P [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]
- **solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

#### Returns

T [float] Temperature, [K]

### **Notes**

The exact solution can be derived as follows; it is excluded for breviety.

```
>>> from sympy import *
>>> P, T, V, R = symbols('P, T, V, R')
>>> Tc, Pc = symbols('Tc, Pc')
>>> a, b = symbols('a, b')
>>> RK = Eq(P, R*T/(V-b) - a/sqrt(T)/(V*V + b*V))
>>> solve(RK, T)
```

# 7.7.7 Ideal Gas Equation of State

```
class thermo.eos.IG(Tc=None, Pc=None, omega=None, T=None, P=None, V=None)
Bases: thermo.eos.GCEOS
```

Class for solving the ideal gas equation in the *GCEOS* framework. This provides access to a number of derivatives and properties easily. It also keeps a common interface for all gas models. However, it is somewhat slow.

Subclasses *GCEOS*, which provides the methods for solving the EOS and calculating its assorted relevant thermodynamic properties. Solves the EOS on initialization.

Two of T, P, and V are needed to solve the EOS; values for Tc and Pc and omega, which are not used in the calculates, are set to those of methane by default to allow use without specifying them.

$$P = \frac{RT}{V}$$

# Parameters

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

omega [float, optional] Acentric factor, [-]

- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

## References

[1]

## **Examples**

T-P initialization, and exploring each phase's properties:

```
>>> eos = IG(T=400., P=1E6)
>>> eos.V_g, eos.phase
(0.003325785047261296, 'g')
>>> eos.H_dep_g, eos.S_dep_g, eos.U_dep_g, eos.G_dep_g, eos.A_dep_g
(0.0, 0.0, 0.0, 0.0, 0.0)
>>> eos.beta_g, eos.kappa_g, eos.Cp_dep_g, eos.Cv_dep_g
(0.0025, 1e-06, 0.0, 0.0)
>>> eos.fugacity_g, eos.PIP_g, eos.Z_g, eos.dP_dT_g
(1000000.0, 0.9999999999999999, 1.0, 2500.0)
```

## **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for this EOS.
a_alpha_pure(T)	Method to calculate $a\alpha$ for the ideal gas law, which
	is zero.
<pre>solve_T(P, V[, solution])</pre>	Method to calculate $T$ from a specified $P$ and $V$ for
	the ideal gas equation of state.
volume_solutions(T, P[, b, delta, epsilon,])	Calculate the ideal-gas molar volume in a format
	compatible with the other cubic EOS solvers.

## Zc = 1.0

float: Critical compressibility for an ideal gas is 1

#### a = 0.0

float: a parameter for an ideal gas is 0

#### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for this EOS. All values are zero.

#### **Parameters**

T [float] Temperature at which to calculate the values, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

## a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for the ideal gas law, which is zero.

#### **Parameters**

**T** [float] Temperature at which to calculate the values, [-]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## b = 0.0

float: b parameter for an ideal gas is 0

delta = 0.0

float: delta parameter for an ideal gas is 0

epsilon = 0.0

float: epsilon parameter for an ideal gas is 0

solve\_T(P, V, solution=None)

Method to calculate T from a specified P and V for the ideal gas equation of state.

$$T = \frac{PV}{R}$$

### **Parameters**

P [float] Pressure, [Pa]

V [float] Molar volume, [m^3/mol]

solution [str or None, optional] Not used, [-]

#### Returns

T [float] Temperature, [K]

#### static volume\_solutions(T, P, b=0.0, delta=0.0, epsilon=0.0, a\_alpha=0.0)

Calculate the ideal-gas molar volume in a format compatible with the other cubic EOS solvers. The ideal gas volume is the first element; and the second and third elements are zero. This is implemented to allow the ideal-gas model to be compatible with the cubic models, whose equations do not work with parameters of zero.

#### **Parameters**

T [float] Temperature, [K]

- **P** [float] Pressure, [Pa]
- **b** [float, optional] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float, optional] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float, optional] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float, optional] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Returns

Vs [list[float]] Three possible molar volumes, [m^3/mol]

## **Examples**

```
>>> volume_solutions_ideal(T=300, P=1e7)
(0.0002494338785445972, 0.0, 0.0)
```

## 7.7.8 Lists of Equations of State

```
thermo.eos.eos_list = [<class 'thermo.eos.IG'>, <class 'thermo.eos.PR'>, <class
'thermo.eos.PR78'>, <class 'thermo.eos.PRSV'>, <class 'thermo.eos.PRSV2'>, <class
'thermo.eos.VDW'>, <class 'thermo.eos.RK'>, <class 'thermo.eos.SRK'>, <class
'thermo.eos.APISRK'>, <class 'thermo.eos.TWUPR'>, <class 'thermo.eos.TWUSRK'>, <class
'thermo.eos.PRTranslatedPPJP'>, <class 'thermo.eos.SRKTranslatedPPJP'>, <class
'thermo.eos.MSRKTranslated'>, <class 'thermo.eos.PRTranslatedConsistent'>, <class
'thermo.eos.SRKTranslatedConsistent'>]
```

list : List of all cubic equation of state classes.

```
thermo.eos.eos_2P_list = [<class 'thermo.eos.PR'>, <class 'thermo.eos.PR78'>, <class
'thermo.eos.PRSV'>, <class 'thermo.eos.PRSV2'>, <class 'thermo.eos.VDW'>, <class
'thermo.eos.RK'>, <class 'thermo.eos.SRK'>, <class 'thermo.eos.APISRK'>, <class
'thermo.eos.TWUPR'>, <class 'thermo.eos.TWUSRK'>, <class 'thermo.eos.PRTranslatedPPJP'>,
<class 'thermo.eos.SRKTranslatedPPJP'>, <class 'thermo.eos.MSRKTranslated'>, <class
'thermo.eos.PRTranslatedConsistent'>, <class 'thermo.eos.SRKTranslatedConsistent'>]
list: List of all cubic equation of state classes that can represent multiple phases.
```

## 7.7.9 Demonstrations of Concepts

## **Maximum Pressure at Constant Volume**

Some equations of state show this behavior. At a liquid volume, if the temperature is increased, the pressure should increase as well to create that same volume. However in some cases this is not the case as can be demonstrated for this hypothetical dodecane-like fluid:

Through experience, it is observed that this behavior is only shown for some sets of critical constants. It was found that if the expression for  $\frac{\partial P}{\partial T_V}$  is set to zero, an analytical expression can be determined for exactly what that maximum pressure is. Some EOSs implement this function as  $P_max_at_V$ ; those that don't, and fluids where there is no maximum pressure, will have that method but it will return None.

## **Debug Plots to Understand EOSs**

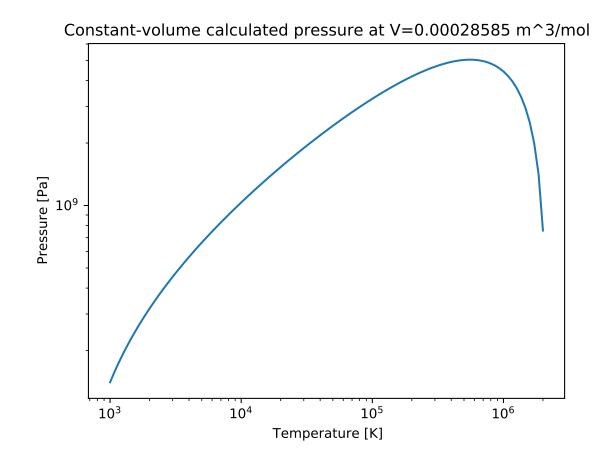
The *GCEOS.volume\_errors* method shows the relative error in the volume solution. *mpmath* is required for this functionality. It is not likely there is an error here but many problems have been found in the past.

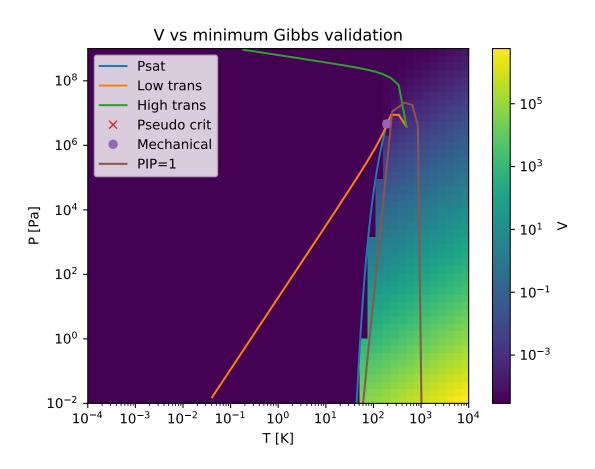
The GCEOS.PT\_surface\_special method shows some of the special curves of the EOS.

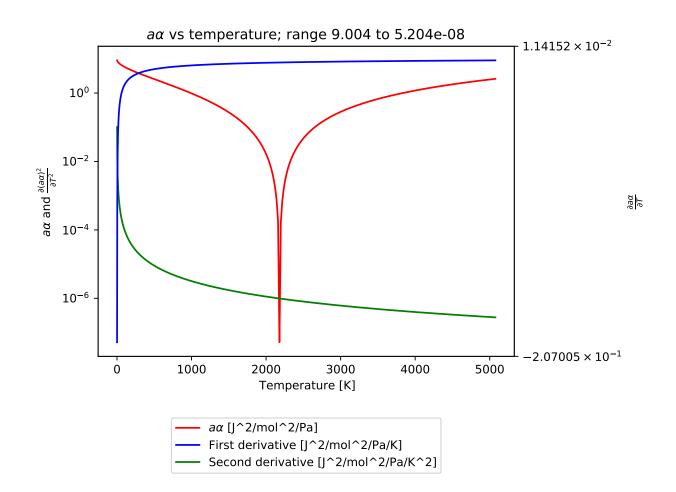
The *GCEOS.a\_alpha\_plot* method shows the alpha function curve. The following sample shows the SRK's default alpha function for methane.

If this doesn't look healthy, that is because it is not. There are strict thermodynamic consistency requirements that we know of today:

- The alpha function must be positive and continuous
- The first derivative must be negative and continuous
- The second derivative must be positive and continuous



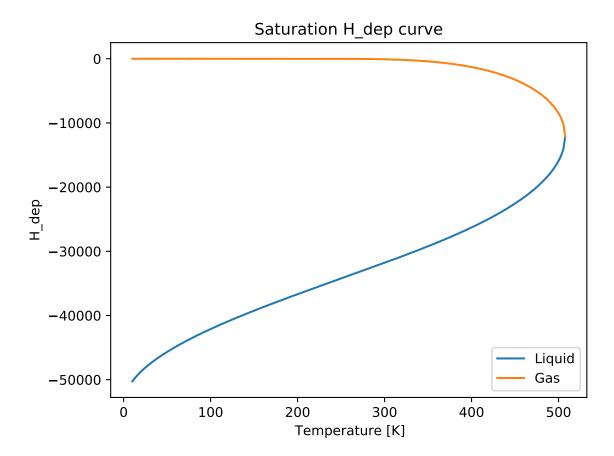




• The third derivative must be negative

The first criterial and second criteria fail here.

There are two methods to review the saturation properties solution. The more general way is to review saturation properties as a plot:



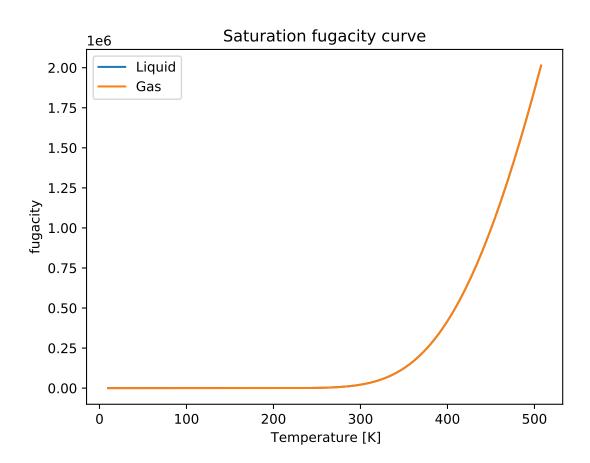
The second plot is more detailed, and is focused on the direct calculation of vapor pressure without using an iterative solution. It shows the relative error of the fit, which normally way below where it would present any issue - only 10-100x more error than it is possible to get with floating point numbers at all.

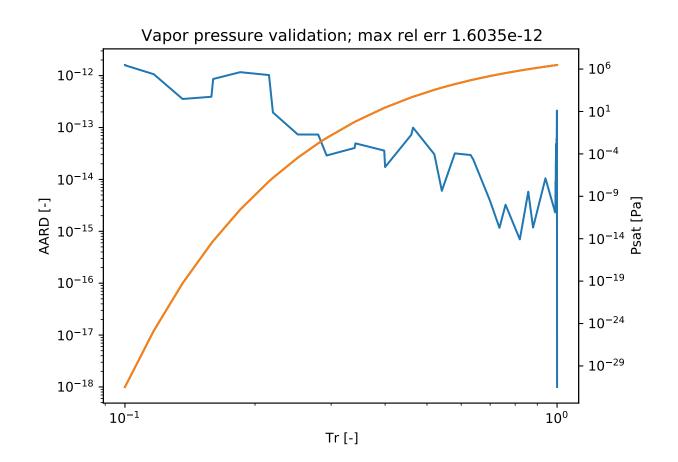
# 7.8 Cubic Equations of State for Mixtures (thermo.eos\_mix)

This module contains implementations of most cubic equations of state for mixtures. This includes Peng-Robinson, SRK, Van der Waals, PRSV, TWU and many other variants.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Base Class
- Peng-Robinson Family EOSs
  - Standard Peng Robinson
  - Peng Robinson (1978)





- Peng Robinson Stryjek-Vera
- Peng Robinson Stryjek-Vera 2
- Peng Robinson Twu (1995)
- Peng Robinson Translated
- Peng Robinson Translated-Consistent
- Peng Robinson Translated (Pina-Martinez, Privat, and Jaubert Variant)
- SRK Family EOSs
  - Standard SRK
  - Twu SRK (1995)
  - API SRK
  - SRK Translated
  - SRK Translated-Consistent
  - MSRK Translated
- Cubic Equation of State with Activity Coefficients
- Van der Waals Equation of State
- Redlich-Kwong Equation of State
- Ideal Gas Equation of State
- Different Mixing Rules
- Lists of Equations of State

## 7.8.1 Base Class

#### class thermo.eos\_mix.GCEOSMIX

Bases: thermo.eos.GCEOS

Class for solving a generic pressure-explicit three-parameter cubic equation of state for a mixture. Does not implement any parameters itself; must be subclassed by a mixture equation of state class which subclasses it.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V^2 + \delta V + \epsilon}$$

Attributes

A\_dep\_g Departure molar Helmholtz energy from ideal gas behavior for the gas phase, [J/mol].

A\_dep\_1 Departure molar Helmholtz energy from ideal gas behavior for the liquid phase, [J/mol].

**Cp\_minus\_Cv\_g** Cp - Cv for the gas phase, [J/mol/K].

**Cp\_minus\_Cv\_1** Cp - Cv for the liquid phase, [J/mol/K].

**U\_dep\_g** Departure molar internal energy from ideal gas behavior for the gas phase, [J/mol].

**U\_dep\_1** Departure molar internal energy from ideal gas behavior for the liquid phase, [J/mol].

V\_dep\_g Departure molar volume from ideal gas behavior for the gas phase, [m^3/mol].

- **V\_dep\_1** Departure molar volume from ideal gas behavior for the liquid phase, [m^3/mol].
- **V\_g\_mpmath** The molar volume of the gas phase calculated with *mpmath* to a higher precision, [m^3/mol].
- **V\_1\_mpmath** The molar volume of the liquid phase calculated with *mpmath* to a higher precision, [m^3/mol].

Vc Critical volume, [m<sup>3</sup>/mol].

**a\_alpha\_ijs** Calculate and return the matrix  $(a\alpha)_{ij} = (1 - k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$ .

**beta\_g** Isobaric (constant-pressure) expansion coefficient for the gas phase, [1/K].

**beta\_1** Isobaric (constant-pressure) expansion coefficient for the liquid phase, [1/K].

c1

c2

- **d2H\_dep\_dT2\_g** Second temperature derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K^2].
- **d2H\_dep\_dT2\_g\_P** Second temperature derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K^2].
- **d2H\_dep\_dT2\_g\_V** Second temperature derivative of departure enthalpy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^2].
- **d2H\_dep\_dT2\_1** Second temperature derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K^2].
- **d2H\_dep\_dT2\_1\_P** Second temperature derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K^2].
- **d2H\_dep\_dT2\_1\_V** Second temperature derivative of departure enthalpy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^2].
- **d2H\_dep\_dTdP\_g** Temperature and pressure derivative of departure enthalpy at constant pressure then temperature for the gas phase, [(J/mol)/K/Pa].
- **d2H\_dep\_dTdP\_1** Temperature and pressure derivative of departure enthalpy at constant pressure then temperature for the liquid phase, [(J/mol)/K/Pa].
- d2P\_dT2\_PV\_g Second derivative of pressure with respect to temperature twice, but with pressure held constant the first time and volume held constant the second time for the gas phase, [Pa/K^2].
- d2P\_dT2\_PV\_1 Second derivative of pressure with respect to temperature twice, but with pressure held constant the first time and volume held constant the second time for the liquid phase, [Pa/K^2].
- **d2P\_dTdP\_g** Second derivative of pressure with respect to temperature and, then pressure; and with volume held constant at first, then temperature, for the gas phase, [1/K].
- **d2P\_dTdP\_1** Second derivative of pressure with respect to temperature and, then pressure; and with volume held constant at first, then temperature, for the liquid phase, [1/K].
- **d2P\_dTdrho\_g** Derivative of pressure with respect to molar density, and temperature for the gas phase, [Pa/(K\*mol/m^3)].
- **d2P\_dTdrho\_1** Derivative of pressure with respect to molar density, and temperature for the liquid phase, [Pa/(K\*mol/m^3)].

- **d2P\_dVdP\_g** Second derivative of pressure with respect to molar volume and then pressure for the gas phase, [mol/m^3].
- **d2P\_dVdP\_1** Second derivative of pressure with respect to molar volume and then pressure for the liquid phase, [mol/m^3].
- **d2P\_dVdT\_TP\_g** Second derivative of pressure with respect to molar volume and then temperature at constant temperature then pressure for the gas phase, [Pa\*mol/m^3/K].
- **d2P\_dVdT\_TP\_1** Second derivative of pressure with respect to molar volume and then temperature at constant temperature then pressure for the liquid phase, [Pa\*mol/m^3/K].
- d2P\_dVdT\_g Alias of GCEOS.d2P\_dTdV\_g
- d2P\_dVdT\_1 Alias of GCEOS.d2P\_dTdV\_1
- **d2P\_drho2\_g** Second derivative of pressure with respect to molar density for the gas phase, [Pa/(mol/m^3)^2].
- **d2P\_drho2\_1** Second derivative of pressure with respect to molar density for the liquid phase, [Pa/(mol/m^3)^2].
- **d2S\_dep\_dT2\_g** Second temperature derivative of departure entropy with respect to temperature for the gas phase, [(J/mol)/K^3].
- **d2S\_dep\_dT2\_g\_V** Second temperature derivative of departure entropy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^3].
- **d2S\_dep\_dT2\_1** Second temperature derivative of departure entropy with respect to temperature for the liquid phase, [(J/mol)/K^3].
- **d2S\_dep\_dT2\_1\_V** Second temperature derivative of departure entropy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^3].
- **d2S\_dep\_dTdP\_g** Temperature and pressure derivative of departure entropy at constant pressure then temperature for the gas phase, [(J/mol)/K^2/Pa].
- **d2S\_dep\_dTdP\_1** Temperature and pressure derivative of departure entropy at constant pressure then temperature for the liquid phase, [(J/mol)/K^2/Pa].
- **d2T\_dP2\_g** Second partial derivative of temperature with respect to pressure (constant volume) for the gas phase, [K/Pa^2].
- **d2T\_dP2\_1** Second partial derivative of temperature with respect to pressure (constant temperature) for the liquid phase, [K/Pa^2].
- **d2T\_dPdV\_g** Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the gas phase, [K\*mol/(Pa\*m^3)].
- **d2T\_dPdV\_1** Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the liquid phase, [K\*mol/(Pa\*m^3)].
- **d2T\_dPdrho\_g** Derivative of temperature with respect to molar density, and pressure for the gas phase, [K/(Pa\*mol/m^3)].
- d2T\_dPdrho\_1 Derivative of temperature with respect to molar density, and pressure for the liquid phase, [K/(Pa\*mol/m^3)].
- **d2T\_dV2\_g** Second partial derivative of temperature with respect to volume (constant pressure) for the gas phase, [K\*mol^2/m^6].
- **d2T\_dV2\_1** Second partial derivative of temperature with respect to volume (constant pressure) for the liquid phase, [K\*mol^2/m^6].

- **d2T\_dVdP\_g** Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the gas phase, [K\*mol/(Pa\*m^3)].
- **d2T\_dVdP\_1** Second partial derivative of temperature with respect to pressure (constant volume) and then volume (constant pressure) for the liquid phase, [K\*mol/(Pa\*m^3)].
- **d2T\_drho2\_g** Second derivative of temperature with respect to molar density for the gas phase, [K/(mol/m^3)^2].
- d2T\_drho2\_1 Second derivative of temperature with respect to molar density for the liquid phase, [K/(mol/m<sup>3</sup>)<sup>2</sup>].
- **d2V\_dP2\_g** Second partial derivative of volume with respect to pressure (constant temperature) for the gas phase, [m^3/(Pa^2\*mol)].
- **d2V\_dP2\_1** Second partial derivative of volume with respect to pressure (constant temperature) for the liquid phase, [m^3/(Pa^2\*mol)].
- **d2V\_dPdT\_g** Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the gas phase, [m^3/(K\*Pa\*mol)].
- **d2V\_dPdT\_1** Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the liquid phase, [m^3/(K\*Pa\*mol)].
- **d2V\_dT2\_g** Second partial derivative of volume with respect to temperature (constant pressure) for the gas phase, [m^3/(mol\*K^2)].
- **d2V\_dT2\_1** Second partial derivative of volume with respect to temperature (constant pressure) for the liquid phase, [m^3/(mol\*K^2)].
- $d2V_dTdP_g$  Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the gas phase,  $[m^3/(K*Pa*mol)]$ .
- **d2V\_dTdP\_1** Second partial derivative of volume with respect to pressure (constant temperature) and then pressure (constant temperature) for the liquid phase, [m^3/(K\*Pa\*mol)].
- *d2a\_alpha\_dT2\_dns* Helper method for calculating the mole number derivatives of *d2a\_alpha\_dT2*.
- **d2a\_alpha\_dT2\_dzs** Helper method for calculating the mole number derivatives of *d2a\_alpha\_dT2*.
- d2a\_alpha\_dT2\_ijs Calculate and return the matrix of the second temperature derivatives of the alpha terms.
- **d2a\_alpha\_dTdP\_g\_V** Derivative of the temperature derivative of *a\_alpha* with respect to pressure at constant volume (varying T) for the gas phase, [J^2/mol^2/Pa^2/K].
- **d2a\_alpha\_dTdP\_1\_V** Derivative of the temperature derivative of *a\_alpha* with respect to pressure at constant volume (varying T) for the liquid phase, [J^2/mol^2/Pa^2/K].
- **d2a\_alpha\_dninjs** Helper method for calculating the second partial molar derivatives of *a\_alpha* (hessian).
- **d2a\_alpha\_dzizjs** Helper method for calculating the second composition derivatives of *a\_alpha* (hessian).
- *d2b\_dninjs* Helper method for calculating the second partial mole number derivatives of b.
- *d2b\_dzizjs* Helper method for calculating the second partial mole fraction derivatives of b.
- **d2rho\_dP2\_g** Second derivative of molar density with respect to pressure for the gas phase, [(mol/m^3)/Pa^2].

- **d2rho\_dP2\_1** Second derivative of molar density with respect to pressure for the liquid phase, [(mol/m^3)/Pa^2].
- **d2rho\_dPdT\_g** Second derivative of molar density with respect to pressure and temperature for the gas phase, [(mol/m^3)/(K\*Pa)].
- **d2rho\_dPdT\_1** Second derivative of molar density with respect to pressure and temperature for the liquid phase, [(mol/m^3)/(K\*Pa)].
- **d2rho\_dT2\_g** Second derivative of molar density with respect to temperature for the gas phase, [(mol/m^3)/K^2].
- **d2rho\_dT2\_1** Second derivative of molar density with respect to temperature for the liquid phase, [(mol/m^3)/K^2].
- **d3a\_alpha\_dT3** Method to calculate the third temperature derivative of  $a\alpha$ , [J^2/mol^2/Pa/K^3].
- *d3a\_alpha\_dninjnks* Helper method for calculating the third mole number derivatives of *a\_alpha*.
- **d3a\_alpha\_dzizjzks** Helper method for calculating the third composition derivatives of *a\_alpha*.
- *d3b\_dninjnks* Helper method for calculating the third partial mole number derivatives of b.

*d3b\_dzizjzks* Helper method for calculating the third partial mole fraction derivatives of b.

d3delta\_dzizjzks Helper method for calculating the third composition derivatives of delta.

- *d3epsilon\_dzizjzks* Helper method for calculating the third composition derivatives of *epsilon*.
- **dH\_dep\_dP\_g** Derivative of departure enthalpy with respect to pressure for the gas phase, [(J/mol)/Pa].
- **dH\_dep\_dP\_g\_V** Derivative of departure enthalpy with respect to pressure at constant volume for the liquid phase, [(J/mol)/Pa].
- **dH\_dep\_dP\_1** Derivative of departure enthalpy with respect to pressure for the liquid phase, [(J/mol)/Pa].
- **dH\_dep\_dP\_1\_V** Derivative of departure enthalpy with respect to pressure at constant volume for the gas phase, [(J/mol)/Pa].
- **dH\_dep\_dT\_g** Derivative of departure enthalpy with respect to temperature for the gas phase, [(J/mol)/K].
- **dH\_dep\_dT\_g\_V** Derivative of departure enthalpy with respect to temperature at constant volume for the gas phase, [(J/mol)/K].
- **dH\_dep\_dT\_1** Derivative of departure enthalpy with respect to temperature for the liquid phase, [(J/mol)/K].
- **dH\_dep\_dT\_1\_V** Derivative of departure enthalpy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K].
- **dH\_dep\_dV\_g\_P** Derivative of departure enthalpy with respect to volume at constant pressure for the gas phase, [J/m^3].
- **dH\_dep\_dV\_g\_T** Derivative of departure enthalpy with respect to volume at constant temperature for the gas phase, [J/m^3].
- **dH\_dep\_dV\_1\_P** Derivative of departure enthalpy with respect to volume at constant pressure for the liquid phase, [J/m^3].

- **dH\_dep\_dV\_1\_T** Derivative of departure enthalpy with respect to volume at constant temperature for the gas phase, [J/m^3].
- **dP\_drho\_g** Derivative of pressure with respect to molar density for the gas phase, [Pa/(mol/m^3)].
- **dP\_drho\_1** Derivative of pressure with respect to molar density for the liquid phase, [Pa/(mol/m^3)].
- **dS\_dep\_dP\_g** Derivative of departure entropy with respect to pressure for the gas phase, [(J/mol)/K/Pa].
- **dS\_dep\_dP\_g\_V** Derivative of departure entropy with respect to pressure at constant volume for the gas phase, [(J/mol)/K/Pa].
- **dS\_dep\_dP\_1** Derivative of departure entropy with respect to pressure for the liquid phase, [(J/mol)/K/Pa].
- **dS\_dep\_dP\_1\_V** Derivative of departure entropy with respect to pressure at constant volume for the liquid phase, [(J/mol)/K/Pa].
- **dS\_dep\_dT\_g** Derivative of departure entropy with respect to temperature for the gas phase, [(J/mol)/K^2].
- **dS\_dep\_dT\_g\_V** Derivative of departure entropy with respect to temperature at constant volume for the gas phase, [(J/mol)/K^2].
- **dS\_dep\_dT\_1** Derivative of departure entropy with respect to temperature for the liquid phase, [(J/mol)/K^2].
- **dS\_dep\_dT\_1\_V** Derivative of departure entropy with respect to temperature at constant volume for the liquid phase, [(J/mol)/K^2].
- **dS\_dep\_dV\_g\_P** Derivative of departure entropy with respect to volume at constant pressure for the gas phase, [J/K/m<sup>3</sup>].
- **dS\_dep\_dV\_g\_T** Derivative of departure entropy with respect to volume at constant temperature for the gas phase, [J/K/m^3].
- **dS\_dep\_dV\_1\_P** Derivative of departure entropy with respect to volume at constant pressure for the liquid phase, [J/K/m<sup>3</sup>].
- **dS\_dep\_dV\_1\_T** Derivative of departure entropy with respect to volume at constant temperature for the gas phase, [J/K/m^3].
- **dT\_drho\_g** Derivative of temperature with respect to molar density for the gas phase, [K/(mol/m^3)].
- **dT\_drho\_1** Derivative of temperature with respect to molar density for the liquid phase, [K/(mol/m^3)].
- dZ\_dP\_g Derivative of compressibility factor with respect to pressure for the gas phase, [1/Pa].
- dZ\_dP\_1 Derivative of compressibility factor with respect to pressure for the liquid phase, [1/Pa].
- **dZ\_dT\_g** Derivative of compressibility factor with respect to temperature for the gas phase, [1/K].
- **dZ\_dT\_1** Derivative of compressibility factor with respect to temperature for the liquid phase, [1/K].
- **da\_alpha\_dP\_g\_V** Derivative of the *a\_alpha* with respect to pressure at constant volume (varying T) for the gas phase, [J^2/mol^2/Pa^2].

- **da\_alpha\_dP\_1\_V** Derivative of the *a\_alpha* with respect to pressure at constant volume (varying T) for the liquid phase, [J^2/mol^2/Pa^2].
- *da\_alpha\_dT\_dns* Helper method for calculating the mole number derivatives of *da\_alpha\_dT*.
- *da\_alpha\_dT\_dzs* Helper method for calculating the composition derivatives of *da\_alpha\_dT*.
- da\_alpha\_dT\_ijs Calculate and return the matrix for the temperature derivatives of the alpha terms.
- *da\_alpha\_dns* Helper method for calculating the mole number derivatives of *a\_alpha*.
- *da\_alpha\_dzs* Helper method for calculating the composition derivatives of *a\_alpha*.
- *db\_dns* Helper method for calculating the mole number derivatives of b.
- *db\_dzs* Helper method for calculating the composition derivatives of *b*.
- **dbeta\_dP\_g** Derivative of isobaric expansion coefficient with respect to pressure for the gas phase, [1/(Pa\*K)].
- **dbeta\_dP\_1** Derivative of isobaric expansion coefficient with respect to pressure for the liquid phase, [1/(Pa\*K)].
- **dbeta\_dT\_g** Derivative of isobaric expansion coefficient with respect to temperature for the gas phase, [1/K^2].
- **dbeta\_dT\_1** Derivative of isobaric expansion coefficient with respect to temperature for the liquid phase, [1/K^2].
- **dfugacity\_dP\_g** Derivative of fugacity with respect to pressure for the gas phase, [-].
- dfugacity\_dP\_1 Derivative of fugacity with respect to pressure for the liquid phase, [-].
- dfugacity\_dT\_g Derivative of fugacity with respect to temperature for the gas phase, [Pa/K].
- **dfugacity\_dT\_1** Derivative of fugacity with respect to temperature for the liquid phase, [Pa/K].
- **dna\_alpha\_dT\_dns** Helper method for calculating the mole number derivatives of *da\_alpha\_dT*.
- *dna\_alpha\_dns* Helper method for calculating the partial molar derivatives of *a\_alpha*.
- *dnb\_dns* Helper method for calculating the partial molar derivative of *b*.
- **dphi\_dP\_g** Derivative of fugacity coefficient with respect to pressure for the gas phase, [1/Pa].
- **dphi\_dP\_1** Derivative of fugacity coefficient with respect to pressure for the liquid phase, [1/Pa].
- **dphi\_dT\_g** Derivative of fugacity coefficient with respect to temperature for the gas phase, [1/K].
- **dphi\_dT\_1** Derivative of fugacity coefficient with respect to temperature for the liquid phase, [1/K].
- **drho\_dP\_g** Derivative of molar density with respect to pressure for the gas phase, [(mol/m^3)/Pa].
- **drho\_dP\_1** Derivative of molar density with respect to pressure for the liquid phase, [(mol/m^3)/Pa].
- **drho\_dT\_g** Derivative of molar density with respect to temperature for the gas phase, [(mol/m^3)/K].

**drho\_dT\_1** Derivative of molar density with respect to temperature for the liquid phase, [(mol/m^3)/K].

fugacity\_g Fugacity for the gas phase, [Pa].

fugacity\_l Fugacity for the liquid phase, [Pa].

- **kappa\_g** Isothermal (constant-temperature) expansion coefficient for the gas phase, [1/Pa].
- **kappa\_1** Isothermal (constant-temperature) expansion coefficient for the liquid phase, [1/Pa].
- **lnphi\_g** The natural logarithm of the fugacity coefficient for the gas phase, [-].
- **lnphi\_1** The natural logarithm of the fugacity coefficient for the liquid phase, [-].
- **more\_stable\_phase** Checks the Gibbs energy of each possible phase, and returns 'l' if the liquid-like phase is more stable, and 'g' if the vapor-like phase is more stable.
- **mpmath\_volume\_ratios** Method to compare, as ratios, the volumes of the implemented cubic solver versus those calculated using *mpmath*.
- **mpmath\_volumes** Method to calculate to a high precision the exact roots to the cubic equation, using *mpmath*.
- **mpmath\_volumes\_float** Method to calculate real roots of a cubic equation, using *mpmath*, but returned as floats.
- phi\_g Fugacity coefficient for the gas phase, [Pa].
- phi\_1 Fugacity coefficient for the liquid phase, [Pa].
- *pseudo\_Pc* Apply a linear mole-fraction mixing rule to compute the average critical pressure, [Pa].
- *pseudo\_Tc* Apply a linear mole-fraction mixing rule to compute the average critical temperature, [K].
- **pseudo\_a** Apply a linear mole-fraction mixing rule to compute the average *a* coefficient, [-].
- pseudo\_omega Apply a linear mole-fraction mixing rule to compute the average omega, [-].
- rho\_g Gas molar density, [mol/m^3].
- **rho\_1** Liquid molar density, [mol/m<sup>3</sup>].
- **sorted\_volumes** List of lexicographically-sorted molar volumes available from the root finding algorithm used to solve the PT point.
- **state\_specs** Convenience method to return the two specified state specs (T, P, or V) as a dictionary.

## **Methods**

Hvap(T)	Method to calculate enthalpy of vaporization for a		
	pure fluid from an equation of state, without iteration.		
PT_surface_special([Tmin, Tmax, Pmin, Pmax,	Method to create a plot of the special curves of a fluid		
])	- vapor pressure, determinant zeros, pseudo critical		
	point, and mechanical critical point.		
P_PIP_transition(T[, low_P_limit])	Method to calculate the pressure which makes the		
	phase identification parameter exactly 1.		
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Table 20 – continue	d from previous page		
P_discriminant_zero_g()	Method to calculate the pressure which zero the dis-		
	criminant function of the general cubic eos, and is		
	likely to sit on a boundary between not having a		
	vapor-like volume; and having a vapor-like volume.		
P_discriminant_zero_l()	Method to calculate the pressure which zero the dis-		
	criminant function of the general cubic eos, and is		
	likely to sit on a boundary between not having a		
	liquid-like volume; and having a liquid-like volume.		
P_discriminant_zeros()	Method to calculate the pressures which zero the dis-		
	criminant function of the general cubic eos, at the cur-		
	rent temperature.		
P_discriminant_zeros_analytical(T, b, delta,	Method to calculate the pressures which zero the dis-		
)	criminant function of the general cubic eos.		
P_max_at_V(V)	Dummy method.		
Psat(T[, polish])	Generic method to calculate vapor pressure of a pure-		
-	component equation of state for a specified T.		
<pre>Psat_errors([Tmin, Tmax, pts, plot, show,])</pre>	Method to create a plot of vapor pressure and the rel-		
	ative error of its calculation vs.		
T_discriminant_zero_g([T_guess])	Method to calculate the temperature which zeros the		
	discriminant function of the general cubic eos, and		
	is likely to sit on a boundary between not having a		
	vapor-like volume; and having a vapor-like volume.		
T_discriminant_zero_1([T_guess])	Method to calculate the temperature which zeros the		
	discriminant function of the general cubic eos, and		
	is likely to sit on a boundary between not having a		
	liquid-like volume; and having a liquid-like volume.		
T_max_at_V(V[, Pmax])	Method to calculate the maximum temperature the		
	EOS can create at a constant volume, if one exists;		
	returns None otherwise.		
T_min_at_V(V[, Pmin])	Returns the minimum temperature for the EOS to		
	have the volume as specified.		
Tsat(P[, polish])	Generic method to calculate the temperature for a		
	specified vapor pressure of the pure fluid.		
V_g_sat(T)	Method to calculate molar volume of the vapor phase		
	along the saturation line.		
V_l_sat(T)	Method to calculate molar volume of the liquid phase		
( )	along the saturation line.		
Vs_mpmath()	Method to calculate real roots of a cubic equation,		
- ~	using <i>mpmath</i> .		
a_alpha_and_derivatives(T[, full, quick,])	Method to calculate <i>a_alpha</i> and its first and second		
	derivatives for an EOS with the Van der Waals mixing		
	rules.		
a_alpha_and_derivatives_pure(T)	Dummy method to calculate $a\alpha$ and its first and sec-		
• — • • • • · /	ond derivatives.		
a_alpha_for_Psat(T, Psat[, a_alpha_guess])	Method to calculate which value of $a\alpha$ is required for		
· · · · · · · · · · · · · · · · · ·	a given T, Psat pair.		
a_alpha_for_V(T, P, V)	Method to calculate which value of $a\alpha$ is required for		
	a given <i>T</i> , <i>P</i> pair to match a specified <i>V</i> .		
a_alpha_plot([Tmin, Tmax, pts, plot, show])	Method to create a plot of the $a\alpha$ parameter and its		
	first two derivatives.		
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Table 20 – continued from previous page

as_json()	continued from previous page Method to create a JSON-friendly serialization of the
	eos which can be stored, and reloaded later.
<pre>check_sufficient_inputs()</pre>	Method to an exception if none of the pairs (T, P), (T,
	V), or (P, V) are given.
d2G_dep_dninjs(Z)	Calculates the molar departure Gibbs energy mole
	number derivatives (where the mole fractions sum to
	1).
d2G_dep_dzizjs(Z)	Calculates the molar departure Gibbs energy second composition derivative (where the mole fractions do
	not sum to 1).
d2V_dninjs(Z)	Calculates the molar volume second mole number derivatives (where the mole fractions sum to 1).
d2V_dzizjs(Z)	Calculates the molar volume second composition
	derivative (where the mole fractions do not sum to 1).
d2lnphi_dninjs(Z)	Calculates the mixture log <i>fugacity coefficient</i> sec-
	ond mole number derivatives (where the mole frac-
	tion sum to 1).
d2lnphi_dzizjs(Z)	Calculates the mixture log fugacity coefficient second
	mole fraction derivatives (where the mole fractions
	do not sum to 1).
d2phi_sat_dT2(T[, polish])	Method to calculate the second temperature deriva-
	tive of saturation fugacity coefficient of the com-
	pound.
dG_dep_dns(Z)	Calculates the molar departure Gibbs energy mole
	number derivatives (where the mole fractions sum to 1).
$dG_{dep}_{dzs}(Z)$	Calculates the molar departure Gibbs energy compo-
- *- ()	sition derivative (where the mole fractions do not sum
	to 1).
dH_dep_dT_sat_g(T[, polish])	Method to calculate and return the temperature
	derivative of saturation vapor excess enthalpy.
dH_dep_dT_sat_1(T[, polish])	Method to calculate and return the temperature
	derivative of saturation liquid excess enthalpy.
dH_dep_dns(Z)	Calculates the molar departure enthalpy mole num-
	ber derivatives (where the mole fractions sum to 1).
dH_dep_dzs(Z)	Calculates the molar departure enthalpy composition
	derivative (where the mole fractions do not sum to 1).
dPsat_dT(T[, polish, also_Psat])	Generic method to calculate the temperature deriva-
	tive of vapor pressure for a specified <i>T</i> .
dS_dep_dT_sat_g(T[, polish])	Method to calculate and return the temperature
ds don dt cat 1/T[ naligh])	derivative of saturation vapor excess entropy. Method to calculate and return the temperature
dS_dep_dT_sat_1(T[, polish])	derivative of saturation liquid excess entropy.
dS_dep_dns(Z)	Calculates the molar departure entropy mole number
u5_ucp_ui5(L)	derivatives (where the mole fractions sum to 1).
dS_dep_dzs(Z)	Calculates the molar departure entropy composition
	derivative (where the mole fractions do not sum to 1).
dV_dns(Z)	Calculates the molar volume mole number deriva-
	tives (where the mole fractions sum to 1).
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Table 20 – con	tinued from previous page
$dV_dzs(Z)$	Calculates the molar volume composition derivative
	(where the mole fractions do not sum to 1).
$dZ_dns(Z)$	Calculates the compressibility mole number deriva-
	tives (where the mole fractions sum to 1).
$dZ_dzs(Z)$	Calculates the compressibility composition deriva-
_ ()	tives (where the mole fractions do not sum to 1).
dfugacities_dns(phase)	Generic formula for calculating the mole number
	derivatives of fugacities for each species in a mixture.
discriminant([T, P])	Method to compute the discriminant of the cubic vol-
	ume solution with the current EOS parameters, op-
	tionally at the same (assumed) <i>T</i> , and <i>P</i> or at different
	ones, if values are specified.
dlnfugacities_dns(phase)	Generic formula for calculating the mole number
unitugaci ci ci s_unis(pilase)	derivatives of log fugacities for each species in a mix-
	ture.
dlnphi_dns(Z)	
	Calculates the mixture log <i>fugacity coefficient</i> mole number derivatives (where the mole fractions sum to
	•
1 - $1$ - $(7)$	
dlnphi_dzs(Z)	Calculates the mixture log <i>fugacity coefficient</i> mole
	fraction derivatives (where the mole fractions do not
	sum to 1).
dlnphis_dP(phase)	Generic formula for calculating the pressure
	derivative of log fugacity coefficients for each
	species in a mixture.
dlnphis_dT(phase)	Generic formula for calculating the temperature
	derivaitve of log fugacity coefficients for each species
	in a mixture.
dlnphis_dns(Z)	Generic formula for calculating the mole number
	derivaitves of log fugacity coefficients for each
	species in a mixture.
dlnphis_dzs(Z)	Generic formula for calculating the mole fraction
	derivaitves of log fugacity coefficients for each
	species in a mixture.
dnG_dep_dns(Z)	Calculates the partial molar departure Gibbs energy.
dnH_dep_dns(Z)	Calculates the partial molar departure enthalpy.
dnV_dns(Z)	Calculates the partial molar volume of the specified
	phase No specific formula is implemented for this
	property - it is calculated from the molar volume
	mole fraction derivative.
dnZ_dns(Z)	Calculates the partial compressibility of the specified
	phase No specific formula is implemented for this
	property - it is calculated from the compressibility
	mole fraction derivative.
<pre>dphi_sat_dT(T[, polish])</pre>	Method to calculate the temperature derivative of sat-
	uration fugacity coefficient of the combound.
from ison(ison repr)	uration fugacity coefficient of the compound. Method to create a mixture cubic equation of state
<pre>from_j son(json_repr)</pre>	Method to create a mixture cubic equation of state
<pre>from_json(json_repr)</pre>	

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lable	20 – continued	from	previous	page

Table 20 – continue	d from previous page		
<pre>fugacities([only_l, only_g])</pre>	Helper method for calculating fugacity coefficients for any phases present, using either the overall mole fractions for both phases or using specified mole frac- tions for each phase.		
<pre>fugacity_coefficients(Z)</pre>	Generic formula for calculating log fugacity coefficients for each species in a mixture.		
<pre>mechanical_critical_point()</pre>	Method to calculate the mechanical critical point of a mixture of defined composition.		
<pre>model_hash()</pre>	Basic method to calculate a hash of the non-state parts of the model This is useful for comparing to models to determine if they are the same, i.e. in a VLL flash it is important to know if both liquids have the same model.		
<pre>phi_sat(T[, polish])</pre>	Method to calculate the saturation fugacity coefficient of the compound.		
pures()	Helper method which returns a list of pure $EOSs$ at the same $T$ and $P$ and base EOS as the mixture.		
resolve_full_alphas()	Generic method to resolve the eos with fully calcu- lated alpha derviatives.		
<pre>saturation_prop_plot(prop[, Tmin, Tmax,])</pre>	Method to create a plot of a specified property of the EOS along the (pure component) saturation line.		
<pre>set_dnzs_derivatives_and_departures([n, x,])</pre>	Sets a number of mole number and/or composition partial derivatives of thermodynamic partial deriva- tives.		
<pre>set_from_PT(Vs[, only_l, only_g])</pre>	Counts the number of real volumes in <i>Vs</i> , and determines what to do.		
<pre>set_properties_from_solution(T, P, V, b,)</pre>	Sets all interesting properties which can be calculated from an EOS alone.		
<pre>solve([pure_a_alphas, only_l, only_g,])</pre>	First EOS-generic method; should be called by all specific EOSs.		
<pre>solve_T(P, V[, quick, solution])</pre>	Generic method to calculate $T$ from a specified $P$ and $V$ .		
<pre>solve_missing_volumes()</pre>	Generic method to ensure both volumes, if solutions are physical, have calculated properties.		
<pre>state_hash()</pre>	Basic method to calculate a hash of the state of the model and its model parameters.		
<pre>subset(idxs, **state_specs)</pre>	Method to construct a new <i>GCEOSMIX</i> that removes all components not specified in the <i>idxs</i> argument.		
to([zs, T, P, V, fugacities])	Method to construct a new <i>GCEOSMIX</i> object at two of <i>T</i> , <i>P</i> or <i>V</i> with the specified composition.		
$to_PV(P, V)$	Method to construct a new $GCEOSMIX$ object at the specified $P$ and $V$ with the current composition.		
to_PV_zs(P, V, zs[, fugacities, only_l, only_g])	Method to construct a new <i>GCEOSMIX</i> instance at $P$ , $V$ , and $zs$ with the same parameters as the existing object.		
$to_TP(T, P)$	Method to construct a new <i>GCEOSMIX</i> object at the specified $T$ and $P$ with the current composition.		
to_TPV_pure(i[, T, P, V])	Helper method which returns a pure $EOSs$ at the specs (two of $T$ , $P$ and $V$ ) and base EOS as the mixture for a particular index.		
	continues on next page		

Table 20 – continued from previous page

Method to construct a new <i>GCEOSMIX</i> instance at <i>T</i> ,
P, and $zs$ with the same parameters as the existing
object.
Method to construct a new GCEOSMIX instance with
the same parameters as the existing object.
Method to construct a new GCEOSMIX object at the
specified $T$ and $V$ with the current composition.
Method to construct a new GCEOSMIX object at
the current object's properties and composition, but
which is at the mechanical critical point.
Method to calculate the relative absolute error in the
calculated molar volumes.
Method to create a plot of the relative absolute error
in the cubic volume solution as compared to a higher-
precision calculation.
Halley's method based solver for cubic EOS volumes
based on the idea of initializing from a single liquid-
like guess which is solved precisely, deflating the cu-
bic analytically, solving the quadratic equation for the
next two volumes, and then performing two halley
steps on each of them to obtain the final solutions.
Newton-Raphson based solver for cubic EOS vol-
umes based on the idea of initializing from an ana-
lytical solver.
Solution of this form of the cubic EOS in terms of vol-

Table	20 –	continued	from	previous	page
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## Psat(T, polish=False)

Generic method to calculate vapor pressure of a pure-component equation of state for a specified *T*. An explicit solution is used unless *polish* is True.

The result of this function has no physical meaning for multicomponent mixtures, and does not represent either a dew point or a bubble point!

## Parameters

T [float] Temperature, [K]

**polish** [bool, optional] Whether to attempt to use a numerical solver to make the solution more precise or not

## Returns

Psat [float] Vapor pressure using the pure-component approach, [Pa]

For multicomponent mixtures this may serve as a useful guess for the dew and the bubble pressure.

**a\_alpha\_and\_derivatives**(*T*, *full=True*, *quick=True*, *pure\_a\_alphas=True*)

Method to calculate  $a\_alpha$  and its first and second derivatives for an EOS with the Van der Waals mixing rules. Uses the parent class's interface to compute pure component values. Returns  $a\_alpha$ ,  $da\_alpha\_dT$ , and  $d2a\_alpha\_dT2$ .

For use in *solve\_T* this returns only *a\_alpha* if *full* is False.

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1 - k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$

#### Parameters

T [float] Temperature, [K]

- full [bool, optional] If False, calculates and returns only a\_alpha
- quick [bool, optional] Only the quick variant is implemented; it is little faster anyhow
- **pure\_a\_alphas** [bool, optional] Whether or not to recalculate the a\_alpha terms of pure components (for the case of mixtures only) which stay the same as the composition changes (i.e in a PT flash), [-]

#### Returns

- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

#### Notes

The exact expressions can be obtained with the following SymPy expression below, commented out for brevity.

```
>>> from sympy import *
>>> kij, T = symbols('kij, T ')
>>> a_alpha_i, a_alpha_j = symbols('a_alpha_i, a_alpha_j', cls=Function)
>>> a_alpha_ij = (1-kij)*sqrt(a_alpha_i(T)*a_alpha_j(T))
>>> diff(a_alpha_ij, T)
>>> diff(a_alpha_ij, T, T)
```

## property a\_alpha\_ijs

Calculate and return the matrix  $(a\alpha)_{ij} = (1 - k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$ .

#### Returns

**a\_alpha\_ijs** [list[list[float]]] *a\_alpha* terms for each component with every other component, [J^2/mol^2/Pa]

In an earlier implementation this matrix was stored each EOS solve; however, allocating that much memory becomes quite expensive for large number of component cases and this is now calculated on-demand only.

#### d2G\_dep\_dninjs(Z)

Calculates the molar departure Gibbs energy mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial^2 G_{dep}}{\partial n_j \partial n_i}\right)_{T,P,n_{i,j\neq k}} = f\left(\left(\frac{\partial^2 G_{dep}}{\partial x_j \partial x_i}\right)_{T,P,x_{i,j\neq k}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

Returns

**d2G\_dep\_dninjs** [float] Departure Gibbs energy second mole number derivatives, [J/mol^3]

#### d2G\_dep\_dzizjs(Z)

Calculates the molar departure Gibbs energy second composition derivative (where the mole fractions do not sum to 1). Verified numerically. Useful in solving for gibbs minimization calculations or for solving for the true critical point. Also forms the basis for the molar departure Gibbs energy mole second number derivative.

$$\left(\frac{\partial^2 G_{dep}}{\partial x_j \partial x_i}\right)_{T,P,x_{i,j \neq k}} = \text{run SymPy code to obtain - very long!}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

## Returns

**d2G\_dep\_dzizjs** [float] Departure Gibbs free energy second composition derivatives, [J/mol]

#### Notes

The derivation for the derivative is performed as follows using SymPy. The function source code is an optimized variant created with the *cse* SymPy function, and hand optimized further.

```
>>> from sympy import *
>>> P, T, R, x1, x2 = symbols('P, T, R, x1, x2')
>>> a_alpha, delta, epsilon, V, b = symbols('a\ \\alpha, delta, epsilon, V, b',__
..., cls=Function)
>>> da_alpha_dT, d2a_alpha_dT2 = symbols('da_alpha_dT, d2a_alpha_dT2',__
..., cls=Function)
>>> S_dep = R*log(P*V(x1, x2)/(R*T)) + R*log(V(x1, x2)-b(x1, x2))+2*da_alpha_
..., dT(x1, x2)*atanh((2*V(x1, x2)+delta(x1, x2))/sqrt(delta(x1, x2)*2-
..., 4*epsilon(x1, x2))/sqrt(delta(x1, x2)*2-4*epsilon(x1, x2))-R*log(V(x1, x2))
>>> H_dep = P*V(x1, x2) - R*T + 2*atanh((2*V(x1, x2)+delta(x1, x2))/
..., sqrt(delta(x1, x2)**2-4*epsilon(x1, x2)))*(da_alpha_dT(x1, x2)*T-a_alpha(x1, ..., x2))/sqrt(delta(x1, x2)**2-4*epsilon(x1, x2))
>>> G_dep = simplify(H_dep - T*S_dep)
>>> diff(G_dep, x1, x2)
```

### d2V\_dninjs(Z)

Calculates the molar volume second mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the second mole fraction derivatives.

$$\left(\frac{\partial^2 V}{\partial n_i \partial n_j}\right)_{T,P,n_{k \neq i,j}} = f\left(\left(\frac{\partial^2 V}{\partial x_i \partial x_j}\right)_{T,P,x_{k \neq i,j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

**d2V\_dninjs** [float] Molar volume second mole number derivatives, [m^3/mol^3]

#### d2V\_dzizjs(Z)

Calculates the molar volume second composition derivative (where the mole fractions do not sum to 1). Verified numerically. Used in many other derivatives, and for the molar volume second mole number derivative.

$$\left(\frac{\partial^2 V}{\partial x_i \partial x_j}\right)_{T,P,x_{k \neq i,j}} = \text{run SymPy code to obtain - very long!}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

## Returns

d2V\_dzizjs [float] Molar volume second composition derivatives, [m^3/mol]

## **Notes**

The derivation for the derivative is performed as follows using SymPy. The function source code is an optimized variant created with the *cse* SymPy function, and hand optimized further.

#### property d2a\_alpha\_dT2\_dns

Helper method for calculating the mole number derivatives of *d2a\_alpha\_dT2*. Note this is independent of the phase.

$$\left(\frac{\partial^3 a\alpha}{\partial n_i \partial T^2}\right)_{P,n_{i\neq j}} = f\left(\left(\frac{\partial^3 a\alpha}{\partial z_i \partial T^2}\right)_{P,z_{i\neq j}}\right)$$

Returns

**d2a\_alpha\_dT2\_dns** [list[float]] Mole number derivative of *d2a\_alpha\_dT2* of each component, [kg\*m^5/(mol^3\*s^2\*K^2)]

This derivative is checked numerically.

## property d2a\_alpha\_dT2\_dzs

Helper method for calculating the mole number derivatives of *d2a\_alpha\_dT2*. Note this is independent of the phase.

$$\left(\frac{\partial^3 a \alpha}{\partial z_i \partial T^2}\right)_{P, z_i \neq j} = \text{large expression}$$

Returns

**d2a\_alpha\_dT2\_dzs** [list[float]] Composition derivative of *d2a\_alpha\_dT2* of each component, [kg\*m^5/(mol^2\*s^2\*K^2)]

## Notes

This derivative is checked numerically.

## property d2a\_alpha\_dT2\_ijs

Calculate and return the matrix of the second temperature derivatives of the alpha terms.

$$\frac{\partial^2 (a\alpha)_{ij}}{\partial T^2} = -\frac{\sqrt{a\alpha_i (T) a\alpha_j (T)} (k_{ij} - 1) \left(\frac{\left(a\alpha_i (T) \frac{d}{dT} a\alpha_j (T) + a\alpha_j (T) \frac{d}{dT} a\alpha_i (T)\right)^2}{4 a\alpha_i (T) a\alpha_j (T)} - \frac{\left(a\alpha_i (T) \frac{d}{dT} a\alpha_j (T) + a\alpha_j (T) \frac{d}{dT} a\alpha_i (T)\right) \frac{d}{dT} a\alpha_i (T)\right)^2}{2 a\alpha_j (T)}}{2 a\alpha_j (T)}$$

Returns

**d2a\_alpha\_dT2\_ijs** [list[list[float]]] Second temperature derivative of *a\_alpha* terms for each component with every other component, [J^2/mol^2/Pa/K^2]

#### Notes

In an earlier implementation this matrix was stored each EOS solve; however, allocating that much memory becomes quite expensive for large number of component cases and this is now calculated on-demand only.

## property d2a\_alpha\_dninjs

Helper method for calculating the second partial molar derivatives of *a\_alpha* (hessian). Note this is independent of the phase.

$$\begin{pmatrix} \frac{\partial^2 a\alpha}{\partial n_i \partial n_j} \end{pmatrix}_{T,P,n_{k \neq i,j}} = 2 \left[ 3(a\alpha) + (a\alpha)_{ij} - 2(\operatorname{term}_{i,j}) \right]$$
$$\operatorname{term}_{i,j} = \sum_k z_k \left( (a\alpha)_{ik} + (a\alpha)_{jk} \right)$$
$$(a\alpha)_{ij} = (1 - k_{ij}) \sqrt{(a\alpha)_i (a\alpha)_j}$$

Returns

**d2a\_alpha\_dninjs** [list[float]] Second partial molar derivative of *alpha* of each component, [kg\*m^5/(mol^4\*s^2)]

This derivative is checked numerically.

## property d2a\_alpha\_dzizjs

Helper method for calculating the second composition derivatives of *a\_alpha* (hessian). Note this is independent of the phase.

$$\left(\frac{\partial^2 a\alpha}{\partial x_i \partial x_j}\right)_{T,P,x_{k\neq i,j}} = 2(1-k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$$

#### Returns

**d2a\_alpha\_dzizjs** [list[float]] Second composition derivative of *alpha* of each component, [kg\*m^5/(mol^2\*s^2)]

## Notes

This derivative is checked numerically.

## property d2b\_dninjs

Helper method for calculating the second partial mole number derivatives of *b*. Note this is independent of the phase.

$$\left(\frac{\partial^2 b}{\partial n_i \partial n_j}\right)_{T,P,n_k \neq i,k} = 2b - b_i - b_j$$

#### Returns

**d2b\_dninjs** [list[list[float]]] Second Composition derivative of *b* of each component, [m^3/mol^3]

## **Notes**

This derivative is checked numerically.

#### property d2b\_dzizjs

Helper method for calculating the second partial mole fraction derivatives of *b*. Note this is independent of the phase.

$$\left(\frac{\partial^2 b}{\partial x_i \partial x_j}\right)_{T,P,n_{k \neq i,j}} = 0$$

## Returns

**d2b\_dzizjs** [list[list[float]]] Second mole fraction derivatives of *b* of each component, [m^3/mol]

This derivative is checked numerically.

## d2lnphi\_dninjs(Z)

Calculates the mixture log *fugacity coefficient* second mole number derivatives (where the mole fraction sum to 1). No specific formula is implemented for this property - it is calculated from the second mole fraction derivative of Gibbs free energy.

$$\left(\frac{\partial^2 \ln \phi}{\partial n_i \partial n_j}\right)_{T,P,n_{i,j\neq k}} f\left(\left(\frac{\partial^2 G_{dep}}{\partial x_j \partial x_i}\right)_{T,P,x_{i,j\neq k}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

d2lnphi\_dninjs [float] Mixture log fugacity coefficient second mole number derivatives, [-]

## d2lnphi\_dzizjs(Z)

Calculates the mixture log *fugacity coefficient* second mole fraction derivatives (where the mole fractions do not sum to 1). No specific formula is implemented for this property - it is calculated from the second mole fraction derivative of Gibbs free energy.

$$\left(\frac{\partial^2 \ln \phi}{\partial x_i \partial x_j}\right)_{T,P,x_{i,j\neq k}} = \frac{1}{RT} \left( \left(\frac{\partial^2 G_{dep}}{\partial x_j \partial x_i}\right)_{T,P,x_{i,j\neq k}} \right)$$

## **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

d2lnphi\_dzizjs [float] Mixture log fugacity coefficient second mole fraction derivatives, [-]

### property d3a\_alpha\_dninjnks

Helper method for calculating the third mole number derivatives of  $a_alpha$ . Note this is independent of the phase.

$$\left(\frac{\partial^3 a\alpha}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 4 \left(-6(a\alpha) - \left[(a\alpha)_{i,j} + (a\alpha)_{i,k} + (a\alpha)_{j,k}\right] + 3\sum_m z_m \left[(a\alpha)_{i,m} + (a\alpha)_{j,m} + (a\alpha)_{k,m}\right]\right)$$

Returns

**d3a\_alpha\_dninjnks** [list[float]] Third mole number derivative of *alpha* of each component, [kg\*m^5/(mol^5\*s^2)]

## Notes

This derivative is checked numerically.

#### property d3a\_alpha\_dzizjzks

Helper method for calculating the third composition derivatives of  $a_alpha$ . Note this is independent of the phase.

$$\left(\frac{\partial^3 a\alpha}{\partial x_i \partial x_j \partial x_k}\right)_{T,P,x_{m \neq i,j,k}} = 0$$

## Returns

**d3a\_alpha\_dzizjzks** [list[float]] Third composition derivative of *alpha* of each component, [kg\*m^5/(mol^2\*s^2)]

#### Notes

This derivative is checked numerically.

## property d3b\_dninjnks

Helper method for calculating the third partial mole number derivatives of *b*. Note this is independent of the phase.

$$\left(\frac{\partial^3 b}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 2(-3b + b_i + b_j + b_k)$$

## Returns

**d3b\_dninjnks** [list[list[float]]]] Third mole number derivative of *b* of each component, [m^3/mol^4]

## Notes

This derivative is checked numerically.

## property d3b\_dzizjzks

Helper method for calculating the third partial mole fraction derivatives of *b*. Note this is independent of the phase.

$$\left(\frac{\partial^3 b}{\partial x_i \partial x_j \partial x_k}\right)_{T,P,n_{k \neq i,j,k}} = 0$$

#### Returns

**d3b\_dzizjzks** [list[list[float]]]] Third mole fraction derivatives of *b* of each component, [m^3/mol]

#### Notes

This derivative is checked numerically.

#### property d3delta\_dzizjzks

Helper method for calculating the third composition derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \delta}{\partial x_i \partial x_j \partial x_k}\right)_{T,P,x_{m \neq i,j,k}} = 0$$

#### Returns

**d3delta\_dzizjzks** [list[list[list[float]]]] Third composition derivative of *epsilon* of each component, [m^6/mol^5]

This derivative is checked numerically.

## property d3epsilon\_dzizjzks

Helper method for calculating the third composition derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \epsilon}{\partial x_i \partial x_j \partial x_k}\right)_{T, P, x_m \neq i, j, k} = 0$$

#### Returns

**d2epsilon\_dzizjzks** [list[list[float]]]] Composition derivative of *epsilon* of each component,  $[m^6/mol^2]$ 

## **Notes**

This derivative is checked numerically.

## $dG_dep_dns(Z)$

Calculates the molar departure Gibbs energy mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial G_{dep}}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial G_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

Apart from the ideal term, this is the formulation for chemical potential.

## **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dG\_dep\_dns [float] Departure Gibbs energy mole number derivatives, [J/mol^2]

### $dG_dep_dzs(Z)$

Calculates the molar departure Gibbs energy composition derivative (where the mole fractions do not sum to 1). Verified numerically. Useful in solving for gibbs minimization calculations or for solving for the true critical point. Also forms the basis for the molar departure Gibbs energy mole number derivative and molar partial departure Gibbs energy.

$$\left(\frac{\partial G_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}} = P\frac{d}{dx}V(x) - \frac{RT\left(\frac{d}{dx}V(x) - \frac{d}{dx}b(x)\right)}{V(x) - b(x)} - \frac{2\left(-\delta(x)\frac{d}{dx}\delta(x) + 2\frac{d}{dx}\epsilon(x)\right)\alpha\left(x\right)\operatorname{atanh}\left(\frac{2V(x)}{\sqrt{\delta^2(x) - 4\epsilon(x)}}\right)}{\left(\delta^2(x) - 4\epsilon(x)\right)^{\frac{3}{2}}}$$

## Parameters

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dG\_dep\_dzs [float] Departure Gibbs free energy composition derivatives, [J/mol]

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The derivation for the derivative is performed as follows using SymPy. The function source code is an optimized variant created with the *cse* SymPy function, and hand optimized further.

```
>>> from sympy import *
>>> P, T, R, x = symbols('P, T, R, x')
>>> a_alpha, a, delta, epsilon, V, b, da_alpha_dT = symbols('a\ \\alpha, a,_
→delta, epsilon, V, b, da_alpha_dT', cls=Function)
>>> S_dep = R^{1}\log(P^{V}(x)/(R^{T})) + R^{1}\log(V(x)-b(x))+2^{da_alpha_}
\rightarrow dT(x)*atanh((2*V(x)+delta(x))/sqrt(delta(x)*2-4*epsilon(x)))/
\rightarrow sqrt(delta(x)**2-4*epsilon(x))-R*log(V(x))
>>> H_dep = P*V(x) - R*T + 2*atanh((2*V(x)+delta(x))/sqrt(delta(x)**2-
\rightarrow4*epsilon(x)))*(da_alpha_dT(x)*T-a_alpha(x))/sqrt(delta(x)**2-4*epsilon(x)))
>>> G_dep = simplify(H_dep - T*S_dep)
>>> diff(G_dep, x)
P*Derivative(V(x), x) - R*T*(Derivative(V(x), x) - Derivative(b(x), x))/(V(x) -
→b(x)) - 2*(-delta(x)*Derivative(delta(x), x) + 2*Derivative(epsilon(x), x))*a_

¬\alpha(x)*atanh(2*V(x)/sqrt(delta(x)**2 - 4*epsilon(x)) + delta(x)/
→ sqrt(delta(x)**2 - 4*epsilon(x)))/(delta(x)**2 - 4*epsilon(x))**(3/2) -
\rightarrow2*atanh(2*V(x)/sqrt(delta(x)**2 - 4*epsilon(x)) + delta(x)/sqrt(delta(x)**2 -
\rightarrow4*epsilon(x)))*Derivative(a \alpha(x), x)/sqrt(delta(x)**2 - 4*epsilon(x)) -
\rightarrow 2^{(2^{(-delta(x))^{Derivative(delta(x), x) + 2^{Derivative(epsilon(x), x))^{V(x)/}}
\rightarrow (delta(x)**2 - 4*epsilon(x))**(3/2) + (-delta(x)*Derivative(delta(x), x) +
\rightarrow 2*Derivative(epsilon(x), x))*delta(x)/(delta(x)**2 - 4*epsilon(x))**(3/2) +
\rightarrow 2*Derivative(V(x), x)/sqrt(delta(x)**2 - 4*epsilon(x)) + Derivative(delta(x),
\rightarrow x/sqrt(delta(x)**2 - 4*epsilon(x)))*a \alpha(x)/((1 - (2*V(x)/
\rightarrow sqrt(delta(x)**2 - 4*epsilon(x)) + delta(x)/sqrt(delta(x)**2 -
```

#### $dH_dep_dns(Z)$

Calculates the molar departure enthalpy mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial H_{dep}}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial H_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dH\_dep\_dns [float] Departure enthalpy mole number derivatives, [J/mol^2]

#### $dH_dep_dzs(Z)$

Calculates the molar departure enthalpy composition derivative (where the mole fractions do not sum to 1). Verified numerically. Useful in solving for enthalpy specifications in newton-type methods, and forms the basis for the molar departure enthalpy mole number derivative and molar partial departure enthalpy.

$$\left(\frac{\partial H_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}} = P\frac{d}{dx}V(x) + \frac{2\left(T\frac{\partial}{\partial T}\operatorname{a}\alpha\left(T,x\right) - \operatorname{a}\alpha\left(x\right)\right)\left(-\delta(x)\frac{d}{dx}\delta(x) + 2\frac{d}{dx}\epsilon(x)\right)\operatorname{atanh}\left(\frac{2V(x) + \delta(x)}{\sqrt{\delta^2(x) - 4\epsilon(x)}}\right)}{\left(\delta^2(x) - 4\epsilon(x)\right)^{\frac{3}{2}}} + \frac{2}{\left(\delta^2(x) - 4\epsilon(x)\right)^{\frac{3}{2}}}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dH\_dep\_dzs [float] Departure enthalpy composition derivatives, [J/mol]

## Notes

The derivation for the derivative is performed as follows using SymPy. The function source code is an optimized variant created with the *cse* SymPy function, and hand optimized further.

```
>>> from sympy import *
>>> P, T, V, R, b, a, delta, epsilon, x = symbols('P, T, V, R, b, a, delta,
\rightarrowepsilon, x')
>>> V, delta, epsilon, a_alpha, b = symbols('V, delta, epsilon, a_alpha, b',__
\rightarrow cls=Function)
>>> H_dep = (P*V(x) - R*T + 2/sqrt(delta(x)**2 - 4*epsilon(x))*(T*Derivative(a_
\rightarrowalpha(T, x), T)
... - a_alpha(x))*atanh((2*V(x)+delta(x))/sqrt(delta(x)**2-4*epsilon(x))))
>>> diff(H_dep, x)
P*Derivative(V(x), x) + 2*(T*Derivative(a \alpha(T, x), T) - a \alpha(x))*(-

→delta(x)*Derivative(delta(x), x) + 2*Derivative(epsilon(x), x))*atanh((2*V(x))

    delta(x))/sqrt(delta(x)**2 - 4*epsilon(x)))/(delta(x)**2 -

\rightarrow4*epsilon(x))**(3/2) + 2*(T*Derivative(a \alpha(T, x), T) - a \alpha(x))*((-
→delta(x)*Derivative(delta(x), x) + 2*Derivative(epsilon(x), x))*(2*V(x) +
\rightarrow delta(x)/(delta(x)**2 - 4*epsilon(x))**(3/2) + (2*Derivative(V(x), x) +
\rightarrow Derivative(delta(x), x))/sqrt(delta(x)**2 - 4*epsilon(x)))/((-(2*V(x) +
\rightarrow delta(x))*2/(delta(x)*2 - 4*epsilon(x)) + 1)*sqrt(delta(x)*2 -
\rightarrow4*epsilon(x))) + 2*(T*Derivative(a \alpha(T, x), T, x) - Derivative(a \
\rightarrowalpha(x), x))*atanh((2*V(x) + delta(x))/sqrt(delta(x)**2 - 4*epsilon(x)))/

sqrt(delta(x)**2 - 4*epsilon(x))
```

#### $dS_dep_dns(Z)$

Calculates the molar departure entropy mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial S_{dep}}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial S_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dS\_dep\_dns [float] Departure entropy mole number derivatives, [J/mol^2/K]

#### dS\_dep\_dzs(Z)

Calculates the molar departure entropy composition derivative (where the mole fractions do not sum to 1). Verified numerically. Useful in solving for entropy specifications in newton-type methods, and forms the basis for the molar departure entropy mole number derivative and molar partial departure entropy.

$$\left(\frac{\partial S_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}} = \frac{1}{T} \left( \left(\frac{\partial H_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}} - \left(\frac{\partial G_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}} \right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dS\_dep\_dzs [float] Departure entropy composition derivatives, [J/mol/K]

 $dV_dns(Z)$ 

Calculates the molar volume mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial V}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial V}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

**Parameters** 

Z [float] Compressibility of the mixture for a desired phase, [-]

Returns

dV\_dns [float] Molar volume mole number derivatives, [m^3/mol^2]

 $dV_dzs(Z)$ 

Calculates the molar volume composition derivative (where the mole fractions do not sum to 1). Verified numerically. Used in many other derivatives, and for the molar volume mole number derivative and partial molar volume calculation.

$$\left(\frac{\partial V}{\partial x_i}\right)_{T,P,x_{i\neq j}} = \frac{-RT\left(V^2(x) + V(x)\delta(x) + \epsilon(x)\right)^3 \frac{d}{dx}b(x) + (V(x) - b(x))^2 \left(V^2(x) + V(x)\delta(x) + \epsilon(x)\right)^2 \frac{d}{dx}a\alpha(x)}{-RT\left(V^2(x) + V(x)\delta(x) + \epsilon(x)\right)^3 - \epsilon^2}$$

Parameters

Z [float] Compressibility of the mixture for a desired phase, [-]

Returns

dV\_dzs [float] Molar volume composition derivatives, [m^3/mol]

#### Notes

The derivation for the derivative is performed as follows using SymPy. The function source code is an optimized variant created with the *cse* SymPy function, and hand optimized further.

```
>>> from sympy import *
>>> P, T, R, x = symbols('P, T, R, x')
>>> V, delta, epsilon, a_alpha, b = symbols('V, delta, epsilon, a\ \\alpha, b',
\rightarrow cls=Function)
>>> CUBIC = R*T/(V(x) - b(x)) - a_alpha(x)/(V(x)*V(x) + delta(x)*V(x) +__
\rightarrowepsilon(x)) - P
>>> solve(diff(CUBIC, x), Derivative(V(x), x))
[(-R*T*(V(x)*2 + V(x)*delta(x) + epsilon(x))**3*Derivative(b(x), x) + (V(x) - 
\rightarrowb(x))*2*(V(x)*2 + V(x)*delta(x) + epsilon(x))*2*Derivative(a \alpha), x).
\rightarrow (V(x) - b(x))**2*V(x)**3*a \alpha(x)*Derivative(delta(x), x) - (V(x) -
\rightarrowb(x))*2*V(x)*2*a \alpha(x)*delta(x)*Derivative(delta(x), x) - (V(x) -
\rightarrow b(x))**2*V(x)**2*a \alpha(x)*Derivative(epsilon(x), x) - (V(x) -
\rightarrow b(x))*2*V(x)*a \alpha(x)*delta(x)*Derivative(epsilon(x), x) - (V(x) -
\rightarrow b(x) *2*V(x)*a \alpha(x)*epsilon(x)*Derivative(delta(x), x) - (V(x) -
\rightarrow b(x))**2*a \alpha(x)*epsilon(x)*Derivative(epsilon(x), x))/(-R*T*(V(x)**2 +
\rightarrow V(x)*delta(x) + epsilon(x))**3 + 2*(V(x) - b(x))**2*V(x)**3*a \alpha(x) +
\rightarrow 3^{*}(V(x) - b(x))^{*2}V(x)^{*2}a \ (alpha(x)^{*}delta(x) + (V(x) - b(x))^{*2}V(x)^{*a} \ (x)^{*a}
\rightarrowalpha(x)*delta(x)**2 + 2*(V(x) - b(x))**2*V(x)*a \alpha(x)*epsilon(x) + (V(x))

→- b(x))**2*a \alpha(x)*delta(x)*epsilon(x))]
```

## $dZ_dns(Z)$

Calculates the compressibility mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial Z}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial Z}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

## Returns

dZ\_dns [float] Compressibility number derivatives, [1/mol]

#### $dZ_dzs(Z)$

Calculates the compressibility composition derivatives (where the mole fractions do not sum to 1). No specific formula is implemented for this property - it is calculated from the composition derivative of molar volume, which does have its formula implemented.

$$\left(\frac{\partial Z}{\partial x_i}\right)_{T,P,x_{i\neq j}} = \frac{P}{RT} \left(\frac{\partial V}{\partial x_i}\right)_{T,P,x_{i\neq j}}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dZ\_dzs [float] Compressibility composition derivative, [-]

## property da\_alpha\_dT\_dns

Helper method for calculating the mole number derivatives of  $da\_alpha\_dT$ . Note this is independent of the phase.

$$\left(\frac{\partial^2 a\alpha}{\partial n_i \partial T}\right)_{P,n_{i\neq j}} = 2\left[\sum_j -z_j(k_{ij}-1)(a\alpha)_i(a\alpha)_j\frac{\partial(a\alpha)_i}{\partial T}\frac{\partial(a\alpha)_j}{\partial T}\left((a\alpha)_i(a\alpha)_j\right)^{-0.5} - \frac{\partial a\alpha}{\partial T}\right]$$

#### Returns

**da\_alpha\_dT\_dns** [list[float]] Composition derivative of *da\_alpha\_dT* of each component, [kg\*m^5/(mol^3\*s^2\*K)]

#### **Notes**

This derivative is checked numerically.

## property da\_alpha\_dT\_dzs

Helper method for calculating the composition derivatives of  $da\_alpha\_dT$ . Note this is independent of the phase.

$$\left(\frac{\partial^2 a\alpha}{\partial x_i \partial T}\right)_{P,x_{i\neq j}} = 2\sum_j -z_j (k_{ij} - 1)(a\alpha)_i (a\alpha)_j \frac{\partial (a\alpha)_i}{\partial T} \frac{\partial (a\alpha)_j}{\partial T} \left((a\alpha)_i (a\alpha)_j\right)^{-0.5}$$

#### Returns

**da\_alpha\_dT\_dzs** [list[float]] Composition derivative of *da\_alpha\_dT* of each component, [kg\*m^5/(mol^2\*s^2\*K)]

This derivative is checked numerically.

## property da\_alpha\_dT\_ijs

Calculate and return the matrix for the temperature derivatives of the alpha terms.

$$\frac{\partial (a\alpha)_{ij}}{\partial T} = \frac{\sqrt{\mathrm{a}\alpha_{\mathrm{i}}\left(T\right)\mathrm{a}\alpha_{\mathrm{j}}\left(T\right)}\left(1-k_{ij}\right)\left(\frac{\mathrm{a}\alpha_{\mathrm{i}}\left(T\right)\frac{d}{dT}\,\mathrm{a}\alpha_{\mathrm{j}}\left(T\right)}{2}+\frac{\mathrm{a}\alpha_{\mathrm{j}}\left(T\right)\frac{d}{dT}\,\mathrm{a}\alpha_{\mathrm{i}}\left(T\right)}{2}\right)}{\mathrm{a}\alpha_{\mathrm{i}}\left(T\right)\mathrm{a}\alpha_{\mathrm{j}}\left(T\right)}$$

#### Returns

**da\_alpha\_dT\_ijs** [list[list[float]]] First temperature derivative of *a\_alpha* terms for each component with every other component, [J^2/mol^2/Pa/K]

#### Notes

In an earlier implementation this matrix was stored each EOS solve; however, allocating that much memory becomes quite expensive for large number of component cases and this is now calculated on-demand only.

#### property da\_alpha\_dns

Helper method for calculating the mole number derivatives of *a\_alpha*. Note this is independent of the phase.

$$\left(\frac{\partial a\alpha}{\partial n_i}\right)_{T,P,n_{i\neq j}} = 2(-a\alpha + \sum_j z_j(1-k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j})$$

Returns

**da\_alpha\_dns** [list[float]] Mole number derivative of *alpha* of each component, [kg\*m^5/(mol^3\*s^2)]

## Notes

This derivative is checked numerically.

## property da\_alpha\_dzs

Helper method for calculating the composition derivatives of  $a_alpha$ . Note this is independent of the phase.

$$\left(\frac{\partial a\alpha}{\partial x_i}\right)_{T,P,x_{i\neq j}} = 2 \cdot \sum_j z_j (1-k_{ij}) \sqrt{(a\alpha)_i (a\alpha)_j}$$

#### Returns

**da\_alpha\_dzs** [list[float]] Composition derivative of *alpha* of each component, [kg\*m^5/(mol^2\*s^2)]

This derivative is checked numerically.

#### property db\_dns

Helper method for calculating the mole number derivatives of b. Note this is independent of the phase.

$$\left(\frac{\partial b}{\partial n_i}\right)_{T,P,n_i\neq j} = b_i - b$$

#### Returns

**db\_dns** [list[float]] Composition derivative of *b* of each component, [m<sup>3</sup>/mol<sup>2</sup>]

## Notes

This derivative is checked numerically.

#### property db\_dzs

Helper method for calculating the composition derivatives of b. Note this is independent of the phase.

$$\left(\frac{\partial b}{\partial x_i}\right)_{T,P,x_{i\neq j}} = b_i$$

Returns

**db\_dzs** [list[float]] Composition derivative of *b* of each component, [m^3/mol]

#### Notes

This derivative is checked numerically.

### dfugacities\_dns(phase)

Generic formula for calculating the mole number derivatives of fugacities for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here.

$$\left(\frac{\partial f_i}{\partial n_i}\right)_{P,n_{j\neq i}}$$

#### **Parameters**

phase [str] One of 'l' or 'g', [-]

Returns

dfugacities\_dns [list[list[float]]] Mole number derivatives of fugacities for each species, [-]

#### dlnfugacities\_dns(phase)

Generic formula for calculating the mole number derivatives of log fugacities for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here.

$$\left(\frac{\partial \ln f_i}{\partial n_i}\right)_{P,n_{j\neq i}}$$

#### **Parameters**

phase [str] One of 'l' or 'g', [-]

Returns

**dlnfugacities\_dns** [list[float]]] Mole number derivatives of log fugacities for each species, [-]

#### dlnphi\_dns(Z)

Calculates the mixture log *fugacity coefficient* mole number derivatives (where the mole fractions sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative of Gibbs free energy.

$$\left(\frac{\partial \ln \phi}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial G_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

This property can be converted into a partial molar property to obtain the individual fugacity coefficients.

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

**dlnphi\_dns** [float] Mixture log fugacity coefficient mole number derivatives, [1/mol]

#### dlnphi\_dzs(Z)

Calculates the mixture log *fugacity coefficient* mole fraction derivatives (where the mole fractions do not sum to 1). No specific formula is implemented for this property - it is calculated from the mole fraction derivative of Gibbs free energy.

$$\left(\frac{\partial \ln \phi}{\partial x_i}\right)_{T,P,x_{i\neq j}} = \frac{1}{RT} \left( \left(\frac{\partial G_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}} \right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dlnphi\_dzs [float] Mixture log fugacity coefficient mole fraction derivatives, [-]

#### dlnphis\_dP(phase)

Generic formula for calculating the pressure derivative of log fugacity coefficients for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here.

Normally this routine is slower than EOS-specific ones, as it does not make assumptions that certain parameters are zero or equal to other parameters.

$$\left(\frac{\partial \ln \phi_i}{\partial P}\right)_{T,nj \neq i} = \frac{G_{dep}}{\partial P}_{T,n} + \left(\frac{\partial^2 \ln \phi}{\partial P \partial n_i}\right)_{T,P,n_{j \neq i}}$$

Parameters

phase [str] One of 'l' or 'g', [-]

Returns

dlnphis\_dP [float] Pressure derivatives of log fugacity coefficient for each species, [1/Pa]

This expression for the partial derivative of the mixture *lnphi* with respect to pressure and mole number can be derived as follows; to convert to the partial molar *lnphi* pressure and temperature derivative, add ::math:: $frac[G_{dep}]/(RT)$  [partial P]\_{T, n}.

```
>>> from sympy import *
>>> P, T, R, n = symbols('P, T, R, n')
>>> a_alpha, a, delta, epsilon, V, b, da_alpha_dT, d2a_alpha_dT2 = symbols('a_
→alpha, a, delta, epsilon, V, b, da_alpha_dT, d2a_alpha_dT2', cls=Function)
>>> S_dep = R*log(P*V(n, P)/(R*T)) + R*log(V(n, P)-b(n))+2*da_alpha_dT(n,_
Got State and Got State and Got State and State an
\Rightarrow sqrt(delta(n)**2-4*epsilon(n))-R*log(V(n, P))
>>> H_dep = P*V(n, P) - R*T + 2*atanh((2*V(n, P)+delta(n))/sqrt(delta(n)**2-
\rightarrow4*epsilon(n)))*(da_alpha_dT(n, T)*T-a_alpha(n, T))/sqrt(delta(n)**2-
\rightarrow4*epsilon(n))
>>> G_dep = H_dep - T*S_dep
>>> lnphi = simplify(G_dep/(R*T))
>>> diff(diff(lnphi, P), n)
P*Derivative(V(n, P), P, n)/(R*T) + Derivative(V(n, P), P, n)/V(n, P) -
\rightarrow P, n)/(V(n, P) - b(n)) - (-Derivative(V(n, P), n) + Derivative(b(n),
\rightarrown))*Derivative(V(n, P), P)/(V(n, P) - b(n))**2 + Derivative(V(n, P), n)/(R*T)
→- 4*(-2*delta(n)*Derivative(delta(n), n) + 4*Derivative(epsilon(n), n))*a_
→alpha(n, T)*Derivative(V(n, P), P)/(R*T*(1 - (2*V(n, P)/sqrt(delta(n)**2 -
\rightarrow4*epsilon(n)) + delta(n)/sqrt(delta(n)**2 - 4*epsilon(n)))**2)*(delta(n)**2 -
\rightarrow4*epsilon(n))**2) - 4*a_alpha(n, T)*Derivative(V(n, P), P, n)/(R*T*(1 -
\rightarrow (2*V(n, P)/sqrt(delta(n)**2 - 4*epsilon(n)) + delta(n)/sqrt(delta(n)**2 -
→4*epsilon(n)))**2)*(delta(n)**2 - 4*epsilon(n))) - 4*Derivative(V(n, P),
\rightarrow P)*Derivative(a_alpha(n, T), n)/(R*T*(1 - (2*V(n, P)/sqrt(delta(n)**2 -
\rightarrow4*epsilon(n)) + delta(n)/sqrt(delta(n)**2 - 4*epsilon(n)))**2)*(delta(n)**2 -
\rightarrow4*epsilon(n))) - 4*(2*V(n, P)/sqrt(delta(n)**2 - 4*epsilon(n)) + delta(n)/
→ sqrt(delta(n)**2 - 4*epsilon(n)))*(4*(-delta(n)*Derivative(delta(n), n) +
\rightarrow 2*Derivative(epsilon(n), n))*V(n, P)/(delta(n)**2 - 4*epsilon(n))**(3/2) +
\rightarrow 2^{*}(-delta(n) Derivative(delta(n), n) + 2^{*}Derivative(epsilon(n), n))^{*}delta(n)/
\rightarrow (delta(n)**2 - 4*epsilon(n))**(3/2) + 4*Derivative(V(n, P), n)/
→ sqrt(delta(n)**2 - 4*epsilon(n)) + 2*Derivative(delta(n), n)/sqrt(delta(n)**2
\rightarrow 4*epsilon(n)))*a_alpha(n, T)*Derivative(V(n, P), P)/(R*T*(1 - (2*V(n, P)/
→sqrt(delta(n)**2 - 4*epsilon(n)) + delta(n)/sqrt(delta(n)**2 -
→4*epsilon(n)))*2)*2*(delta(n)*2 - 4*epsilon(n))) + R*T*(P*Derivative(V(n,
\rightarrowP), P)/(R*T) + V(n, P)/(R*T))*Derivative(V(n, P), n)/(P*V(n, P)**2) -
\rightarrow R*T*(P*Derivative(V(n, P), P, n)/(R*T) + Derivative(V(n, P), n)/(R*T))/(P*V(n, P))
→ P))
```

## dlnphis\_dT(phase)

Generic formula for calculating the temperature derivative of log fugacity coefficients for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here.

Normally this routine is slower than EOS-specific ones, as it does not make assumptions that certain parameters are zero or equal to other parameters.

$$\left(\frac{\partial \ln \phi_i}{\partial T}\right)_{P,nj \neq i} = \frac{\frac{G_{dep}}{RT}}{\partial T}_{P,n} + \left(\frac{\partial^2 \ln \phi}{\partial T \partial n_i}\right)_{P,n_{j \neq i}}$$

Parameters

phase [str] One of 'l' or 'g', [-]

Returns

dlnphis\_dT [float] Temperature derivatives of log fugacity coefficient for each species, [1/K]

## **Notes**

This expression for the partial derivative of the mixture *lnphi* with respect to pressure and mole number can be derived as follows; to convert to the partial molar *lnphi* pressure and temperature derivative, add ::math:: $frac{G_{dep}}{RT}$ 

#### dlnphis\_dns(Z)

Generic formula for calculating the mole number derivatives of log fugacity coefficients for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here.

$$\left(\frac{\partial \ln \phi_i}{\partial n_i}\right)_{P,n_{j\neq i}}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

Returns

**dlnphis\_dns** [list[list[float]]] Mole number derivatives of log fugacity coefficient for each species, [-]

## dlnphis\_dzs(Z)

Generic formula for calculating the mole fraction derivatives of log fugacity coefficients for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here.

$$\left(\frac{\partial \ln \phi_i}{\partial z_i}\right)_{P, z_{i\neq j}}$$

#### Parameters

Z [float] Compressibility of the mixture for a desired phase, [-]

Returns

**dlnphis\_dzs** [list[list[float]]] Mole fraction derivatives of log fugacity coefficient for each species (such that the mole fractions do not sum to 1), [-]

## $dnG_dep_dns(Z)$

Calculates the partial molar departure Gibbs energy. No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial nG_{dep}}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial G_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dnG\_dep\_dns [float] Partial molar departure Gibbs energy of the phase, [J/mol]

## $dnH_dep_dns(Z)$

Calculates the partial molar departure enthalpy. No specific formula is implemented for this property - it is calculated from the mole fraction derivative.

$$\left(\frac{\partial nH_{dep}}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial H_{dep}}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

## Returns

dnH\_dep\_dns [float] Partial molar departure enthalpies of the phase, [J/mol]

## $dnV_dns(Z)$

Calculates the partial molar volume of the specified phase No specific formula is implemented for this property - it is calculated from the molar volume mole fraction derivative.

$$\left(\frac{\partial nV}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial V}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

dnV\_dns [float] Partial molar volume of the mixture of the specified phase, [m^3/mol]

## $dnZ_dns(Z)$

Calculates the partial compressibility of the specified phase No specific formula is implemented for this property - it is calculated from the compressibility mole fraction derivative.

$$\left(\frac{\partial nZ}{\partial n_i}\right)_{T,P,n_{i\neq j}} = f\left(\left(\frac{\partial Z}{\partial x_i}\right)_{T,P,x_{i\neq j}}\right)$$

## Parameters

Z [float] Compressibility of the mixture for a desired phase, [-]

## Returns

dnZ\_dns [float] Partial compressibility of the mixture of the specified phase, [-]

#### property dna\_alpha\_dT\_dns

Helper method for calculating the mole number derivatives of  $da\_alpha\_dT$ . Note this is independent of the phase.

$$\left(\frac{\partial^2 na\alpha}{\partial n_i \partial T}\right)_{P,n_{i\neq j}} = 2\left[\sum_j -z_j(k_{ij}-1)(a\alpha)_i(a\alpha)_j\frac{\partial(a\alpha)_i}{\partial T}\frac{\partial(a\alpha)_j}{\partial T}\left((a\alpha)_i(a\alpha)_j\right)^{-0.5} - 0.5\frac{\partial a\alpha}{\partial T}\right]$$

Returns

**dna\_alpha\_dT\_dns** [list[float]] Composition derivative of *da\_alpha\_dT* of each component, [kg\*m^5/(mol^2\*s^2\*K)]

## Notes

This derivative is checked numerically.

# property dna\_alpha\_dns

Helper method for calculating the partial molar derivatives of *a\_alpha*. Note this is independent of the phase.

$$\left(\frac{\partial a\alpha}{\partial n_i}\right)_{T,P,n_{i\neq j}} = 2(-0.5a\alpha + \sum_j z_j(1-k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j})$$

#### Returns

**dna\_alpha\_dns** [list[float]] Partial molar derivative of *alpha* of each component, [kg\*m^5/(mol^2\*s^2)]

#### Notes

This derivative is checked numerically.

#### property dnb\_dns

Helper method for calculating the partial molar derivative of b. Note this is independent of the phase.

$$\left(\frac{\partial n \cdot b}{\partial n_i}\right)_{T,P,n_{i \neq j}} = b_i$$

Returns

dnb\_dns [list[float]] Partial molar derivative of b of each component, [m^3/mol]

## Notes

This derivative is checked numerically.

#### classmethod from\_json(json\_repr)

Method to create a mixture cubic equation of state from a JSON friendly serialization of another mixture cubic equation of state.

## **Parameters**

json\_repr [dict] Json representation, [-]

#### Returns

eos\_mix [GCEOSMIX] Newly created object from the json serialization, [-]

It is important that the input string be in the same format as that created by GCEOS.as\_json.

## **Examples**

```
>>> import pickle
>>> eos = PRSV2MIX(Tcs=[507.6], Pcs=[3025000], omegas=[0.2975], zs=[1], T=299.,__
...
P=1E6, kappa1s=[0.05104], kappa2s=[0.8634], kappa3s=[0.460])
>>> json_stuff = pickle.dumps(eos.as_json())
>>> new_eos = GCEOSMIX.from_json(pickle.loads(json_stuff))
>>> assert new_eos == eos
```

## fugacities(only\_l=False, only\_g=False)

Helper method for calculating fugacity coefficients for any phases present, using either the overall mole fractions for both phases or using specified mole fractions for each phase.

Requires *fugacity\_coefficients* to be implemented by each subclassing EOS.

In addition to setting *fugacities\_l* and/or *fugacities\_g*, this also sets the fugacity coefficients *phis\_l* and/or *phis\_g*.

$$\hat{\phi}_{i}^{g} = \frac{\hat{f}_{i}^{g}}{y_{i}P}$$
$$\hat{\phi}_{i}^{l} = \frac{\hat{f}_{i}^{l}}{x_{i}P}$$

Note that in a flash calculation, each phase requires their own EOS object.

1

#### **Parameters**

- **only\_l** [bool] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set.
- **only\_g** [bool] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set.

#### Notes

It is helpful to check that *fugacity\_coefficients* has been implemented correctly using the following expression, from [1].

$$\ln \hat{\phi}_i = \left[\frac{\partial(n\ln\phi)}{\partial n_i}\right]_{T,P,n_j,V_i}$$

For reference, several expressions for fugacity of a component are as follows, shown in [1] and [2].

$$\ln \hat{\phi}_i = \int_0^P \left(\frac{\hat{V}_i}{RT} - \frac{1}{P}\right) dP$$
$$\ln \hat{\phi}_i = \int_V^\infty \left[\frac{1}{RT} \frac{\partial P}{\partial n_i} - \frac{1}{V}\right] dV - \ln Z$$

## References

[1], [2]

## fugacity\_coefficients(Z)

Generic formula for calculating log fugacity coefficients for each species in a mixture. Verified numerically. Applicable to all cubic equations of state which can be cast in the form used here. Normally this routine is slower than EOS-specific ones, as it does not make assumptions that certain parameters are zero or equal to other parameters.

$$\left(\frac{\partial n \ln \phi}{\partial n_i}\right)_{n_{k\neq i}} = \ln \phi_i = \ln \phi + n \left(\frac{\partial \ln \phi}{\partial n_i}\right)_{n_{k\neq i}}$$
$$\left(\frac{\partial \ln \phi}{\partial n_i}\right)_{T,P,n_{i\neq j}} = \frac{1}{RT} \left(\left(\frac{\partial G_{dep}}{\partial n_i}\right)_{T,P,n_{i\neq j}}\right)$$

## Parameters

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

log\_phis [float] Log fugacity coefficient for each species, [-]

## kwargs\_linear = ()

Tuple of 1D arguments used by the specific EOS in addition to the conventional ones.

## kwargs\_square = ('kijs',)

Tuple of 2D arguments used by the specific EOS.

## mechanical\_critical\_point()

Method to calculate the mechanical critical point of a mixture of defined composition.

The mechanical critical point is where:

$$\frac{\partial P}{\partial \rho}|_T = \frac{\partial^2 P}{\partial \rho^2}|_T = 0$$

## Returns

T [float] Mechanical critical temperature, [K]

P [float] Mechanical critical temperature, [Pa]

#### Notes

One useful application of the mechanical critical temperature is that the phase identification approach of Venkatarathnam is valid only up to it.

Note that the equation of state, when solved at these conditions, will have fairly large (1e-3 - 1e-6) results for the derivatives; but they are the minimum. This is just from floating point precision.

It can also be checked looking at the calculated molar volumes - all three (available with sorted\_volumes) will be very close (1e-5 difference in practice), again differing because of floating point error.

The algorithm here is a custom implementation, using Newton-Raphson's method with the initial guesses described in [1] (mole-weighted critical pressure average, critical temperature average using a quadratic mixing rule). Normally ~4 iterations are needed to solve the system. It is relatively fast, as only one evaluation of  $a_alpha$  and  $da_alpha_dT$  are needed per call to function and its jacobian.

## References

[1], [2]

```
mix_kwargs_to_pure = {}
```

## multicomponent = True

All inherited classes of GCEOSMIX are multicomponent.

```
nonstate_constants = ('N', 'cmps', 'Tcs', 'Pcs', 'omegas', 'kijs', 'kwargs', 'ais',
'bs')
```

## property pseudo\_Pc

Apply a linear mole-fraction mixing rule to compute the average critical pressure, [Pa].

## **Examples**

```
>>> base = RKMIX(T=150.0, P=4e6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

→omegas=[0.04, 0.011], zs=[0.6, 0.4])

>>> base.pseudo_Pc

3878000.0
```

## property pseudo\_Tc

Apply a linear mole-fraction mixing rule to compute the average critical temperature, [K].

## **Examples**

```
>>> base = RKMIX(T=150.0, P=4e6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], 

→omegas=[0.04, 0.011], zs=[0.6, 0.4])
>>> base.pseudo_Tc
151.9
```

## property pseudo\_a

Apply a linear mole-fraction mixing rule to compute the average *a* coefficient, [-].

## **Examples**

```
>>> base = RKMIX(T=150.0, P=4e6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

→omegas=[0.04, 0.011], zs=[0.6, 0.4])
>>> base.pseudo_a
0.17634464184
```

## property pseudo\_omega

Apply a linear mole-fraction mixing rule to compute the average omega, [-].

## **Examples**

```
>>> base = RKMIX(T=150.0, P=4e6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

→omegas=[0.04, 0.011], zs=[0.6, 0.4])
>>> base.pseudo_omega
0.0284
```

## pures()

Helper method which returns a list of pure *EOSs* at the same *T* and *P* and base EOS as the mixture.

## Returns

eos\_pures [list[eos]] A list of pure-species EOSs at the same T and P as the system, [-]

## Notes

This is useful for i.e. comparing mixture fugacities with the Lewis-Randall rule or when using an activity coefficient model which require pure component fugacities.

#### scalar = True

Whether the model is implemented using pure-Python lists of floats, or numpy arrays of float64.

## set\_dnzs\_derivatives\_and\_departures(n=True, x=True, only\_l=False, only\_g=False)

Sets a number of mole number and/or composition partial derivatives of thermodynamic partial derivatives.

The list of properties set is as follows, with all properties suffixed with '\_l' or '\_g'

if *n* is True: d2P\_dTdns, d2P\_dVdns, d2V\_dTdns, d2V\_dPdns, d2T\_dVdns, d2T\_dPdns, d3P\_dT2dns, d3P\_dV2dns, d3V\_dT2dns, d3V\_dP2dns, d3T\_dV2dns, d3T\_dP2dns, d3V\_dPdTdns, d3P\_dTdVdns, d3T\_dPdVdns, dV\_dep\_dns, dG\_dep\_dns, dH\_dep\_dns, dU\_dep\_dns, dS\_dep\_dns, dA\_dep\_dns

if *x* is True: d2P\_dTdzs, d2P\_dVdzs, d2V\_dTdzs, d2V\_dPdzs, d2T\_dVdzs, d2T\_dPdzs, d3P\_dT2dzs, d3P\_dV2dzs, d3V\_dT2dzs, d3V\_dP2dzs, d3T\_dV2dzs, d3T\_dP2dzs, d3V\_dPdTdzs, d3P\_dTdVdzs, d3T\_dPdVdzs, dV\_dep\_dzs, dG\_dep\_dzs, dH\_dep\_dzs, dU\_dep\_dzs, dS\_dep\_dzs, dA\_dep\_dzs

## Parameters

- **n** [bool, optional] Whether or not to set the mole number derivatives (sums up to one), [-]
- x [bool, optional] Whether or not to set the composition derivatives (does not sum up to one),
   [-]
- **only\_l** [bool, optional] Whether or not to set only the liquid-like phase properties (if there are two phases), [-]
- **only\_g** [bool, optional] Whether or not to set only the gas-like phase properties (if there are two phases), [-]

## solve\_T(P, V, quick=True, solution=None)

Generic method to calculate T from a specified P and V. Provides SciPy's *newton* solver, and iterates to solve the general equation for P, recalculating  $a_alpha$  as a function of temperature using  $a_alpha_and_derivatives$  each iteration.

## Parameters

- P [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]
- **quick** [bool, optional] Unimplemented, although it may be possible to derive explicit expressions as done for many pure-component EOS

**solution** [str or None, optional] 'l' or 'g' to specify a liquid of vapor solution (if one exists); if None, will select a solution more likely to be real (closer to STP, attempting to avoid temperatures like 60000 K or 0.0001 K).

## Returns

T [float] Temperature, [K]

```
stabiliy_iteration_Michelsen(T, P, zs, Ks_initial=None, maxiter=20, xtol=1e-12, liq=True)
```

```
subset(idxs, **state_specs)
```

Method to construct a new GCEOSMIX that removes all components not specified in the idxs argument.

## Parameters

idxs [list[int] or Slice] Indexes of components that should be included, [-]

## Returns

- **subset\_eos** [*GCEOSMIX*] Multicomponent *GCEOSMIX* at the same specified specs but with a composition normalized to 1 and with fewer components, [-]
- **state\_specs** [float] Keyword arguments which can be any of T, P, V, zs; zs is optional, as are (T, P, V), but if any of (T, P, V) are specified, a second one is required as well, [various]

## Notes

Subclassing equations of state require their *kwargs\_linear* and *kwargs\_square* attributes to be correct for this to work. *Tcs*, *Pcs*, and *omegas* are always assumed to be used.

## **Examples**

```
>>> kijs = [[0.0, 0.00076, 0.00171], [0.00076, 0.0, 0.00061], [0.00171, 0.00061,

... 0.0]]

>>> PR3 = PRMIX(Tcs=[469.7, 507.4, 540.3], zs=[0.8168, 0.1501, 0.0331],_

... omegas=[0.249, 0.305, 0.349], Pcs=[3.369E6, 3.012E6, 2.736E6], T=322.29,_

... P=101325.0, kijs=kijs)

>>> PR3.subset([1,2])

PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349],_

... kijs=[[0.0, 0.00061], [0.00061, 0.0]], zs=[0.8193231441048036, 0.

... 1806768558951965], T=322.29, P=101325.0)

>>> PR3.subset([1,2], T=500.0, P=1e5, zs=[.2, .8])

PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349],_

... kijs=[[0.0, 0.00061], [0.00061, 0.0]], zs=[0.2, 0.8], T=500.0, P=100000.0)

>>> PR3.subset([1,2], zs=[.2, .8])

PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349],_

... kijs=[[0.0, 0.00061], [0.00061, 0.0]], zs=[0.2, 0.8], T=500.0, P=100000.0)

>>> PR3.subset([1,2], zs=[.2, .8])

PRMIX(Tcs=[507.4, 540.3], Pcs=[3012000.0, 2736000.0], omegas=[0.305, 0.349],_

... kijs=[[0.0, 0.00061], [0.00061, 0.0]], zs=[0.2, 0.8], T=322.29, P=101325.0)
```

to(zs=None, T=None, P=None, V=None, fugacities=True)

Method to construct a new *GCEOSMIX* object at two of T, P or V with the specified composition. In the event the specs match those of the current object, it will be returned unchanged.

## **Parameters**

zs [list[float], optional] Mole fractions of EOS, [-]

**T** [float or None, optional] Temperature, [K]

P [float or None, optional] Pressure, [Pa]

V [float or None, optional] Molar volume, [m^3/mol]

fugacities [bool] Whether or not to calculate fugacities, [-]

### Returns

obj [GCEOSMIX] Pure component GCEOSMIX at the two specified specs, [-]

### Notes

Constructs the object with parameters Tcs, Pcs, omegas, and kwargs.

## **Examples**

```
>>> base = PRMIX(T=500.0, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

omegas=[0.04, 0.011], zs=[0.6, 0.4])

>>> base.to(T=300.0, P=1e9).state_specs

{'T': 300.0, 'P': 100000000.0}

>>> base.to(T=300.0, V=1.0).state_specs

{'T': 300.0, 'V': 1.0}

>>> base.to(P=1e5, V=1.0).state_specs

{'P': 100000.0, 'V': 1.0}
```

## $to_PV(P, V)$

Method to construct a new *GCEOSMIX* object at the specified P and V with the current composition. In the event the P and V match the current object's P and V, it will be returned unchanged.

#### Parameters

P [float] Pressure, [Pa]

V [float] Molar volume, [m^3/mol]

### Returns

obj [GCEOSMIX] Pure component GCEOSMIX at specified P and V, [-]

#### Notes

Constructs the object with parameters *Tcs*, *Pcs*, *omegas*, and *kwargs*.

## Examples

## to\_PV\_zs(P, V, zs, fugacities=True, only\_l=False, only\_g=False)

Method to construct a new *GCEOSMIX* instance at *P*, *V*, and *zs* with the same parameters as the existing object. Optionally, only one set of phase properties can be solved for, increasing speed. The fugacities calculation can be be skipped by by setting *fugacities* to False.

## Parameters

- P [float] Pressure, [Pa]
- V [float] Molar volume, [m^3/mol]
- zs [list[float]] Mole fractions of each component, [-]

fugacities [bool] Whether or not to calculate and set the fugacities of each component, [-]

**only\_l** [bool] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set.

**only\_g** [bool] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set.

## Returns

eos [GCEOSMIX] Multicomponent GCEOSMIX at the specified conditions [-]

## Notes

A check for whether or not P, V, and zs are the same as the existing instance is performed; if it is, the existing object is returned.

# Examples

```
>>> base = RKMIX(T=500.0, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

→ omegas=[0.04, 0.011], zs=[0.6, 0.4])

>>> base.to_PV_zs(V=0.004162, P=1e5, zs=[.1, 0.9])

RKMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011],

→ kijs=[[0.0, 0.0], [0.0, 0.0]], zs=[0.1, 0.9], P=100000.0, V=0.004162)
```

# $to_TP(T, P)$

Method to construct a new *GCEOSMIX* object at the specified T and P with the current composition. In the event the T and P match the current object's T and P, it will be returned unchanged.

## **Parameters**

- T [float] Temperature, [K]
- **P** [float] Pressure, [Pa]

# Returns

obj [GCEOSMIX] Pure component GCEOSMIX at specified T and P, [-]

## Notes

Constructs the object with parameters *Tcs*, *Pcs*, *omegas*, and *kwargs*.

## **Examples**

## to\_TPV\_pure(i, T=None, P=None, V=None)

Helper method which returns a pure EOSs at the specs (two of T, P and V) and base EOS as the mixture for a particular index.

## **Parameters**

i [int] Index of specified compound, [-]

T [float or None, optional] Specified temperature, [K]

P [float or None, optional] Specified pressure, [Pa]

V [float or None, optional] Specified volume, [m^3/mol]

## Returns

eos\_pure [eos] A pure-species EOSs at the two specified T, P, and V for component i, [-]

to\_TP\_zs(T, P, zs, fugacities=True, only\_l=False, only\_g=False)

Method to construct a new *GCEOSMIX* instance at T, P, and zs with the same parameters as the existing object. Optionally, only one set of phase properties can be solved for, increasing speed. The fugacities calculation can be be skipped by by setting *fugacities* to False.

## **Parameters**

- **T** [float] Temperature, [K]
- **P** [float] Pressure, [Pa]

zs [list[float]] Mole fractions of each component, [-]

fugacities [bool] Whether or not to calculate and set the fugacities of each component, [-]

**only\_l** [bool] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set.

**only\_g** [bool] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set.

#### Returns

eos [GCEOSMIX] Multicomponent GCEOSMIX at the specified conditions [-]

## Notes

A check for whether or not T, P, and zs are the same as the existing instance is performed; if it is, the existing object is returned.

### **Examples**

```
>>> base = RKMIX(T=500.0, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],_

omegas=[0.04, 0.011], zs=[0.6, 0.4])

>>> base.to_TP_zs(T=300, P=1e5, zs=[.1, 0.9])

RKMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011],_

okijs=[[0.0, 0.0], [0.0, 0.0]], zs=[0.1, 0.9], T=300, P=100000.0)
```

### to\_TP\_zs\_fast(T, P, zs, only\_l=False, only\_g=False, full\_alphas=True)

Method to construct a new *GCEOSMIX* instance with the same parameters as the existing object. If both instances are at the same temperature,  $a_alphas$  and  $da_alpha_dTs$  and  $d2a_alpha_dT2s$  are shared between the instances. It is always assumed the new object has a differet composition. Optionally, only one set of phase properties can be solved for, increasing speed. Additionally, if *full\_alphas* is set to False no temperature derivatives of  $a_alpha$  will be computed. Those derivatives are not needed in the context of a PT or PVF flash.

#### Parameters

- T [float] Temperature, [K]
- **P** [float] Pressure, [Pa]
- zs [list[float]] Mole fractions of each component, [-]
- **only\_l** [bool] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set.
- **only\_g** [bool] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set.

#### Returns

eos [GCEOSMIX] Multicomponent GCEOSMIX at the specified conditions [-]

# **Examples**

```
>>> base = RKMIX(T=500.0, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

omegas=[0.04, 0.011], zs=[0.6, 0.4])

>>> base.to_TP_zs_fast(T=300, P=1e5, zs=base.zs)

RKMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011],

okijs=[[0.0, 0.0], [0.0, 0.0]], zs=[0.6, 0.4], T=300, P=100000.0)
```

# $to_TV(T, V)$

Method to construct a new *GCEOSMIX* object at the specified T and V with the current composition. In the event the T and V match the current object's T and V, it will be returned unchanged.

### Parameters

T [float] Temperature, [K]

V [float] Molar volume, [m^3/mol]

## Returns

obj [GCEOSMIX] Pure component GCEOSMIX at specified T and V, [-]

Constructs the object with parameters Tcs, Pcs, omegas, and kwargs.

## **Examples**

#### to\_mechanical\_critical\_point()

Method to construct a new *GCEOSMIX* object at the current object's properties and composition, but which is at the mechanical critical point.

#### Returns

**obj** [GCEOSMIX] Pure component GCEOSMIX at mechanical critical point [-]

### **Examples**

```
>>> base = RKMIX(T=500.0, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],_

omegas=[0.04, 0.011], zs=[0.6, 0.4])

>>> base.to_mechanical_critical_point()

RKMIX(Tcs=[126.1, 190.6], Pcs=[3394000.0, 4604000.0], omegas=[0.04, 0.011],_

okijs=[[0.0, 0.0], [0.0, 0.0]], zs=[0.6, 0.4], T=151.861, P=3908737.9)
```

## translated = False

Whether or not the model implements volume translation.

# 7.8.2 Peng-Robinson Family EOSs

## **Standard Peng Robinson**

```
class thermo.eos_mix.PRMIX(Tcs, Pcs, omegas, zs, kijs=None, T=None, P=None, V=None, fugacities=True, 
only_l=False, only_g=False)
```

Bases: thermo.eos\_mix.GCEOSMIX, thermo.eos.PR

Class for solving the Peng-Robinson [1] [2] cubic equation of state for a mixture of any number of compounds. Subclasses *PR*. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$
$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1-k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$
$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = 0.45724 \frac{R^{2}T_{c,i}^{2}}{P_{c,i}}$$

$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_{i} = [1 + \kappa_{i}(1 - \sqrt{T_{r,i}})]^{2}$$

$$\kappa_{i} = 0.37464 + 1.54226\omega_{i} - 0.26992\omega_{i}^{2}$$

## Parameters

- Tcs [float] Critical temperatures of all compounds, [K]
- Pcs [float] Critical pressures of all compounds, [Pa]
- omegas [float] Acentric factors of all compounds, [-]
- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

## Notes

For P-V initializations, a numerical solver is used to find T.

# References

## [1], [2]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

### Attributes

- *d2delta\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *delta*.
- **d2delta\_dzizjs** Helper method for calculating the second composition derivatives (hessian) of *delta*.
- *d2epsilon\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *epsilon*.
- *d2epsilon\_dzizjs* Helper method for calculating the second composition derivatives (hessian) of *epsilon*.
- **d3a\_alpha\_dT3** Method to calculate approximately the third temperature derivative of *a\_alpha* for the PR EOS.
- **d3delta\_dninjnks** Helper method for calculating the third partial mole number derivatives of *delta*.
- **d3epsilon\_dninjnks** Helper method for calculating the third partial mole number derivatives of *epsilon*.

*ddelta\_dns* Helper method for calculating the mole number derivatives of *delta*.

*ddelta\_dzs* Helper method for calculating the composition derivatives of *delta*.

depsilon\_dns Helper method for calculating the mole number derivatives of epsilon.

depsilon\_dzs Helper method for calculating the composition derivatives of epsilon.

## **Methods**

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i>
	and their first and second derivatives for the PR EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i>
	for the PR EOS.
d3a_alpha_dT3_vectorized(T)	Method to calculate the third temperature derivative
	of pure-component <i>a_alphas</i> for the PR EOS.
dlnphis_dP(phase)	Generic formula for calculating the pressure
	derivative of log fugacity coefficients for each
	species in a mixture for the Peng-Robinson EOS.
dlnphis_dT(phase)	Formula for calculating the temperature derivative of
	log fugacity coefficients for each species in a mixture
	for the Peng-Robinson equation of state.
dlnphis_dzs(Z)	Calculate and return the mole fraction derivatives of
	log fugacity coefficients for each species in a mixture.
eos_pure	alias of thermo.eos.PR
<pre>fugacity_coefficients(Z)</pre>	Literature formula for calculating fugacity coeffi-
	cients for each species in a mixture.

#### a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the PR EOS. This vectorized implementation is added for extra speed.

$$a\alpha = a\left(\kappa\left(-\frac{T^{0.5}}{Tc^{0.5}} + 1\right) + 1\right)^2$$
$$\frac{da\alpha}{dT} = -\frac{1.0a\kappa}{T^{0.5}Tc^{0.5}}\left(\kappa\left(-\frac{T^{0.5}}{Tc^{0.5}} + 1\right) + 1\right)$$

$$\frac{d^2 a \alpha}{dT^2} = 0.5 a \kappa \left( -\frac{1}{T^{1.5} T c^{0.5}} \left( \kappa \left( \frac{T^{0.5}}{T c^{0.5}} - 1 \right) - 1 \right) + \frac{\kappa}{T^{1.0} T c^{1.0}} \right)$$

## **Parameters**

T [float] Temperature, [K]

Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

# a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the PR EOS. This vectorized implementation is added for extra speed.

$$a\alpha = a\left(\kappa\left(-\frac{T^{0.5}}{Tc^{0.5}}+1\right)+1\right)^2$$

#### Parameters

T [float] Temperature, [K]

Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

### property d2delta\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial n_i \partial n_j}\right)_{T,P,n_{k \neq i,j}} = 4b - 2b_i - 2b_j$$

#### Returns

**d2delta\_dninjs** [list[list[float]]] Second mole number derivative of *delta* of each component, [m^3/mol^3]

### Notes

This derivative is checked numerically.

#### property d2delta\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial x_i \partial x_j}\right)_{T, P, x_{k \neq i, j}} = 0$$

### Returns

**d2delta\_dzizjs** [list[float]] Second Composition derivative of *delta* of each component, [m^3/mol]

This derivative is checked numerically.

## property d2epsilon\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \epsilon}{\partial n_i n_j}\right)_{T,P,n_{k\neq i,j}} = -2b(2b - b_i - b_j) - 2(b - b_i)(b - b_j)$$

#### Returns

**d2epsilon\_dninjs** [list[list[float]]] Second mole number derivative of *epsilon* of each component, [m^6/mol^4]

## Notes

This derivative is checked numerically.

## property d2epsilon\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \epsilon}{\partial x_i \partial x_j}\right)_{T,P,x_{k \neq i,j}} = 2b_i b_j$$

#### Returns

**d2epsilon\_dzizjs** [list[list[float]]] Second composition derivative of *epsilon* of each component, [m^6/mol^2]

## Notes

This derivative is checked numerically.

#### property d3a\_alpha\_dT3

Method to calculate approximately the third temperature derivative of *a\_alpha* for the PR EOS. A rigorous calculation has not been implemented.

## Parameters

T [float] Temperature, [K]

### Returns

d3a\_alpha\_dT3 [float] Third temperature derivative  $a\alpha$ , [J^2/mol^2/Pa/K^3]

### d3a\_alpha\_dT3\_vectorized(T)

Method to calculate the third temperature derivative of pure-component *a\_alphas* for the PR EOS. This vectorized implementation is added for extra speed.

#### **Parameters**

T [float] Temperature, [K]

## Returns

**d3a\_alpha\_dT3s** [list[float]] Third temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^3]

### property d3delta\_dninjnks

Helper method for calculating the third partial mole number derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \delta}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 4(-3b + b_i + b_j + b_k)$$

Returns

**d3delta\_dninjnks** [list[list[float]]]] Third mole number derivative of *delta* of each component, [m^3/mol^4]

## Notes

This derivative is checked numerically.

## property d3epsilon\_dninjnks

Helper method for calculating the third partial mole number derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \epsilon}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 24b^2 - 12b(b_i + b_j + b_k) + 4(b_i b_j + b_i b_k + b_j b_k)$$

Returns

**d3epsilon\_dninjnks** [list[list[float]]]] Third mole number derivative of *epsilon* of each component, [m^6/mol^5]

### **Notes**

This derivative is checked numerically.

#### property ddelta\_dns

Helper method for calculating the mole number derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial \delta}{\partial n_i}\right)_{T,P,n_i \neq j} = 2(b_i - b)$$

Returns

ddelta\_dns [list[float]] Mole number derivative of delta of each component, [m^3/mol^2]

#### Notes

This derivative is checked numerically.

#### property ddelta\_dzs

Helper method for calculating the composition derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial\delta}{\partial x_i}\right)_{T,P,x_{i\neq j}} = 2b_i$$

Returns

ddelta\_dzs [list[float]] Composition derivative of *delta* of each component, [m^3/mol]

This derivative is checked numerically.

## property depsilon\_dns

Helper method for calculating the mole number derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial \epsilon}{\partial n_i}\right)_{T,P,n_{i\neq j}} = 2b(b-b_i)$$

#### Returns

**depsilon\_dns** [list[float]] Composition derivative of *epsilon* of each component, [m^6/mol^3]

## Notes

This derivative is checked numerically.

#### property depsilon\_dzs

Helper method for calculating the composition derivatives of epsilon. Note this is independent of the phase.

$$\left(\frac{\partial \epsilon}{\partial x_i}\right)_{T,P,x_{i\neq j}} = -2b_i \cdot b$$

## Returns

**depsilon\_dzs** [list[float]] Composition derivative of *epsilon* of each component, [m^6/mol^2]

## Notes

This derivative is checked numerically.

#### dlnphis\_dP(phase)

Generic formula for calculating the pressure derivative of log fugacity coefficients for each species in a mixture for the Peng-Robinson EOS. Verified numerically.

$$\left(\frac{\partial \ln \phi_i}{\partial P}\right)_{T,nj \neq i}$$

**Parameters** 

phase [str] One of 'l' or 'g', [-]

Returns

dlnphis\_dP [float] Pressure derivatives of log fugacity coefficient for each species, [1/Pa]

This expression was derived using SymPy and optimized with the cse technique.

## dlnphis\_dT(phase)

Formula for calculating the temperature derivative of log fugacity coefficients for each species in a mixture for the Peng-Robinson equation of state. Verified numerically.

$$\left(\frac{\partial \ln \phi_i}{\partial T}\right)_{P,nj \neq i}$$

**Parameters** 

phase [str] One of 'l' or 'g', [-]

Returns

dlnphis\_dT [float] Temperature derivatives of log fugacity coefficient for each species, [1/K]

#### **Notes**

This expression was derived using SymPy and optimized with the *cse* technique.

## dlnphis\_dzs(Z)

Calculate and return the mole fraction derivatives of log fugacity coefficients for each species in a mixture. This formula is specific to the Peng-Robinson equation of state.

$$\left(\frac{\partial \ln \phi_i}{\partial z_i}\right)_{P, z_{j \neq i}}$$

### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

## Returns

**dlnphis\_dzs** [list[list[float]]] Mole fraction derivatives of log fugacity coefficient for each species (such that the mole fractions do not sum to 1), [-]

## **Notes**

This formula is from [1] but is validated to match the generic implementation.

#### References

[1]

## **Examples**

```
>>> kijs = [[0, 0.00076, 0.00171], [0.00076, 0, 0.00061], [0.00171, 0.00061, 0]]
>>> eos = PRMIX(Tcs=[469.7, 507.4, 540.3], zs=[0.8168, 0.1501, 0.0331],.
→omegas=[0.249, 0.305, 0.349], Pcs=[3.369E6, 3.012E6, 2.736E6], T=322.29,
→P=101325, kijs=kijs)
>>> eos.dlnphis_dzs(eos.Z_1)
[[0.009938069276, 0.0151503498382, 0.018297235797], [-0.038517738793, -0.
→05958926042, -0.068438990795], [-0.07057106923, -0.10363920720, -0.
<u>→14116283024]]</u>
```

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#### eos\_pure

alias of thermo.eos.PR

## fugacity\_coefficients(Z)

Literature formula for calculating fugacity coefficients for each species in a mixture. Verified numerically. Applicable to most derivatives of the Peng-Robinson equation of state as well. Called by *fugacities* on initialization, or by a solver routine which is performing a flash calculation.

$$\ln \hat{\phi}_i = \frac{B_i}{B}(Z-1) - \ln(Z-B) + \frac{A}{2\sqrt{2}B} \left[\frac{B_i}{B} - \frac{2}{a\alpha}\sum_i y_i(a\alpha)_{ij}\right] \ln \left[\frac{Z + (1+\sqrt{2})B}{Z - (\sqrt{2}-1)B}\right]$$
$$A = \frac{(a\alpha)P}{R^2T^2}$$
$$B = \frac{bP}{RT}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

log\_phis [float] Log fugacity coefficient for each species, [-]

## Peng Robinson (1978)

**class** thermo.eos\_mix.**PR78MIX**(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.PRMIX

Class for solving the Peng-Robinson cubic equation of state for a mixture of any number of compounds according to the 1978 variant. Subclasses *PR*. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

$$(a\alpha)_{ij} = (1-k_{ij})\sqrt{(a\alpha)_{i}(a\alpha)_{j}}$$

$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = 0.45724 \frac{R^{2}T_{c,i}^{2}}{P_{c,i}}$$

$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_{i} = [1 + \kappa_{i}(1 - \sqrt{T_{r,i}})]^{2}$$

$$\kappa_{i} = 0.37464 + 1.54226\omega_{i} - 0.26992\omega_{i}^{2} \text{ if } \omega_{i} \le 0.491$$

$$\kappa_{i} = 0.379642 + 1.48503\omega_{i} - 0.164423\omega_{i}^{2} + 0.016666\omega_{i}^{3} \text{ if } \omega_{i} > 0.491$$

#### Parameters

- Tcs [float] Critical temperatures of all compounds, [K]
- Pcs [float] Critical pressures of all compounds, [Pa]
- omegas [float] Acentric factors of all compounds, [-]
- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

### Notes

This variant is recommended over the original.

#### References

## [1], [2]

## **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa, with modified acentric factors to show the difference between *PRMIX* 

```
>>> eos = PR78MIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],_

omegas=[0.6, 0.7], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.V_l, eos.V_g

(3.2396438915e-05, 0.00050433802024)

>>> eos.fugacities_l, eos.fugacities_g

([833048.45119, 6160.9088153], [460717.27767, 279598.90103])
```

# Methods

eos\_pure

alias of thermo.eos.PR78

eos\_pure

alias of thermo.eos.PR78

## Peng Robinson Stryjek-Vera

**class** thermo.eos\_mix.**PRSVMIX**(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *T=None*, *P=None*, *V=None*, *kappa1s=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.PRMIX, thermo.eos.PRSV

Class for solving the Peng-Robinson-Stryjek-Vera equations of state for a mixture as given in [1]. Subclasses *PRMIX* and *PRSV*. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Inherits the method of calculating fugacity coefficients from *PRMIX*. Two of *T*, *P*, and *V* are needed to solve the EOS.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

$$(a\alpha)_{ij} = (1 - k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$

$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = 0.45724 \frac{R^{2} T_{c,i}^{2}}{P_{c,i}}$$

$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_{i} = [1 + \kappa_{i} (1 - \sqrt{T_{r,i}})]^{2}$$

$$\kappa_{i} = \kappa_{0,i} + \kappa_{1,i} (1 + T_{r,i}^{0.5}) (0.7 - T_{r,i})$$

$$\kappa_{0,i} = 0.378893 + 1.4897153\omega_{i} - 0.17131848\omega_{i}^{2} + 0.0196554\omega_{i}^{3}$$

**Parameters** 

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

zs [float] Overall mole fractions of all species, [-]

- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]

- **kappa1s** [list[float], optional] Fit parameter; available in [1] for over 90 compounds, SRKMIXTranslated[-]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

[1] recommends that kappal be set to 0 for Tr > 0.7. This is not done by default; the class boolean  $kappal_Tr_limit$  may be set to True and the problem re-solved with that specified if desired.  $kappal_Tr_limit$  is not supported for P-V inputs.

For P-V initializations, a numerical solver is used to find T.

[2] and [3] are two more resources documenting the PRSV EOS. [4] lists *kappa* values for 69 additional compounds. See also *PRSV2MIX*. Note that tabulated *kappa* values should be used with the critical parameters used in their fits. Both [1] and [4] only considered vapor pressure in fitting the parameter.

## References

[1], [2], [3], [4]

## **Examples**

P-T initialization, two-phase, nitrogen and methane

```
>>> eos = PRSVMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.phase, eos.V_l, eos.H_dep_l, eos.S_dep_l

('1/g', 3.6235536165e-05, -6349.0055583, -49.1240502472)
```

## **Methods**

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> and their first and second derivatives for the PRSV EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> for the PRSV EOS.
eos_pure	alias of thermo.eos.PRSV

## a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the PRSV EOS. This vectorized implementation is added for extra speed.

$$a\alpha = a\left(\left(\kappa_0 + \kappa_1\left(\sqrt{\frac{T}{Tc}} + 1\right)\left(-\frac{T}{Tc} + \frac{7}{10}\right)\right)\left(-\sqrt{\frac{T}{Tc}} + 1\right) + 1\right)^2$$

#### **Parameters**

T [float] Temperature, [K]

## Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- **da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

## a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the PRSV EOS. This vectorized implementation is added for extra speed.

$$a\alpha = a\left(\left(\kappa_0 + \kappa_1\left(\sqrt{\frac{T}{Tc}} + 1\right)\left(-\frac{T}{Tc} + \frac{7}{10}\right)\right)\left(-\sqrt{\frac{T}{Tc}} + 1\right) + 1\right)^2$$

**Parameters** 

T [float] Temperature, [K]

#### Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### eos\_pure

alias of thermo.eos.PRSV

## Peng Robinson Stryjek-Vera 2

Bases: thermo.eos\_mix.PRMIX, thermo.eos.PRSV2

Class for solving the Peng-Robinson-Stryjek-Vera 2 equations of state for a Mixture as given in [1]. Subclasses *PRMIX* and *PRSV2 < thermo.eos.PRSV2>*. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Inherits the method of calculating fugacity coefficients from *PRMIX*. Two of *T*, *P*, and *V* are needed to solve the EOS.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$
$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1-k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$
$$b = \sum_{i} z_{i} b_{i}$$
$$a_{i} = 0.45724 \frac{R^{2} T_{c,i}^{2}}{P_{c,i}}$$

$$b_i = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_i = [1 + \kappa_i (1 - \sqrt{T_{r,i}})]^2$$

$$\kappa_i = \kappa_{0,i} + [\kappa_{1,i} + \kappa_{2,i} (\kappa_{3,i} - T_{r,i})(1 - T_{r,i}^{0.5})](1 + T_{r,i}^{0.5})(0.7 - T_{r,i})$$

$$\kappa_{0,i} = 0.378893 + 1.4897153\omega_i - 0.17131848\omega_i^2 + 0.0196554\omega_i^3$$

## Parameters

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

zs [float] Overall mole fractions of all species, [-]

- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]

**P** [float, optional] Pressure, [Pa]

V [float, optional] Molar volume, [m^3/mol]

kappa1s [list[float], optional] Fit parameter; available in [1] for over 90 compounds, [-]

kappa2s [list[float], optional] Fit parameter; available in [1] for over 90 compounds, [-]

kappa3s [list[float], optional] Fit parameter; available in [1] for over 90 compounds, [-]

- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

### **Notes**

For P-V initializations, a numerical solver is used to find T.

Note that tabulated *kappa* values should be used with the critical parameters used in their fits. [1] considered only vapor pressure in fitting the parameter.

#### References

[1]

## **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = PRSV2MIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.V_l, eos.V_g

(3.6235536165e-05, 0.00070024238654)

>>> eos.fugacities_l, eos.fugacities_g

([794057.58318, 72851.22327], [436553.65618, 357878.11066])
```

## Methods

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> and their first and second derivatives for the PRSV2 EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i>
	for the PRSV2 EOS.
eos_pure	alias of thermo.eos.PRSV2

## a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the PRSV2 EOS. This vectorized implementation is added for extra speed.

## Parameters

**T** [float] Temperature, [K]

## Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- **da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

## a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the PRSV2 EOS. This vectorized implementation is added for extra speed.

## Parameters

T [float] Temperature, [K]

# Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### **Examples**

```
>>> eos = PRSV2MIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.a_alphas_vectorized(300)

[0.0860568595, 0.20174345803]
```

#### eos\_pure

alias of thermo.eos.PRSV2

## Peng Robinson Twu (1995)

**class** thermo.eos\_mix.TWUPRMIX(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_alpha\_functions.TwuPR95\_a\_alpha, thermo.eos\_mix.PRMIX

Class for solving the Twu [1] variant of the Peng-Robinson cubic equation of state for a mixture. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{v-b} - \frac{a\alpha(T)}{v(v+b) + b(v-b)}$$
$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1-k_{ij})\sqrt{(a\alpha)_{i}(a\alpha)_{j}}$$
$$b = \sum_{i} z_{i} b_{i}$$
$$a_{i} = 0.45724 \frac{R^{2}T_{c,i}^{2}}{P_{c,i}}$$
$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$
$$\alpha_{i} = \alpha_{i}^{(0)} + \omega_{i} (\alpha_{i}^{(1)} - \alpha_{i}^{(0)})$$
$$\alpha^{(0 \text{ or } 1)} = T_{r,i}^{N(M-1)} \exp[L(1 - T_{r,i}^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.125283, 0.911807, 1.948150;

L1, M1, N1 = 0.511614, 0.784054, 2.812520

For supercritical conditions:

- L0, M0, N0 = 0.401219, 4.963070, -0.2;
- L1, M1, N1 = 0.024955, 1.248089, -8.

## **Parameters**

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T. Claimed to be more accurate than the PR, PR78 and PRSV equations.

### References

[1]

## **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

## Methods

#### eos\_pure

alias of thermo.eos.TWUPR

eos\_pure

alias of thermo.eos.TWUPR

#### **Peng Robinson Translated**

**class** thermo.eos\_mix.**PRMIXTranslated**(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *cs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.PRMIX

Class for solving the Peng-Robinson [1] [2] translated cubic equation of state for a mixture of any number of compounds. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

$$(a\alpha)_{ij} = (1-k_{ij})\sqrt{(a\alpha)_{i}(a\alpha)_{j}}$$

$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = 0.45724 \frac{R^{2}T_{c,i}^{2}}{P_{c,i}}$$

$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_{i} = [1 + \kappa_{i}(1 - \sqrt{T_{r,i}})]^{2}$$

$$\kappa_{i} = 0.37464 + 1.54226\omega_{i} - 0.26992\omega^{2}$$

#### **Parameters**

Tcs [float] Critical temperatures of all compounds, [K]

**Pcs** [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- **cs** [list[float], optional] Volume translation parameters; always zero in the original implementation, [m^3/mol]
- **T** [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

### References

[1], [2]

## **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = PRMIXTranslated(T=115, P=1E6, cs=[-4.4e-6, -4.35e-6], Tcs=[126.1, 190.6],..

...Pcs=[33.94E5, 46.04E5], omegas=[0.04, 0.011], zs=[0.2, 0.8], kijs=[[0,0.03],[0.03,

...0]])

>>> eos.V_1, eos.V_g

(3.9079056337e-05, 0.00060231393016)

>>> eos.fugacities_1, eos.fugacities_g

([442838.8615, 108854.48589], [184396.972, 565531.7709])
```

### Attributes

- **d2delta\_dninjs** Helper method for calculating the second mole number derivatives (hessian) of *delta*.
- **d2delta\_dzizjs** Helper method for calculating the second composition derivatives (hessian) of *delta*.
- *d2epsilon\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *epsilon*.
- *d2epsilon\_dzizjs* Helper method for calculating the second composition derivatives (hessian) of *epsilon*.
- *d3delta\_dninjnks* Helper method for calculating the third partial mole number derivatives of *delta*.
- d3delta\_dzizjzks Helper method for calculating the third composition derivatives of delta.
- *d3epsilon\_dninjnks* Helper method for calculating the third partial mole number derivatives of *epsilon*.
- *d3epsilon\_dzizjzks* Helper method for calculating the third composition derivatives of *epsilon*.
- *ddelta\_dns* Helper method for calculating the mole number derivatives of *delta*.

*ddelta\_dzs* Helper method for calculating the composition derivatives of *delta*.

depsilon\_dns Helper method for calculating the mole number derivatives of epsilon.

*depsilon\_dzs* Helper method for calculating the composition derivatives of *epsilon*.

## **Methods**

eos\_pure

alias of thermo.eos.PRTranslated

## property d2delta\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial^2 \delta}{\partial n_i \partial n_j}\right)_{T,P,n_{k \neq i,j}} = 2\left(\delta - b_i^0 - b_j^0 - c_i - c_j\right)$$

#### Returns

**d2delta\_dninjs** [list[list[float]]] Second mole number derivative of *delta* of each component, [m^3/mol^3]

## **Notes**

This derivative is checked numerically.

## property d2delta\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial x_i \partial x_j}\right)_{T, P, x_{k \neq i, j}} = 0$$

## Returns

**d2delta\_dzizjs** [list[float]] Second Composition derivative of *delta* of each component, [m^3/mol]

## Notes

This derivative is checked numerically.

## property d2epsilon\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \epsilon}{\partial n_i n_j}\right)_{T,P,n_{k\neq i,j}} = -2b^0(2b^0 - b_i^0 - b_j^0) + c(4b^0 - 2b_i^0 - 2b_j^0 + 2c - c_i - c_j) - 2(b^0 - b_i^0)(b^0 - b_j^0) + (c - c_i)(2b^0 - b_j^0)$$

# Returns

**d2epsilon\_dninjs** [list[list[float]]] Second mole number derivative of *epsilon* of each component, [m^6/mol^4]

This derivative is checked numerically.

## property d2epsilon\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \epsilon}{\partial x_i \partial x_j}\right)_{T,P,x_{k \neq i,j}} = -2b_i^0 b_j^0 + 2b_i^0 c_j + 2b_j^0 c_i + 2c_i c_j$$

#### Returns

**d2epsilon\_dzizjs** [list[list[float]]] Second composition derivative of *epsilon* of each component, [m^6/mol^2]

## Notes

This derivative is checked numerically.

## property d3delta\_dninjnks

Helper method for calculating the third partial mole number derivatives of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial^3 \delta}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 4\left(b_i^0 + b_j^0 + b_k^0 + c_i + c_j + c_k\right) - 6\delta$$

#### Returns

**d3delta\_dninjnks** [list[list[float]]]] Third mole number derivative of *delta* of each component, [m^3/mol^4]

## **Notes**

This derivative is checked numerically.

## property d3delta\_dzizjzks

Helper method for calculating the third composition derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \delta}{\partial x_i \partial x_j \partial x_k}\right)_{T,P,x_{m \neq i,j,k}} = 0$$

## Returns

**d3delta\_dzizjzks** [list[list[list[float]]]] Third composition derivative of *epsilon* of each component, [m^6/mol^5]

This derivative is checked numerically.

## property d3epsilon\_dninjnks

Helper method for calculating the third partial mole number derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \epsilon}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 4b^0(3b^0 - b_i^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2c(6b^0 - 2(b_i^0 + b_j^0 + b_k^0) + 3c - (c_i + c_j + c_k)) + 2(b^0 - b_i^0)(b_j^0 - b_j^0 - b_k^0) - 2(b_j^0 - b_k^0 - b_j^0 - b_k^0) - 2(b_j^0 - b_k^0 - b_k^0) + 2(b^0 - b_k^0 - b_k^0 - b_k^0) + 2(b^0 - b_k^0 - b_k^0 - b_k^0) - 2(b^0 - b_k^0 - b_k^0 - b_k^0 - b_k^0) - 2(b^0 - b_k^0 - b_k^0 - b_k^0 - b_k^0) + 2(b^0 - b_k^0 - b_k^0 - b_k^0 - b_k^0) + 2(b^0 - b_k^0 -$$

Returns

0

**d3epsilon\_dninjnks** [list[list[float]]]] Third mole number derivative of *epsilon* of each component, [m^6/mol^5]

## Notes

This derivative is checked numerically.

## property d3epsilon\_dzizjzks

Helper method for calculating the third composition derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \epsilon}{\partial x_i \partial x_j \partial x_k}\right)_{T, P, x_{m \neq i, j, k}} = 0$$

#### Returns

**d2epsilon\_dzizjzks** [list[list[float]]]] Composition derivative of *epsilon* of each component, [m^6/mol^2]

#### Notes

This derivative is checked numerically.

## property ddelta\_dns

Helper method for calculating the mole number derivatives of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \delta}{\partial n_i}\right)_{T,P,n_{i\neq j}} = 2(c_i + b_i^0) - \delta$$

#### Returns

ddelta\_dns [list[float]] Mole number derivative of *delta* of each component, [m^3/mol^2]

### **Notes**

This derivative is checked numerically.

## property ddelta\_dzs

Helper method for calculating the composition derivatives of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \delta}{\partial x_i}\right)_{T,P,x_i \neq j} = 2(c_i + b_i^0)$$

#### Returns

ddelta\_dzs [list[float]] Composition derivative of *delta* of each component, [m^3/mol]

#### Notes

This derivative is checked numerically.

### property depsilon\_dns

Helper method for calculating the mole number derivatives of *epsilon*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \epsilon}{\partial n_i}\right)_{T,P,n_{i\neq j}} = 2b^0(b^0 - b_i^0) - c(2b^0 - 2b_i^0 + c - c_i) - (c - c_i)(2b^0 + c)$$

#### Returns

**depsilon\_dns** [list[float]] Composition derivative of *epsilon* of each component, [m^6/mol^3]

#### **Notes**

This derivative is checked numerically.

### property depsilon\_dzs

Helper method for calculating the composition derivatives of *epsilon*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \epsilon}{\partial x_i}\right)_{T,P,x_{i\neq j}} = c_i(2b_i^0 + c) + c(2b_i^0 + c_i) - 2b^0b_i^0$$

#### Returns

**depsilon\_dzs** [list[float]] Composition derivative of *epsilon* of each component, [m^6/mol^2]

#### Notes

This derivative is checked numerically.

eos\_pure

alias of thermo.eos.PRTranslated

### Peng Robinson Translated-Consistent

class thermo.eos\_mix.PRMIXTranslatedConsistent(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *cs=None*, *alpha\_coeffs=None*, *T=None*, *V=None*,

fugacities=True, only\_l=False, only\_g=False)

Bases: thermo.eos\_alpha\_functions.Twu91\_a\_alpha, thermo.eos\_mix.PRMIXTranslated

Class for solving the volume translated Le Guennec, Privat, and Jaubert revision of the Peng-Robinson equation of state according to [1].

Two of *T*, *P*, and *V* are needed to solve the EOS.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1 - k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$
$$b = \sum_{i} z_{i} b_{i}$$
$$a_{i} = 0.45724 \frac{R^{2} T_{c,i}^{2}}{P_{c,i}}$$
$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$
$$\alpha_{i} = \left(\frac{T}{T_{c}}\right)^{c_{3}(c_{2}-1)} e^{c_{1}\left(-\left(\frac{T}{T_{c}}\right)^{c_{2}c_{3}}+1\right)}$$

If *c* is not provided, they are estimated as:

$$c = \frac{RT_c}{P_c} (0.0198\omega - 0.0065)$$

If *alpha\_coeffs* is not provided, the parameters L and M are estimated from the acentric factor as follows:

$$L = 0.1290\omega^2 + 0.6039\omega + 0.0877$$
$$M = 0.1760\omega^2 - 0.2600\omega + 0.8884$$

#### **Parameters**

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- cs [list[float], optional] Volume translation parameters, [m^3/mol]
- alpha\_coeffs [list[tuple(float[3])], optional] Coefficients L, M, N (also called C1, C2, C3) of TWU 1991 form, [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

#### References

[1]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = PRMIXTranslatedConsistent(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5,_

-46.04E5], omegas=[0.04, 0.011], zs=[0.2, 0.8], kijs=[[0,0.03],[0.03,0]])

>>> eos.V_l, eos.V_g

(3.675235812e-05, 0.00059709319879)

>>> eos.fugacities_l, eos.fugacities_g

([443454.9336, 106184.004057], [184122.74082, 563037.785])
```

### **Methods**

eos\_pure alias of thermo.eos.PRTranslatedConsistent

eos\_pure

alias of thermo.eos.PRTranslatedConsistent

### Peng Robinson Translated (Pina-Martinez, Privat, and Jaubert Variant)

class thermo.eos\_mix.PRMIXTranslatedPPJP(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *cs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.PRMIXTranslated

Class for solving the Pina-Martinez, Privat, Jaubert, and Peng revision of the Peng-Robinson equation of state. Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{v+c-b} - \frac{a\alpha(T)}{(v+c)(v+c+b) + b(v+c-b)}$$
$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1-k_{ij}) \sqrt{(a\alpha)_{i}(a\alpha)_{j}}$$
$$b = \sum_{i} z_{i} b_{i}$$
$$a_{i} = 0.45724 \frac{R^{2} T_{c,i}^{2}}{P_{c,i}}$$
$$b_{i} = 0.07780 \frac{RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_i = [1 + \kappa_i (1 - \sqrt{T_{r,i}})]^2$$
  
$$\kappa_i = 0.3919 + 1.4996\omega - 0.2721\omega^2 + 0.1063\omega^3$$

### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- cs [list[float], optional] Volume translation parameters, [m^3/mol]
- **T** [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

### **Notes**

For P-V initializations, a numerical solver is used to find T.

#### References

[1]

#### Examples

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

### **Methods**

eos\_pure

alias of thermo.eos.PRTranslatedPPJP

eos\_pure

alias of thermo.eos.PRTranslatedPPJP

## 7.8.3 SRK Family EOSs

### Standard SRK

**class** thermo.eos\_mix.**SRKMIX**(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.EpsilonZeroMixingRules, thermo.eos\_mix.GCEOSMIX, thermo.eos.SRK

Class for solving the Soave-Redlich-Kwong cubic equation of state for a mixture of any number of compounds. Solves the EOS on initialization and calculates fugacities for all components in all phases.

The implemented method here is *fugacity\_coefficients*, which implements the formula for fugacity coefficients in a mixture as given in [1]. Two of *T*, *P*, and *V* are needed to solve the EOS.

$$P = \frac{RT}{V - b} - \frac{a\alpha(T)}{V(V + b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

$$(a\alpha)_{ij} = (1 - k_{ij})\sqrt{(a\alpha)_{i}(a\alpha)_{j}}$$

$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2} - 1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$

$$b_{i} = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right) \frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_{i} = \left[1 + m_{i} \left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\right]^{2}$$

$$m_{i} = 0.480 + 1.574\omega_{i} - 0.176\omega_{i}^{2}$$

### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

zs [float] Overall mole fractions of all species, [-]

- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]

- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

### References

[1], [2], [3]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> SRK_mix = SRKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> SRK_mix.V_1, SRK_mix.V_g

(4.1047569614e-05, 0.0007110158049)
```

### **Methods**

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> and their first and second derivatives for the SRK EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i>
	for the SRK EOS.
dlnphis_dP(phase)	Generic formula for calculating the pressure
	derivaitve of log fugacity coefficients for each
	species in a mixture for the SRK EOS.
dlnphis_dT(phase)	Formula for calculating the temperature derivative of
	log fugacity coefficients for each species in a mixture
	for the SRK equation of state.
eos_pure	alias of thermo.eos.SRK
<pre>fugacity_coefficients(Z)</pre>	Literature formula for calculating fugacity coeffi-
	cients for each species in a mixture.

#### a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the SRK EOS.

This vectorized implementation is added for extra speed.

$$a\alpha = a\left(m\left(-\sqrt{\frac{T}{Tc}}+1\right)+1\right)^2$$
$$\frac{da\alpha}{dT} = \frac{am}{T}\sqrt{\frac{T}{Tc}}\left(m\left(\sqrt{\frac{T}{Tc}}-1\right)-1\right)$$
$$\frac{d^2a\alpha}{dT^2} = \frac{am\sqrt{\frac{T}{Tc}}}{2T^2}\left(m+1\right)$$

### **Parameters**

T [float] Temperature, [K]

#### Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

### a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the SRK EOS. This vectorized implementation is added for extra speed.

$$a\alpha = a\left(m\left(-\sqrt{\frac{T}{Tc}}+1\right)+1\right)^2$$

#### **Parameters**

T [float] Temperature, [K]

### Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

### dlnphis\_dP(phase)

Generic formula for calculating the pressure derivative of log fugacity coefficients for each species in a mixture for the SRK EOS. Verified numerically.

$$\left(\frac{\partial \ln \phi_i}{\partial P}\right)_{T,nj \neq i}$$

#### **Parameters**

phase [str] One of 'l' or 'g', [-]

Returns

dlnphis\_dP [float] Pressure derivatives of log fugacity coefficient for each species, [1/Pa]

This expression was derived using SymPy and optimized with the cse technique.

### dlnphis\_dT(phase)

Formula for calculating the temperature derivative of log fugacity coefficients for each species in a mixture for the SRK equation of state. Verified numerically.

$$\left(\frac{\partial \ln \phi_i}{\partial T}\right)_{P,nj \neq i}$$

### **Parameters**

phase [str] One of 'l' or 'g', [-]

#### Returns

dlnphis\_dT [float] Temperature derivatives of log fugacity coefficient for each species, [1/K]

#### Notes

This expression was derived using SymPy and optimized with the cse technique.

#### eos\_pure

alias of thermo.eos.SRK

### fugacity\_coefficients(Z)

Literature formula for calculating fugacity coefficients for each species in a mixture. Verified numerically. Applicable to most derivatives of the SRK equation of state as well. Called by *fugacities* on initialization, or by a solver routine which is performing a flash calculation.

$$\ln \hat{\phi}_i = \frac{B_i}{B}(Z-1) - \ln(Z-B) + \frac{A}{B} \left[ \frac{B_i}{B} - \frac{2}{a\alpha} \sum_i y_i(a\alpha)_{ij} \right] \ln \left( 1 + \frac{B}{Z} \right)$$
$$A = \frac{a\alpha P}{R^2 T^2}$$
$$B = \frac{bP}{RT}$$

### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

#### Returns

log\_phis [float] Log fugacity coefficient for each species, [-]

### Twu SRK (1995)

class thermo.eos\_mix.TWUSRKMIX(Tcs, Pcs, omegas, zs, kijs=None, T=None, P=None, V=None, fugacities=True, only\_l=False, only\_g=False)

Bases: thermo.eos\_alpha\_functions.TwuSRK95\_a\_alpha, thermo.eos\_mix.SRKMIX

Class for solving the Twu variant of the Soave-Redlich-Kwong cubic equation of state for a mixture. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V(V+b)}$$

$$\begin{split} a_{i} &= \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2}-1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}\\ b_{i} &= \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}\\ a\alpha &= \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}\\ (a\alpha)_{ij} &= (1-k_{ij}) \sqrt{(a\alpha)_{i}(a\alpha)_{j}}\\ b &= \sum_{i} z_{i} b_{i}\\ \alpha_{i} &= \alpha^{(0,i)} + \omega_{i} (\alpha^{(1,i)} - \alpha^{(0,i)})\\ \alpha^{(0 \text{ or } 1, i)} &= T_{r,i}^{N(M-1)} \exp[L(1-T_{r,i}^{NM})] \end{split}$$

For sub-critical conditions:

L0, M0, N0 = 0.141599, 0.919422, 2.496441

L1, M1, N1 = 0.500315, 0.799457, 3.291790

For supercritical conditions:

- L0, M0, N0 = 0.441411, 6.500018, -0.20
- L1, M1, N1 = 0.032580, 1.289098, -8.0

### **Parameters**

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T. Claimed to be more accurate than the SRK equation.

#### References

[1]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = TWUSRKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],_

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.V_l, eos.V_g

(4.1087927542e-05, 0.00071170732525)

>>> eos.fugacities_l, eos.fugacities_g

([809692.830826, 74093.6388157], [441783.431489, 362470.3174107])
```

### **Methods**

eos\_pure

alias of thermo.eos.TWUSRK

eos\_pure

alias of thermo.eos.TWUSRK

### **API SRK**

class thermo.eos\_mix.APISRKMIX(Tcs, Pcs, zs, omegas=None, kijs=None, T=None, P=None, V=None, S1s=None, S2s=None, fugacities=True, only\_l=False, only\_g=False) Bases: thermo.eos\_mix.SRKMIX, thermo.eos.APISRK

Class for solving the Refinery Soave-Redlich-Kwong cubic equation of state for a mixture of any number of compounds, as shown in the API Databook [1]. Subclasses *APISRK*. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V(V+b)}$$
$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1-k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$
$$b = \sum_{i} z_{i} b_{i}$$
$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2}-1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$

$$b_{i} = \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$
$$\alpha(T)_{i} = \left[1 + S_{1,i} \left(1 - \sqrt{T_{r,i}}\right) + S_{2,i} \frac{1 - \sqrt{T_{r,i}}}{\sqrt{T_{r,i}}}\right]^{2}$$

 $S_{1,i} = 0.48508 + 1.55171\omega_i - 0.15613\omega_i^2$  if S1 is not tabulated

### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

- Pcs [float] Critical pressures of all compounds, [Pa]
- omegas [float] Acentric factors of all compounds, [-]
- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- S1s [float, optional] Fit constant or estimated from acentric factor if not provided [-]
- S2s [float, optional] Fit constant or 0 if not provided [-]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

### Notes

For P-V initializations, a numerical solver is used to find T.

### References

[1]

## **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = APISRKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],_

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.V_l, eos.V_g

(4.101592310e-05, 0.00071046883030)

>>> eos.fugacities_l, eos.fugacities_g

([817882.3033, 71620.4823812], [442158.29113, 361519.79877])
```

#### Methods

eos\_pure

alias of thermo.eos.APISRK

eos\_pure

alias of thermo.eos.APISRK

## **SRK Translated**

**class** thermo.eos\_mix.**SRKMIXTranslated**(*Tcs*, *Pcs*, *omegas*, *zs*, *kijs=None*, *cs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.SRKMIX

Class for solving the volume translated Soave-Redlich-Kwong cubic equation of state for a mixture of any number of compounds. Subclasses *SRKMIX*. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

$$(a\alpha)_{ij} = (1-k_{ij})\sqrt{(a\alpha)_{i}(a\alpha)_{j}}$$

$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2}-1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$

$$b_{i} = \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$

$$\alpha(T)_{i} = \left[1 + m_{i} \left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\right]^{2}$$

$$m_{i} = 0.480 + 1.574\omega_{i} - 0.176\omega_{i}^{2}$$

#### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

zs [float] Overall mole fractions of all species, [-]

- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- **cs** [list[float], optional] Volume translation parameters; always zero in the original implementation, [m^3/mol]
- T [float, optional] Temperature, [K]

- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

#### Examples

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

#### Attributes

- *d2delta\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *delta*.
- *d2delta\_dzizjs* Helper method for calculating the second composition derivatives (hessian) of *delta*.
- *d2epsilon\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *epsilon*.
- *d2epsilon\_dzizjs* Helper method for calculating the second composition derivatives (hessian) of *epsilon*.
- *d3delta\_dninjnks* Helper method for calculating the third partial mole number derivatives of *delta*.
- d3delta\_dzizjzks Helper method for calculating the third composition derivatives of delta.
- *d3epsilon\_dninjnks* Helper method for calculating the third partial mole number derivatives of *epsilon*.
- *d3epsilon\_dzizjzks* Helper method for calculating the third composition derivatives of *epsilon*.
- ddelta\_dns Helper method for calculating the mole number derivatives of delta.

*ddelta\_dzs* Helper method for calculating the composition derivatives of *delta*.

depsilon\_dns Helper method for calculating the mole number derivatives of epsilon.

depsilon\_dzs Helper method for calculating the composition derivatives of epsilon.

### **Methods**

eos\_pure

alias of thermo.eos.SRKTranslated

### property d2delta\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial^2 \delta}{\partial n_i \partial n_j}\right)_{T,P,n_{k \neq i,j}} = \left((b^0 - c_i - c_j) + 4c - b_i^0 - b_j^0\right)$$

#### Returns

**d2delta\_dninjs** [list[list[float]]] Second mole number derivative of *delta* of each component, [m^3/mol^3]

### **Notes**

This derivative is checked numerically.

### property d2delta\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial x_i \partial x_j}\right)_{T, P, x_{k \neq i, j}} = 0$$

### Returns

**d2delta\_dzizjs** [list[float]] Second Composition derivative of *delta* of each component, [m^3/mol]

### Notes

This derivative is checked numerically.

### property d2epsilon\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \epsilon}{\partial n_i n_j}\right)_{T,P,n_{k\neq i,j}} = b^0 (2c - c_i - c_j) + c(2b^0 - b_i^0 - b_j^0) + 2c(2c - c_i - c_j) + (b^0 - b_i^0)(c - c_j) + (b^0 - b_j^0)(c - c_i) + (b^0 - b_j^0)(c - c_j) + (b^0 -$$

## Returns

**d2epsilon\_dninjs** [list[list[float]]] Second mole number derivative of *epsilon* of each component, [m^6/mol^4]

This derivative is checked numerically.

### property d2epsilon\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \epsilon}{\partial x_i \partial x_j}\right)_{T,P,x_{k \neq i,j}} = b_i^0 c_j + b_j^0 c_i + 2c_i c_j$$

Returns

**d2epsilon\_dzizjs** [list[list[float]]] Second composition derivative of *epsilon* of each component, [m^6/mol^2]

### Notes

This derivative is checked numerically.

### property d3delta\_dninjnks

Helper method for calculating the third partial mole number derivatives of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial^3 \delta}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = -6b^0 + 2(b_i^0 + b_j^0 + b_k^0) + -12c + 4(c_i + c_j + c_k)$$

#### Returns

**d3delta\_dninjnks** [list[list[float]]]] Third mole number derivative of *delta* of each component, [m^3/mol^4]

### **Notes**

This derivative is checked numerically.

### property d3delta\_dzizjzks

Helper method for calculating the third composition derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \delta}{\partial x_i \partial x_j \partial x_k}\right)_{T,P,x_{m \neq i,j,k}} = 0$$

### Returns

**d3delta\_dzizjzks** [list[list[list[float]]]] Third composition derivative of *epsilon* of each component, [m^6/mol^5]

This derivative is checked numerically.

### property d3epsilon\_dninjnks

Helper method for calculating the third partial mole number derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \epsilon}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = -2b^0(3c - c_i - c_j - c_k) - 2c(3b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_k^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_k^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0)(2b^0 - b_i^0 - b_j^0 - b_k^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0) - (b^0 - b_i^0 - b_i^0 - b_i^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0 - b_i^0 - b_i^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0 - b_i^0 - b_i^0 - b_i^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0 - b_i^0 - b_i^0 - b_i^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0 - b_i^0 - b_i^0 - b_i^0) - 4c(3c - c_i - c_j - c_k) - (b^0 - b_i^0 - b_i^0$$

### Returns

0

**d3epsilon\_dninjnks** [list[list[float]]]] Third mole number derivative of *epsilon* of each component, [m^6/mol^5]

### Notes

This derivative is checked numerically.

### property d3epsilon\_dzizjzks

Helper method for calculating the third composition derivatives of *epsilon*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \epsilon}{\partial x_i \partial x_j \partial x_k}\right)_{T, P, x_{m \neq i, j, k}} = 0$$

#### Returns

**d2epsilon\_dzizjzks** [list[list[float]]]] Composition derivative of *epsilon* of each component, [m^6/mol^2]

#### Notes

This derivative is checked numerically.

### property ddelta\_dns

Helper method for calculating the mole number derivatives of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \delta}{\partial n_i}\right)_{T,P,n_{i\neq j}} = (2c_i + b_i^0) - \delta$$

#### Returns

ddelta\_dns [list[float]] Mole number derivative of delta of each component, [m^3/mol^2]

### **Notes**

This derivative is checked numerically.

### property ddelta\_dzs

Helper method for calculating the composition derivatives of *delta*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \delta}{\partial x_i}\right)_{T,P,x_i \neq j} = 2(c_i + b_i^0)$$

#### Returns

ddelta\_dzs [list[float]] Composition derivative of *delta* of each component, [m^3/mol]

#### **Notes**

This derivative is checked numerically.

### property depsilon\_dns

Helper method for calculating the mole number derivatives of *epsilon*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \epsilon}{\partial n_i}\right)_{T,P,n_{i\neq j}} = -b^0(c-c_i) - c(b^0 - b_i^0) - 2c(c-c_i)$$

#### Returns

**depsilon\_dns** [list[float]] Composition derivative of *epsilon* of each component, [m^6/mol^3]

#### **Notes**

This derivative is checked numerically.

### property depsilon\_dzs

Helper method for calculating the composition derivatives of *epsilon*. Note this is independent of the phase.  $b^0$  refers to the original *b* parameter not involving any translation.

$$\left(\frac{\partial \epsilon}{\partial x_i}\right)_{T,P,x_{i\neq j}} = c_i b^0 + 2cc_i + b_i c$$

#### Returns

**depsilon\_dzs** [list[float]] Composition derivative of *epsilon* of each component, [m^6/mol^2]

#### Notes

This derivative is checked numerically.

```
eos_pure
```

alias of thermo.eos.SRKTranslated

### **SRK Translated-Consistent**

Bases: thermo.eos\_alpha\_functions.Twu91\_a\_alpha, thermo.eos\_mix.SRKMIXTranslated

Class for solving the volume translated Le Guennec, Privat, and Jaubert revision of the SRK equation of state according to [1].

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$

$$(a\alpha)_{ij} = (1 - k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$

$$\alpha_{i} = \left(\frac{T}{T_{c,i}}\right)^{c_{3}(c_{2}-1)} e^{c_{1}\left(-\left(\frac{T}{T_{c,i}}\right)^{c_{2}c_{3}}+1\right)}$$

$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2}-1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$

$$b_{i} = \left(\frac{(\sqrt[3]{2}-1)}{3}\right) \frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$

If *cs* is not provided, they are estimated as:

$$c = \frac{RT_c}{P_c} (0.0172\omega - 0.0096)$$

If *alpha\_coeffs* is not provided, the parameters *L* and *M* are estimated from each of the acentric factors as follows:

$$L = 0.0947\omega^{2} + 0.6871\omega + 0.1508$$
$$M = 0.1615\omega^{2} - 0.2349\omega + 0.8876$$

#### **Parameters**

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]

**cs** [list[float], optional] Volume translation parameters, [m<sup>3</sup>/mol]

- **alpha\_coeffs** [list[list[float]]] Coefficients for thermo.eos\_alpha\_functions. Twu91\_a\_alpha, [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

#### References

[1]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

## Methods

eos\_pure

alias of thermo.eos.SRKTranslatedConsistent

#### eos\_pure

alias of thermo.eos.SRKTranslatedConsistent

### **MSRK Translated**

Class for solving the volume translated Soave (1980) alpha function, revision of the Soave-Redlich-Kwong equation of state for a pure compound according to [1]. Uses two fitting parameters N and M to more accurately fit the vapor pressure of pure species.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V+c-b} - \frac{a\alpha(T)}{(V+c)(V+c+b)}$$
$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1-k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$
$$\alpha(T)_{i} = 1 + (1-T_{r,i})(M+\frac{N}{T_{r,i}})$$
$$b = \sum_{i} z_{i} b_{i}$$

$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2} - 1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$
$$b_{i} = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right)\frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$

This is an older correlation that offers lower accuracy on many properties which were sacrificed to obtain the vapor pressure accuracy. The alpha function of this EOS does not meet any of the consistency requirements for alpha functions.

Coefficients can be found in [2], or estimated with the method in [3]. The estimation method in [3] works as follows, using the acentric factor and true critical compressibility:

$$M = 0.4745 + 2.7349(\omega Z_c) + 6.0984(\omega Z_c)^2$$
$$N = 0.0674 + 2.1031(\omega Z_c) + 3.9512(\omega Z_c)^2$$

An alternate estimation scheme is provided in [1], which provides analytical solutions to calculate the parameters M and N from two points on the vapor pressure curve, suggested as 10 mmHg and 1 atm. This is used as an estimation method here if the parameters are not provided, and the two vapor pressure points are obtained from the original SRK equation of state.

#### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

**Pcs** [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- cs [list[float], optional] Volume translation parameters, [m^3/mol]
- **alpha\_coeffs** [list[list[float]]] Coefficients for thermo.eos\_alpha\_functions. Soave\_1979\_a\_alpha, [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

### References

[1], [2], [3]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = MSRKMIXTranslated(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.

...04E5], omegas=[0.04, 0.011], zs=[0.2, 0.8], kijs=[[0,0.03],[0.03,0]])

>>> eos.V_l, eos.V_g

(3.9222990198e-05, 0.00060438075638)
```

## Methods

eos\_pure

alias of thermo.eos.MSRKTranslated

#### eos\_pure

alias of thermo.eos.MSRKTranslated

## 7.8.4 Cubic Equation of State with Activity Coefficients

Class for solving the Predictive Soave-Redlich-Kwong [1] equation of state for a mixture of any number of compounds. Solves the EOS on initialization.

Two of T, P, and V are needed to solve the EOS.

Warning: This class is not complete! Fugacities and their derivatives among others are not yet implemented.

$$P = \frac{RT}{V - b} - \frac{a\alpha(T)}{V(V + b)}$$
$$b = \sum_{i} z_{i}b_{i}$$
$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2} - 1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$
$$b_{i} = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right)\frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$

#### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

omegas [float] Acentric factors of all compounds, [-]

zs [float] Overall mole fractions of all species, [-]

**alpha\_coeffs** [list[list[float]]] Coefficients for thermo.eos\_alpha\_functions. Mathias\_Copeman\_poly\_a\_alpha, [-]

- **ge\_model** [thermo.activity.GibbsExcess object] Excess Gibbs free energy model; to match the *PSRK* model, this is a thermo.unifac.UNIFAC object, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- **cs** [list[float], optional] Volume translation parameters; always zero in the original implementation, [m^3/mol]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

### References

[1]

### **Examples**

T-P initialization, equimolar CO2, n-hexane:

```
>>> from thermo.unifac import UNIFAC, PSRKIP, PSRKSG
>>> Tcs = [304.2, 507.4]
>>> Pcs = [7.37646e6, 3.014419e6]
>>> omegas = [0.2252, 0.2975]
>>> zs = [0.5, 0.5]
>>> Mathias_Copeman_coeffs = [[-1.7039, 0.2515, 0.8252, 1.0], [2.9173, -1.4411, 1.
--1061, 1.0]]
>>> T = 313.
>>> P = 1E6
>>> ge_model = UNIFAC.from_subgroups(T=T, xs=zs, chemgroups=[{117: 1}, {1:2, 2:4}],__
--subgroups=PSRKSG, interaction_data=PSRKIP, version=0)
>>> eos = PSRK(Tcs=Tcs, Pcs=Pcs, omegas=omegas, zs=zs, ge_model=ge_model, alpha_
--coeffs=Mathias_Copeman_coeffs, T=T, P=P)
>>> eos
```

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PSRK(Tcs=[304.2, 507.4], Pcs=[7376460.0, 3014419.0], omegas=[0.2252, 0.2975], →kijs=[[0.0, 0.0], [0.0, 0.0]], alpha\_coeffs=[[-1.7039, 0.2515, 0.8252, 1.0], [2. →9173, -1.4411, 1.1061, 1.0]], cs=[0.0, 0.0], ge\_model=UNIFAC(T=313.0, xs=[0.5, 0. →5], rs=[1.3, 4.499800000000005], qs=[0.982, 3.856], Qs=[0.848, 0.54, 0.982], →vs=[[0, 2], [0, 4], [1, 0]], psi\_abc=([[0.0, 0.0, 919.8], [0.0, 0.0, 919.8], [-38. →672, -38.672, 0.0]], [[0.0, 0.0, -3.9132], [0.0, 0.0, -3.9132], [0.8615, 0.8615, →600]], [[0.0, 0.0, 0.0046309], [0.0, 0.0, 0.0046309], [-0.0017906, -0.0017906, 0. →0]]), version=0), zs=[0.5, 0.5], T=313.0, P=1000000.0) >>> eos.phase, eos.V\_1, eos.V\_g ('1/g', 0.000110889753959, 0.00197520225546)

### **Methods**

eos\_pure

alias of thermo.eos.SRKTranslated

eos\_pure

alias of thermo.eos.SRKTranslated

## 7.8.5 Van der Waals Equation of State

**class** thermo.eos\_mix.VDWMIX(*Tcs*, *Pcs*, *zs*, *kijs=None*, *T=None*, *P=None*, *V=None*, *omegas=None*,

fugacities=True, only\_l=False, only\_g=False)

Bases: thermo.eos\_mix.EpsilonZeroMixingRules, thermo.eos\_mix.GCEOSMIX, thermo.eos.VDW

Class for solving the Van der Waals [1] [2] cubic equation of state for a mixture of any number of compounds. Solves the EOS on initialization and calculates fugacities for all components in all phases.

Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V-b} - \frac{a}{V^2}$$
$$a = \sum_i \sum_j z_i z_j a_{ij}$$
$$b = \sum_i z_i b_i$$
$$a_{ij} = (1-k_{ij})\sqrt{a_i a_j}$$
$$a_i = \frac{27}{64} \frac{(RT_{c,i})^2}{P_{c,i}}$$
$$b_i = \frac{RT_{c,i}}{8P_{c,i}}$$

#### Parameters

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]

- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- omegas [float, optional] Acentric factors of all compounds Not used in equation of state!, [-]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

For P-V initializations, a numerical solver is used to find T.

#### References

[1], [2]

### Examples

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = VDWMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], zs=[0.5, 

→0.5], kijs=[[0,0],[0,0]])
>>> eos.V_l, eos.V_g
(5.881369844883e-05, 0.00077708723758)
>>> eos.fugacities_l, eos.fugacities_g
([854533.266920, 207126.8497276], [448470.736338, 397826.543999])
```

### Attributes

- *d2delta\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *delta*.
- **d2delta\_dzizjs** Helper method for calculating the second composition derivatives (hessian) of *delta*.
- *d3delta\_dninjnks* Helper method for calculating the third partial mole number derivatives of *delta*.

ddelta\_dns Helper method for calculating the mole number derivatives of delta.

*ddelta\_dzs* Helper method for calculating the composition derivatives of *delta*.

## Methods

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i>
	and their first and second derivatives for the VDW
	EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i>
	for the VDW EOS.
dlnphis_dP(phase)	Generic formula for calculating the pressure
	derivative of log fugacity coefficients for each
	species in a mixture for the VDW EOS.
dlnphis_dT(phase)	Formula for calculating the temperature derivative of
	log fugacity coefficients for each species in a mixture
	for the VDW equation of state.
eos_pure	alias of thermo.eos.VDW
<pre>fugacity_coefficients(Z)</pre>	Literature formula for calculating fugacity coeffi-
	cients for each species in a mixture.

### a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the VDW EOS. This vectorized implementation is added for extra speed.

$$\begin{aligned} a\alpha &= a \\ \frac{da\alpha}{dT} &= 0 \\ \frac{d^2a\alpha}{dT^2} &= 0 \end{aligned}$$

### Parameters

T [float] Temperature, [K]

### Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

### a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the VDW EOS. This vectorized implementation is added for extra speed.

 $a\alpha = a$ 

### Parameters

T [float] Temperature, [K]

## Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

### property d2delta\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial n_i \partial n_j}\right)_{T,P,n_{k \neq i,j}} = 0$$

#### Returns

**d2delta\_dninjs** [list[list[float]]] Second mole number derivative of *delta* of each component, [m^3/mol^3]

### Notes

This derivative is checked numerically.

#### property d2delta\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial x_i \partial x_j}\right)_{T, P, x_k \neq i, j} = 0$$

#### Returns

**d2delta\_dzizjs** [list[float]] Second Composition derivative of *delta* of each component, [m^3/mol]

#### Notes

This derivative is checked numerically.

### property d3delta\_dninjnks

Helper method for calculating the third partial mole number derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \delta}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 0$$

#### Returns

**d3delta\_dninjnks** [list[list[float]]]] Third mole number derivative of *delta* of each component, [m^3/mol^4]

#### Notes

This derivative is checked numerically.

### property ddelta\_dns

Helper method for calculating the mole number derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial \delta}{\partial n_i}\right)_{T,P,n_{i\neq j}} = 0$$

Returns

ddelta\_dns [list[float]] Mole number derivative of delta of each component, [m^3/mol^2]

This derivative is checked numerically.

### property ddelta\_dzs

Helper method for calculating the composition derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial\delta}{\partial x_i}\right)_{T,P,x_{i\neq j}} = 0$$

#### Returns

ddelta\_dzs [list[float]] Composition derivative of delta of each component, [m^3/mol]

### Notes

This derivative is checked numerically.

#### dlnphis\_dP(phase)

Generic formula for calculating the pressure derivative of log fugacity coefficients for each species in a mixture for the VDW EOS. Verified numerically.

$$\left(\frac{\partial \ln \phi_i}{\partial P}\right)_{T,nj \neq i}$$

#### **Parameters**

phase [str] One of 'l' or 'g', [-]

### Returns

dlnphis\_dP [float] Pressure derivatives of log fugacity coefficient for each species, [1/Pa]

#### **Notes**

This expression was derived using SymPy and optimized with the cse technique.

### dlnphis\_dT(phase)

Formula for calculating the temperature derivative of log fugacity coefficients for each species in a mixture for the VDW equation of state. Verified numerically.

$$\left(\frac{\partial \ln \phi_i}{\partial T}\right)_{P,nj \neq i}$$

### **Parameters**

phase [str] One of 'l' or 'g', [-]

### Returns

dlnphis\_dT [float] Temperature derivatives of log fugacity coefficient for each species, [1/K]

This expression was derived using SymPy and optimized with the cse technique.

#### eos\_pure

alias of thermo.eos.VDW

#### fugacity\_coefficients(Z)

Literature formula for calculating fugacity coefficients for each species in a mixture. Verified numerically. Called by *fugacities* on initialization, or by a solver routine which is performing a flash calculation.

$$\ln \hat{\phi}_i = \frac{b_i}{V - b} - \ln \left[ Z \left( 1 - \frac{b}{V} \right) \right] - \frac{2\sqrt{aa_i}}{RTV}$$

#### **Parameters**

Z [float] Compressibility of the mixture for a desired phase, [-]

Returns

log\_phis [float] Log fugacity coefficient for each species, [-]

#### References

[1]

## 7.8.6 Redlich-Kwong Equation of State

**class** thermo.eos\_mix.**RKMIX**(*Tcs*, *Pcs*, *zs*, *omegas=None*, *kijs=None*, *T=None*, *P=None*, *V=None*, *fugacities=True*, *only\_l=False*, *only\_g=False*)

Bases: thermo.eos\_mix.EpsilonZeroMixingRules, thermo.eos\_mix.GCEOSMIX, thermo.eos.RK

Class for solving the Redlich Kwong [1] [2] cubic equation of state for a mixture of any number of compounds. Subclasses *thermo.eos.RK*. Solves the EOS on initialization and calculates fugacities for all components in all phases. Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V - b} - \frac{a}{V\sqrt{T}(V + b)}$$

$$a = \sum_{i} \sum_{j} z_{i}z_{j}a_{ij}$$

$$b = \sum_{i} z_{i}b_{i}$$

$$a_{ij} = (1 - k_{ij})\sqrt{a_{i}a_{j}}$$

$$a_{i} = \left(\frac{R^{2}(T_{c,i})^{2}}{9(\sqrt[3]{2} - 1)P_{c,i}}\right) = \frac{0.42748 \cdot R^{2}(T_{c,i})^{2}}{P_{c,i}}$$

$$b_{i} = \left(\frac{(\sqrt[3]{2} - 1)}{3}\right)\frac{RT_{c,i}}{P_{c,i}} = \frac{0.08664 \cdot RT_{c,i}}{P_{c,i}}$$

#### **Parameters**

Tcs [float] Critical temperatures of all compounds, [K]

Pcs [float] Critical pressures of all compounds, [Pa]

- zs [float] Overall mole fractions of all species, [-]
- **kijs** [list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 [-]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- V [float, optional] Molar volume, [m^3/mol]
- **omegas** [float, optional] Acentric factors of all compounds Not used in this equation of state!, [-]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

The PV solution for T is iterative.

#### References

[1], [2]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = RKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], zs=[0.5, 

→0.5], kijs=[[0,0],[0,0]])
>>> eos.V_l, eos.V_g
(4.048414781e-05, 0.00070060605863)
```

#### Attributes

- *d2delta\_dninjs* Helper method for calculating the second mole number derivatives (hessian) of *delta*.
- *d2delta\_dzizjs* Helper method for calculating the second composition derivatives (hessian) of *delta*.
- **d3delta\_dninjnks** Helper method for calculating the third partial mole number derivatives of *delta*.
- *ddelta\_dns* Helper method for calculating the mole number derivatives of *delta*.

*ddelta\_dzs* Helper method for calculating the composition derivatives of *delta*.

### **Methods**

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> and their first and second derivatives for the RK EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> for the RK EOS.
eos_pure	alias of thermo.eos.RK

### a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the RK EOS. This vectorized implementation is added for extra speed.

$$a\alpha = \frac{a}{\sqrt{\frac{T}{Tc}}}$$
$$\frac{da\alpha}{dT} = -\frac{a}{2T\sqrt{\frac{T}{Tc}}}$$
$$\frac{d^2a\alpha}{dT^2} = \frac{3a}{4T^2\sqrt{\frac{T}{Tc}}}$$

#### Parameters

T [float] Temperature, [K]

#### Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

### **Examples**

```
>>> eos = RKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],_

omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.a_alpha_and_derivatives_vectorized(115)

([0.1449810919468, 0.30019773677], [-0.000630352573681, -0.00130520755121], [8.

-2219900915e-06, 1.7024446320e-05])
```

### a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the RK EOS. This vectorized implementation is added for extra speed.

$$a\alpha = \frac{a}{\sqrt{\frac{T}{Tc}}}$$

Parameters

T [float] Temperature, [K]

Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### **Examples**

```
>>> eos = RKMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5],

→omegas=[0.04, 0.011], zs=[0.5, 0.5], kijs=[[0,0],[0,0]])

>>> eos.a_alphas_vectorized(115)

[0.1449810919468, 0.30019773677]
```

### property d2delta\_dninjs

Helper method for calculating the second mole number derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial n_i \partial n_j}\right)_{T,P,n_{k \neq i,j}} = 2b - b_i - b_j$$

#### Returns

**d2delta\_dninjs** [list[list[float]]] Second mole number derivative of *delta* of each component, [m^3/mol^3]

#### **Notes**

This derivative is checked numerically.

### property d2delta\_dzizjs

Helper method for calculating the second composition derivatives (hessian) of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^2 \delta}{\partial x_i \partial x_j}\right)_{T,P,x_{k \neq i,j}} = 0$$

### Returns

**d2delta\_dzizjs** [list[float]] Second Composition derivative of *delta* of each component, [m^3/mol]

### Notes

This derivative is checked numerically.

#### property d3delta\_dninjnks

Helper method for calculating the third partial mole number derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial^3 \delta}{\partial n_i \partial n_j \partial n_k}\right)_{T,P,n_{m \neq i,j,k}} = 2(-3b + b_i + b_j + b_k)$$

### Returns

**d3delta\_dninjnks** [list[list[float]]]] Third mole number derivative of *delta* of each component, [m^3/mol^4]

This derivative is checked numerically.

### property ddelta\_dns

Helper method for calculating the mole number derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial\delta}{\partial n_i}\right)_{T,P,n_{i\neq j}} = (b_i - b)$$

Returns

ddelta\_dns [list[float]] Mole number derivative of delta of each component, [m^3/mol^2]

### Notes

This derivative is checked numerically.

### property ddelta\_dzs

Helper method for calculating the composition derivatives of *delta*. Note this is independent of the phase.

$$\left(\frac{\partial \delta}{\partial x_i}\right)_{T,P,x_{i\neq j}} = b_i$$

Returns

ddelta\_dzs [list[float]] Composition derivative of delta of each component, [m^3/mol]

#### Notes

This derivative is checked numerically.

### eos\_pure

alias of thermo.eos.RK

## 7.8.7 Ideal Gas Equation of State

class thermo.eos\_mix.IGMIX(zs, T=None, P=None, V=None, Tcs=None, Pcs=None, omegas=None, kijs=None, fugacities=True, only\_l=False, only\_g=False)

Bases: thermo.eos\_mix.EpsilonZeroMixingRules, thermo.eos\_mix.GCEOSMIX, thermo.eos.IG

Class for solving the ideal gas [1] [2] equation of state for a mixture of any number of compounds. Subclasses *thermo.eos.IG*. Solves the EOS on initialization. Two of T, P, and V are needed to solve the EOS.

$$P = \frac{RT}{V}$$

### **Parameters**

zs [list[float]] Overall mole fractions of all species, [-]

T [float, optional] Temperature, [K]

**P** [float, optional] Pressure, [Pa]

V [float, optional] Molar volume, [m^3/mol]

Tcs [list[float], optional] Critical temperatures of all compounds, [K]

- Pcs [list[float], optional] Critical pressures of all compounds, [Pa]
- **omegas** [list[float], optional] Acentric factors of all compounds Not used in this equation of state!, [-]
- **kijs** [list[list[float]], optional] n\*n size list of lists with binary interaction parameters for the Van der Waals mixing rules, default all 0 and not used[-]
- **fugacities** [bool, optional] Whether or not to calculate fugacity related values (phis, log phis, and fugacities); default True, [-]
- **only\_l** [bool, optional] When true, if there is a liquid and a vapor root, only the liquid root (and properties) will be set; default False, [-]
- **only\_g** [bool, optional] When true, if there is a liquid and a vapor root, only the vapor root (and properties) will be set; default False, [-]

Many properties of this object are zero. Many of the arguments are not used and are provided for consistency only.

### References

[1], [2]

### **Examples**

T-P initialization, nitrogen-methane at 115 K and 1 MPa:

```
>>> eos = IGMIX(T=115, P=1E6, Tcs=[126.1, 190.6], Pcs=[33.94E5, 46.04E5], omegas=[0.

→04, .008], zs=[0.5, 0.5])
>>> eos.phase, eos.V_g
('g', 0.0009561632010876225)
```

### Methods

a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> and their first and second derivatives for the Ideal Gas EOS.
a_alphas_vectorized(T)	Method to calculate the pure-component a_alphas
	for the Ideal Gas EOS.
eos_pure	alias of thermo.eos.IG

### a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for the Ideal Gas EOS. This vectorized implementation is added for extra speed.

$$a\alpha = 0$$
$$\frac{da\alpha}{dT} = 0$$

$$\frac{d^2 a \alpha}{dT^2} = 0$$

### Parameters

T [float] Temperature, [K]

Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

### a\_alphas\_vectorized(T)

Method to calculate the pure-component *a\_alphas* for the Ideal Gas EOS. This vectorized implementation is added for extra speed.

 $a\alpha = 0$ 

#### **Parameters**

T [float] Temperature, [K]

#### Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### eos\_pure

alias of thermo.eos.IG

## 7.8.8 Different Mixing Rules

### class thermo.eos\_mix.EpsilonZeroMixingRules

### Attributes

- **d2epsilon\_dninjs** Helper method for calculating the second mole number derivatives (hessian) of *epsilon*.
- **d2epsilon\_dzizjs** Helper method for calculating the second composition derivatives (hessian) of *epsilon*.
- **d3epsilon\_dninjnks** Helper method for calculating the third partial mole number derivatives of *epsilon*.
- depsilon\_dns Helper method for calculating the mole number derivatives of epsilon.

**depsilon\_dzs** Helper method for calculating the composition derivatives of *epsilon*.

class thermo.eos\_mix.PSRKMixingRules
 Bases: object

### **Methods**

<pre>a_alpha_and_derivatives(T[, full, quick,])</pre>	Method to calculate <i>a_alpha</i> and its first and second
	derivatives for an EOS with the PSRK mixing rules.

#### $\mathbf{A} = -0.6466271649250525$

### **a\_alpha\_and\_derivatives**(*T*, *full=True*, *quick=True*, *pure\_a\_alphas=True*)

Method to calculate  $a\_alpha$  and its first and second derivatives for an EOS with the PSRK mixing rules. Returns  $a\_alpha$ ,  $da\_alpha\_dT$ , and  $d2a\_alpha\_dT2$ .

For use in some methods, this returns only *a\_alpha* if *full* is False.

$$\alpha = bRT \left[ \sum_{i} \frac{z_{i}\alpha_{i}}{b_{i}RT} + \frac{1}{A} \left( \frac{G^{E}}{RT} + \sum_{i} z_{i} \ln \left( \frac{b}{b_{i}} \right) \right) \right]$$

$$\frac{\partial \alpha}{\partial T} = RTb \left[ \sum_{i} \left( \frac{z_{i}\frac{\partial \alpha_{i}}{\partial T}}{RTb_{i}} - \frac{z_{i}\alpha_{i}}{RT^{2}b_{i}} \right) + \frac{1}{A} \left( \frac{\partial G^{E}}{\partial T} - \frac{G^{E}}{RT^{2}} \right) \right] + \frac{\alpha}{T}$$

$$\frac{\partial^{2}\alpha}{\partial T^{2}} = b \left[ \sum_{i} \left( \frac{z_{i}\frac{\partial^{2}\alpha_{i}}{\partial T}}{b_{i}} - \frac{2z_{i}\frac{\partial \alpha_{i}}{\partial T}}{Tb_{i}} + \frac{2z_{i}\alpha_{i}}{T^{2}b_{i}} \right) + \frac{2}{T} \left[ \sum_{i} \left( \frac{z_{i}\frac{\partial \alpha_{i}}{\partial T}}{b_{i}} - \frac{z_{i}\alpha_{i}}{Tb_{i}} \right) + \frac{1}{A} \left( \frac{\partial G^{E}}{\partial T} - \frac{G^{E}}{T} \right) \right] + \frac{1}{A} \left( \frac{\partial^{2}G^{E}}{\partial T^{2}} - \frac{2}{T}\frac{\partial C}{\partial T} \right)$$

Parameters

T [float] Temperature, [K]

full [bool, optional] If False, calculates and returns only a\_alpha

quick [bool, optional] Only the quick variant is implemented; it is little faster anyhow

**pure\_a\_alphas** [bool, optional] Whether or not to recalculate the a\_alpha terms of pure components (for the case of mixtures only) which stay the same as the composition changes (i.e in a PT flash), [-]

### Returns

a\_alpha [float] Coefficient calculated by PSRK-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by PSRK-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by PSRK-specific method, [J^2/mol^2/Pa/K\*\*2]

u = 1.1

## 7.8.9 Lists of Equations of State

```
thermo.eos_mix.eos_mix_list = [<class 'thermo.eos_mix.PRMIX'>, <class
'thermo.eos_mix.SRKMIX'>, <class 'thermo.eos_mix.PR78MIX'>, <class
'thermo.eos_mix.VDWMIX'>, <class 'thermo.eos_mix.PRSVMIX'>, <class
'thermo.eos_mix.PRSV2MIX'>, <class 'thermo.eos_mix.TWUPRMIX'>, <class
'thermo.eos_mix.TWUSRKMIX'>, <class 'thermo.eos_mix.APISRKMIX'>, <class
'thermo.eos_mix.IGMIX'>, <class 'thermo.eos_mix.RKMIX'>, <class
'thermo.eos_mix.PRMIXTranslatedConsistent'>, <class</pre>
'thermo.eos_mix.PRMIXTranslatedPPJP'>, <class</pre>
'thermo.eos_mix.SRKMIXTranslatedConsistent'>, <class 'thermo.eos_mix.PRMIXTranslated'>,
<class 'thermo.eos_mix.SRKMIXTranslated'>]
     List of all exported EOS classes.
thermo.eos_mix.eos_mix_no_coeffs_list = [<class 'thermo.eos_mix.PRMIX'>, <class
'thermo.eos_mix.SRKMIX'>, <class 'thermo.eos_mix.PR78MIX'>, <class
'thermo.eos_mix.VDWMIX'>, <class 'thermo.eos_mix.TWUPRMIX'>, <class
'thermo.eos_mix.TWUSRKMIX'>, <class 'thermo.eos_mix.IGMIX'>, <class
'thermo.eos_mix.RKMIX'>, <class 'thermo.eos_mix.PRMIXTranslatedConsistent'>, <class
'thermo.eos_mix.PRMIXTranslated'>, <class 'thermo.eos_mix.SRKMIXTranslated'>, <class
'thermo.eos_mix.PRMIXTranslatedPPJP'>, <class
'thermo.eos_mix.SRKMIXTranslatedConsistent'>]
     List of all exported EOS classes that do not require special parameters or can fill in their special parameters from
     other specified parameters.
```

# 7.9 Cubic Equations of State Utilities (thermo.eos\_mix\_methods)

This file contains a number of overflow methods for EOSs which for various reasons are better implemented as functions. Documentation is not provided for this file and no methods are intended to be used outside this library.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

• Alpha Function Mixing Rules

## 7.9.1 Alpha Function Mixing Rules

These are where the bulk of the time is spent in solving the equation of state. For that reason, these functional forms often duplicate functionality but have different performance characteristics.

Implementations which store N^2 matrices for other calculations:

thermo.eos\_mix\_methods.a\_alpha\_aijs\_composition\_independent(a\_alphas, kijs)

Calculates the matrix  $(a\alpha)_{ij}$  as well as the array  $\sqrt{(a\alpha)_i}$  and the matrix  $\frac{1}{\sqrt{(a\alpha)_i}\sqrt{(a\alpha)_j}}$ .

$$(a\alpha)_{ij} = (1 - k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$$

This routine is efficient in both numba and PyPy, but it is generally better to avoid calculating and storing **any**  $N^2$  matrices. However, this particular calculation only depends on *T* so in some circumstances this can be feasible.

### **Parameters**

**a\_alphas** [list[float]] EOS attractive terms, [J^2/mol^2/Pa]

kijs [list[list[float]]] Constant kijs, [-]

Returns

**a\_alpha\_ijs** [list[list[float]]] Matrix of  $(1 - k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$ , [J^2/mol^2/Pa] **a\_alpha\_roots** [list[float]] Array of  $\sqrt{(a\alpha)_i}$  values, [J/mol/Pa^0.5] **a\_alpha\_ij\_roots\_inv** [list[list[float]]] Matrix of  $\frac{1}{\sqrt{(a\alpha)_i}\sqrt{(a\alpha)_j}}$ , [mol^2\*Pa/J^2]

## **Examples**

thermo.eos\_mix\_methods.a\_alpha\_aijs\_composition\_independent\_support\_zeros(a\_alphas, kijs)

thermo.eos\_mix\_methods.a\_alpha\_and\_derivatives\_full(a\_alphas, da\_alpha\_dTs, d2a\_alpha\_dT2s, T, zs, kijs, a\_alpha\_ijs=None, a\_alpha\_roots=None,

a\_alpha\_ij\_roots\_inv=None)

Calculates the *a\_alpha* term, and its first two temperature derivatives, for an equation of state along with the matrix quantities calculated in the process.

$$\begin{aligned} a\alpha &= \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij} \\ \frac{\partial(a\alpha)}{\partial T} &= \sum_{i} \sum_{j} z_{i} z_{j} \frac{\partial(a\alpha)_{ij}}{\partial T} \\ \frac{\partial^{2}(a\alpha)}{\partial T^{2}} &= \sum_{i} \sum_{j} z_{i} z_{j} \frac{\partial^{2}(a\alpha)_{ij}}{\partial T^{2}} \\ (a\alpha)_{ij} &= (1 - k_{ij}) \sqrt{(a\alpha)_{i}(a\alpha)_{j}} \\ \frac{\partial(a\alpha)_{ij}}{\partial T} &= \frac{\sqrt{a\alpha_{i}(T) a\alpha_{j}(T)} (1 - k_{ij}) \left(\frac{a\alpha_{i}(T) \frac{d}{dT} a\alpha_{j}(T)}{2} + \frac{a\alpha_{j}(T) \frac{d}{dT} a\alpha_{i}(T)}{2}\right)}{a\alpha_{i}(T) a\alpha_{j}(T)} \\ \frac{\partial^{2}(a\alpha)_{ij}}{\partial T^{2}} &= -\frac{\sqrt{a\alpha_{i}(T) a\alpha_{j}(T)} (k_{ij} - 1) \left(\frac{(a\alpha_{i}(T) \frac{d}{dT} a\alpha_{j}(T) + a\alpha_{j}(T) \frac{d}{dT} a\alpha_{i}(T))^{2}}{4a\alpha_{i}(T) a\alpha_{j}(T)} - \frac{(a\alpha_{i}(T) \frac{d}{dT} a\alpha_{j}(T) + a\alpha_{j}(T) \frac{d}{dT} a\alpha_{i}(T) \frac{d}{dT} a\alpha_{j}(T)}{a\alpha_{i}(T)} \\ \frac{\partial^{2}(a\alpha)_{ij}}{\partial T^{2}} &= -\frac{\sqrt{a\alpha_{i}(T) a\alpha_{j}(T)} (k_{ij} - 1) \left(\frac{(a\alpha_{i}(T) \frac{d}{dT} a\alpha_{j}(T) + a\alpha_{j}(T) \frac{d}{dT} a\alpha_{i}(T)}{4a\alpha_{i}(T) a\alpha_{j}(T)} - \frac{(a\alpha_{i}(T) \frac{d}{dT} a\alpha_{j}(T) + a\alpha_{i}(T) \frac{d}{dT} a\alpha_{i}(T)}{2a\alpha_{j}(T)} - \frac{a\alpha_{i}(T) \frac{d}{dT} a\alpha_{i}(T) \frac{d}{dT} a\alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \frac{d}{dT} \alpha_{i}(T) \frac{d}{dT} \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \frac{d}{dT} \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \frac{d}{dT} \alpha_{i}(T) \frac{d}{dT} \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha_{i}(T)} - \frac{a\alpha_{i}(T) \alpha_{i}(T) \alpha_{i}(T)}{a\alpha$$

#### **Parameters**

a\_alphas [list[float]] EOS attractive terms, [J^2/mol^2/Pa]

da\_alpha\_dTs [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]

- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]
- T [float] Temperature, not used, [K]
- zs [list[float]] Mole fractions of each species
- kijs [list[list[float]]] Constant kijs, [-]
- **a\_alpha\_ijs** [list[list[float]], optional] Matrix of  $(1 k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$ , [J^2/mol^2/Pa]
- **a\_alpha\_roots** [list[float], optional] Array of  $\sqrt{(a\alpha)_i}$  values, [J/mol/Pa^0.5]
- **a\_alpha\_ij\_roots\_inv** [list[list[float]], optional] Matrix of  $\frac{1}{\sqrt{(a\alpha)_i}\sqrt{(a\alpha)_i}}$ , [mol^2\*Pa/J^2]

#### Returns

- **a\_alpha** [float] EOS attractive term, [J^2/mol^2/Pa]
- **da\_alpha\_dT** [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- d2a\_alpha\_dT2 [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]
- **a\_alpha\_ijs** [list[list[float]], optional] Matrix of  $(1 k_{ij})\sqrt{(a\alpha)_i(a\alpha)_j}$ , [J^2/mol^2/Pa]

**da\_alpha\_dT\_ijs** [list[float]], optional] Matrix of  $\frac{\partial(a\alpha)_{ij}}{\partial T}$ , [J^2/mol^2/Pa/K]

**d2a\_alpha\_dT2\_ijs** [list[list[float]], optional] Matrix of  $\frac{\partial^2(a\alpha)_{ij}}{\partial T^2}$ , [J^2/mol^2/Pa/K^2]

## **Examples**

```
>>> kijs = [[0,.083],[0.083,0]]
>>> zs = [0.1164203, 0.8835797]
>>> a_alphas = [0.2491099357671155, 0.6486495863528039]
>>> da_alpha_dTs = [-0.0005102028006086241, -0.0011131153520304886]
>>> d2a_alpha_dT2s = [1.8651128859234162e-06, 3.884331923127011e-06]
>>> a_alpha, da_alpha_dT, d2a_alpha_dT2, a_alpha_ijs, da_alpha_dT_ijs, d2a_alpha_
→dT2_ijs = a_alpha_and_derivatives_full(a_alphas=a_alphas, da_alpha_dTs=da_alpha_
→dTs, d2a_alpha_dT2s=d2a_alpha_dT2s, T=299.0, zs=zs, kijs=kijs)
>>> a_alpha, da_alpha_dT, d2a_alpha_dT2
(0.58562139582, -0.001018667672, 3.56669817856e-06)
>>> a_alpha_ijs
[[0.2491099357, 0.3686123937], [0.36861239374, 0.64864958635]]
>>> da_alpha_dT_ijs
[[-0.000510202800, -0.0006937567844], [-0.000693756784, -0.00111311535]]
>>> d2a_alpha_dT2_ijs
[[1.865112885e-06, 2.4734471244e-06], [2.4734471244e-06, 3.8843319e-06]]
```

Compute only the alpha term itself:

thermo.eos\_mix\_methods.a\_alpha\_and\_derivatives(a\_alphas, T, zs, kijs, a\_alpha\_ijs=None, a\_alpha\_roots=None, a\_alpha\_ij\_roots\_inv=None)

Faster implementations which do not store N^2 matrices:

thermo.eos\_mix\_methods.a\_alpha\_quadratic\_terms(a\_alphas, a\_alpha\_roots, T, zs, kijs,

a\_alpha\_j\_rows=None, vec0=None)

Calculates the *a\_alpha* term for an equation of state along with the vector quantities needed to compute the fugacities of the mixture. This routine is efficient in both numba and PyPy.

$$a\alpha = \sum_{i} \sum_{j} z_{i} z_{j} (a\alpha)_{ij}$$
$$(a\alpha)_{ij} = (1 - k_{ij}) \sqrt{(a\alpha)_{i} (a\alpha)_{j}}$$

The secondary values are as follows:

$$\sum_{i} y_i(a\alpha)_{ij}$$

#### Parameters

- **a\_alphas** [list[float]] EOS attractive terms, [J^2/mol^2/Pa]
- **a\_alpha\_roots** [list[float]] Square roots of *a\_alphas*; provided for speed [J/mol/Pa^0.5]
- T [float] Temperature, not used, [K]
- zs [list[float]] Mole fractions of each species
- **kijs** [list[list[float]]] Constant kijs, [-]
- **a\_alpha\_j\_rows** [list[float], optional] EOS attractive term row destimation vector (does not need to be zeroed, should be provided to prevent allocations), [J^2/mol^2/Pa]
- **vec0** [list[float], optional] Empty vector, used in internal calculations, provide to avoid the allocations; does not need to be zeroed, [-]

#### Returns

- a\_alpha [float] EOS attractive term, [J^2/mol^2/Pa]
- a\_alpha\_j\_rows [list[float]] EOS attractive term row sums, [J^2/mol^2/Pa]

## Notes

Tried moving the i=j loop out, no difference in speed, maybe got a bit slower in PyPy.

## **Examples**

```
>>> kijs = [[0,.083],[0.083,0]]
>>> zs = [0.1164203, 0.8835797]
>>> a_alphas = [0.2491099357671155, 0.6486495863528039]
>>> a_alpha_roots = [i**0.5 for i in a_alphas]
>>> a_alpha, a_alpha_j_rows = a_alpha_quadratic_terms(a_alphas, a_alpha_roots, 299.
...0, zs, kijs)
>>> a_alpha, a_alpha_j_rows
(0.58562139582, [0.35469988173, 0.61604757237])
```

thermo.eos\_mix\_methods.a\_alpha\_and\_derivatives\_quadratic\_terms(a\_alphas, a\_alpha\_roots, da\_alpha\_dTs, d2a\_alpha\_dT2s,

*T*, *zs*, *kijs*, *a\_alpha\_j\_rows=None*, *da\_alpha\_dT\_j\_rows=None*) Calculates the *a\_alpha* term, and its first two temperature derivatives, for an equation of state along with the vector quantities needed to compute the fugacitie and temperature derivatives of fugacities of the mixture. This routine is efficient in both numba and PyPy.

The secondary values are as follows:

$$\sum_{i} y_{i}(a\alpha)_{ij}$$
$$\sum_{i} y_{i} \frac{\partial (a\alpha)_{ij}}{\partial T}$$

#### **Parameters**

a\_alphas [list[float]] EOS attractive terms, [J^2/mol^2/Pa]

**a\_alpha\_roots** [list[float]] Square roots of *a\_alphas*; provided for speed [J/mol/Pa^0.5]

- da\_alpha\_dTs [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOSspecific method, [J^2/mol^2/Pa/K\*\*2]
- T [float] Temperature, not used, [K]
- zs [list[float]] Mole fractions of each species
- kijs [list[list[float]]] Constant kijs, [-]

#### Returns

a\_alpha [float] EOS attractive term, [J^2/mol^2/Pa]

- **da\_alpha\_dT** [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- d2a\_alpha\_dT2 [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]
- a\_alpha\_j\_rows [list[float]] EOS attractive term row sums, [J^2/mol^2/Pa]
- **da\_alpha\_dT\_j\_rows** [list[float]] Temperature derivative of EOS attractive term row sums, [J^2/mol^2/Pa/K]

#### **Examples**

```
>>> kijs = [[0,.083],[0.083,0]]
>>> zs = [0.1164203, 0.8835797]
>>> a_alphas = [0.2491099357671155, 0.6486495863528039]
>>> a_alpha_roots = [i**0.5 for i in a_alphas]
>>> da_alpha_dTs = [-0.0005102028006086241, -0.0011131153520304886]
>>> d2a_alpha_dT2s = [1.8651128859234162e-06, 3.884331923127011e-06]
>>> a_alpha_and_derivatives_quadratic_terms(a_alphas, a_alpha_roots, da_alpha_dTs,______
___d2a_alpha_dT2s, 299.0, zs, kijs)
(0.58562139582, -0.001018667672, 3.56669817856e-06, [0.35469988173, 0.61604757237],_______
```

# 7.10 Cubic Equations of State Volume Solvers (thermo.eos\_volume)

Some of the methods implemented here are numerical while others are analytical.

The cubic EOS can be rearranged into the following polynomial form:

$$0 = Z^{3} + (\delta' - B' - 1)Z^{2} + [\theta' + \epsilon' - \delta(B' + 1)]Z - [\epsilon'(B' + 1) + \theta'\eta']$$
$$B' = \frac{bP}{RT}$$
$$\delta' = \frac{\delta P}{RT}$$
$$\theta' = \frac{a\alpha P}{(RT)^{2}}$$
$$\epsilon' = \epsilon \left(\frac{P}{RT}\right)^{2}$$

The range of pressures, temperatures, and  $a\alpha$  values is so large that almost all analytical solutions produce huge errors in some conditions. Because the EOS volume cannot be under *b*, this often results in a root being ignored where there should have been a liquid-like root detected.

A number of plots showing the relative error in volume calculation are shown below to demonstrate how different methods work.

• Analytical Solvers

- Numerical Solvers
- Higher-Precision Solvers

# 7.10.1 Analytical Solvers

thermo.eos\_volume.volume\_solutions\_Cardano(T, P, b, delta, epsilon, a\_alpha)

Calculate the molar volume solutions to a cubic equation of state using Cardano's formula, and a few tweaks to improve numerical precision. This solution is quite fast in general although it involves powers or trigonometric functions. However, it has numerical issues at many seemingly random areas in the low pressure region.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]

b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

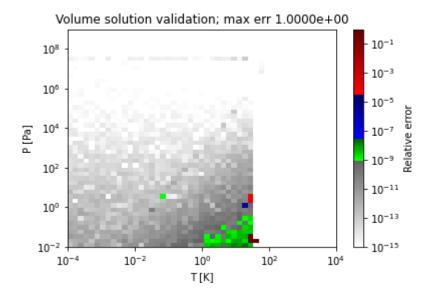
a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

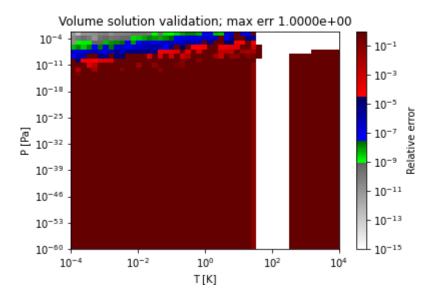
## Returns

Vs [list[float]] Three possible molar volumes, [m^3/mol]

## Notes

Two sample regions where this method does not obtain the correct solution (PR EOS for hydrogen) are as follows:





## References

```
[1]
```

## thermo.eos\_volume.volume\_solutions\_fast(T, P, b, delta, epsilon, a\_alpha)

Solution of this form of the cubic EOS in terms of volumes. Returns three values, all with some complex part. This is believed to be the fastest analytical formula, and while it does not suffer from the same errors as Cardano's formula, it has plenty of its own numerical issues.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]

b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Returns

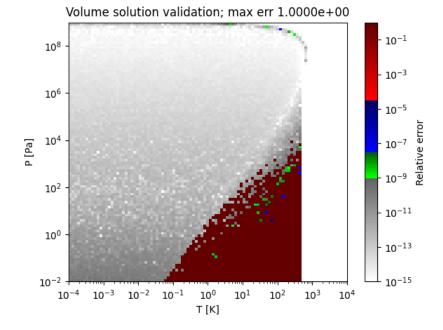
Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]

## Notes

Using explicit formulas, as can be derived in the following example, is faster than most numeric root finding techniques, and finds all values explicitly. It takes several seconds.

```
>>> from sympy import *
>>> P, T, V, R, b, a, delta, epsilon, alpha = symbols('P, T, V, R, b, a, delta, 
→epsilon, alpha')
>>> Tc, Pc, omega = symbols('Tc, Pc, omega')
>>> CUBIC = R*T/(V-b) - a*alpha/(V*V + delta*V + epsilon) - P
>>> #solve(CUBIC, V)
```

A sample region where this method does not obtain the correct solution (PR EOS for methanol) is as follows:



#### References

[1]

## thermo.eos\_volume.volume\_solutions\_a1(T, P, b, delta, epsilon, a\_alpha)

Solution of this form of the cubic EOS in terms of volumes. Returns three values, all with some complex part. This uses an analytical solution for the cubic equation with the leading coefficient set to 1 as in the EOS case; and the analytical solution is the one recommended by Mathematica.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]

b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

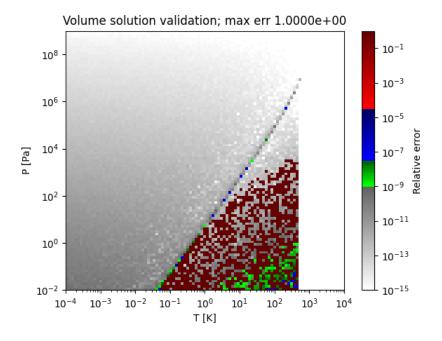
epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Returns

Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]

A sample region where this method does not obtain the correct solution (PR EOS for methanol) is as follows:



## **Examples**

Numerical precision is always challenging and has edge cases. The following results all havev imaginary components, but depending on the math library used by the compiler even the first complex digit may not match!

```
>>> volume_solutions_a1(8837.07874361444, 216556124.0631852, 0.0003990176625589891, 

→0.0010590390565805598, -1.5069972655436541e-07, 7.20417995032918e-15)

((0.000738308-7.5337e-20j), (-0.001186094-6.52444e-20j), (0.000127055+6.52444e-20j))
```

thermo.eos\_volume.volume\_solutions\_a2(T, P, b, delta, epsilon, a\_alpha)

Solution of this form of the cubic EOS in terms of volumes. Returns three values, all with some complex part. This uses an analytical solution for the cubic equation with the leading coefficient set to 1 as in the EOS case; and the analytical solution is the one recommended by Maple.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]
- b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

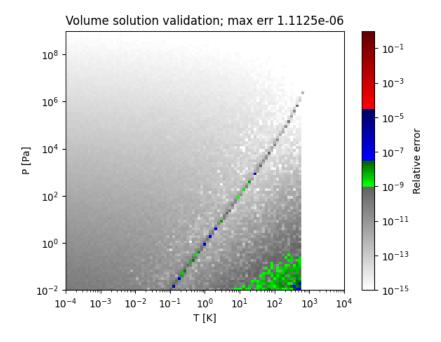
epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Returns

Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]

A sample region where this method does not obtain the correct solution (SRK EOS for decane) is as follows:



thermo.eos\_volume.volume\_solutions\_numpy(T, P, b, delta, epsilon, a\_alpha)

Calculate the molar volume solutions to a cubic equation of state using NumPy's *roots* function, which is a power series iterative matrix solution that is very stable but does not have full precision in some cases.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]

b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

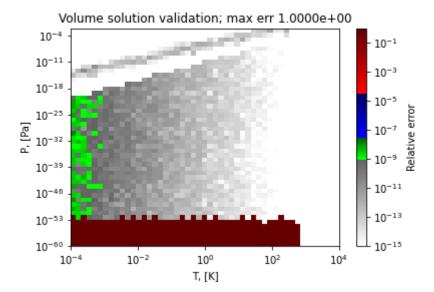
delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

- epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]
- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### Returns

Vs [list[float]] Three possible molar volumes, [m^3/mol]

A sample region where this method does not obtain the correct solution (SRK EOS for ethane) is as follows:



## References

#### [1]

thermo.eos\_volume.volume\_solutions\_ideal( $T, P, b=0.0, delta=0.0, epsilon=0.0, a_alpha=0.0$ ) Calculate the ideal-gas molar volume in a format compatible with the other cubic EOS solvers. The ideal gas volume is the first element; and the second and third elements are zero. This is implemented to allow the ideal-gas model to be compatible with the cubic models, whose equations do not work with parameters of zero.

## Parameters

- T [float] Temperature, [K]
- **P** [float] Pressure, [Pa]

**b** [float, optional] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float, optional] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float, optional] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float, optional] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Returns

Vs [list[float]] Three possible molar volumes, [m^3/mol]

## **Examples**

```
>>> volume_solutions_ideal(T=300, P=1e7)
(0.0002494338785445972, 0.0, 0.0)
```

# 7.10.2 Numerical Solvers

thermo.eos\_volume.volume\_solutions\_halley(T, P, b, delta, epsilon, a\_alpha)

Halley's method based solver for cubic EOS volumes based on the idea of initializing from a single liquid-like guess which is solved precisely, deflating the cubic analytically, solving the quadratic equation for the next two volumes, and then performing two halley steps on each of them to obtain the final solutions. This method does not calculate imaginary roots - they are set to zero on detection. This method has been rigorously tested over a wide range of conditions.

The method uses the standard combination of bisection to provide high and low boundaries as well, to keep the iteration always moving forward.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]

b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Returns

Vs [tuple[float]] Three possible molar volumes, [m^3/mol]

## Notes

A sample region where this method works perfectly is shown below:

thermo.eos\_volume.volume\_solutions\_NR(T, P, b, delta, epsilon, a\_alpha, tries=0)

Newton-Raphson based solver for cubic EOS volumes based on the idea of initializing from an analytical solver. This algorithm can only be described as a monstrous mess. It is fairly fast for most cases, but about 3x slower than *volume\_solutions\_halley*. In the worst case this will fall back to *mpmath*.

## Parameters

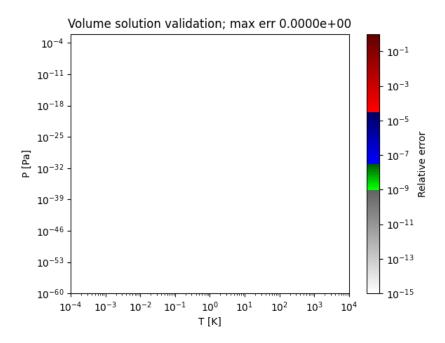
- T [float] Temperature, [K]
- P [float] Pressure, [Pa]
- b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

**tries** [int, optional] Internal parameter as this function will call itself if it needs to; number of previous solve attempts, [-]



## Returns

Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]

## Notes

Sample regions where this method works perfectly are shown below:

## thermo.eos\_volume.volume\_solutions\_NR\_low\_P(T, P, b, delta, epsilon, a\_alpha)

Newton-Raphson based solver for cubic EOS volumes designed specifically for the low-pressure regime. Seeks only two possible solutions - an ideal gas like one, and one near the eos covolume b - as the initializations are R\*T/P and b\*1.000001.

## Parameters

- T [float] Temperature, [K]
- P [float] Pressure, [Pa]
- **b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

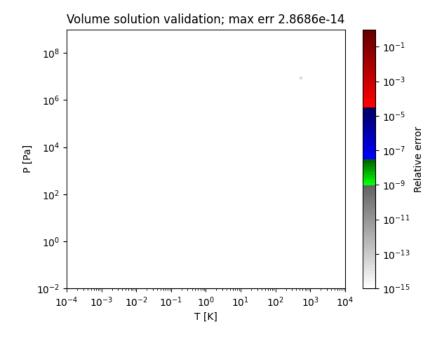
delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

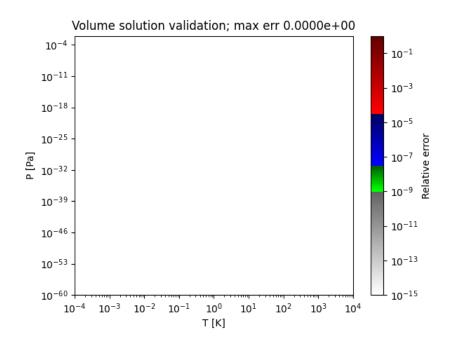
epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- **tries** [int, optional] Internal parameter as this function will call itself if it needs to; number of previous solve attempts, [-]

## Returns

Vs [tuple[complex]] Three possible molar volumes (third one is hardcoded to 1j), [m^3/mol]





The algorithm is NR, with some checks that will switch the solver to brenth some of the time.

# 7.10.3 Higher-Precision Solvers

## thermo.eos\_volume.volume\_solutions\_mpmath(T, P, b, delta, epsilon, a\_alpha, dps=50)

Solution of this form of the cubic EOS in terms of volumes, using the *mpmath* arbitrary precision library. The number of decimal places returned is controlled by the *dps* parameter.

This function is the reference implementation which provides exactly correct solutions; other algorithms are compared against this one.

## Parameters

- **T** [float] Temperature, [K]
- P [float] Pressure, [Pa]
- b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

dps [int] Number of decimal places in the result by mpmath, [-]

## Returns

Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]

## Notes

Although *mpmath* has a cubic solver, it has been found to fail to solve in some cases. Accordingly, the algorithm is as follows:

Working precision is dps plus 40 digits; and if P < 1e-10 Pa, it is dps plus 400 digits. The input parameters are converted exactly to mpf objects on input.

*polyroots* from mpmath is used with *maxsteps=2000*, and extra precision of 15 digits. If the solution does not converge, 20 extra digits are added up to 8 times. If no solution is found, mpmath's *findroot* is called on the pressure error function using three initial guesses from another solver.

Needless to say, this function is quite slow.

## References

[1]

## **Examples**

Test case which presented issues for PR EOS (three roots were not being returned):

```
>>> volume_solutions_mpmath(0.01, 1e-05, 2.5405184201558786e-05, 5.081036840311757e-
→05, -6.454233843151321e-10, 0.3872747173781095)
(mpf('0.0000254054613415548712260258773060137'), mpf('4.
→66038025602155259976574392093252'), mpf('8309.80218708657190094424659859346'))
```

thermo.eos\_volume.volume\_solutions\_mpmath\_float(T, P, b, delta, epsilon, a\_alpha)

Simple wrapper around *volume\_solutions\_mpmath* which uses the default parameters and returns the values as floats.

## **Parameters**

- **T** [float] Temperature, [K]
- P [float] Pressure, [Pa]

**b** [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

dps [int] Number of decimal places in the result by mpmath, [-]

## Returns

Vs [tuple[complex]] Three possible molar volumes, [m^3/mol]

## **Examples**

Test case which presented issues for PR EOS (three roots were not being returned):

```
>>> volume_solutions_mpmath_float(0.01, 1e-05, 2.5405184201558786e-05, 5.

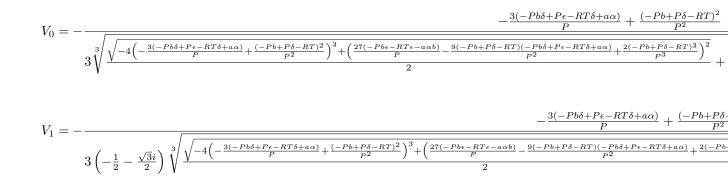
→081036840311757e-05, -6.454233843151321e-10, 0.3872747173781095)

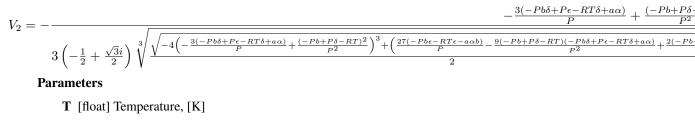
((2.540546134155487e-05+0j), (4.660380256021552+0j), (8309.802187086572+0j))
```

thermo.eos\_volume.volume\_solutions\_sympy(T, P, b, delta, epsilon, a\_alpha)

Solution of this form of the cubic EOS in terms of volumes, using the *sympy* mathematical library with real numbers.

This function is generally slow, and somehow still has more than desired error in the real and complex result.





**P** [float] Pressure, [Pa]

b [float] Coefficient calculated by EOS-specific method, [m^3/mol]

delta [float] Coefficient calculated by EOS-specific method, [m^3/mol]

epsilon [float] Coefficient calculated by EOS-specific method, [m^6/mol^2]

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

#### Returns

Vs [tuple[sympy.Rational]] Three possible molar volumes, [m^3/mol]

## **Notes**

The solution can be derived as follows:

```
>>> from sympy import *
>>> P, T, V, R, b, delta, epsilon = symbols('P, T, V, R, b, delta, epsilon')
>>> a_alpha = Symbol(r'a \alpha')
>>> CUBIC = R*T/(V-b) - a_alpha/(V*V + delta*V + epsilon) - P
>>> V_slns = solve(CUBIC, V)
```

#### References

[1]

## **Examples**

```
>>> Vs = volume_solutions_sympy(0.01, 1e-05, 2.5405184201558786e-05, 5.

~081036840311757e-05, -6.454233843151321e-10, 0.3872747173781095)

>>> [complex(v) for v in Vs]

[(2.540546e-05+2.402202278e-12j), (4.660380256-2.40354958e-12j), (8309.80218+1.

~348096981e-15j)]
```

# 7.11 Cubic Equation of State Alpha Functions (thermo.eos\_alpha\_functions)

This module contains implementations of the calculation of pure-component EOS  $a\alpha$  parameters in a vectorized way. Functions for calculating their temperature derivatives as may be necessary are included as well.

For certain alpha functions, a class is available to provide these functions to and class that inherits from it.

A mixing rule must be used on the *a\_alphas* to get the overall *a\_alpha* term.

- Vectorized Alpha Functions
- Vectorized Alpha Functions With Derivatives
- Class With Alpha Functions
- Pure Alpha Functions

# 7.11.1 Vectorized Alpha Functions

thermo.eos\_alpha\_functions.**PR\_a\_alphas\_vectorized**(*T*, *Tcs*, *ais*, *kappas*, *a\_alphas=None*) Calculates the *a\_alpha* terms for the Peng-Robinson equation of state given the critical temperatures *Tcs*, constants *ais*, and *kappas*.

$$a_i \alpha(T)_i = a_i [1 + \kappa_i (1 - \sqrt{T_{r,i}})]^2$$

## **Parameters**

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

- **ais** [list[float]] *a* parameters of cubic EOS,  $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]
- **kappas** [list[float]] kappa parameters of Peng-Robinson EOS; formulas vary, but the original form uses  $\kappa_i = 0.37464 + 1.54226\omega_i 0.26992\omega_i^2$ , [-]
- **a\_alphas** [list[float], optional] Vector for pure component *a\_alpha* terms in the cubic EOS to be calculated and stored in, [Pa\*m^6/mol^2]

## Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

## **Examples**

```
>>> Tcs = [469.7, 507.4, 540.3]
>>> ais = [2.0698956357716662, 2.7018068455659545, 3.3725793885832323]
>>> kappas = [0.74192743008, 0.819919992, 0.8800122140799999]
>>> PR_a_alphas_vectorized(322.29, Tcs=Tcs, ais=ais, kappas=kappas)
[2.6306811679, 3.6761503348, 4.8593286234]
```

thermo.eos\_alpha\_functions.SRK\_a\_alphas\_vectorized(T, Tcs, ais, ms, a\_alphas=None)

Calculates the *a\_alpha* terms for the SRK equation of state given the critical temperatures *Tcs*, constants *ais*, and *kappas*.

$$a_i \alpha(T)_i = \left[1 + m_i \left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\right]^2$$

#### Parameters

**T** [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

- **ais** [list[float]] *a* parameters of cubic EOS,  $a_i = \frac{0.42748 \cdot R^2(T_{c,i})^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]
- **ms** [list[float]] *m* parameters of SRK EOS; formulas vary, but the original form uses  $m_i = 0.480 + 1.574\omega_i 0.176\omega_i^2$ , [-]

#### Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

#### **Examples**

```
>>> Tcs = [469.7, 507.4, 540.3]
>>> ais = [1.9351940385541342, 2.525982668162287, 3.1531036708059315]
>>> ms = [0.8610138239999999, 0.9436976, 1.007889024]
>>> SRK_a_alphas_vectorized(322.29, Tcs=Tcs, ais=ais, ms=ms)
[2.549485814512, 3.586598245260, 4.76614806648]
```

thermo.eos\_alpha\_functions.**PRSV\_a\_alphas\_vectorized**(*T*, *Tcs*, *ais*, *kappa0s*, *kappa1s*, *a\_alphas=None*) Calculates the *a\_alpha* terms for the Peng-Robinson-Stryjek-Vera equation of state given the critical temperatures *Tcs*, constants *ais*, PRSV parameters *kappa0s* and *kappa1s*.

$$a_i \alpha_i = a_i \left( \left( \kappa_0 + \kappa_1 \left( \sqrt{\frac{T}{T_{c,i}}} + 1 \right) \left( -\frac{T}{T_{c,i}} + \frac{7}{10} \right) \right) \left( -\sqrt{\frac{T}{T_{c,i}}} + 1 \right) + 1 \right)^2$$

#### **Parameters**

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

**kappa0s** [list[float]] *kappa0* parameters of PRSV EOS; the original form uses  $\kappa_{0,i} = 0.378893 + 1.4897153\omega_i - 0.17131848\omega_i^2 + 0.0196554\omega_i^3$ , [-]

kappa1s [list[float]] Fit parameters, can be set to 0 if unknown [-]

#### Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

## **Examples**

Calculates the *a\_alpha* terms for the Peng-Robinson-Stryjek-Vera 2 equation of state given the critical temperatures *Tcs*, constants *ais*, PRSV2 parameters *kappa0s*, *kappa1s*, *kappa2s*, and *kappa3s*.

$$a_i \alpha_i = a_i \left( \left( 1 - \sqrt{\frac{T}{T_{c,i}}} \right) \left( \kappa_{0,i} + \left( \kappa_{1,i} + \kappa_{2,i} \left( 1 - \sqrt{\frac{T}{T_{c,i}}} \right) \left( -\frac{T}{T_{c,i}} + \kappa_{3,i} \right) \right) \left( \sqrt{\frac{T}{T_{c,i}}} + 1 \right) \left( -\frac{T}{T_{c,i}} + \frac{7}{10} \right) \right) + 1 \right)^2$$

Parameters

**T** [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

**kappa0s** [list[float]] *kappa0* parameters of PRSV EOS; the original form uses  $\kappa_{0,i} = 0.378893 + 1.4897153\omega_i - 0.17131848\omega_i^2 + 0.0196554\omega_i^3$ , [-]

kappa1s [list[float]] Fit parameters, can be set to 0 if unknown [-]

kappa2s [list[float]] Fit parameters, can be set to 0 if unknown [-]

kappa3s [list[float]] Fit parameters, can be set to 0 if unknown [-]

#### Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

## **Examples**

```
>>> PRSV2_a_alphas_vectorized(400.0, Tcs=[507.6], ais=[2.6923169620277805],

→kappa0s=[0.8074380841890093], kappa1s=[0.05104], kappa2s=[0.8634], kappa3s=[0.

→460])

[3.2005700986984]
```

thermo.eos\_alpha\_functions.**APISRK\_a\_alphas\_vectorized**(*T*, *Tcs*, *ais*, *S1s*, *S2s*, *a\_alphas=None*) Calculates the *a\_alpha* terms for the API SRK equation of state given the critical temperatures *Tcs*, constants *ais*, and API parameters *S1s* and *S2s*.

$$a_i \alpha(T)_i = a_i \left[ 1 + S_{1,i} \left( 1 - \sqrt{T_{r,i}} \right) + S_{2,i} \frac{1 - \sqrt{T_{r,i}}}{\sqrt{T_{r,i}}} \right]^2$$

#### **Parameters**

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

- **ais** [list[float]] *a* parameters of cubic EOS,  $a_i = \frac{0.42748 \cdot R^2(T_{c,i})^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]
- **S1s** [list[float]] *S1* parameters of API SRK EOS; regressed or estimated with  $S_{1,i} = 0.48508 + 1.55171\omega_i 0.15613\omega_i^2$ , [-]
- S2s [list[float]] S2 parameters of API SRK EOS; regressed or set to zero, [-]

## Returns

a\_alphas [list[float]] Pure component a\_alpha terms in the cubic EOS, [Pa\*m^6/mol^2]

#### **Examples**

```
>>> APISRK_a_alphas_vectorized(T=430.0, Tcs=[514.0], ais=[1.2721974560809934], _

→S1s=[1.678665], S2s=[-0.216396])

[1.60465652994097]
```

thermo.eos\_alpha\_functions.**RK\_a\_alphas\_vectorized**(*T*, *Tcs*, *ais*, *a\_alphas=None*)

Calculates the *a\_alpha* terms for the RK equation of state given the critical temperatures *Tcs*, and *a* parameters *ais*.

$$a_i \alpha_i = \frac{a_i}{\sqrt{\frac{T}{T_{c,i}}}}$$

#### **Parameters**

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = \frac{0.42748 \cdot R^2(T_{c,i})^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

#### Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

## **Examples**

```
>>> Tcs = [469.7, 507.4, 540.3]
>>> ais = [1.9351940385541342, 2.525982668162287, 3.1531036708059315]
>>> RK_a_alphas_vectorized(322.29, Tcs=Tcs, ais=ais)
[2.3362073307, 3.16943743055, 4.0825575798]
```

## 7.11.2 Vectorized Alpha Functions With Derivatives

thermo.eos\_alpha\_functions.PR\_a\_alpha\_and\_derivatives\_vectorized(T, Tcs, ais, kappas,

a\_alphas=None, da\_alpha\_dTs=None, d2a\_alpha\_dT2s=None)

Calculates the *a\_alpha* terms and their first two temperature derivatives for the Peng-Robinson equation of state given the critical temperatures *Tcs*, constants *ais*, and *kappas*.

$$a_i \alpha(T)_i = a_i [1 + \kappa_i (1 - \sqrt{T_{r,i}})]^2$$
$$\frac{da_i \alpha_i}{dT} = -\frac{a_i \kappa_i}{T^{0.5} T_{c_i}^{0.5}} \left(\kappa_i \left(-\frac{T^{0.5}}{T_{c_i}^{0.5}} + 1\right) + 1\right)$$

$$\frac{d^2 a_i \alpha_i}{dT^2} = 0.5 a_i \kappa_i \left( -\frac{1}{T^{1.5} T_{c_i}^{0.5}} \left( \kappa_i \left( \frac{T^{0.5}}{T_{c_i}^{0.5}} - 1 \right) - 1 \right) + \frac{\kappa_i}{TT_{c_i}} \right)$$

#### **Parameters**

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

ais [list[float]] a parameters of cubic EOS,  $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$  [Pa\*m^6/mol^2]

**kappas** [list[float]] kappa parameters of Peng-Robinson EOS; formulas vary, but the original form uses  $\kappa_i = 0.37464 + 1.54226\omega_i - 0.26992\omega_i^2$ , [-]

#### Returns

- **a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]
- **da\_alpha\_dTs** [list[float]] First temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K)]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K^2)]

## **Examples**

da\_alpha\_dTs=None, d2a alpha dT2s=None)

Calculates the *a\_alpha* terms and their first and second temperature derivatives for the SRK equation of state given the critical temperatures *Tcs*, constants *ais*, and *kappas*.

$$a_i \alpha(T)_i = \left[ 1 + m_i \left( 1 - \sqrt{\frac{T}{T_{c,i}}} \right) \right]^2$$
$$\frac{da_i \alpha_i}{dT} = \frac{a_i m_i}{T} \sqrt{\frac{T}{T_{c,i}}} \left( m_i \left( \sqrt{\frac{T}{T_{c,i}}} - 1 \right) - 1 \right)$$
$$\frac{d^2 a_i \alpha_i}{dT^2} = \frac{a_i m_i \sqrt{\frac{T}{T_{c,i}}}}{2T^2} (m_i + 1)$$

#### **Parameters**

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = \frac{0.42748 \cdot R^2(T_{c,i})^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

**ms** [list[float]] *m* parameters of SRK EOS; formulas vary, but the original form uses  $m_i = 0.480 + 1.574\omega_i - 0.176\omega_i^2$ , [-]

#### Returns

- **a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]
- **da\_alpha\_dTs** [list[float]] First temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K)]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K^2)]

## **Examples**

```
>>> Tcs = [469.7, 507.4, 540.3]
>>> ais = [1.9351940385541342, 2.525982668162287, 3.1531036708059315]
>>> ms = [0.8610138239999999, 0.9436976, 1.007889024]
>>> SRK_a_alpha_and_derivatives_vectorized(322.29, Tcs=Tcs, ais=ais, ms=ms)
([2.549485814512, 3.586598245260, 4.76614806648], [-0.004915469296196, -0.
_00702410108423, -0.00936320876945], [1.236441916324e-05, 1.77752796719e-05, 2.
_37231823137e-05])
```

Calculates the *a\_alpha* terms and their first and second derivative for the Peng-Robinson-Stryjek-Vera equation of state given the critical temperatures *Tcs*, constants *ais*, PRSV parameters *kappa0s* and *kappa1s*.

$$a_{i}\alpha_{i} = a_{i}\left(\left(\kappa_{0} + \kappa_{1}\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(-\frac{T}{T_{c,i}} + \frac{7}{10}\right)\right)\left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) + 1\right)^{2}$$

$$\frac{da_{i}\alpha_{i}}{dT} = a_{i}\left(\left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\left(\kappa_{0,i} + \kappa_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(-\frac{T}{T_{c,i}} + \frac{7}{10}\right)\right) + 1\right)\left(2\left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\left(-\frac{\kappa_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)}{T_{c,i}} + \frac{1}{T_{c,i}}\right) + \frac{1}{T_{c,i}}\left(10\kappa_{0,i} - \kappa_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\right)\left(\frac{20\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)}{T_{c,i}} + \frac{\sqrt{\frac{T}{T_{c,i}}\left(\frac{10T}{T_{c,i}} - 7\right)}}{T}\right) - \frac{\sqrt{\frac{T}{T_{c,i}}\left(10\kappa_{0,i} - \kappa_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(\frac{10T}{T_{c,i}} - 7\right)\right)}{T}\right)^{2} - \frac{\sqrt{\frac{T}{T_{c,i}}}}{T}}{\frac{1}{T}}$$

## $\frac{dT^2}{dT^2} =$

#### Parameters

**T** [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

- **kappa0s** [list[float]] *kappa0* parameters of PRSV EOS; the original form uses  $\kappa_{0,i} = 0.378893 + 1.4897153\omega_i 0.17131848\omega_i^2 + 0.0196554\omega_i^3$ , [-]
- kappa1s [list[float]] Fit parameters, can be set to 0 if unknown [-]

#### Returns

- **a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]
- **da\_alpha\_dTs** [list[float]] First temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K)]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K^2)]

## **Examples**

thermo.eos\_alpha\_functions.**PRSV2\_a\_alpha\_and\_derivatives\_vectorized**(*T*, *Tcs*, *ais*, *kappa0s*,

kappa1s, kappa2s, kappa3s, a\_alphas=None, da\_alpha\_dTs=None, d2a\_alpha\_dT2s=None)

Calculates the *a\_alpha* terms and their first and second derivatives for the Peng-Robinson-Stryjek-Vera 2 equation of state given the critical temperatures *Tcs*, constants *ais*, PRSV2 parameters *kappa0s*, *kappa1s*, *kappa2s*, and *kappa3s*.

$$\begin{aligned} a_{i}\alpha_{i} &= a_{i}\left(\left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\left(\kappa_{0,i} + \left(\kappa_{1,i} + \kappa_{2,i}\left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\left(-\frac{T}{T_{c,i}} + \kappa_{3,i}\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(-\frac{T}{T_{c,i}} + \frac{7}{10}\right)\right) + 1\right)^{2} \\ &\frac{da_{i}\alpha_{i}}{dT} = a_{i}\left(\left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\left(\kappa_{0,i} + \left(\kappa_{1,i} + \kappa_{2,i}\left(1 - \sqrt{\frac{T}{T_{c,i}}}\right)\left(-\frac{T}{T_{c,i}} + \kappa_{3,i}\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(-\frac{T}{T_{c,i}} + \frac{7}{10}\right)\right) + 1\right)\left(\frac{da_{i}\alpha_{i}}{dT}\right) \\ &= a_{i}\left(\left(\left(10\kappa_{0,i} - \left(\kappa_{1,i} + \kappa_{2,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right)\left(\frac{T}{T_{c,i}} - \kappa_{3,i}\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} + 1\right)\left(\frac{10T}{T_{c,i}} - 7\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) - 10\right)\left(\left(\sqrt{\frac{T}{T_{c,i}}}\right) + 1\right)\right) \\ &= a_{i}\left(\frac{d^{2}a_{i}\alpha_{i}}{dT^{2}} - \frac{d^{2}a_{i}\alpha_{i}}{dT^{2}}\right) + 1\right)\left(\frac{d^{2}a_{i}\alpha_{i}}{dT^{2}} + 1\right)\left(\frac{10T}{T_{c,i}} - 1\right) - 10\right)\left(\sqrt{\frac{T}{T_{c,i}}}\right) \\ &= a_{i}\left(\frac{d^{2}a_{i}\alpha_{i}}{dT^{2}} - \frac{d^{2}a_{i}\alpha_{i}}{dT^{2}}\right) + 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right) - 10\right)\left(\sqrt{\frac{T}{T_{c,i}}}\right) \\ &= a_{i}\left(\frac{d^{2}a_{i}\alpha_{i}}{dT^{2}} + 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right)\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\right)\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right)\left(\frac{10T}{T_{c,i}} - 1\right)\left(\frac{10T}{T_{$$

**Parameters** 

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = 0.45724 \frac{R^2 T_{c,i}^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

**kappa0s** [list[float]] *kappa0* parameters of PRSV EOS; the original form uses  $\kappa_{0,i} = 0.378893 + 1.4897153\omega_i - 0.17131848\omega_i^2 + 0.0196554\omega_i^3$ , [-]

kappa1s [list[float]] Fit parameters, can be set to 0 if unknown [-]

**kappa2s** [list[float]] Fit parameters, can be set to 0 if unknown [-]

kappa3s [list[float]] Fit parameters, can be set to 0 if unknown [-]

#### Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

- **da\_alpha\_dTs** [list[float]] First temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K)]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K^2)]

## **Examples**

```
>>> PRSV2_a_alpha_and_derivatives_vectorized(400.0, Tcs=[507.6], ais=[2.

$\display$6923169620277805], kappa0s=[0.8074380841890093], kappa1s=[0.05104], kappa2s=[0.

$\display$8634], kappa3s=[0.460])

([3.2005700986], [-0.005301195971], [1.11181477576e-05])
```

thermo.eos\_alpha\_functions.**APISRK\_a\_alpha\_and\_derivatives\_vectorized**(*T*, *Tcs*, *ais*, *S1s*, *S2s*, *a alphas=None*,

da\_alpha\_dTs=None, d2a\_alpha\_dT2s=None)

Calculates the *a\_alpha* terms and their first two temperature derivatives for the API SRK equation of state given the critical temperatures *Tcs*, constants *ais*, and API parameters *S1s* and *S2s*.

$$a_{i}\alpha(T)_{i} = a_{i}\left[1 + S_{1,i}\left(1 - \sqrt{T_{r,i}}\right) + S_{2,i}\frac{1 - \sqrt{T_{r,i}}}{\sqrt{T_{r,i}}}\right]^{2}$$

$$\frac{da_{i}\alpha_{i}}{dT} = a_{i}\frac{T_{c,i}}{T^{2}}\left(-S_{2,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) + \sqrt{\frac{T}{T_{c,i}}}\left(S_{1,i}\sqrt{\frac{T}{T_{c,i}}} + S_{2,i}\right)\right)\left(S_{2,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) + \sqrt{\frac{T}{T_{c,i}}}\left(S_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) + \sqrt{\frac{T}{T_{c,i}}}\left(S_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) + \sqrt{\frac{T}{T_{c,i}}}\right)\right)\right)\left(S_{2,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) + \sqrt{\frac{T}{T_{c,i}}}\left(S_{1,i}\left(\sqrt{\frac{T}{T_{c,i}}} - 1\right) + \sqrt{\frac{T}{T_{c,i}}}\right)\right)\right)$$

#### **Parameters**

**T** [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

ais [list[float]] a parameters of cubic EOS,  $a_i = \frac{0.42748 \cdot R^2(T_{c,i})^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

- **S1s** [list[float]] *S1* parameters of API SRK EOS; regressed or estimated with  $S_{1,i} = 0.48508 + 1.55171\omega_i 0.15613\omega_i^2$ , [-]
- S2s [list[float]] S2 parameters of API SRK EOS; regressed or set to zero, [-]

#### Returns

- a\_alphas [list[float]] Pure component a\_alpha terms in the cubic EOS, [Pa\*m^6/mol^2]
- **da\_alpha\_dTs** [list[float]] First temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K)]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K^2)]

#### **Examples**

```
>>> APISRK_a_alpha_and_derivatives_vectorized(T=430.0, Tcs=[514.0], ais=[1.

→2721974560809934], S1s=[1.678665], S2s=[-0.216396])

([1.60465652994], [-0.0043155855337], [8.9931026263e-06])
```

thermo.eos\_alpha\_functions.**RK\_a\_alpha\_and\_derivatives\_vectorized**(*T*, *Tcs*, *ais*, *a\_alphas=None*, *da\_alpha\_dTs=None*,

d2a\_alpha\_dT2s=None)

Calculates the *a\_alpha* terms and their first and second temperature derivatives for the RK equation of state given the critical temperatures *Tcs*, and *a* parameters *ais*.

$$a_i \alpha_i = \frac{a_i}{\sqrt{\frac{T}{T_{c,i}}}}$$
$$\frac{da_i \alpha_i}{dT} = -\frac{a_i}{2T\sqrt{\frac{T}{T_{c,i}}}}$$
$$\frac{d^2 a_i \alpha_i}{dT^2} = \frac{3a_i}{4T^2\sqrt{\frac{T}{T_{c,i}}}}$$

#### Parameters

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of components, [K]

**ais** [list[float]] *a* parameters of cubic EOS,  $a_i = \frac{0.42748 \cdot R^2(T_{c,i})^2}{P_{c,i}}$ , [Pa\*m^6/mol^2]

#### Returns

**a\_alphas** [list[float]] Pure component *a\_alpha* terms in the cubic EOS, [Pa\*m^6/mol^2]

- **da\_alpha\_dTs** [list[float]] First temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K)]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of pure component *a\_alpha*, [Pa\*m^6/(mol^2\*K^2)]

## **Examples**

# 7.11.3 Class With Alpha Functions

The class-based ones van save a little code when implementing a new EOS. If there is not a standalone function available for an alpha function, it has not yet been accelerated in a nice vectorized way.

class thermo.eos\_alpha\_functions.a\_alpha\_base

Bases: object

class thermo.eos\_alpha\_functions.Almeida\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## Methods

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Almeida et al. (1991) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Almeida et al. (1991) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = e^{c_1 \left( -\frac{T}{T_{c,i}} + 1 \right) \left| \frac{T}{T_{c,i}} - 1 \right|^{c_2 - 1} + c_3 \left( -1 + \frac{T_{c,i}}{T} \right)}$$

## References

[1]

## a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Androulakis\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## Methods

rivatives according to Androulakis et al. (1989)
].
1

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Androulakis et al. (1989) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more

documentation. Three coefficients needed.

$$\alpha = c_1 \left( -\left(\frac{T}{T_{c,i}}\right)^{\frac{2}{3}} + 1 \right) + c_2 \left( -\left(\frac{T}{T_{c,i}}\right)^{\frac{2}{3}} + 1 \right)^2 + c_3 \left( -\left(\frac{T}{T_{c,i}}\right)^{\frac{2}{3}} + 1 \right)^3 + 1$$

#### References

[1]

class thermo.eos\_alpha\_functions.Chen\_Yang\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

#### **Methods**

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Hamid and Yang (2017) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Hamid and Yang (2017) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Seven coefficients needed.

$$\alpha = e^{\left(-c_3^{\ln\left(\frac{T}{T_{c,i}}\right)} + 1\right)\left(-\frac{Tc_2}{T_{c,i}} + c_1\right)}$$

#### References

[1]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Coquelet\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a\_alpha\_and\_derivatives\_pure(T)Method to calculate a\_alpha and its first and second<br/>derivatives according to Coquelet et al. (2004) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Coquelet et al. (2004) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = e^{c_1 \left(-\frac{T}{T_{c,i}} + 1\right) \left(c_2 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)^2 + c_3 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)^3 + 1\right)^2}$$

#### References

[1]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Gasem\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Gasem (2001) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Gasem (2001) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = e^{\left(-\left(\frac{T}{T_{c,i}}\right)^{c_3} + 1\right)\left(\frac{Tc_2}{T_{c,i}} + c_1\right)}$$

References

[1]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Gibbons\_Laughton\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## Methods

a\_alpha\_and\_derivatives\_pure(T)Method to calculate a\_alpha and its first and sec-<br/>ond derivatives according to Gibbons and Laughton<br/>(1984) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Gibbons and Laughton (1984) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficients needed.

$$\alpha = c_1 \left( \frac{T}{T_{c,i}} - 1 \right) + c_2 \left( \sqrt{\frac{T}{T_{c,i}}} - 1 \right) + 1$$

#### References

[1]

class thermo.eos\_alpha\_functions.Haghtalab\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a_alpha_	and	deri	vativ	ves pure	(T)
a_arpna_	_unu_	ucri	vacrv	co_purc	-(1)

Method to calculate *a\_alpha* and its first and second derivatives according to Haghtalab et al. (2010) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\_alpha$  and its first and second derivatives according to Haghtalab et al. (2010) [1]. Returns  $a\_alpha$ ,  $da\_alpha\_dT$ , and  $d2a\_alpha\_dT2$ . See *GCEOS.a\\_alpha\\_and\\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = e^{\left(-c_3^{\ln\left(\frac{T}{T_{c,i}}\right)} + 1\right)\left(-\frac{Tc_2}{T_{c,i}} + c_1\right)}$$

## References

[1]

## a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Harmens\_Knapp\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## Methods

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second
	derivatives according to Harmens and Knapp (1980)
	[1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Harmens and Knapp (1980) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficients needed.

$$\alpha = \left(c_1\left(-\sqrt{\frac{T}{T_{c,i}}}+1\right) - c_2\left(1-\frac{T_{c,i}}{T}\right) + 1\right)^2$$

## References

[1]

## a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Heyen\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Heyen (1980) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Heyen (1980) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficients needed.

$$\alpha = e^{c_1 \left( - \left( \frac{T}{T_{c,i}} \right)^{c_2} + 1 \right)}$$

## References

[1]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Mathias\_1983\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second
	derivatives according to Mathias (1983) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Mathias (1983) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficients needed.

$$\alpha = \left(c_1 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) - c_2 \left(-\frac{T}{T_{c,i}} + 0.7\right) \left(-\frac{T}{T_{c,i}} + 1\right) + 1\right)^2$$

## References

[1]

## a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Mathias\_Copeman\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## Methods

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and sec-
	ond derivatives according to Mathias and Copeman
	(1983) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Mathias and Copeman (1983) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more

documentation. Three coefficients needed.

$$\alpha = \left(c_1 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) + c_2 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)^2 + c_3 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)^3 + 1\right)^2$$

## References

[1]

```
a_alpha_pure(T)
```

class thermo.eos\_alpha\_functions.Mathias\_Copeman\_poly\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a_alpha_and_derivatives_pure	
a_alpha_and_derivatives_vectorized	
a_alpha_pure	
a_alphas_vectorized	

a\_alpha\_and\_derivatives\_pure(T)

a\_alpha\_and\_derivatives\_vectorized(T)

a\_alpha\_pure(T)

a\_alphas\_vectorized(T)

class thermo.eos\_alpha\_functions.Mathias\_Copeman\_untruncated\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and sec-
	ond derivatives according to Mathias and Copeman
	(1983) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Mathias and Copeman (1983) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more

documentation. Three coefficients needed.

$$\alpha = \left(c_1 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) + c_2 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)^2 + c_3 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)^3 + 1\right)^2$$

## References

[1]

```
a_alpha_pure(T)
```

class thermo.eos\_alpha\_functions.Melhem\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Melhem et al. (1989) [1].

a\_alpha\_pure

#### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Melhem et al. (1989) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficients needed.

$$\alpha = e^{c_1\left(-\frac{T}{T_{c,i}}+1\right)+c_2\left(-\sqrt{\frac{T}{T_{c,i}}}+1\right)^2}$$

#### References

[1]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Poly\_a\_alpha
 Bases: object

## **Methods**

te <i>a_alpha</i> and its first and second that there is a polynomial equation
ate $a\_alpha$ given that there is a on for $\alpha$ .
on

#### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives given that there is a polynomial equation for  $\alpha$ .

$$a\alpha = a \cdot \operatorname{poly}(T)$$

#### **Parameters**

T [float] Temperature, [K]

Returns

a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- **da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

## a\_alpha\_pure(T)

Method to calculate  $a\_alpha$  given that there is a polynomial equation for  $\alpha$ .

$$a\alpha = a \cdot \operatorname{poly}(T)$$

**Parameters** 

T [float] Temperature, [K]

Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

class thermo.eos\_alpha\_functions.Saffari\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

#### **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second
	derivatives according to Saffari and Zahedi (2013)
	[1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Saffari and Zahedi (2013) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = e^{\frac{Tc_1}{T_{c,i}} + c_2 \ln\left(\frac{T}{T_{c,i}}\right) + c_3\left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right)}$$

## References

[1]

a\_alpha\_pure(T)

**class** thermo.eos\_alpha\_functions.**Schwartzentruber\_a\_alpha** Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## Methods

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and sec-
	ond derivatives according to Schwartzentruber et al.
	(1990) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Schwartzentruber et al. (1990) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = \left(c_4 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) - \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) \left(\frac{T^2 c_3}{T c^2} + \frac{T c_2}{T_{c,i}} + c_1\right) + 1\right)^2$$

## References

[1]

class thermo.eos\_alpha\_functions.Soave\_1972\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

## **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second
	derivatives according to Soave (1972) [1].

a\_alpha\_pure

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Soave (1972) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Same as *SRK.a\_alpha\_and\_derivatives* but slower and requiring *alpha\_coeffs* to be set. One coeffi-

cient needed.

$$\alpha = \left(c_0 \left(-\sqrt{\frac{T}{T_{c,i}}} + 1\right) + 1\right)^2$$

# References

[1], [2]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Soave\_1984\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

### **Methods**

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Soave (1984) [1].

a\_alpha\_pure

#### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Soave (1984) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficients needed.

$$\alpha = c_1 \left( -\frac{T}{T_{c,i}} + 1 \right) + c_2 \left( -1 + \frac{T_{c,i}}{T} \right) + 1$$

#### References

[1]

#### a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Soave\_1979\_a\_alpha
Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

# Methods

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Soave (1979) [1].

a\_alpha\_and\_derivatives\_vectorizeda\_alpha\_purea\_alphas\_vectorized

## a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a_alpha$  and its first and second derivatives according to Soave (1979) [1]. Returns  $a_alpha, da_alpha_dT$ , and  $d2a_alpha_dT2$ . Three coefficients are needed.

$$\alpha = 1 + (1 - T_r)(M + \frac{N}{T_r})$$

References

[1]

a\_alpha\_and\_derivatives\_vectorized(T)

a\_alpha\_pure(T)

a\_alphas\_vectorized(T)

class thermo.eos\_alpha\_functions.Soave\_1993\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

# **Methods**

a\_alpha\_and\_derivatives\_pure(T)Method to calculate a\_alpha and its first and second<br/>derivatives according to Soave (1983) [1].

a\_alpha\_pure

# a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Soave (1983) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Two coefficient needed.

$$\alpha = c_1 \left( -\frac{T}{T_{c,i}} + 1 \right) + c_2 \left( -\sqrt{\frac{T}{T_{c,i}}} + 1 \right)^2 + 1$$

# References

[1]

a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Trebble\_Bishnoi\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

# Methods

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second
	derivatives according to Trebble and Bishnoi (1987)
	[1].

a\_alpha\_pure

# a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Trebble and Bishnoi (1987) [1]. Returns *a\_alpha*, *da\_alpha\_dT*, and *d2a\_alpha\_dT2*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. One coefficient needed.

$$\alpha = e^{c_1 \left( -\frac{T}{T_{c,i}} + 1 \right)}$$

# References

[1]

# a\_alpha\_pure(T)

class thermo.eos\_alpha\_functions.Twu91\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

# **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate <i>a_alpha</i> and its first and second derivatives according to Twu et al. (1991) [1].
a_alpha_and_derivatives_vectorized(T)	Method to calculate the pure-component <i>a_alphas</i> and their first and second derivatives for TWU91 alpha function EOS.

a_alpha_pure	
a_alphas_vectorized	

# a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Twu et al. (1991) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Three coefficients needed.

$$\alpha = \left(\frac{T}{T_{c,i}}\right)^{c_3(c_2-1)} e^{c_1\left(-\left(\frac{T}{T_{c,i}}\right)^{c_2c_3}+1\right)}$$

#### References

[1]

#### a\_alpha\_and\_derivatives\_vectorized(T)

Method to calculate the pure-component *a\_alphas* and their first and second derivatives for TWU91 alpha function EOS. This vectorized implementation is added for extra speed.

$$\alpha = \left(\frac{T}{T_{c,i}}\right)^{c_3(c_2-1)} e^{c_1\left(-\left(\frac{T}{T_{c,i}}\right)^{c_2c_3}+1\right)}$$

#### **Parameters**

T [float] Temperature, [K]

# Returns

- a\_alphas [list[float]] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- **da\_alpha\_dTs** [list[float]] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2s** [list[float]] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K\*\*2]

# a\_alpha\_pure(T)

#### a\_alphas\_vectorized(T)

class thermo.eos\_alpha\_functions.TwuPR95\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

# Methods

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for the Twu alpha function.
a_alpha_pure(T)	Method to calculate $a\alpha$ for the Twu alpha function.

a\_alpha\_and\_derivatives\_vectorized a\_alphas\_vectorized

# a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for the Twu alpha function. Uses the set values of *Tc*, *omega* and *a*.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.125283, 0.911807, 1.948150;

L1, M1, N1 = 0.511614, 0.784054, 2.812520

For supercritical conditions:

L0, M0, N0 = 0.401219, 4.963070, -0.2;

L1, M1, N1 = 0.024955, 1.248089, -8.

# Parameters

T [float] Temperature at which to calculate the values, [-]

## Returns

- a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]
- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

# Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

The derivatives are somewhat long and are not described here for brevity; they are obtainable from the following SymPy expression.

```
>>> from sympy import *
>>> T, Tc, omega, N1, N0, M1, M0, L1, L0 = symbols('T, Tc, omega, N1, N0, M1,
___M0, L1, L0')
>>> Tr = T/Tc
>>> alpha0 = Tr**(N0*(M0-1))*exp(L0*(1-Tr**(N0*M0)))
>>> alpha1 = Tr**(N1*(M1-1))*exp(L1*(1-Tr**(N1*M1)))
>>> alpha = alpha0 + omega*(alpha1-alpha0)
>>> diff(alpha, T)
>>> diff(alpha, T, T)
```

#### a\_alpha\_and\_derivatives\_vectorized(T)

#### a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for the Twu alpha function. Uses the set values of *Tc*, *omega* and *a*.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$
$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.125283, 0.911807, 1.948150;

L1, M1, N1 = 0.511614, 0.784054, 2.812520

For supercritical conditions:

L0, M0, N0 = 0.401219, 4.963070, -0.2;

L1, M1, N1 = 0.024955, 1.248089, -8.

# Parameters

T [float] Temperature at which to calculate the value, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

## Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

a\_alphas\_vectorized(T)

class thermo.eos\_alpha\_functions.TwuSRK95\_a\_alpha Bases: thermo.eos\_alpha\_functions.a\_alpha\_base

#### **Methods**

a_alpha_and_derivatives_pure(T)	Method to calculate $a\alpha$ and its first and second
	derivatives for the Twu alpha function.
a_alpha_pure(T)	Method to calculate $a\alpha$ for the Twu alpha function.

a_alpha_and_derivatives_vectorized	
a_alphas_vectorized	

#### a\_alpha\_and\_derivatives\_pure(T)

Method to calculate  $a\alpha$  and its first and second derivatives for the Twu alpha function. Uses the set values of *Tc*, *omega* and *a*.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$

$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.141599, 0.919422, 2.496441

L1, M1, N1 = 0.500315, 0.799457, 3.291790

For supercritical conditions:

L0, M0, N0 = 0.441411, 6.500018, -0.20

L1, M1, N1 = 0.032580, 1.289098, -8.0

#### **Parameters**

T [float] Temperature at which to calculate the values, [-]

# Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

- da\_alpha\_dT [float] Temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K]
- **d2a\_alpha\_dT2** [float] Second temperature derivative of coefficient calculated by EOS-specific method, [J^2/mol^2/Pa/K^2]

#### Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

The derivatives are somewhat long and are not described here for brevity; they are obtainable from the following SymPy expression.

#### a\_alpha\_and\_derivatives\_vectorized(T)

#### a\_alpha\_pure(T)

Method to calculate  $a\alpha$  for the Twu alpha function. Uses the set values of *Tc*, *omega* and *a*.

$$\alpha = \alpha^{(0)} + \omega(\alpha^{(1)} - \alpha^{(0)})$$
$$\alpha^{(i)} = T_r^{N(M-1)} \exp[L(1 - T_r^{NM})]$$

For sub-critical conditions:

L0, M0, N0 = 0.141599, 0.919422, 2.496441

L1, M1, N1 = 0.500315, 0.799457, 3.291790

For supercritical conditions:

L0, M0, N0 = 0.441411, 6.500018, -0.20

L1, M1, N1 = 0.032580, 1.289098, -8.0

#### Parameters

T [float] Temperature at which to calculate the value, [-]

#### Returns

a\_alpha [float] Coefficient calculated by EOS-specific method, [J^2/mol^2/Pa]

# Notes

This method does not alter the object's state and the temperature provided can be a different than that of the object.

a\_alphas\_vectorized(T)

```
class thermo.eos_alpha_functions.Yu_Lu_a_alpha
Bases: thermo.eos_alpha_functions.a_alpha_base
```

# **Methods**

a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Yu and Lu (1987) [1].

a\_alpha\_pure

# a\_alpha\_and\_derivatives\_pure(T)

Method to calculate *a\_alpha* and its first and second derivatives according to Yu and Lu (1987) [1]. Returns *a\_alpha, da\_alpha\_dT*, and *d2a\_alpha\_dT*. See *GCEOS.a\_alpha\_and\_derivatives* for more documentation. Four coefficients needed.

$$\alpha = 10^{c_4 \left(-\frac{T}{T_{c,i}} + 1\right) \left(\frac{T^2 c_3}{T c^2} + \frac{T c_2}{T_{c,i}} + c_1\right)}$$

References

[1]

a\_alpha\_pure(T)

# 7.11.4 Pure Alpha Functions

thermo.eos\_alpha\_functions.Twu91\_alpha\_pure(T, Tc, c0, c1, c2)

thermo.eos\_alpha\_functions.Soave\_1972\_alpha\_pure(T, Tc, c0)

thermo.eos\_alpha\_functions.Soave\_1979\_alpha\_pure(T, Tc, M, N)

thermo.eos\_alpha\_functions.Heyen\_alpha\_pure(T, Tc, c1, c2)

thermo.eos\_alpha\_functions.Harmens\_Knapp\_alpha\_pure(T, Tc, c1, c2)

thermo.eos\_alpha\_functions.Mathias\_1983\_alpha\_pure(T, Tc, c1, c2)

thermo.eos\_alpha\_functions.Mathias\_Copeman\_untruncated\_alpha\_pure(T, Tc, c1, c2, c3)

thermo.eos\_alpha\_functions.Gibbons\_Laughton\_alpha\_pure(T, Tc, c1, c2)

thermo.eos\_alpha\_functions.Soave\_1984\_alpha\_pure(T, Tc, c1, c2)

thermo.eos\_alpha\_functions.Yu\_Lu\_alpha\_pure(T, Tc, c1, c2, c3, c4)

thermo.eos\_alpha\_functions.Trebble\_Bishnoi\_alpha\_pure(T, Tc, cl)

thermo.eos\_alpha\_functions.Melhem\_alpha\_pure(T, Tc, c1, c2)

```
thermo.eos_alpha_functions.Androulakis_alpha_pure(T, Tc, c1, c2, c3)
```

thermo.eos\_alpha\_functions.Schwartzentruber\_alpha\_pure(T, Tc, c1, c2, c3, c4)

thermo.eos\_alpha\_functions.Almeida\_alpha\_pure(T, Tc, c1, c2, c3)

thermo.eos\_alpha\_functions.Soave\_1993\_alpha\_pure(T, Tc, c1, c2)

thermo.eos\_alpha\_functions.Gasem\_alpha\_pure(T, Tc, c1, c2, c3)

thermo.eos\_alpha\_functions.Coquelet\_alpha\_pure(T, Tc, c1, c2, c3)

thermo.eos\_alpha\_functions.Haghtalab\_alpha\_pure(T, Tc, c1, c2, c3)

thermo.eos\_alpha\_functions.Saffari\_alpha\_pure(T, Tc, c1, c2, c3)

thermo.eos\_alpha\_functions.Chen\_Yang\_alpha\_pure(T, Tc, omega, c1, c2, c3, c4, c5, c6, c7)

# 7.12 Equilibrium State (thermo.equilibrium)

This module contains an object designed to store the result of a flash calculation and provide convinient access to all properties of the calculated phases and bulks.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

• EquilibriumState

# 7.12.1 EquilibriumState

settings=<thermo.bulk.BulkSettings object>)

Class to represent a thermodynamic equilibrium state with one or more phases in it. This object is designed to be the output of the *thermo.flash.Flash* interface and to provide easy access to all properties of the mixture.

Properties like *Cp* are calculated using the mixing rules configured by the *BulkSettings* object. For states with a single phase, this will always reduce to the properties of that phase.

This interface allows calculation of thermodynamic properties, and transport properties. Both molar and mass outputs are provided, as separate calls (ex. *Cp* and *Cp\_mass*).

# Parameters

T [float] Temperature of state, [K]

- **P** [float] Pressure of state, [Pa]
- zs [list[float]] Overall mole fractions of all species in the state, [-]
- gas [Phase] The calcualted gas phase object, if one was found, [-]
- liquids [list[Phase]] A list of liquid phase objects, if any were found, [-]
- solids [list[Phase]] A list of solid phase objects, if any were found, [-]
- **betas** [list[float]] Molar phase fractions of every phase, ordered [*gas beta*, *liquid beta0*, *liquid beta1*, ..., *solid beta0*, *solid beta1*, ...]
- **flash\_specs** [dict[str][float], optional] A dictionary containing the specifications for the flash calculations, [-]
- **flash\_convergence** [dict[str][float], optional] A dictionary containing the convergence results for the flash calculations; this is to help support development of the library only and the contents of this dictionary is subject to change, [-]
- **constants** [*ChemicalConstantsPackage*, optional] Package of chemical constants; all cases these properties are accessible as attributes of this object, [-] *EquilibriumState* object, [-]
- **correlations** [*PropertyCorrelationsPackage*, optional] Package of chemical T-dependent properties; these properties are accessible as attributes of this object object, [-]
- **flasher** [*Flash* object, optional] This reference can be provided to this object to allow the object to return properties which are themselves calculated from results of flash calculations, [-]
- **settings** [*BulkSettings*, optional] Object containing settings for calculating bulk and transport properties, [-]

#### Examples

The following sample shows a flash for the CO2-n-hexane system with all constants provided, using no data from thermo.

```
>>> from thermo import *
>>> constants = ChemicalConstantsPackage(names=['carbon dioxide', 'hexane'], CASs=[
→ '124-38-9', '110-54-3'], MWs=[44.0095, 86.17536], omegas=[0.2252, 0.2975],
→Pcs=[7376460.0, 3025000.0], Tbs=[194.67, 341.87], Tcs=[304.2, 507.6], Tms=[216.65,
→ 178.075])
>>> correlations = PropertyCorrelationsPackage(constants=constants, skip_
\rightarrow missing=True,
. . .
→HeatCapacityGases=[HeatCapacityGas(poly_fit=(50.0, 1000.0, [-3.1115474168865828e-
→21, 1.39156078498805e-17, -2.5430881416264243e-14, 2.4175307893014295e-11, -1.
\rightarrow 2437314771044867e-08, 3.1251954264658904e-06, -0.00021220221928610925, 0.
\rightarrow 000884685506352987, 29.266811602924644])),
. . .
→HeatCapacityGas(poly_fit=(200.0, 1000.0, [1.3740654453881647e-21, -8.
→344496203280677e-18, 2.2354782954548568e-14, -3.4659555330048226e-11, 3.
→410703030634579e-08, -2.1693611029230923e-05, 0.008373280796376588, -1.
\rightarrow 356180511425385, 175.67091124888998]))])
>>> eos_kwargs = {'Pcs': constants.Pcs, 'Tcs': constants.Tcs, 'omegas': constants.
\rightarrowomegas}
>>> gas = CEOSGas(PRMIX, eos_kwargs, HeatCapacityGases=correlations.
→HeatCapacityGases)
```

(continued from previous page)

```
>>> liq = CEOSLiquid(PRMIX, eos_kwargs, HeatCapacityGases=correlations.
→HeatCapacityGases)
>>> flasher = FlashVL(constants, correlations, liquid=liq, gas=gas)
>>> state = flasher.flash(P=1e5, T=196.0, zs=[0.5, 0.5])
>>> type(state) is EquilibriumState
True
>>> state.phase_count
2
>>> state.bulk.Cp()
108.3164692
>>> state.flash_specs
{'zs': [0.5, 0.5], 'T': 196.0, 'P': 100000.0}
>>> state.Tms
[216.65, 178.075]
>>> state.liquid0.H()
-34376.4853
>>> state.gas.H()
-3608.0551
```

#### Attributes

```
gas_count [int] Number of gas phases present (0 or 1), [-]
liquid_count [int] Number of liquid phases present, [-]
solid_count [int] Number of solid phases present, [-]
phase_count [int] Number of phases present, [-]
gas_beta [float] Molar phase fraction of the gas phase; 0 if no gas phase is present, [-]
liquids_betas [list[float]] Liquid molar phase fractions, [-]
solids_betas [list[float]] Solid molar phase fractions, [-]
liquid_zs [list[float]] Overall mole fractions of each component in the overall liquid phase, [-]
liquid_bulk [Bulk] Liquid phase bulk, [-]
solid_zs [list[float]] Overall mole fractions of each component in the overall solid phase, [-]
solid bulk [Bulk] Solid phase bulk, [-]
bulk [Bulk] Overall phase bulk, [-]
IDs Alias of CASs.
LF Method to return the liquid fraction of the equilibrium state.
VF Method to return the vapor fraction of the equilibrium state.
betas_liquids Method to calculate and return the fraction of the liquid phase that each liquid
    phase is, by molar phase fraction.
betas_mass Method to calculate and return the mass fraction of all of the phases in the system.
betas_mass_liquids Method to calculate and return the fraction of the liquid phase that each
    liquid phase is, by mass phase fraction.
betas_mass_states Method to return the mass phase fractions of each of the three fundamen-
```

tal types of phases.

- **betas\_states** Method to return the molar phase fractions of each of the three fundamental *types* of phases.
- **betas\_volume** Method to calculate and return the volume fraction of all of the phases in the system.
- **betas\_volume\_liquids** Method to calculate and return the fraction of the liquid phase that each liquid phase is, by volume phase fraction.
- **betas\_volume\_states** Method to return the volume phase fractions of each of the three fundamental *types* of phases.

heaviest\_liquid The liquid-like phase with the highest mass density, [-]

*lightest\_liquid* The liquid-like phase with the lowest mass density, [-]

**phase** Method to calculate and return a string representing the phase of the mixture.

quality Method to return the mass vapor fraction of the equilibrium state.

water\_index The index of the component water in the components.

water\_phase The liquid-like phase with the highest water mole fraction, [-]

water\_phase\_index The liquid-like phase with the highest mole fraction of water, [-]

atomss Breakdown of each component into its elements and their counts, as a dict, [-].

Carcinogens Status of each component in cancer causing registries, [-].

CASs CAS registration numbers for each component, [-].

*Ceilings* Ceiling exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].

charges Charge number (valence) for each component, [-].

conductivities Electrical conductivities for each component, [S/m].

dipoles Dipole moments for each component, [debye].

*economic\_statuses* Status of each component in in relation to import and export from various regions, [-].

formulas Formulas of each component, [-].

Gfgs Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

**Gfgs\_mass** Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

*GWPs* Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

*Hcs* Higher standard molar heats of combustion for each component, [J/mol].

*Hcs\_lower* Lower standard molar heats of combustion for each component, [J/mol].

Hcs\_lower\_mass Lower standard heats of combustion for each component, [J/kg].

Hcs\_mass Higher standard heats of combustion for each component, [J/kg].

**Hfgs** Ideal gas standard molar enthalpies of formation for each component, [J/mol].

Hfgs\_mass Ideal gas standard enthalpies of formation for each component, [J/kg].

Hfus\_Tms Molar heats of fusion for each component at their respective melting points, [J/mol].

**Hfus\_Tms\_mass** Heats of fusion for each component at their respective melting points, [J/kg].

**Hsub\_Tts** Heats of sublimation for each component at their respective triple points, [J/mol].

- Hsub\_Tts\_mass Heats of sublimation for each component at their respective triple points, [J/kg].
- Hvap\_298s Molar heats of vaporization for each component at 298.15 K, [J/mol].
- Hvap\_298s\_mass Heats of vaporization for each component at 298.15 K, [J/kg].
- *Hvap\_Tbs* Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].
- Hvap\_Tbs\_mass Heats of vaporization for each component at their respective normal boiling points, [J/kg].
- InChI\_Keys InChI Keys for each component, [-].
- InChIs InChI strings for each component, [-].
- legal\_statuses Status of each component in in relation to import and export rules from various regions, [-].
- LFLs Lower flammability limits for each component, [-].

*logPs* Octanol-water partition coefficients for each component, [-].

molecular\_diameters Lennard-Jones molecular diameters for each component, [angstrom].

MWs Similatiry variables for each component, [g/mol].

names Names for each component, [-].

*ODPs* Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

omegas Acentric factors for each component, [-].

Parachors Parachors for each component, [N^0.25\*m^2.75/mol].

**Pcs** Critical pressures for each component, [Pa].

phase\_STPs Standard states ('g', 'l', or 's') for each component, [-].

Psat\_298s Vapor pressures for each component at 298.15 K, [Pa].

PSRK\_groups PSRK subgroup: count groups for each component, [-].

Pts Triple point pressures for each component, [Pa].

**PubChems** Pubchem IDs for each component, [-].

*rhocs* Molar densities at the critical point for each component, [mol/m^3].

*rhocs\_mass* Densities at the critical point for each component, [kg/m^3].

*rhol\_STPs* Molar liquid densities at STP for each component, [mol/m<sup>3</sup>].

*rhol\_STPs\_mass* Liquid densities at STP for each component, [kg/m^3].

**RIs** Refractive indexes for each component, [-].

**S0gs** Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].

**S0gs\_mass** Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].

*Sfgs* Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

*Sfgs\_mass* Ideal gas standard entropies of formation for each component, [J/(kg\*K)].

similarity\_variables Similarity variables for each component, [mol/g].

*Skins* Whether each compound can be absorbed through the skin or not, [-].

smiless SMILES identifiers for each component, [-].

STELS Short term exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

- StielPolars Stiel polar factors for each component, [-].
- *Stockmayers* Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].
- **Tautoignitions** Autoignition temperatures for each component, [K].
- Tbs Boiling temperatures for each component, [K].
- Tcs Critical temperatures for each component, [K].
- Tflashs Flash point temperatures for each component, [K].
- *Tms* Melting temperatures for each component, [K].
- *Tts* Triple point temperatures for each component, [K].
- **TWAS** Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m^3), [various].
- **UFLs** Upper flammability limits for each component, [-].
- UNIFAC\_Dortmund\_groups UNIFAC\_Dortmund\_group: count groups for each component, [-].
- UNIFAC\_groups UNIFAC\_group: count groups for each component, [-].
- Van\_der\_Waals\_areas Unnormalized Van der Waals areas for each component, [m^2/mol].
- Van\_der\_Waals\_volumes Unnormalized Van der Waals volumes for each component, [m^3/mol].
- Vcs Critical molar volumes for each component, [m^3/mol].
- *Vml\_STPs* Liquid molar volumes for each component at STP, [m<sup>3</sup>/mol].
- Vml\_Tms Liquid molar volumes for each component at their respective melting points, [m^3/mol].
- Zcs Critical compressibilities for each component, [-].
- UNIFAC\_Rs UNIFAC R parameters for each component, [-].
- **UNIFAC\_Qs** UNIFAC Q parameters for each component, [-].
- *rhos\_Tms* Solid molar densities for each component at their respective melting points, [mol/m^3].
- *Vms\_Tms* Solid molar volumes for each component at their respective melting points, [m^3/mol].
- **rhos\_Tms\_mass** Solid mass densities for each component at their melting point, [kg/m^3].
- solubility\_parameters Solubility parameters for each component at 298.15 K, [Pa^0.5].
- *Vml\_60Fs* Liquid molar volumes for each component at 60 °F, [m^3/mol].

*rhol\_60Fs* Liquid molar densities for each component at 60 °F, [mol/m<sup>3</sup>].

rhol\_60Fs\_mass Liquid mass densities for each component at 60 °F, [kg/m^3].

- *conductivity\_Ts* Temperatures at which the electrical conductivities for each component were measured, [K].
- **RI\_Ts** Temperatures at which the refractive indexes were reported for each component, [K].

- Vmg\_STPs Gas molar volumes for each component at STP; metastable if normally another state, [m^3/mol].
- *rhog\_STPs* Molar gas densities at STP for each component; metastable if normally another state, [mol/m^3].
- *rhog\_STPs\_mass* Gas densities at STP for each component; metastable if normally another state, [kg/m^3].
- *sigma\_STPs* Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].
- sigma\_Tms Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].
- sigma\_Tbs Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].
- **Hf\_STPs** Standard state molar enthalpies of formation for each component, [J/mol].
- Hf\_STPs\_mass Standard state mass enthalpies of formation for each component, [J/kg].
- VaporPressures Wrapper to obtain the list of VaporPressures objects of the associated PropertyCorrelationsPackage.
- **VolumeLiquids** Wrapper to obtain the list of VolumeLiquids objects of the associated *PropertyCorrelationsPackage*.
- **VolumeGases** Wrapper to obtain the list of VolumeGases objects of the associated *PropertyCorrelationsPackage*.
- **VolumeSolids** Wrapper to obtain the list of VolumeSolids objects of the associated *PropertyCorrelationsPackage*.
- *HeatCapacityGases* Wrapper to obtain the list of HeatCapacityGases objects of the associated *PropertyCorrelationsPackage*.
- *HeatCapacitySolids* Wrapper to obtain the list of HeatCapacitySolids objects of the associated *PropertyCorrelationsPackage*.
- *HeatCapacityLiquids* Wrapper to obtain the list of HeatCapacityLiquids objects of the associated *PropertyCorrelationsPackage*.
- **EnthalpyVaporizations** Wrapper to obtain the list of EnthalpyVaporizations objects of the associated *PropertyCorrelationsPackage*.
- **EnthalpySublimations** Wrapper to obtain the list of EnthalpySublimations objects of the associated *PropertyCorrelationsPackage*.
- SublimationPressures Wrapper to obtain the list of SublimationPressures objects of the associated PropertyCorrelationsPackage.
- **PermittivityLiquids** Wrapper to obtain the list of PermittivityLiquids objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityLiquids** Wrapper to obtain the list of ViscosityLiquids objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityGases** Wrapper to obtain the list of ViscosityGases objects of the associated *PropertyCorrelationsPackage*.
- **ThermalConductivityLiquids** Wrapper to obtain the list of ThermalConductivityLiquids objects of the associated *PropertyCorrelationsPackage*.
- *ThermalConductivityGases* Wrapper to obtain the list of ThermalConductivityGases objects of the associated *PropertyCorrelationsPackage*.

- SurfaceTensions Wrapper to obtain the list of SurfaceTensions objects of the associated PropertyCorrelationsPackage.
- **VolumeGasMixture** Wrapper to obtain the list of VolumeGasMixture objects of the associated *PropertyCorrelationsPackage*.
- **VolumeLiquidMixture** Wrapper to obtain the list of VolumeLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- **VolumeSolidMixture** Wrapper to obtain the list of VolumeSolidMixture objects of the associated *PropertyCorrelationsPackage*.
- *HeatCapacityGasMixture* Wrapper to obtain the list of HeatCapacityGasMixture objects of the associated *PropertyCorrelationsPackage*.
- *HeatCapacityLiquidMixture* Wrapper to obtain the list of HeatCapacityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- *HeatCapacitySolidMixture* Wrapper to obtain the list of HeatCapacitySolidMixture objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityGasMixture** Wrapper to obtain the list of ViscosityGasMixture objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityLiquidMixture** Wrapper to obtain the list of ViscosityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- **ThermalConductivityGasMixture** Wrapper to obtain the list of ThermalConductivityGas-Mixture objects of the associated *PropertyCorrelationsPackage*.
- *ThermalConductivityLiquidMixture* Wrapper to obtain the list of ThermalConductivityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- SurfaceTensionMixture Wrapper to obtain the list of SurfaceTensionMixture objects of the associated PropertyCorrelationsPackage.

# **Methods**

A()	Method to calculate and return the Helmholtz energy
	of the phase.
API([phase])	Method to calculate and return the API of the phase.
A_dep()	Method to calculate and return the departure
	Helmholtz energy of the phase.
<pre>A_formation_ideal_gas([phase])</pre>	Method to calculate and return the ideal-gas
	Helmholtz energy of formation of the phase (as if
	the phase was an ideal gas).
A_ideal_gas([phase])	Method to calculate and return the ideal-gas
	Helmholtz energy of the phase.
A_mass([phase])	Method to calculate and return mass Helmholtz en-
	ergy of the phase.
A_reactive()	Method to calculate and return the Helmholtz free en-
	ergy of the phase on a reactive basis.
Bvirial([phase])	Method to calculate and return the <i>B</i> virial coefficient
	of the phase at its current conditions.
<i>Cp</i> ()	Method to calculate and return the constant-
	temperature and constant phase-fraction heat
	capacity of the bulk phase.

Table 65 – conti	nued from previous page
Cp_Cv_ratio()	Method to calculate and return the Cp/Cv ratio of the
Cp_Cv_ratio_ideal_gas([phase])	phase. Method to calculate and return the ratio of the ideal-
cp_cv_ratio_ruear_gas([phase])	
	gas heat capacity to its constant-volume heat capac-
(re_dem/[rhead])	ity. Method to calculate and return the difference between
Cp_dep([phase])	
	the actual $Cp$ and the ideal-gas heat capacity $C_p^{ig}$ of
(re ideal gas([rebase])	the phase.
Cp_ideal_gas([phase])	Method to calculate and return the ideal-gas heat ca-
	pacity of the phase. Method to calculate and return mass constant pres-
Cp_mass([phase])	1
<b>6</b> -0	sure heat capacity of the phase.
Cv()	Method to calculate and return the constant-volume
	heat capacity <i>Cv</i> of the phase.
Cv_dep([phase])	Method to calculate and return the difference between
	the actual $Cv$ and the ideal-gas constant volume heat
	capacity $C_v^{ig}$ of the phase.
Cv_ideal_gas([phase])	Method to calculate and return the ideal-gas constant
	volume heat capacity of the phase.
Cv_mass([phase])	Method to calculate and return mass constant volume
	heat capacity of the phase.
G()	Method to calculate and return the Gibbs free energy
	of the phase.
G_dep()	Method to calculate and return the departure Gibbs
	free energy of the phase.
<pre>G_formation_ideal_gas([phase])</pre>	Method to calculate and return the ideal-gas Gibbs
	free energy of formation of the phase (as if the phase
	was an ideal gas).
G_ideal_gas([phase])	Method to calculate and return the ideal-gas Gibbs
	free energy of the phase.
G_mass([phase])	Method to calculate and return mass Gibbs energy of
	the phase.
G_reactive()	Method to calculate and return the Gibbs free energy
	of the phase on a reactive basis.
Н()	Method to calculate and return the constant-
	temperature and constant phase-fraction enthalpy of
	the bulk phase.
H_C_ratio([phase])	Method to calculate and return the atomic ratio of hy-
	drogen atoms to carbon atoms, based on the current
	composition of the phase.
<pre>H_C_ratio_mass([phase])</pre>	Method to calculate and return the mass ratio of hy-
	drogen atoms to carbon atoms, based on the current
	composition of the phase.
H_dep([phase])	Method to calculate and return the difference between
	the actual <i>H</i> and the ideal-gas enthalpy of the phase.
<pre>H_formation_ideal_gas([phase])</pre>	Method to calculate and return the ideal-gas enthalpy
<pre>H_formation_ideal_gas([phase])</pre>	of formation of the phase (as if the phase was an ideal
	of formation of the phase (as if the phase was an ideal gas).
<pre>H_formation_ideal_gas([phase]) H_ideal_gas([phase])</pre>	of formation of the phase (as if the phase was an ideal

Table 65 – continued from previous page

	ontinued from previous page
<i>H_mass</i> ([phase])	Method to calculate and return mass enthalpy of the
	phase.
H_reactive()	Method to calculate and return the constant-
	temperature and constant phase-fraction reactive
	enthalpy of the bulk phase.
Hc([phase])	Method to calculate and return the molar ideal-gas
-	higher heat of combustion of the object, [J/mol]
<pre>Hc_lower([phase])</pre>	Method to calculate and return the molar ideal-gas
	lower heat of combustion of the object, [J/mol]
<pre>Hc_lower_mass([phase])</pre>	Method to calculate and return the mass ideal-gas
-	lower heat of combustion of the object, [J/mol]
<pre>Hc_lower_normal([phase])</pre>	Method to calculate and return the volumetric ideal-
	gas lower heat of combustion of the object using the
	normal gas volume, [J/m^3]
<pre>Hc_lower_standard([phase])</pre>	Method to calculate and return the volumetric ideal-
	gas lower heat of combustion of the object using the
	standard gas volume, [J/m^3]
<pre>Hc_mass([phase])</pre>	Method to calculate and return the mass ideal-gas
- (1 )	higher heat of combustion of the object, [J/mol]
<pre>Hc_normal([phase])</pre>	Method to calculate and return the volumetric ideal-
	gas higher heat of combustion of the object using the
	normal gas volume, [J/m^3]
<pre>Hc_standard([phase])</pre>	Method to calculate and return the volumetric ideal-
	gas higher heat of combustion of the object using the
	standard gas volume, [J/m^3]
Joule_Thomson()	Method to calculate and return the Joule-Thomson
	coefficient of the bulk according to the selected cal-
	culation methodology.
<i>Ks</i> (phase[, phase_ref])	Method to calculate and return the K-values of each
	phase.
MW([phase])	Method to calculate and return the molecular weight
	of the phase.
PIP()	Method to calculate and return the phase identifica-
	tion parameter of the phase.
<i>Pmc</i> ([phase])	Method to calculate and return the mechanical criti-
	cal pressure of the phase.
S()	Method to calculate and return the constant-
v	temperature and constant phase-fraction entropy of
	the bulk phase.
SG([phase])	Method to calculate and return the standard liquid
	specific gravity of the phase, using constant liquid
	pure component densities not calculated by the phase
	object, at 60 °F.
<i>SG_gas</i> ([phase])	Method to calculate and return the specific gravity of
	the phase with respect to a gas reference density.
<i>S_dep</i> ([phase])	Method to calculate and return the difference between
- (01 - 27	the actual S and the ideal-gas entropy of the phase.
<pre>S_formation_ideal_gas([phase])</pre>	Method to calculate and return the ideal-gas entropy
	of formation of the phase (as if the phase was an ideal
	gas).
	continues on next page
	· · · · · · · · · · · · · · · · · · ·

Table 65 – continued from previous page

Table 65 – co	ontinued from previous page
S_ideal_gas([phase])	Method to calculate and return the ideal-gas entropy
-	of the phase.
S_mass([phase])	Method to calculate and return mass entropy of the
	phase.
S_reactive()	Method to calculate and return the constant-
5_100000	temperature and constant phase-fraction reactive
	entropy of the bulk phase.
Tmc([phase])	Method to calculate and return the mechanical criti-
([phase])	
	cal temperature of the phase.
U()	Method to calculate and return the internal energy of
	the phase.
U_dep()	Method to calculate and return the departure internal
	energy of the phase.
<pre>U_formation_ideal_gas([phase])</pre>	Method to calculate and return the ideal-gas internal
	energy of formation of the phase (as if the phase was
	an ideal gas).
U_ideal_gas([phase])	Method to calculate and return the ideal-gas internal
	energy of the phase.
U_mass([phase])	Method to calculate and return mass internal energy
	of the phase.
U_reactive()	Method to calculate and return the internal energy of
	the phase on a reactive basis.
V()	Method to calculate and return the molar volume of
	the bulk phase.
V_dep()	Method to calculate and return the departure (from
v_uep()	ideal gas behavior) molar volume of the phase.
V ree([share])	
V_gas([phase])	Method to calculate and return the ideal-gas molar
	volume of the phase at the chosen reference tempera-
	ture and pressure, according to the temperature vari-
	able <i>T_gas_ref</i> and pressure variable <i>P_gas_ref</i> of
	the thermo.bulk.BulkSettings.
V_gas_normal([phase])	Method to calculate and return the ideal-gas mo-
	lar volume of the phase at the normal temperature
	and pressure, according to the temperature variable
	<i>T_normal</i> and pressure variable <i>P_normal</i> of the
	thermo.bulk.BulkSettings.
V_gas_standard([phase])	Method to calculate and return the ideal-gas mo-
	lar volume of the phase at the standard temperature
	and pressure, according to the temperature variable
	$T_{standard}$ and pressure variable $P_{standard}$ of the
	thermo.bulk.BulkSettings.
V_ideal_gas([phase])	Method to calculate and return the ideal-gas molar
	volume of the phase.
<i>V_iter</i> ([phase, force])	Method to calculate and return the volume of the
([phuse, loree])	phase in a way suitable for a TV resolution to con-
	verge on the same pressure.
V liquid raf([phase])	
V_liquid_ref([phase])	Method to calculate and return the liquid refer-
	ence molar volume according to the temperature
	variable <i>T_liquid_volume_ref</i> of thermo.bulk.
	BulkSettings and the composition of the phase.
	continues on next page

Table 65 – conti	nued from previous page
V_liquids_ref()	Method to calculate and return the liquid refer-
	ence molar volumes according to the temperature
	variable <i>T_liquid_volume_ref</i> of thermo.bulk.
	BulkSettings.
V_mass([phase])	Method to calculate and return the specific volume of
- ( <b>1</b> )/	the phase.
<i>Vfgs</i> ([phase])	Method to calculate and return the ideal-gas volume
	fractions of the components of the phase.
Vfls([phase])	Method to calculate and return the ideal-liquid vol-
	ume fractions of the components of the phase,
	using the standard liquid densities at the tem-
	perature variable <i>T_liquid_volume_ref</i> of thermo.
	bulk.BulkSettings and the composition of the
	phase.
Vmc([phase])	Method to calculate and return the mechanical criti-
([Prime])	cal volume of the phase.
<pre>Wobbe_index([phase])</pre>	Method to calculate and return the molar Wobbe in-
"OBDE_INGEA([pilase])	dex of the object, [J/mol].
<pre>Wobbe_index_lower([phase])</pre>	Method to calculate and return the molar lower
wobbe_index_iowei([phase])	Wobbe index of the
<pre>Wobbe_index_lower_mass([phase])</pre>	Method to calculate and return the lower mass Wobbe
wobbe_index_iower_mass([pnase])	
Webbe index lever nervel([rhose])	index of the object, [J/kg]. Method to calculate and return the volumetric normal
<pre>Wobbe_index_lower_normal([phase])</pre>	
	lower Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_lower_standard([phase])</pre>	Method to calculate and return the volumetric stan-
	dard lower Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_mass([phase])</pre>	Method to calculate and return the mass Wobbe index
	of the object, [J/kg].
<pre>Wobbe_index_normal([phase])</pre>	Method to calculate and return the volumetric normal
	Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_standard([phase])</pre>	Method to calculate and return the volumetric stan- dord Waha index of the abiast $[I(m^{2})]$
7()	dard Wobbe index of the object, [J/m^3].
Z()	Method to calculate and return the compressibility
	factor of the phase.
Zmc([phase])	Method to calculate and return the mechanical criti-
	cal compressibility of the phase.
alpha([phase])	Method to calculate and return the thermal diffusivity
	of the equilibrium state.
<pre>atom_fractions([phase])</pre>	Method to calculate and return the atomic composi-
	tion of the phase; returns a dictionary of atom frac-
	tion (by count), containing only those elements who
	are present.
<pre>atom_mass_fractions([phase])</pre>	Method to calculate and return the atomic mass frac-
	tions of the phase; returns a dictionary of atom frac-
	tion (by mass), containing only those elements who
	are present.
d2P_dT2()	Method to calculate and return the second tempera-
	ture derivative of pressure of the bulk according to
	the selected calculation methodology.
	continues on next page

	65 – continued from previous page
d2P_dT2_frozen()	Method to calculate and return the second constant-
	volume derivative of pressure with respect to temper-
	ature of the bulk phase, at constant phase fractions
	and phase compositions.
d2P_dTdV()	Method to calculate and return the second deriva-
	tive of pressure with respect to temperature and vol-
	ume of the bulk according to the selected calculation
	methodology.
d2P_dTdV_frozen()	Method to calculate and return the second derivative
uzr_u1uv_110zen()	
	of pressure with respect to volume and temperature of
	the bulk phase, at constant phase fractions and phase
	compositions.
d2P_dV2()	Method to calculate and return the second volume
	derivative of pressure of the bulk according to the se-
	lected calculation methodology.
d2P_dV2_frozen()	Method to calculate and return the constant-
	temperature second derivative of pressure with
	respect to volume of the bulk phase, at constant
	phase fractions and phase compositions.
dA_dP()	Method to calculate and return the constant-
	temperature pressure derivative of Helmholtz
	energy.
$dA_dP_T()$	Method to calculate and return the constant-
	temperature pressure derivative of Helmholtz
	energy.
$dA_dP_V()$	Method to calculate and return the constant-volume
	pressure derivative of Helmholtz energy.
dA_dT()	Method to calculate and return the constant-pressure
	*
	temperature derivative of Helmholtz energy.
$dA_dT_P()$	Method to calculate and return the constant-pressure
	temperature derivative of Helmholtz energy.
dA_dT_V()	Method to calculate and return the constant-volume
	temperature derivative of Helmholtz energy.
$dA_dV_P()$	Method to calculate and return the constant-pressure
	volume derivative of Helmholtz energy.
$dA_dV_T()$	Method to calculate and return the constant-
	temperature volume derivative of Helmholtz energy.
dA_mass_dP()	Method to calculate and return the pressure derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
dA_mass_dP_T()	Method to calculate and return the pressure derivative
~	of mass Helmholtz energy of the phase at constant
	temperature.
dA_mass_dP_V()	Method to calculate and return the pressure derivative
()	of mass Helmholtz energy of the phase at constant
	volume.
dA mass dT()	
dA_mass_dT()	Method to calculate and return the temperature
	derivative of mass Helmholtz energy of the phase at
	constant pressure.

	Table 65 – continued from previous page
dA_mass_dT_P()	Method to calculate and return the temperature
V	derivative of mass Helmholtz energy of the phase at
	constant pressure.
dA_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass Helmholtz energy of the phase at
	constant volume.
dA_mass_dV_P()	Method to calculate and return the volume derivative
uA_mass_uv_P()	
	of mass Helmholtz energy of the phase at constant
	pressure.
dA_mass_dV_T()	Method to calculate and return the volume derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
$dCv_dP_T()$	Method to calculate the pressure derivative of Cv,
	constant volume heat capacity, at constant tempera-
	ture.
$dCv_dT_P()$	Method to calculate the temperature derivative of Cv,
	constant volume heat capacity, at constant pressure.
dCv_mass_dP_T()	Method to calculate and return the pressure derivative
	of mass Constant-volume heat capacity of the phase
	at constant temperature.
dCv_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass Constant-volume heat capacity of
	the phase at constant pressure.
$dG_dP()$	Method to calculate and return the constant-
	temperature pressure derivative of Gibbs free
	energy.
$dG_dP_T()$	Method to calculate and return the constant-
uo_u _1()	temperature pressure derivative of Gibbs free
	energy.
dG_dP_V()	Method to calculate and return the constant-volume
	pressure derivative of Gibbs free energy.
dG_dT()	Method to calculate and return the constant-pressure
u0_u1()	temperature derivative of Gibbs free energy.
$dG_dT_P()$	Method to calculate and return the constant-pressure
	temperature derivative of Gibbs free energy.
$dG_dT_V()$	Method to calculate and return the constant-volume
	temperature derivative of Gibbs free energy.
$dG_dV_P()$	Method to calculate and return the constant-pressure
	volume derivative of Gibbs free energy.
$dG_dV_T()$	Method to calculate and return the constant-
	temperature volume derivative of Gibbs free energy.
dG_mass_dP()	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dG_mass_dP_T()	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dG_mass_dP_V()	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	volume.
	continues on next page

Table 65 – 0	continued from previous page
dG_mass_dT()	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant pressure.
dG_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant pressure.
dG_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant volume.
dG_mass_dV_P()	Method to calculate and return the volume derivative
	of mass Gibbs free energy of the phase at constant
	pressure.
dG_mass_dV_T()	Method to calculate and return the volume derivative
uo_mass_uv_1()	of mass Gibbs free energy of the phase at constant
	temperature.
dH_dP()	
un_ur()	Method to calculate and return the pressure derivative
$dH_dP_T()$	of enthalpy of the phase at constant pressure.Method to calculate and return the pressure derivative
un_ur_1()	
dH_dT()	of enthalpy of the phase at constant pressure. Method to calculate and return the constant-
	temperature and constant phase-fraction heat
	capacity of the bulk phase.
$dH_dT_P()$	Method to calculate and return the temperature
	derivative of enthalpy of the phase at constant pres-
	sure.
dH_mass_dP()	Method to calculate and return the pressure deriva-
	tive of mass enthalpy of the phase at constant tem-
	perature.
dH_mass_dP_T()	Method to calculate and return the pressure deriva-
	tive of mass enthalpy of the phase at constant tem-
	perature.
dH_mass_dP_V()	Method to calculate and return the pressure derivative
	of mass enthalpy of the phase at constant volume.
dH_mass_dT()	Method to calculate and return the temperature
	derivative of mass enthalpy of the phase at constant
	pressure.
dH_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass enthalpy of the phase at constant
	pressure.
dH_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass enthalpy of the phase at constant
	volume.
dH_mass_dV_P()	Method to calculate and return the volume derivative
	of mass enthalpy of the phase at constant pressure.
dH_mass_dV_T()	Method to calculate and return the volume derivative
	of mass enthalpy of the phase at constant tempera-
	ture.
$dP_dP_A()$	Method to calculate and return the pressure derivative
~	of pressure of the phase at constant Helmholtz energy.
$dP_dP_G()$	Method to calculate and return the pressure derivative
- •	of pressure of the phase at constant Gibbs energy.

	able 65 – continued from previous page
dP_dP_H()	Method to calculate and return the pressure derivative
	of pressure of the phase at constant enthalpy.
$dP_dP_S()$	Method to calculate and return the pressure derivative
	of pressure of the phase at constant entropy.
$dP_dP_U()$	Method to calculate and return the pressure derivative
	of pressure of the phase at constant internal energy.
$dP_dT()$	Method to calculate and return the first temperature
_ •	derivative of pressure of the bulk according to the se-
	lected calculation methodology.
$dP_dT_A()$	Method to calculate and return the temperature
V	derivative of pressure of the phase at constant
	Helmholtz energy.
$dP_dT_G()$	Method to calculate and return the temperature
	derivative of pressure of the phase at constant Gibbs
	energy.
dP_dT_H()	Method to calculate and return the temperature
	derivative of pressure of the phase at constant en-
	thalpy.
$dP_dT_S()$	Method to calculate and return the temperature
ur_ur_5()	derivative of pressure of the phase at constant en-
	tropy.
$dP_dT_U()$	Method to calculate and return the temperature
ur_ur_0()	derivative of pressure of the phase at constant internal
	energy.
dP_dT_frozen()	Method to calculate and return the constant-volume
	derivative of pressure with respect to temperature of
	the bulk phase, at constant phase fractions and phase
	compositions.
$dP_dV()$	Method to calculate and return the first volume
	derivative of pressure of the bulk according to the se-
	lected calculation methodology.
$dP_dV_A()$	Method to calculate and return the volume derivative
	of pressure of the phase at constant Helmholtz energy.
$dP_dV_G()$	Method to calculate and return the volume derivative
	of pressure of the phase at constant Gibbs energy.
dP_dV_H()	Method to calculate and return the volume derivative
	of pressure of the phase at constant enthalpy.
$dP_dV_S()$	Method to calculate and return the volume derivative
$\operatorname{dr}_{\operatorname{dv}}_{\operatorname{S}}()$	of pressure of the phase at constant entropy.
$dP_dV_U()$	Method to calculate and return the volume derivative
	of pressure of the phase at constant internal energy.
dP_dV_frozen()	Method to calculate and return the constant-
	temperature derivative of pressure with respect to
	volume of the bulk phase, at constant phase fractions
	and phase compositions.
dP_drho_A() dP_drho_G()	Method to calculate and return the density derivative
	•
	of pressure of the phase at constant Helmholtz energy.
	Method to calculate and return the density derivative
	of pressure of the phase at constant Gibbs energy.
dD data II()	
dP_drho_H()	Method to calculate and return the density derivative of pressure of the phase at constant enthalpy.

Table 65 – continued from previous page

dP_drho_S()         Method to calculate and return the density derivative of pressure of the phase at constant entropy.           dP_drho_U()         Method to calculate and return the density derivative of pressure of the phase at constant internal energy.           dS_dP()         Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.           dS_dP_T()         Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.           dS_dV_P()         Method to calculate and return the volume derivative of entropy of the phase at constant pressure.           dS_dV_T()         Method to calculate and return the volume derivative of entropy of the phase at constant temperature.           dS_mass_dP()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           dS_mass_dP_T()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           dS_mass_dP_T()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           dS_mass_dT()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.           dS_mass_dT_P()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.           dS_mass_dT_P()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.	Table 6	65 – continued from previous page
dP_drho_U()         Method to calculate and return the density derivative of pressure of the phase at constant internal energy.           d5_dP()         Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.           d5_dP_T()         Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.           d5_dV_P()         Method to calculate and return the volume derivative of entropy of the phase at constant pressure.           d5_dV_T()         Method to calculate and return the volume derivative of entropy of the phase at constant temperature.           d5_mass_dP()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           d5_mass_dP_T()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           d5_mass_dP_V()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           d5_mass_dT()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature derivative of mass entropy of the phase at constant pressure.           d5_mass_dT_P()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature derivative of mass entropy of the phase at constant pressure.           d5_mass_dV_P()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.           d5_mass_dV_P()	dP_drho_S()	Method to calculate and return the density derivative
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dS_dP()       Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.         dS_dP_T()       Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.         dS_dV_P()       Method to calculate and return the volume derivative of entropy of the phase at constant pressure.         dS_dV_T()       Method to calculate and return the volume derivative of entropy of the phase at constant temperature.         dS_mass_dP()       Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.         dS_mass_dP_T()       Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.         dS_mass_dP_V()       Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_V()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_P()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.         dS_mass_dT_P()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_P()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_P()       Method to calculate and return the temperature.         df_mass_dP_D()       Method to calculat	dP_drho_U()	Method to calculate and return the density derivative
dS_dP()       Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.         dS_dP_T()       Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.         dS_dV_P()       Method to calculate and return the volume derivative of entropy of the phase at constant pressure.         dS_dV_T()       Method to calculate and return the volume derivative of entropy of the phase at constant temperature.         dS_mass_dP()       Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.         dS_mass_dP_T()       Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.         dS_mass_dP_V()       Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_V()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_P()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.         dS_mass_dT_P()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_P()       Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.         dS_mass_dT_P()       Method to calculate and return the temperature.         df_mass_dP_D()       Method to calculat		•
of entropy of the phase at constant pressure.           dS_dP_T()         Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.           dS_dV_P()         Method to calculate and return the volume derivative of entropy of the phase at constant temperature.           dS_dV_T()         Method to calculate and return the volume derivative of entropy of the phase at constant temperature.           dS_mass_dP()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           dS_mass_dP_T()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           dS_mass_dP_T()         Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.           dS_mass_dT_V()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature.           dS_mass_dT_P()         Method to calculate and return the temperature derivative of mass entropy of the phase at constant temperature derivative of mass entropy of the phase at constant pressure.           dS_mass_dT_P()         Method to calculate and return the volume derivative of mass entropy of the phase at constant temperature.           dS_mass_dT_P()         Method to calculate and return the volume derivative of temperature of mass entropy of the phase at constant temperature.           df_mass_d_T_V()         Method to calculate and return the volume derivative of temperature of the phase at constant temper	$dS_dP()$	
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$ \begin{array}{c} dT\_dT\_A() & \text{Method to calculate and return the temperature} \\ derivative of temperature of the phase at constant} \\ Helmholtz energy. \\ \hline dT\_dT\_G() & \text{Method to calculate and return the temperature} \\ derivative of temperature of the phase at constant} \\ Gibbs energy. \end{array} $		
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dT_dT_G()       Helmholtz energy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant Gibbs energy.	~	
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V V	$dU_{dV_{T}}$	
	V	temperature volume derivative of internal energy.
continues on next page		

Table 65 - continu	led from previous page
dU_mass_dP()	Method to calculate and return the pressure deriva-
	tive of mass internal energy of the phase at constant
	temperature.
dU_mass_dP_T()	Method to calculate and return the pressure deriva-
	tive of mass internal energy of the phase at constant
	temperature.
dU_mass_dP_V()	Method to calculate and return the pressure deriva-
	tive of mass internal energy of the phase at constant
	volume.
dU_mass_dT()	Method to calculate and return the temperature
	derivative of mass internal energy of the phase at con-
	stant pressure.
dU_mass_dT_P()	Method to calculate and return the temperature
0	derivative of mass internal energy of the phase at con-
	stant pressure.
dU_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass internal energy of the phase at con-
	stant volume.
dU_mass_dV_P()	Method to calculate and return the volume derivative
	of mass internal energy of the phase at constant pres-
	sure.
dU_mass_dV_T()	Method to calculate and return the volume derivative
	of mass internal energy of the phase at constant tem-
	perature.
$dV_dP_A()$	Method to calculate and return the pressure derivative
uu()	of volume of the phase at constant Helmholtz energy.
$dV_dP_G()$	Method to calculate and return the pressure derivative
	of volume of the phase at constant Gibbs energy.
dV_dP_H()	Method to calculate and return the pressure derivative
	of volume of the phase at constant enthalpy.
$dV_dP_S()$	Method to calculate and return the pressure derivative
0	of volume of the phase at constant entropy.
$dV_dP_U()$	Method to calculate and return the pressure derivative
	of volume of the phase at constant internal energy.
$dV_dT_A()$	Method to calculate and return the temperature
~	derivative of volume of the phase at constant
	Helmholtz energy.
$dV_dT_G()$	Method to calculate and return the temperature
~	derivative of volume of the phase at constant Gibbs
	energy.
dV_dT_H()	Method to calculate and return the temperature
	derivative of volume of the phase at constant en-
	thalpy.
$dV_dT_S()$	Method to calculate and return the temperature
**	derivative of volume of the phase at constant entropy.
$dV_dT_U()$	Method to calculate and return the temperature
~	derivative of volume of the phase at constant inter-
	nal energy.
$dV_{dV}_{A()}$	Method to calculate and return the volume derivative
- •	of volume of the phase at constant Helmholtz energy.
	or volume of the phase at constant menulouz chergy.

Table	e 65 – continued from previous page
$dV_dV_G()$	Method to calculate and return the volume derivative
	of volume of the phase at constant Gibbs energy.
$dV_dV_H()$	Method to calculate and return the volume derivative
	of volume of the phase at constant enthalpy.
$dV_dV_S()$	Method to calculate and return the volume derivative
	of volume of the phase at constant entropy.
dV_dV_U()	Method to calculate and return the volume derivative
uv_uv_0()	
	of volume of the phase at constant internal energy.
dV_drho_A()	Method to calculate and return the density derivative
	of volume of the phase at constant Helmholtz energy.
dV_drho_G()	Method to calculate and return the density derivative
	of volume of the phase at constant Gibbs energy.
dV_drho_H()	Method to calculate and return the density derivative
	of volume of the phase at constant enthalpy.
dV_drho_S()	Method to calculate and return the density derivative
	of volume of the phase at constant entropy.
dV_drho_U()	Method to calculate and return the density derivative
- •	of volume of the phase at constant internal energy.
drho_dP_A()	Method to calculate and return the pressure derivative
	of density of the phase at constant Helmholtz energy.
drho_dP_G()	Method to calculate and return the pressure derivative
u1110_ur_G()	
	of density of the phase at constant Gibbs energy.
drho_dP_H()	Method to calculate and return the pressure derivative
	of density of the phase at constant enthalpy.
drho_dP_S()	Method to calculate and return the pressure derivative
	of density of the phase at constant entropy.
drho_dP_U()	Method to calculate and return the pressure derivative
	of density of the phase at constant internal energy.
drho_dT_A()	Method to calculate and return the temperature
	derivative of density of the phase at constant
	Helmholtz energy.
drho_dT_G()	Method to calculate and return the temperature
	derivative of density of the phase at constant Gibbs
	energy.
drho_dT_H()	Method to calculate and return the temperature
	derivative of density of the phase at constant en-
	thalpy.
drho_dT_S()	Method to calculate and return the temperature
u1110_u1_3()	±
	derivative of density of the phase at constant entropy.
drho_dT_U()	Method to calculate and return the temperature
	derivative of density of the phase at constant internal
	energy.
drho_dV_A()	Method to calculate and return the volume derivative
	of density of the phase at constant Helmholtz energy.
drho_dV_G()	Method to calculate and return the volume derivative
	of density of the phase at constant Gibbs energy.
drho_dV_H()	Method to calculate and return the volume derivative
~	of density of the phase at constant enthalpy.
drho_dV_S()	Method to calculate and return the volume derivative
	of density of the phase at constant entropy.

Table 65 – continued from previous page

drho_dV_U()	Method to calculate and return the volume derivative
	of density of the phase at constant internal energy.
drho_drho_A()	Method to calculate and return the density derivative
v	of density of the phase at constant Helmholtz energy
drho_drho_G()	Method to calculate and return the density derivative
	of density of the phase at constant Gibbs energy.
drho_drho_H()	Method to calculate and return the density derivative
	of density of the phase at constant enthalpy.
drho_drho_S()	Method to calculate and return the density derivative
	of density of the phase at constant entropy.
drho_drho_U()	Method to calculate and return the density derivative
	of density of the phase at constant internal energy.
isentropic_exponent()	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$PV^k = \text{const.}$
<pre>isentropic_exponent_PT()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$P^{(1-k)}T^k = \text{const.}$
<pre>isentropic_exponent_PV()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$PV^k = \text{const.}$
<pre>isentropic_exponent_TV()</pre>	Method to calculate and return the real gas isentropi
	exponent of the phase, which satisfies the relationship
	$TV^{k-1} = \text{const.}$
isobaric_expansion()	Method to calculate and return the isobatic expansion
	coefficient of the bulk according to the selected cal
	culation methodology.
isothermal_bulk_modulus()	Method to calculate and return the isothermal bul
	modulus of the phase.
<b>k</b> ()	Calculate and return the thermal conductivity
	of the bulk according to the selected therma
	conductivity settings in BulkSettings, the set
	tings in ThermalConductivityGasMixtur
	and ThermalConductivityLiquidMixture
	and the configured pure-component set
	tings in ThermalConductivityGas an
	ThermalConductivityLiquid.
kappa()	Method to calculate and return the isothermal com
	pressibility of the bulk according to the selected cal
	culation methodology.
log_zs()	Method to calculate and return the log of mole frac
	tions specified.
<pre>molar_water_content([phase])</pre>	Method to calculate and return the molar water con
	tent; this is the g/mol of the fluid which is coming
	from water, [g/mol].

Table 65 – co	ontinued from previous page
mu()	Calculate and return the viscosity of the bulk according to the selected viscos- ity settings in BulkSettings, the set- tings in ViscosityGasMixture and ViscosityLiquidMixture, and the config- ured pure-component settings in ViscosityGas and ViscosityLiquid.
nu([phase])	Method to calculate and return the kinematic viscos- ity of the equilibrium state.
<pre>pseudo_Pc([phase])</pre>	Method to calculate and return the pseudocritical pressure calculated using Kay's rule (linear mole fractions):
<pre>pseudo_Tc([phase])</pre>	Method to calculate and return the pseudocritical temperature calculated using Kay's rule (linear mole fractions):
<pre>pseudo_Vc([phase])</pre>	Method to calculate and return the pseudocritical vol- ume calculated using Kay's rule (linear mole frac- tions):
<pre>pseudo_Zc([phase])</pre>	Method to calculate and return the pseudocritical compressibility calculated using Kay's rule (linear mole fractions):
rho()	Method to calculate and return the molar density of the phase.
<pre>rho_mass([phase])</pre>	Method to calculate and return mass density of the phase.
<pre>rho_mass_liquid_ref([phase])</pre>	Method to calculate and return the liquid refer- ence mass density according to the temperature variable <i>T_liquid_volume_ref</i> of <i>thermo.bulk</i> . <i>BulkSettings</i> and the composition of the phase.
sigma()	Calculate and return the surface tension of the bulk according to the selected surface ten- sion settings in BulkSettings, the settings in SurfaceTensionMixture and the configured pure-component settings in SurfaceTension.
<pre>speed_of_sound()</pre>	Method to calculate and return the molar speed of sound of the bulk according to the selected calcula- tion methodology.
<pre>speed_of_sound_mass()</pre>	Method to calculate and return the speed of sound of the phase.
value(name[, phase])	Method to retrieve a property from a string.
ws([phase])	Method to calculate and return the mass fractions of the phase, [-]
<pre>ws_no_water([phase])</pre>	Method to calculate and return the mass fractions of all species in the phase, normalized to a water-free basis (the mass fraction of water returned is zero).
<pre>zs_no_water([phase])</pre>	Method to calculate and return the mole fractions of all species in the phase, normalized to a water-free basis (the mole fraction of water returned is zero).

a d fua ma Table CE 

**A**()

Method to calculate and return the Helmholtz energy of the phase.

# Returns

A [float] Helmholtz energy, [J/mol]

**API**(phase=None)

Method to calculate and return the API of the phase.

API gravity = 
$$\frac{141.5}{\text{SG}} - 131.5$$

Returns

API [float] API of the fluid [-]

#### A\_dep()

Method to calculate and return the departure Helmholtz energy of the phase.

$$A_{dep} = U_{dep} - TS_{dep}$$

Returns

A\_dep [float] Departure Helmholtz energy, [J/mol]

#### A\_formation\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas Helmholtz energy of formation of the phase (as if the phase was an ideal gas).

$$A_{reactive}^{ig} = U_{reactive}^{ig} - T_{ref}^{ig} S_{reactive}^{ig}$$

Returns

**A\_formation\_ideal\_gas** [float] Helmholtz energy of formation of the phase on a reactive basis as an ideal gas, [J/(mol)]

Method to calculate and return the ideal-gas Helmholtz energy of the phase.

$$A^{ig} = U^{ig} - TS^{ig}$$

Returns

A\_ideal\_gas [float] Ideal gas Helmholtz free energy, [J/(mol)]

#### A\_mass(phase=None)

Method to calculate and return mass Helmholtz energy of the phase.

$$A_{mass} = \frac{1000A_{molar}}{MW}$$

Returns

A\_mass [float] Mass Helmholtz energy, [J/(kg)]

#### A\_reactive()

Method to calculate and return the Helmholtz free energy of the phase on a reactive basis.

$$A_{reactive} = U_{reactive} - TS_{reactive}$$

Returns

A\_reactive [float] Helmholtz free energy of the phase on a reactive basis, [J/(mol)]

#### Bvirial(phase=None)

Method to calculate and return the *B* virial coefficient of the phase at its current conditions.

Returns

Bvirial [float] Virial coefficient, [m^3/mol]

# property CASs

CAS registration numbers for each component, [-].

Returns

CASs [list[str]] CAS registration numbers for each component, [-].

# property Carcinogens

Status of each component in cancer causing registries, [-].

Returns

Carcinogens [list[dict]] Status of each component in cancer causing registries, [-].

# property Ceilings

Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

# Returns

**Ceilings** [list[tuple[(float, str)]]] Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

# Cp()

Method to calculate and return the constant-temperature and constant phase-fraction heat capacity of the bulk phase. This is a phase-fraction weighted calculation.

$$C_p = \sum_{i}^{p} C_{p,i} \beta_i$$

# Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

#### Cp\_Cv\_ratio()

Method to calculate and return the Cp/Cv ratio of the phase.

$$\frac{C_p}{C_v}$$

#### Returns

Cp\_Cv\_ratio [float] Cp/Cv ratio, [-]

# Cp\_Cv\_ratio\_ideal\_gas(phase=None)

Method to calculate and return the ratio of the ideal-gas heat capacity to its constant-volume heat capacity.

$$\frac{C_p^{ig}}{C_v^{ig}}$$

Returns

Cp\_Cv\_ratio\_ideal\_gas [float] Cp/Cv for the phase as an ideal gas, [-]

#### **Cp\_dep**(*phase=None*)

Method to calculate and return the difference between the actual Cp and the ideal-gas heat capacity  $C_p^{ig}$  of the phase.

$$C_p^{dep} = C_p - C_p^{ig}$$

Returns

**Cp\_dep** [float] Departure ideal gas heat capacity, [J/(mol\*K)]

### Cp\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas heat capacity of the phase.

$$C_p^{ig} = \sum_i z_i C_{p,i}^{ig}$$

Returns

**Cp** [float] Ideal gas heat capacity, [J/(mol\*K)]

**Cp\_mass**(*phase=None*)

Method to calculate and return mass constant pressure heat capacity of the phase.

$$Cp_{mass} = \frac{1000Cp_{molar}}{MW}$$

Returns

**Cp\_mass** [float] Mass heat capacity, [J/(kg\*K)]

**Cv**()

Method to calculate and return the constant-volume heat capacity Cv of the phase.

$$C_v = T \left(\frac{\partial P}{\partial T}\right)_V^2 / \left(\frac{\partial P}{\partial V}\right)_T + Cp$$

Returns

Cv [float] Constant volume molar heat capacity, [J/(mol\*K)]

**Cv\_dep**(*phase=None*)

Method to calculate and return the difference between the actual Cv and the ideal-gas constant volume heat capacity  $C_v^{ig}$  of the phase.

$$C_v^{dep} = C_v - C_v^{ig}$$

Returns

Cv\_dep [float] Departure ideal gas constant volume heat capacity, [J/(mol\*K)]

## Cv\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas constant volume heat capacity of the phase.

$$C_v^{ig} = \sum_i z_i C_{p,i}^{ig} - R$$

Returns

Cv [float] Ideal gas constant volume heat capacity, [J/(mol\*K)]

**Cv\_mass**(*phase=None*)

Method to calculate and return mass constant volume heat capacity of the phase.

$$Cv_{mass} = \frac{1000Cv_{molar}}{MW}$$

Returns

**Cv\_mass** [float] Mass constant volume heat capacity, [J/(kg\*K)]

#### property EnthalpySublimations

Wrapper to obtain the list of EnthalpySublimations objects of the associated *PropertyCorrelationsPackage*.

#### property EnthalpyVaporizations

Wrapper to obtain the list of EnthalpyVaporizations objects of the associated *PropertyCorrelationsPackage*.

#### **G**()

Method to calculate and return the Gibbs free energy of the phase.

G = H - TS

## Returns

G [float] Gibbs free energy, [J/mol]

#### property GWPs

Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

#### Returns

**GWPs** [list[float]] Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

# G\_dep()

Method to calculate and return the departure Gibbs free energy of the phase.

$$G_{dep} = H_{dep} - TS_{dep}$$

#### Returns

G\_dep [float] Departure Gibbs free energy, [J/mol]

# G\_formation\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas Gibbs free energy of formation of the phase (as if the phase was an ideal gas).

$$G_{reactive}^{ig} = H_{reactive}^{ig} - T_{ref}^{ig} S_{reactive}^{ig}$$

## Returns

**G\_formation\_ideal\_gas** [float] Gibbs free energy of formation of the phase on a reactive basis as an ideal gas, [J/(mol)]

Method to calculate and return the ideal-gas Gibbs free energy of the phase.

$$G^{ig} = H^{ig} - TS^{ig}$$

Returns

**G\_ideal\_gas** [float] Ideal gas free energy, [J/(mol)]

**G\_mass**(*phase=None*)

Method to calculate and return mass Gibbs energy of the phase.

$$G_{mass} = \frac{1000G_{molar}}{MW}$$

Returns

G\_mass [float] Mass Gibbs energy, [J/(kg)]

#### G\_reactive()

Method to calculate and return the Gibbs free energy of the phase on a reactive basis.

 $G_{reactive} = H_{reactive} - TS_{reactive}$ 

# Returns

G\_reactive [float] Gibbs free energy of the phase on a reactive basis, [J/(mol)]

# property Gfgs

Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

# Returns

**Gfgs** [list[float]] Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

# property Gfgs\_mass

Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

#### Returns

**Gfgs\_mass** [list[float]] Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

#### **H**()

Method to calculate and return the constant-temperature and constant phase-fraction enthalpy of the bulk phase. This is a phase-fraction weighted calculation.

$$H = \sum_{i}^{p} H_{i}\beta_{i}$$

#### Returns

H [float] Molar enthalpy, [J/(mol)]

#### **H\_C\_ratio**(*phase=None*)

Method to calculate and return the atomic ratio of hydrogen atoms to carbon atoms, based on the current composition of the phase.

#### Returns

H\_C\_ratio [float] H/C ratio on a molar basis, [-]

#### Notes

None is returned if no species are present that have carbon atoms.

#### H\_C\_ratio\_mass(phase=None)

Method to calculate and return the mass ratio of hydrogen atoms to carbon atoms, based on the current composition of the phase.

# Returns

H\_C\_ratio\_mass [float] H/C ratio on a mass basis, [-]

#### Notes

None is returned if no species are present that have carbon atoms.

H\_dep(phase=None)

Method to calculate and return the difference between the actual H and the ideal-gas enthalpy of the phase.

$$H^{dep} = H - H^{ig}$$

Returns

H\_dep [float] Departure enthalpy, [J/(mol)]

#### H\_formation\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas enthalpy of formation of the phase (as if the phase was an ideal gas).

$$H_{reactive}^{ig} = \sum_{i} z_i H_{f,i}$$

#### Returns

**H\_formation\_ideal\_gas** [float] Enthalpy of formation of the phase on a reactive basis as an ideal gas, [J/mol]

#### H\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas enthalpy of the phase.

$$H^{ig} = \sum_{i} z_i H_i^{ig}$$

# Returns

H [float] Ideal gas enthalpy, [J/(mol)]

H\_mass(phase=None)

Method to calculate and return mass enthalpy of the phase.

$$H_{mass} = \frac{1000H_{molar}}{MW}$$

Returns

H\_mass [float] Mass enthalpy, [J/kg]

#### H\_reactive()

Method to calculate and return the constant-temperature and constant phase-fraction reactive enthalpy of the bulk phase. This is a phase-fraction weighted calculation.

$$H_{\text{reactive}} = \sum_{i}^{p} H_{\text{reactive},i} \beta_{i}$$

Returns

H\_reactive [float] Reactive molar enthalpy, [J/(mol)]

#### Hc(phase=None)

Method to calculate and return the molar ideal-gas higher heat of combustion of the object, [J/mol]

#### Returns

Hc [float] Molar higher heat of combustion, [J/(mol)]

# Hc\_lower(phase=None)

Method to calculate and return the molar ideal-gas lower heat of combustion of the object, [J/mol]

Returns

Hc\_lower [float] Molar lower heat of combustion, [J/(mol)]

## Hc\_lower\_mass(phase=None)

Method to calculate and return the mass ideal-gas lower heat of combustion of the object, [J/mol]

Returns

Hc\_lower\_mass [float] Mass lower heat of combustion, [J/(kg)]

### Hc\_lower\_normal(phase=None)

Method to calculate and return the volumetric ideal-gas lower heat of combustion of the object using the normal gas volume, [J/m^3]

### Returns

Hc\_lower\_normal [float] Volumetric (normal) lower heat of combustion, [J/(m^3)]

### Hc\_lower\_standard(phase=None)

Method to calculate and return the volumetric ideal-gas lower heat of combustion of the object using the standard gas volume, [J/m^3]

# Returns

Hc\_lower\_standard [float] Volumetric (standard) lower heat of combustion, [J/(m^3)]

### Hc\_mass(phase=None)

Method to calculate and return the mass ideal-gas higher heat of combustion of the object, [J/mol]

Returns

Hc\_mass [float] Mass higher heat of combustion, [J/(kg)]

# Hc\_normal(phase=None)

Method to calculate and return the volumetric ideal-gas higher heat of combustion of the object using the normal gas volume, [J/m^3]

# Returns

Hc\_normal [float] Volumetric (normal) higher heat of combustion, [J/(m^3)]

# Hc\_standard(phase=None)

Method to calculate and return the volumetric ideal-gas higher heat of combustion of the object using the standard gas volume, [J/m^3]

#### Returns

Hc\_normal [float] Volumetric (standard) higher heat of combustion, [J/(m^3)]

### property Hcs

Higher standard molar heats of combustion for each component, [J/mol].

# Returns

Hcs [list[float]] Higher standard molar heats of combustion for each component, [J/mol].

### property Hcs\_lower

Lower standard molar heats of combustion for each component, [J/mol].

# Returns

**Hcs\_lower** [list[float]] Lower standard molar heats of combustion for each component, [J/mol].

#### property Hcs\_lower\_mass

Lower standard heats of combustion for each component, [J/kg].

### Returns

Hcs\_lower\_mass [list[float]] Lower standard heats of combustion for each component, [J/kg].

# property Hcs\_mass

Higher standard heats of combustion for each component, [J/kg].

Returns

Hcs\_mass [list[float]] Higher standard heats of combustion for each component, [J/kg].

### property HeatCapacityGasMixture

Wrapper to obtain the list of HeatCapacityGasMixture objects of the associated *PropertyCorrelationsPackage*.

#### property HeatCapacityGases

Wrapper to obtain the list of HeatCapacityGases objects of the associated *PropertyCorrelationsPackage*.

## property HeatCapacityLiquidMixture

Wrapper to obtain the list of HeatCapacityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.

### property HeatCapacityLiquids

Wrapper to obtain the list of HeatCapacityLiquids objects of the associated *PropertyCorrelationsPackage*.

# property HeatCapacitySolidMixture

Wrapper to obtain the list of HeatCapacitySolidMixture objects of the associated *PropertyCorrelationsPackage*.

### property HeatCapacitySolids

Wrapper to obtain the list of HeatCapacitySolids objects of the associated *PropertyCorrelationsPackage*.

# property Hf\_STPs

Standard state molar enthalpies of formation for each component, [J/mol].

#### Returns

**Hf\_STPs** [list[float]] Standard state molar enthalpies of formation for each component, [J/mol].

# property Hf\_STPs\_mass

Standard state mass enthalpies of formation for each component, [J/kg].

#### Returns

**Hf\_STPs\_mass** [list[float]] Standard state mass enthalpies of formation for each component, [J/kg].

### property Hfgs

Ideal gas standard molar enthalpies of formation for each component, [J/mol].

# Returns

**Hfgs** [list[float]] Ideal gas standard molar enthalpies of formation for each component, [J/mol].

# property Hfgs\_mass

Ideal gas standard enthalpies of formation for each component, [J/kg].

Returns

Hfgs\_mass [list[float]] Ideal gas standard enthalpies of formation for each component, [J/kg].

## property Hfus\_Tms

Molar heats of fusion for each component at their respective melting points, [J/mol].

### Returns

**Hfus\_Tms** [list[float]] Molar heats of fusion for each component at their respective melting points, [J/mol].

# property Hfus\_Tms\_mass

Heats of fusion for each component at their respective melting points, [J/kg].

#### Returns

**Hfus\_Tms\_mass** [list[float]] Heats of fusion for each component at their respective melting points, [J/kg].

# property Hsub\_Tts

Heats of sublimation for each component at their respective triple points, [J/mol].

# Returns

**Hsub\_Tts** [list[float]] Heats of sublimation for each component at their respective triple points, [J/mol].

# property Hsub\_Tts\_mass

Heats of sublimation for each component at their respective triple points, [J/kg].

## Returns

Hsub\_Tts\_mass [list[float]] Heats of sublimation for each component at their respective triple points, [J/kg].

# property Hvap\_298s

Molar heats of vaporization for each component at 298.15 K, [J/mol].

#### Returns

Hvap\_298s [list[float]] Molar heats of vaporization for each component at 298.15 K, [J/mol].

### property Hvap\_298s\_mass

Heats of vaporization for each component at 298.15 K, [J/kg].

#### Returns

Hvap\_298s\_mass [list[float]] Heats of vaporization for each component at 298.15 K, [J/kg].

# property Hvap\_Tbs

Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].

# Returns

**Hvap\_Tbs** [list[float]] Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].

# property Hvap\_Tbs\_mass

Heats of vaporization for each component at their respective normal boiling points, [J/kg].

**Hvap\_Tbs\_mass** [list[float]] Heats of vaporization for each component at their respective normal boiling points, [J/kg].

### property IDs

Alias of CASs.

# property InChI\_Keys

InChI Keys for each component, [-].

Returns

InChI\_Keys [list[str]] InChI Keys for each component, [-].

# property InChIs

InChI strings for each component, [-].

#### Returns

InChIs [list[str]] InChI strings for each component, [-].

## Joule\_Thomson()

Method to calculate and return the Joule-Thomson coefficient of the bulk according to the selected calculation methodology.

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_H$$

#### Returns

mu\_JT [float] Joule-Thomson coefficient [K/Pa]

## Ks(phase, phase\_ref=None)

Method to calculate and return the K-values of each phase. These are NOT just liquid-vapor K values; these are thermodynamic K values. The reference phase can be specified with *phase\_ref*, and then the K-values will be with respect to that phase.

$$K_i = \frac{z_{i,\text{phase}}}{z_{i,\text{ref phase}}}$$

If no reference phase is provided, the following criteria is used to select one:

- If the flash algorithm provided a reference phase, use that
- Otherwise use the liquid0 phase if one is present
- · Otherwise use the solid0 phase if one is present
- · Otherwise use the gas phase if one is present

## Returns

Ks [list[float]] Equilibrium K values, [-]

#### property LF

Method to return the liquid fraction of the equilibrium state. If no liquid is present, 0 is always returned.

#### Returns

LF [float] Liquid molar fraction, [-]

# property LFLs

Lower flammability limits for each component, [-].

LFLs [list[float]] Lower flammability limits for each component, [-].

#### MW(phase=None)

Method to calculate and return the molecular weight of the phase.

$$MW = \sum_i z_i MW_i$$

Returns

**MW** [float] Molecular weight of the phase, [g/mol]

# property MWs

Similativy variables for each component, [g/mol].

### Returns

MWs [list[float]] Similatiry variables for each component, [g/mol].

## property ODPs

Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

### Returns

**ODPs** [list[float]] Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

# PIP()

Method to calculate and return the phase identification parameter of the phase.

$$\Pi = V \begin{bmatrix} \frac{\partial^2 P}{\partial V \partial T} & \frac{\partial^2 P}{\partial V} \\ \frac{\partial P}{\partial T} & -\frac{\partial^2 P}{\partial V} \end{bmatrix}$$

Returns

**PIP** [float] Phase identification parameter, [-]

# property PSRK\_groups

PSRK subgroup: count groups for each component, [-].

### Returns

PSRK\_groups [list[dict]] PSRK subgroup: count groups for each component, [-].

## $P_{REF_{IG}} = 101325.0$

### P\_REF\_IG\_INV = 9.869232667160129e-06

# property Parachors

Parachors for each component, [N^0.25\*m^2.75/mol].

## Returns

Parachors [list[float]] Parachors for each component, [N^0.25\*m^2.75/mol].

### property Pcs

Critical pressures for each component, [Pa].

#### Returns

**Pcs** [list[float]] Critical pressures for each component, [Pa].

# property PermittivityLiquids

Wrapper to obtain the list of PermittivityLiquids objects of the associated *PropertyCorrelationsPackage*.

### Pmc(phase=None)

Method to calculate and return the mechanical critical pressure of the phase.

## Returns

Pmc [float] Mechanical critical pressure, [Pa]

## property Psat\_298s

Vapor pressures for each component at 298.15 K, [Pa].

#### Returns

Psat\_298s [list[float]] Vapor pressures for each component at 298.15 K, [Pa].

#### property Pts

Triple point pressures for each component, [Pa].

#### Returns

Pts [list[float]] Triple point pressures for each component, [Pa].

# property PubChems

Pubchem IDs for each component, [-].

#### Returns

PubChems [list[int]] Pubchem IDs for each component, [-].

# property RI\_Ts

Temperatures at which the refractive indexes were reported for each component, [K].

### Returns

**RI\_Ts** [list[float]] Temperatures at which the refractive indexes were reported for each component, [K].

# property RIs

Refractive indexes for each component, [-].

#### Returns

**RIs** [list[float]] Refractive indexes for each component, [-].

# **S**()

Method to calculate and return the constant-temperature and constant phase-fraction entropy of the bulk phase. This is a phase-fraction weighted calculation.

$$S = \sum_{i}^{p} S_{i} \beta_{i}$$

#### Returns

**S** [float] Molar entropy, [J/(mol\*K)]

# property S0gs

Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].

#### Returns

**S0gs** [list[float]] Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].

# property S0gs\_mass

Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].

**S0gs\_mass** [list[float]] Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].

SG(phase=None)

Method to calculate and return the standard liquid specific gravity of the phase, using constant liquid pure component densities not calculated by the phase object, at 60 °F.

## Returns

SG [float] Specific gravity of the liquid, [-]

## Notes

The reference density of water is from the IAPWS-95 standard - 999.0170824078306 kg/m^3.

#### SG\_gas(phase=None)

Method to calculate and return the specific gravity of the phase with respect to a gas reference density.

Returns

SG\_gas [float] Specific gravity of the gas, [-]

### Notes

The reference molecular weight of air used is 28.9586 g/mol.

# property STELs

Short term exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].

# Returns

**STELs** [list[tuple[(float, str)]]] Short term exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

#### S\_dep(phase=None)

Method to calculate and return the difference between the actual S and the ideal-gas entropy of the phase.

$$S^{dep} = S - S^{ig}$$

Returns

**S\_dep** [float] Departure entropy, [J/(mol\*K)]

# S\_formation\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas entropy of formation of the phase (as if the phase was an ideal gas).

$$S_{reactive}^{ig} = \sum_{i} z_i S_{f,i}$$

Returns

**S\_formation\_ideal\_gas** [float] Entropy of formation of the phase on a reactive basis as an ideal gas, [J/(mol\*K)]

## S\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas entropy of the phase.

$$S^{ig} = \sum_{i} z_i S_i^{ig} - R \ln\left(\frac{P}{P_{ref}}\right) - R \sum_{i} z_i \ln(z_i)$$

**S** [float] Ideal gas molar entropy, [J/(mol\*K)]

# S\_mass(phase=None)

Method to calculate and return mass entropy of the phase.

$$S_{mass} = \frac{1000S_{molar}}{MW}$$

Returns

**S\_mass** [float] Mass enthalpy, [J/(kg\*K)]

# S\_reactive()

Method to calculate and return the constant-temperature and constant phase-fraction reactive entropy of the bulk phase. This is a phase-fraction weighted calculation.

$$S_{\text{reactive}} = \sum_{i}^{p} S_{\text{reactive},i} \beta_{i}$$

Returns

**S\_reactive** [float] Reactive molar entropy, [J/(mol\*K)]

## property Sfgs

Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

# Returns

**Sfgs** [list[float]] Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

# property Sfgs\_mass

Ideal gas standard entropies of formation for each component, [J/(kg\*K)].

# Returns

**Sfgs\_mass** [list[float]] Ideal gas standard entropies of formation for each component, [J/(kg\*K)].

## property Skins

Whether each compound can be absorbed through the skin or not, [-].

#### Returns

Skins [list[bool]] Whether each compound can be absorbed through the skin or not, [-].

# property StielPolars

Stiel polar factors for each component, [-].

Returns

StielPolars [list[float]] Stiel polar factors for each component, [-].

# property Stockmayers

Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].

#### Returns

**Stockmayers** [list[float]] Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].

#### property SublimationPressures

Wrapper to obtain the list of SublimationPressures objects of the associated *PropertyCorrelationsPackage*.

#### property SurfaceTensionMixture

Wrapper to obtain the list of SurfaceTensionMixture objects of the associated *PropertyCorrelationsPackage*.

#### property SurfaceTensions

Wrapper to obtain the list of SurfaceTensions objects of the associated PropertyCorrelationsPackage.

### property TWAs

Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].

#### Returns

**TWAs** [list[tuple[(float, str)]]] Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].

# $T\_REF\_IG = 298.15$

#### T\_REF\_IG\_INV = 0.0033540164346805303

#### property Tautoignitions

Autoignition temperatures for each component, [K].

Returns

Tautoignitions [list[float]] Autoignition temperatures for each component, [K].

#### property Tbs

Boiling temperatures for each component, [K].

### Returns

**Tbs** [list[float]] Boiling temperatures for each component, [K].

# property Tcs

Critical temperatures for each component, [K].

# Returns

**Tcs** [list[float]] Critical temperatures for each component, [K].

## property Tflashs

Flash point temperatures for each component, [K].

### Returns

Tflashs [list[float]] Flash point temperatures for each component, [K].

## property ThermalConductivityGasMixture

Wrapper to obtain the list of ThermalConductivityGasMixture objects of the associated *PropertyCorrelationsPackage*.

# property ThermalConductivityGases

Wrapper to obtain the list of ThermalConductivityGases objects of the associated *PropertyCorrelationsPackage*.

# property ThermalConductivityLiquidMixture

Wrapper to obtain the list of ThermalConductivityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.

## property ThermalConductivityLiquids

Wrapper to obtain the list of ThermalConductivityLiquids objects of the associated *PropertyCorrelationsPackage*.

## Tmc(phase=None)

Method to calculate and return the mechanical critical temperature of the phase.

### Returns

Tmc [float] Mechanical critical temperature, [K]

# property Tms

Melting temperatures for each component, [K].

Returns

Tms [list[float]] Melting temperatures for each component, [K].

# property Tts

Triple point temperatures for each component, [K].

## Returns

**Tts** [list[float]] Triple point temperatures for each component, [K].

#### **U**()

Method to calculate and return the internal energy of the phase.

$$U = H - PV$$

### Returns

U [float] Internal energy, [J/mol]

# property UFLs

Upper flammability limits for each component, [-].

## Returns

UFLs [list[float]] Upper flammability limits for each component, [-].

# property UNIFAC\_Dortmund\_groups

UNIFAC\_Dortmund\_group: count groups for each component, [-].

### Returns

**UNIFAC\_Dortmund\_groups** [list[dict]] UNIFAC\_Dortmund\_group: count groups for each component, [-].

# property UNIFAC\_Qs

UNIFAC Q parameters for each component, [-].

### Returns

UNIFAC\_Qs [list[float]] UNIFAC Q parameters for each component, [-].

# property UNIFAC\_Rs

UNIFAC R parameters for each component, [-].

#### Returns

UNIFAC\_Rs [list[float]] UNIFAC R parameters for each component, [-].

# property UNIFAC\_groups

UNIFAC\_group: count groups for each component, [-].

UNIFAC\_groups [list[dict]] UNIFAC\_group: count groups for each component, [-].

U\_dep()

Method to calculate and return the departure internal energy of the phase.

$$U_{dep} = H_{dep} - PV_{dep}$$

Returns

U\_dep [float] Departure internal energy, [J/mol]

#### U\_formation\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas internal energy of formation of the phase (as if the phase was an ideal gas).

$$U_{reactive}^{ig} = H_{reactive}^{ig} - P_{ref}^{ig} V^{ig}$$

Returns

**U\_formation\_ideal\_gas** [float] Internal energy of formation of the phase on a reactive basis as an ideal gas, [J/(mol)]

```
U_ideal_gas(phase=None)
```

Method to calculate and return the ideal-gas internal energy of the phase.

$$U^{ig} = H^{ig} - PV^{ig}$$

Returns

U\_ideal\_gas [float] Ideal gas internal energy, [J/(mol)]

U\_mass(phase=None)

Method to calculate and return mass internal energy of the phase.

$$U_{mass} = \frac{1000U_{molar}}{MW}$$

Returns

U\_mass [float] Mass internal energy, [J/(kg)]

#### U\_reactive()

Method to calculate and return the internal energy of the phase on a reactive basis.

$$U_{reactive} = H_{reactive} - PV$$

Returns

U\_reactive [float] Internal energy of the phase on a reactive basis, [J/(mol)]

**V**()

Method to calculate and return the molar volume of the bulk phase. This is a phase-fraction weighted calculation.

$$V = \sum_{i}^{p} V_{i}\beta_{i}$$

Returns

V [float] Molar volume, [m^3/mol]

#### property VF

Method to return the vapor fraction of the equilibrium state. If no vapor/gas is present, 0 is always returned.

VF [float] Vapor molar fraction, [-]

V\_dep()

Method to calculate and return the departure (from ideal gas behavior) molar volume of the phase.

$$V_{dep} = V - \frac{RT}{P}$$

Returns

V\_dep [float] Departure molar volume, [m^3/mol]

V\_gas(phase=None)

Method to calculate and return the ideal-gas molar volume of the phase at the chosen reference temperature and pressure, according to the temperature variable  $T\_gas\_ref$  and pressure variable  $P\_gas\_ref$  of the thermo.bulk.BulkSettings.

$$V^{ig} = \frac{RT_{ref}}{P_{ref}}$$

Returns

V\_gas [float] Ideal gas molar volume at the reference temperature and pressure, [m^3/mol]

### V\_gas\_normal(phase=None)

Method to calculate and return the ideal-gas molar volume of the phase at the normal temperature and pressure, according to the temperature variable *T\_normal* and pressure variable *P\_normal* of the thermo. bulk.BulkSettings.

$$V^{ig} = \frac{RT_{norm}}{P_{norm}}$$

Returns

V\_gas\_normal [float] Ideal gas molar volume at normal temperature and pressure, [m^3/mol]

### V\_gas\_standard(phase=None)

Method to calculate and return the ideal-gas molar volume of the phase at the standard temperature and pressure, according to the temperature variable *T\_standard* and pressure variable *P\_standard* of the *thermo*. *bulk.BulkSettings*.

$$V^{ig} = \frac{RT_{std}}{P_{std}}$$

Returns

**V\_gas\_standard** [float] Ideal gas molar volume at standard temperature and pressure, [m^3/mol]

# V\_ideal\_gas(phase=None)

Method to calculate and return the ideal-gas molar volume of the phase.

$$V^{ig} = \frac{RT}{P}$$

#### Returns

V [float] Ideal gas molar volume, [m^3/mol]

# **V\_iter**(*phase=None*, *force=False*)

Method to calculate and return the volume of the phase in a way suitable for a TV resolution to converge on the same pressure. This often means the return value of this method is an mpmath *mpf*. This dummy method simply returns the implemented V method.

### Returns

V [float or mpf] Molar volume, [m^3/mol]

## V\_liquid\_ref(phase=None)

Method to calculate and return the liquid reference molar volume according to the temperature variable *T\_liquid\_volume\_ref* of *thermo.bulk.BulkSettings* and the composition of the phase.

$$V = \sum_{i} z_i V_i$$

# Returns

V\_liquid\_ref [float] Liquid molar volume at the reference condition, [m^3/mol]

# V\_liquids\_ref()

Method to calculate and return the liquid reference molar volumes according to the temperature variable *T\_liquid\_volume\_ref* of *thermo.bulk.BulkSettings*.

### Returns

V\_liquids\_ref [list[float]] Liquid molar volumes at the reference condition, [m^3/mol]

### V\_mass(phase=None)

Method to calculate and return the specific volume of the phase.

$$V_{mass} = \frac{1000 \cdot VM}{MW}$$

Returns

V\_mass [float] Specific volume of the phase, [m^3/kg]

#### property Van\_der\_Waals\_areas

Unnormalized Van der Waals areas for each component, [m^2/mol].

# Returns

Van\_der\_Waals\_areas [list[float]] Unnormalized Van der Waals areas for each component, [m^2/mol].

# property Van\_der\_Waals\_volumes

Unnormalized Van der Waals volumes for each component, [m^3/mol].

## Returns

Van\_der\_Waals\_volumes [list[float]] Unnormalized Van der Waals volumes for each component, [m^3/mol].

## property VaporPressures

Wrapper to obtain the list of VaporPressures objects of the associated PropertyCorrelationsPackage.

# property Vcs

Critical molar volumes for each component, [m<sup>3</sup>/mol].

### Returns

Vcs [list[float]] Critical molar volumes for each component, [m^3/mol].

# Vfgs(phase=None)

Method to calculate and return the ideal-gas volume fractions of the components of the phase. This is the same as the mole fractions.

## Returns

Vfgs [list[float]] Ideal-gas volume fractions of the components of the phase, [-]

# Vfls(phase=None)

Method to calculate and return the ideal-liquid volume fractions of the components of the phase, using the standard liquid densities at the temperature variable *T\_liquid\_volume\_ref* of thermo.bulk. BulkSettings and the composition of the phase.

### Returns

Vfls [list[float]] Ideal-liquid volume fractions of the components of the phase, [-]

## property ViscosityGasMixture

Wrapper to obtain the list of ViscosityGasMixture objects of the associated *PropertyCorrelationsPackage*.

# property ViscosityGases

Wrapper to obtain the list of ViscosityGases objects of the associated PropertyCorrelationsPackage.

# property ViscosityLiquidMixture

Wrapper to obtain the list of ViscosityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.

### property ViscosityLiquids

Wrapper to obtain the list of ViscosityLiquids objects of the associated PropertyCorrelationsPackage.

## Vmc(phase=None)

Method to calculate and return the mechanical critical volume of the phase.

#### Returns

Vmc [float] Mechanical critical volume, [m^3/mol]

# property Vmg\_STPs

Gas molar volumes for each component at STP; metastable if normally another state, [m^3/mol].

#### Returns

Vmg\_STPs [list[float]] Gas molar volumes for each component at STP; metastable if normally another state, [m<sup>3</sup>/mol].

# property Vml\_60Fs

Liquid molar volumes for each component at 60 °F, [m^3/mol].

### Returns

Vml\_60Fs [list[float]] Liquid molar volumes for each component at 60 °F, [m^3/mol].

# property Vml\_STPs

Liquid molar volumes for each component at STP, [m<sup>3</sup>/mol].

## Returns

Vml\_STPs [list[float]] Liquid molar volumes for each component at STP, [m^3/mol].

# property Vml\_Tms

Liquid molar volumes for each component at their respective melting points, [m^3/mol].

**Vml\_Tms** [list[float]] Liquid molar volumes for each component at their respective melting points, [m^3/mol].

# property Vms\_Tms

Solid molar volumes for each component at their respective melting points, [m^3/mol].

Returns

Vms\_Tms [list[float]] Solid molar volumes for each component at their respective melting points, [m^3/mol].

### property VolumeGasMixture

Wrapper to obtain the list of VolumeGasMixture objects of the associated *PropertyCorrelationsPackage*.

#### property VolumeGases

Wrapper to obtain the list of VolumeGases objects of the associated PropertyCorrelationsPackage.

## property VolumeLiquidMixture

Wrapper to obtain the list of VolumeLiquidMixture objects of the associated *PropertyCorrelationsPackage*.

#### property VolumeLiquids

Wrapper to obtain the list of VolumeLiquids objects of the associated PropertyCorrelationsPackage.

### property VolumeSolidMixture

Wrapper to obtain the list of VolumeSolidMixture objects of the associated *PropertyCorrelationsPackage*.

### property VolumeSolids

Wrapper to obtain the list of VolumeSolids objects of the associated PropertyCorrelationsPackage.

### Wobbe\_index(phase=None)

Method to calculate and return the molar Wobbe index of the object, [J/mol].

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{\text{SG}}}$$

Returns

Wobbe\_index [float] Molar Wobbe index, [J/(mol)]

Wobbe\_index\_lower(phase=None)

Method to calculate and return the molar lower Wobbe index of the object, [J/mol].

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

Returns

Wobbe\_index\_lower [float] Molar lower Wobbe index, [J/(mol)]

# Wobbe\_index\_lower\_mass(phase=None)

Method to calculate and return the lower mass Wobbe index of the object, [J/kg].

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

### Wobbe\_index\_lower\_normal(phase=None)

Method to calculate and return the volumetric normal lower Wobbe index of the object, [J/m^3]. The normal gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

Returns

#### Wobbe\_index\_lower\_standard(phase=None)

Method to calculate and return the volumetric standard lower Wobbe index of the object, [J/m^3]. The standard gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

Returns

Wobbe\_index\_lower\_standard [float] Volumetric standard lower Wobbe index, [J/(m^3)]

#### Wobbe\_index\_mass(phase=None)

Method to calculate and return the mass Wobbe index of the object, [J/kg].

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{\text{SG}}}$$

Returns

Wobbe\_index\_mass [float] Mass Wobbe index, [J/(kg)]

#### Wobbe\_index\_normal(phase=None)

Method to calculate and return the volumetric normal Wobbe index of the object, [J/m<sup>3</sup>]. The normal gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{SG}}$$

Returns

**Wobbe\_index** [float] Volumetric normal Wobbe index, [J/(m^3)]

# Wobbe\_index\_standard(phase=None)

Method to calculate and return the volumetric standard Wobbe index of the object, [J/m<sup>3</sup>]. The standard gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{\text{SG}}}$$

#### Returns

Wobbe\_index\_standard [float] Volumetric standard Wobbe index, [J/(m^3)]

Z()

Method to calculate and return the compressibility factor of the phase.

$$Z = \frac{PV}{RT}$$

#### Returns

Z [float] Compressibility factor, [-]

# property Zcs

Critical compressibilities for each component, [-].

# Returns

Zcs [list[float]] Critical compressibilities for each component, [-].

# Zmc(phase=None)

Method to calculate and return the mechanical critical compressibility of the phase.

# Returns

**Zmc** [float] Mechanical critical compressibility, [-]

# alpha(phase=None)

Method to calculate and return the thermal diffusivity of the equilibrium state.

$$\alpha = \frac{k}{\rho C p}$$

Returns

alpha [float] Thermal diffusivity, [m<sup>2</sup>/s]

# atom\_fractions(phase=None)

Method to calculate and return the atomic composition of the phase; returns a dictionary of atom fraction (by count), containing only those elements who are present.

# Returns

atom\_fractions [dict[str: float]] Atom fractions, [-]

# atom\_mass\_fractions(phase=None)

Method to calculate and return the atomic mass fractions of the phase; returns a dictionary of atom fraction (by mass), containing only those elements who are present.

# Returns

atom\_mass\_fractions [dict[str: float]] Atom mass fractions, [-]

# property atomss

Breakdown of each component into its elements and their counts, as a dict, [-].

# Returns

atomss [list[dict]] Breakdown of each component into its elements and their counts, as a dict,

[-].

# property betas\_liquids

Method to calculate and return the fraction of the liquid phase that each liquid phase is, by molar phase fraction. If the system is VLLL with phase fractions of 0.125 vapor, and [.25, .125, .5] for the three liquids phases respectively, the return value would be [0.28571428, 0.142857142, 0.57142857].

# Returns

betas\_liquids [list[float]] Molar phase fractions of the overall liquid phase, [-]

# property betas\_mass

Method to calculate and return the mass fraction of all of the phases in the system.

# Returns

**betas\_mass** [list[float]] Mass phase fractions of all the phases, ordered vapor, liquid, then solid , [-]

# property betas\_mass\_liquids

Method to calculate and return the fraction of the liquid phase that each liquid phase is, by mass phase fraction. If the system is VLLL with mass phase fractions of 0.125 vapor, and [.25, .125, .5] for the three liquids phases respectively, the return value would be [0.28571428, 0.142857142, 0.57142857].

Returns

betas\_mass\_liquids [list[float]] Mass phase fractions of the overall liquid phase, [-]

#### property betas\_mass\_states

Method to return the mass phase fractions of each of the three fundamental types of phases.

# Returns

**betas\_mass\_states** [list[float, 3]] List containing the mass phase fraction of gas, liquid, and solid, [-]

# property betas\_states

Method to return the molar phase fractions of each of the three fundamental types of phases.

### Returns

**betas\_states** [list[float, 3]] List containing the molar phase fraction of gas, liquid, and solid, [-]

# property betas\_volume

Method to calculate and return the volume fraction of all of the phases in the system.

#### Returns

**betas\_volume** [list[float]] Volume phase fractions of all the phases, ordered vapor, liquid, then solid, [-]

# property betas\_volume\_liquids

Method to calculate and return the fraction of the liquid phase that each liquid phase is, by volume phase fraction. If the system is VLLL with volume phase fractions of 0.125 vapor, and [.25, .125, .5] for the three liquids phases respectively, the return value would be [0.28571428, 0.142857142, 0.57142857].

### Returns

betas\_volume\_liquids [list[float]] Volume phase fractions of the overall liquid phase, [-]

## property betas\_volume\_states

Method to return the volume phase fractions of each of the three fundamental types of phases.

#### Returns

**betas\_volume\_states** [list[float, 3]] List containing the volume phase fraction of gas, liquid, and solid, [-]

#### property charges

Charge number (valence) for each component, [-].

# Returns

charges [list[float]] Charge number (valence) for each component, [-].

# property conductivities

Electrical conductivities for each component, [S/m].

#### Returns

conductivities [list[float]] Electrical conductivities for each component, [S/m].

## property conductivity\_Ts

Temperatures at which the electrical conductivities for each component were measured, [K].

**conductivity\_Ts** [list[float]] Temperatures at which the electrical conductivities for each component were measured, [K].

#### d2P\_dT2()

Method to calculate and return the second temperature derivative of pressure of the bulk according to the selected calculation methodology.

Returns

d2P\_dT2 [float] Second temperature derivative of pressure, [Pa/K^2]

# d2P\_dT2\_frozen()

Method to calculate and return the second constant-volume derivative of pressure with respect to temperature of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial^2 P}{\partial T^2}\right)_{V,\beta,zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial^2 P}{\partial T^2}\right)_{i,V_i,\beta_i,zs_i}$$

#### Returns

**d2P\_dT2\_frozen** [float] Frozen constant-volume second derivative of pressure with respect to temperature of the bulk phase, [Pa/K^2]

# $d2P_dTdV()$

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the bulk according to the selected calculation methodology.

#### Returns

d2P\_dTdV [float] Second volume derivative of pressure, [mol\*Pa^2/(J\*K)]

# d2P\_dTdV\_frozen()

Method to calculate and return the second derivative of pressure with respect to volume and temperature of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial^2 P}{\partial V \partial T}\right)_{\beta, zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial^2 P}{\partial V \partial T}\right)_{i, \beta_i, zs_i}$$

Returns

**d2P\_dTdV\_frozen** [float] Frozen second derivative of pressure with respect to volume and temperature of the bulk phase, [Pa\*mol^2/m^6]

# d2P\_dV2()

Method to calculate and return the second volume derivative of pressure of the bulk according to the selected calculation methodology.

#### Returns

d2P\_dV2 [float] Second volume derivative of pressure, [Pa\*mol^2/m^6]

## d2P\_dV2\_frozen()

Method to calculate and return the constant-temperature second derivative of pressure with respect to volume of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial^2 P}{\partial V^2}\right)_{T,\beta,zs} = \sum_i^{\text{phases}} \beta_i \left(\frac{\partial^2 P}{\partial V^2}\right)_{i,T,\beta_i,zs_i}$$

**d2P\_dV2\_frozen** [float] Frozen constant-temperature second derivative of pressure with respect to volume of the bulk phase, [Pa\*mol^2/m^6]

 $dA_dP()$ 

Method to calculate and return the constant-temperature pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial U}{\partial P}\right)_T$$

Returns

dA\_dP [float] Constant-temperature pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

 $dA_dP_T()$ 

Method to calculate and return the constant-temperature pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial U}{\partial P}\right)_T$$

Returns

dA\_dP [float] Constant-temperature pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

## $dA_dP_V()$

Method to calculate and return the constant-volume pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_{V} = \left(\frac{\partial H}{\partial P}\right)_{V} - V - S\left(\frac{\partial T}{\partial P}\right)_{V} - T\left(\frac{\partial S}{\partial P}\right)_{V}$$

Returns

dA\_dP\_V [float] Constant-volume pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

 $dA_dT()$ 

Method to calculate and return the constant-pressure temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial U}{\partial T}\right)_P$$

Returns

dA\_dT [float] Constant-pressure temperature derivative of Helmholtz energy, [J/(mol\*K)]

 $dA_dT_P()$ 

Method to calculate and return the constant-pressure temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial U}{\partial T}\right)_P$$

Returns

dA\_dT [float] Constant-pressure temperature derivative of Helmholtz energy, [J/(mol\*K)]

 $dA_dT_V()$ 

Method to calculate and return the constant-volume temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_{V} = \left(\frac{\partial H}{\partial T}\right)_{V} - V\left(\frac{\partial P}{\partial T}\right)_{V} - T\left(\frac{\partial S}{\partial T}\right)_{V} - S$$

dA\_dT\_V [float] Constant-volume temperature derivative of Helmholtz energy, [J/(mol\*K)]

# $dA_dV_P()$

Method to calculate and return the constant-pressure volume derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial V}\right)_P = \left(\frac{\partial A}{\partial T}\right)_P \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

dA\_dV\_P [float] Constant-pressure volume derivative of Helmholtz energy, [J/(m^3)]

 $dA_dV_T()$ 

Method to calculate and return the constant-temperature volume derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial V}\right)_T = \left(\frac{\partial A}{\partial P}\right)_T \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

 $dA_dV_T$  [float] Constant-temperature volume derivative of Helmholtz energy,  $[J/(m^3)]$ 

### dA\_mass\_dP()

Method to calculate and return the pressure derivative of mass Helmholtz energy of the phase at constant temperature.

$$\left(\frac{\partial A_{\text{mass}}}{\partial P}\right)_T$$

Returns

**dA\_mass\_dP** [float] The pressure derivative of mass Helmholtz energy of the phase at constant temperature, [J/mol/Pa]

#### dA\_mass\_dP\_T()

Method to calculate and return the pressure derivative of mass Helmholtz energy of the phase at constant temperature.

$$\left(\frac{\partial A_{\text{mass}}}{\partial P}\right)_{T}$$

Returns

**dA\_mass\_dP\_T** [float] The pressure derivative of mass Helmholtz energy of the phase at constant temperature, [J/mol/Pa]

# dA\_mass\_dP\_V()

Method to calculate and return the pressure derivative of mass Helmholtz energy of the phase at constant volume.

$$\left(\frac{\partial A_{\text{mass}}}{\partial P}\right)_V$$

**dA\_mass\_dP\_V** [float] The pressure derivative of mass Helmholtz energy of the phase at constant volume, [J/mol/Pa]

## dA\_mass\_dT()

Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at constant pressure.

$$\left(\frac{\partial A_{\text{mass}}}{\partial T}\right)_P$$

## Returns

**dA\_mass\_dT** [float] The temperature derivative of mass Helmholtz energy of the phase at constant pressure, [J/mol/K]

# dA\_mass\_dT\_P()

Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at constant pressure.

$$\left(\frac{\partial A_{\text{mass}}}{\partial T}\right)_P$$

# Returns

**dA\_mass\_dT\_P** [float] The temperature derivative of mass Helmholtz energy of the phase at constant pressure, [J/mol/K]

## dA\_mass\_dT\_V()

Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at constant volume.

$$\left(\frac{\partial A_{\text{mass}}}{\partial T}\right)_V$$

# Returns

**dA\_mass\_dT\_V** [float] The temperature derivative of mass Helmholtz energy of the phase at constant volume, [J/mol/K]

# dA\_mass\_dV\_P()

Method to calculate and return the volume derivative of mass Helmholtz energy of the phase at constant pressure.

$$\left(\frac{\partial A_{\text{mass}}}{\partial V}\right)_P$$

# Returns

**dA\_mass\_dV\_P** [float] The volume derivative of mass Helmholtz energy of the phase at constant pressure, [J/mol/m^3/mol]

# dA\_mass\_dV\_T()

Method to calculate and return the volume derivative of mass Helmholtz energy of the phase at constant temperature.

$$\left(\frac{\partial A_{\text{mass}}}{\partial V}\right)_T$$

# Returns

**dA\_mass\_dV\_T** [float] The volume derivative of mass Helmholtz energy of the phase at constant temperature, [J/mol/m^3/mol]

# $dCv_dP_T()$

Method to calculate the pressure derivative of Cv, constant volume heat capacity, at constant temperature.

$$\left(\frac{\partial C_v}{\partial P}\right)_T = -T \,\mathrm{dPdT_V}\left(P\right) \frac{d}{dP} \,\mathrm{dVdT_P}\left(P\right) - T \,\mathrm{dVdT_P}\left(P\right) \frac{d}{dP} \,\mathrm{dPdT_V}\left(P\right) + \frac{d}{dP} \,\mathrm{Cp}\left(P\right)$$

Returns

dCv\_dP\_T [float] Pressure derivative of constant volume heat capacity at constant temperature, [J/mol/K/Pa]

### Notes

Requires d2V\_dTdP, d2P\_dTdP, and d2H\_dTdP.

# dCv\_dT\_P()

Method to calculate the temperature derivative of Cv, constant volume heat capacity, at constant pressure.

$$\left(\frac{\partial C_{v}}{\partial T}\right)_{P} = -\frac{T \operatorname{dPdT_{V}}^{2}(T) \frac{d}{dT} \operatorname{dPdV_{T}}(T)}{\operatorname{dPdV_{T}}^{2}(T)} + \frac{2T \operatorname{dPdT_{V}}(T) \frac{d}{dT} \operatorname{dPdT_{V}}(T)}{\operatorname{dPdV_{T}}(T)} + \frac{\operatorname{dPdT_{V}}^{2}(T)}{\operatorname{dPdV_{T}}(T)} + \frac{d}{dT} \operatorname{Cp}(T)$$

Returns

**dCv\_dT\_P** [float] Temperature derivative of constant volume heat capacity at constant pressure, [J/mol/K^2]

# **Notes**

Requires *d2P\_dT2\_PV*, *d2P\_dVdT\_TP*, and *d2H\_dT2*.

# dCv\_mass\_dP\_T()

Method to calculate and return the pressure derivative of mass Constant-volume heat capacity of the phase at constant temperature.

$$\left(\frac{\partial Cv_{\text{mass}}}{\partial P}\right)_T$$

# Returns

**dCv\_mass\_dP\_T** [float] The pressure derivative of mass Constant-volume heat capacity of the phase at constant temperature, [J/(mol\*K)/Pa]

## dCv\_mass\_dT\_P()

Method to calculate and return the temperature derivative of mass Constant-volume heat capacity of the phase at constant pressure.

$$\left(\frac{\partial C v_{\text{mass}}}{\partial T}\right)_P$$

# Returns

 $dCv_mass_dT_P$  [float] The temperature derivative of mass Constant-volume heat capacity of the phase at constant pressure,  $[J/(mol^*K)/K]$ 

### $dG_dP()$

Method to calculate and return the constant-temperature pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dG\_dP [float] Constant-temperature pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

## $dG_dP_T()$

Method to calculate and return the constant-temperature pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dG\_dP [float] Constant-temperature pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

 $dG_dP_V()$ 

Method to calculate and return the constant-volume pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_{V} = -T\left(\frac{\partial S}{\partial P}\right)_{V} - S\left(\frac{\partial T}{\partial P}\right)_{V} + \left(\frac{\partial H}{\partial P}\right)_{V}$$

Returns

dG\_dP\_V [float] Constant-volume pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

dG\_dT()

Method to calculate and return the constant-pressure temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

**dG\_dT** [float] Constant-pressure temperature derivative of Gibbs free energy, [J/(mol\*K)]

 $dG_dT_P()$ 

Method to calculate and return the constant-pressure temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial H}{\partial T}\right)_P$$

**dG\_dT** [float] Constant-pressure temperature derivative of Gibbs free energy, [J/(mol\*K)]

# $dG_dT_V()$

Method to calculate and return the constant-volume temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_V = -T\left(\frac{\partial S}{\partial T}\right)_V - S + \left(\frac{\partial H}{\partial T}\right)_V$$

Returns

 $dG_dT_V$  [float] Constant-volume temperature derivative of Gibbs free energy, [J/(mol\*K)]

 $dG_dV_P()$ 

Method to calculate and return the constant-pressure volume derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial V}\right)_P = \left(\frac{\partial G}{\partial T}\right)_P \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

**dG\_dV\_P** [float] Constant-pressure volume derivative of Gibbs free energy, [J/(m^3)]

 $dG_dV_T()$ 

Method to calculate and return the constant-temperature volume derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial V}\right)_T = \left(\frac{\partial G}{\partial P}\right)_T \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

 $dG_dV_T$  [float] Constant-temperature volume derivative of Gibbs free energy,  $[J/(m^3)]$ 

dG\_mass\_dP()

Method to calculate and return the pressure derivative of mass Gibbs free energy of the phase at constant temperature.

$$\left(\frac{\partial G_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dG\_mass\_dP** [float] The pressure derivative of mass Gibbs free energy of the phase at constant temperature, [J/mol/Pa]

## dG\_mass\_dP\_T()

Method to calculate and return the pressure derivative of mass Gibbs free energy of the phase at constant temperature.

$$\left(\frac{\partial G_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dG\_mass\_dP\_T** [float] The pressure derivative of mass Gibbs free energy of the phase at constant temperature, [J/mol/Pa]

## dG\_mass\_dP\_V()

Method to calculate and return the pressure derivative of mass Gibbs free energy of the phase at constant volume.

$$\left(\frac{\partial G_{\text{mass}}}{\partial P}\right)_V$$

**dG\_mass\_dP\_V** [float] The pressure derivative of mass Gibbs free energy of the phase at constant volume, [J/mol/Pa]

## dG\_mass\_dT()

Method to calculate and return the temperature derivative of mass Gibbs free energy of the phase at constant pressure.

$$\left(\frac{\partial G_{\text{mass}}}{\partial T}\right)_P$$

#### Returns

**dG\_mass\_dT** [float] The temperature derivative of mass Gibbs free energy of the phase at constant pressure, [J/mol/K]

# dG\_mass\_dT\_P()

Method to calculate and return the temperature derivative of mass Gibbs free energy of the phase at constant pressure.

$$\left(\frac{\partial G_{\text{mass}}}{\partial T}\right)_P$$

#### Returns

**dG\_mass\_dT\_P** [float] The temperature derivative of mass Gibbs free energy of the phase at constant pressure, [J/mol/K]

# $dG_mass_dT_V()$

Method to calculate and return the temperature derivative of mass Gibbs free energy of the phase at constant volume.

$$\left(\frac{\partial G_{\text{mass}}}{\partial T}\right)_V$$

#### Returns

**dG\_mass\_dT\_V** [float] The temperature derivative of mass Gibbs free energy of the phase at constant volume, [J/mol/K]

# dG\_mass\_dV\_P()

Method to calculate and return the volume derivative of mass Gibbs free energy of the phase at constant pressure.

$$\left(\frac{\partial G_{\text{mass}}}{\partial V}\right)_P$$

**dG\_mass\_dV\_P** [float] The volume derivative of mass Gibbs free energy of the phase at constant pressure, [J/mol/m^3/mol]

# dG\_mass\_dV\_T()

Method to calculate and return the volume derivative of mass Gibbs free energy of the phase at constant temperature.

$$\left(\frac{\partial G_{\text{mass}}}{\partial V}\right)_T$$

#### Returns

**dG\_mass\_dV\_T** [float] The volume derivative of mass Gibbs free energy of the phase at constant temperature, [J/mol/m^3/mol]

# dH\_dP()

Method to calculate and return the pressure derivative of enthalpy of the phase at constant pressure.

### Returns

**dH\_dP\_T** [float] Pressure derivative of enthalpy, [J/(mol\*Pa)]

# $dH_dP_T()$

Method to calculate and return the pressure derivative of enthalpy of the phase at constant pressure.

#### Returns

**dH\_dP\_T** [float] Pressure derivative of enthalpy, [J/(mol\*Pa)]

### $dH_dT()$

Method to calculate and return the constant-temperature and constant phase-fraction heat capacity of the bulk phase. This is a phase-fraction weighted calculation.

$$C_p = \sum_{i}^{p} C_{p,i} \beta_i$$

#### Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

# dH\_dT\_P()

Method to calculate and return the temperature derivative of enthalpy of the phase at constant pressure.

#### Returns

**dH\_dT\_P** [float] Temperature derivative of enthalpy, [J/(mol\*K)]

#### dH\_mass\_dP()

Method to calculate and return the pressure derivative of mass enthalpy of the phase at constant temperature.

$$\left(\frac{\partial H_{\text{mass}}}{\partial P}\right)_{T}$$

#### Returns

**dH\_mass\_dP** [float] The pressure derivative of mass enthalpy of the phase at constant temperature, [J/mol/Pa]

### dH\_mass\_dP\_T()

Method to calculate and return the pressure derivative of mass enthalpy of the phase at constant temperature.

$$\left(\frac{\partial H_{\text{mass}}}{\partial P}\right)_T$$

Returns

**dH\_mass\_dP\_T** [float] The pressure derivative of mass enthalpy of the phase at constant temperature, [J/mol/Pa]

## dH\_mass\_dP\_V()

Method to calculate and return the pressure derivative of mass enthalpy of the phase at constant volume.

$$\left(\frac{\partial H_{\rm mass}}{\partial P}\right)_V$$

#### Returns

**dH\_mass\_dP\_V** [float] The pressure derivative of mass enthalpy of the phase at constant volume, [J/mol/Pa]

#### dH\_mass\_dT()

Method to calculate and return the temperature derivative of mass enthalpy of the phase at constant pressure.

$$\left(\frac{\partial H_{\text{mass}}}{\partial T}\right)_P$$

# Returns

**dH\_mass\_dT** [float] The temperature derivative of mass enthalpy of the phase at constant pressure, [J/mol/K]

## dH\_mass\_dT\_P()

Method to calculate and return the temperature derivative of mass enthalpy of the phase at constant pressure.

$$\left(\frac{\partial H_{\text{mass}}}{\partial T}\right)_P$$

## Returns

**dH\_mass\_dT\_P** [float] The temperature derivative of mass enthalpy of the phase at constant pressure, [J/mol/K]

# dH\_mass\_dT\_V()

Method to calculate and return the temperature derivative of mass enthalpy of the phase at constant volume.

$$\left(\frac{\partial H_{\text{mass}}}{\partial T}\right)_V$$

**dH\_mass\_dT\_V** [float] The temperature derivative of mass enthalpy of the phase at constant volume, [J/mol/K]

## dH\_mass\_dV\_P()

Method to calculate and return the volume derivative of mass enthalpy of the phase at constant pressure.

$$\left(\frac{\partial H_{\text{mass}}}{\partial V}\right)_P$$

# Returns

**dH\_mass\_dV\_P** [float] The volume derivative of mass enthalpy of the phase at constant pressure, [J/mol/m^3/mol]

#### dH\_mass\_dV\_T()

Method to calculate and return the volume derivative of mass enthalpy of the phase at constant temperature.

$$\left(\frac{\partial H_{\text{mass}}}{\partial V}\right)_T$$

### Returns

**dH\_mass\_dV\_T** [float] The volume derivative of mass enthalpy of the phase at constant temperature, [J/mol/m^3/mol]

# $dP_dP_A()$

Method to calculate and return the pressure derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial P}\right)_A$$

### Returns

**dP\_dP\_A** [float] The pressure derivative of pressure of the phase at constant Helmholtz energy, [Pa/Pa]

# $dP_dP_G()$

Method to calculate and return the pressure derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial P}\right)_G$$

## Returns

**dP\_dP\_G** [float] The pressure derivative of pressure of the phase at constant Gibbs energy, [Pa/Pa]

# dP\_dP\_H()

Method to calculate and return the pressure derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial P}\right)_H$$

**dP\_dP\_H** [float] The pressure derivative of pressure of the phase at constant enthalpy, [Pa/Pa]

# $dP_dP_S()$

Method to calculate and return the pressure derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial P}\right)_S$$

#### Returns

dP\_dP\_S [float] The pressure derivative of pressure of the phase at constant entropy, [Pa/Pa]

# $dP_dP_U()$

Method to calculate and return the pressure derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial P}\right)_U$$

### Returns

**dP\_dP\_U** [float] The pressure derivative of pressure of the phase at constant internal energy, [Pa/Pa]

# $dP_dT()$

Method to calculate and return the first temperature derivative of pressure of the bulk according to the selected calculation methodology.

#### Returns

**dP\_dT** [float] First temperature derivative of pressure, [Pa/K]

#### $dP_dT_A()$

Method to calculate and return the temperature derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial T}\right)_A$$

#### Returns

**dP\_dT\_A** [float] The temperature derivative of pressure of the phase at constant Helmholtz energy, [Pa/K]

# $dP_dT_G()$

Method to calculate and return the temperature derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial T}\right)_G$$

**dP\_dT\_G** [float] The temperature derivative of pressure of the phase at constant Gibbs energy, [Pa/K]

# $dP_dT_H()$

Method to calculate and return the temperature derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial T}\right)_H$$

# Returns

**dP\_dT\_H** [float] The temperature derivative of pressure of the phase at constant enthalpy, [Pa/K]

# $dP_dT_S()$

Method to calculate and return the temperature derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial T}\right)_S$$

### Returns

**dP\_dT\_S** [float] The temperature derivative of pressure of the phase at constant entropy, [Pa/K]

# dP\_dT\_U()

Method to calculate and return the temperature derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial T}\right)_U$$

### Returns

**dP\_dT\_U** [float] The temperature derivative of pressure of the phase at constant internal energy, [Pa/K]

# dP\_dT\_frozen()

Method to calculate and return the constant-volume derivative of pressure with respect to temperature of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial P}{\partial T}\right)_{V,\beta,zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial P}{\partial T}\right)_{i,V_i,\beta_i,zs_i}$$

Returns

**dP\_dT\_frozen** [float] Frozen constant-volume derivative of pressure with respect to temperature of the bulk phase, [Pa/K]

 $dP_dV()$ 

Method to calculate and return the first volume derivative of pressure of the bulk according to the selected calculation methodology.

**dP\_dV** [float] First volume derivative of pressure, [Pa\*mol/m^3]

# $dP_dV_A()$

Method to calculate and return the volume derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial V}\right)_A$$

## Returns

**dP\_dV\_A** [float] The volume derivative of pressure of the phase at constant Helmholtz energy, [Pa/m^3/mol]

# $dP_dV_G()$

Method to calculate and return the volume derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial V}\right)_G$$

## Returns

**dP\_dV\_G** [float] The volume derivative of pressure of the phase at constant Gibbs energy, [Pa/m^3/mol]

# dP\_dV\_H()

Method to calculate and return the volume derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial V}\right)_{H}$$

### Returns

**dP\_dV\_H** [float] The volume derivative of pressure of the phase at constant enthalpy, [Pa/m^3/mol]

# $dP_dV_S()$

Method to calculate and return the volume derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial V}\right)_S$$

### Returns

**dP\_dV\_S** [float] The volume derivative of pressure of the phase at constant entropy, [Pa/m^3/mol]

# $dP_dV_U()$

Method to calculate and return the volume derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial V}\right)_U$$

**dP\_dV\_U** [float] The volume derivative of pressure of the phase at constant internal energy, [Pa/m^3/mol]

# dP\_dV\_frozen()

Method to calculate and return the constant-temperature derivative of pressure with respect to volume of the bulk phase, at constant phase fractions and phase compositions. This is a molar phase-fraction weighted calculation.

$$\left(\frac{\partial P}{\partial V}\right)_{T,\beta,zs} = \sum_{i}^{\text{phases}} \beta_i \left(\frac{\partial P}{\partial V}\right)_{i,T,\beta_i,zs_i}$$

#### Returns

**dP\_dV\_frozen** [float] Frozen constant-temperature derivative of pressure with respect to volume of the bulk phase, [Pa\*mol/m^3]

# dP\_drho\_A()

Method to calculate and return the density derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial \rho}\right)_A$$

#### Returns

**dP\_drho\_A** [float] The density derivative of pressure of the phase at constant Helmholtz energy, [Pa/mol/m^3]

# dP\_drho\_G()

Method to calculate and return the density derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial \rho}\right)_G$$

### Returns

**dP\_drho\_G** [float] The density derivative of pressure of the phase at constant Gibbs energy, [Pa/mol/m^3]

## dP\_drho\_H()

Method to calculate and return the density derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial\rho}\right)_{H}$$

## Returns

**dP\_drho\_H** [float] The density derivative of pressure of the phase at constant enthalpy, [Pa/mol/m^3]

## dP\_drho\_S()

Method to calculate and return the density derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial \rho}\right)_S$$

**dP\_drho\_S** [float] The density derivative of pressure of the phase at constant entropy, [Pa/mol/m^3]

## dP\_drho\_U()

Method to calculate and return the density derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial \rho}\right)_U$$

#### Returns

**dP\_drho\_U** [float] The density derivative of pressure of the phase at constant internal energy, [Pa/mol/m^3]

# dS\_dP()

Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.

### Returns

**dS\_dP\_T** [float] Pressure derivative of entropy, [J/(mol\*K\*Pa)]

# $dS_dP_T()$

Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.

### Returns

**dS\_dP\_T** [float] Pressure derivative of entropy, [J/(mol\*K\*Pa)]

### dS\_dV\_P()

Method to calculate and return the volume derivative of entropy of the phase at constant pressure.

#### Returns

**dS\_dV\_P** [float] Volume derivative of entropy, [J/(K\*m^3)]

### dS\_dV\_T()

Method to calculate and return the volume derivative of entropy of the phase at constant temperature.

#### Returns

 $dS_dV_T$  [float] Volume derivative of entropy, [J/(K\*m^3)]

## dS\_mass\_dP()

Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.

$$\left(\frac{\partial S_{\text{mass}}}{\partial P}\right)_T$$

# Returns

**dS\_mass\_dP** [float] The pressure derivative of mass entropy of the phase at constant temperature, [J/(mol\*K)/Pa]

# dS\_mass\_dP\_T()

Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.

$$\left(\frac{\partial S_{\text{mass}}}{\partial P}\right)_T$$

### Returns

**dS\_mass\_dP\_T** [float] The pressure derivative of mass entropy of the phase at constant temperature, [J/(mol\*K)/Pa]

## dS\_mass\_dP\_V()

Method to calculate and return the pressure derivative of mass entropy of the phase at constant volume.

$$\left(\frac{\partial S_{\rm mass}}{\partial P}\right)_V$$

#### Returns

dS\_mass\_dP\_V [float] The pressure derivative of mass entropy of the phase at constant volume, [J/(mol\*K)/Pa]

#### dS\_mass\_dT()

Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.

$$\left(\frac{\partial S_{\text{mass}}}{\partial T}\right)_P$$

# Returns

**dS\_mass\_dT** [float] The temperature derivative of mass entropy of the phase at constant pressure, [J/(mol\*K)/K]

## dS\_mass\_dT\_P()

Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.

$$\left(\frac{\partial S_{\text{mass}}}{\partial T}\right)_P$$

# Returns

dS\_mass\_dT\_P [float] The temperature derivative of mass entropy of the phase at constant pressure, [J/(mol\*K)/K]

# dS\_mass\_dT\_V()

Method to calculate and return the temperature derivative of mass entropy of the phase at constant volume.

$$\left(\frac{\partial S_{\text{mass}}}{\partial T}\right)_V$$

**dS\_mass\_dT\_V** [float] The temperature derivative of mass entropy of the phase at constant volume, [J/(mol\*K)/K]

## dS\_mass\_dV\_P()

Method to calculate and return the volume derivative of mass entropy of the phase at constant pressure.

$$\left(\frac{\partial S_{\text{mass}}}{\partial V}\right)_P$$

# Returns

dS\_mass\_dV\_P [float] The volume derivative of mass entropy of the phase at constant pressure, [J/(mol\*K)/m^3/mol]

# dS\_mass\_dV\_T()

Method to calculate and return the volume derivative of mass entropy of the phase at constant temperature.

$$\left(\frac{\partial S_{\text{mass}}}{\partial V}\right)_T$$

### Returns

dS\_mass\_dV\_T [float] The volume derivative of mass entropy of the phase at constant temperature, [J/(mol\*K)/m^3/mol]

# $dT_dP_A()$

Method to calculate and return the pressure derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial P}\right)_A$$

### Returns

**dT\_dP\_A** [float] The pressure derivative of temperature of the phase at constant Helmholtz energy, [K/Pa]

# $dT_dP_G()$

Method to calculate and return the pressure derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial P}\right)_G$$

# Returns

**dT\_dP\_G** [float] The pressure derivative of temperature of the phase at constant Gibbs energy, [K/Pa]

# dT\_dP\_H()

Method to calculate and return the pressure derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial P}\right)_{H}$$

**dT\_dP\_H** [float] The pressure derivative of temperature of the phase at constant enthalpy, [K/Pa]

# $dT_dP_S()$

Method to calculate and return the pressure derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial P}\right)_S$$

#### Returns

**dT\_dP\_S** [float] The pressure derivative of temperature of the phase at constant entropy, [K/Pa]

# dT\_dP\_U()

Method to calculate and return the pressure derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial P}\right)_U$$

# Returns

**dT\_dP\_U** [float] The pressure derivative of temperature of the phase at constant internal energy, [K/Pa]

# $dT_dT_A()$

Method to calculate and return the temperature derivative of temperature of the phase at constant Helmholtz energy.



### Returns

**dT\_dT\_A** [float] The temperature derivative of temperature of the phase at constant Helmholtz energy, [K/K]

# dT\_dT\_G()

Method to calculate and return the temperature derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial T}\right)_G$$

**dT\_dT\_G** [float] The temperature derivative of temperature of the phase at constant Gibbs energy, [K/K]

# $dT_dT_H()$

Method to calculate and return the temperature derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial T}\right)_H$$

#### Returns

**dT\_dT\_H** [float] The temperature derivative of temperature of the phase at constant enthalpy, [K/K]

# dT\_dT\_S()

Method to calculate and return the temperature derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial T}\right)_S$$

#### Returns

**dT\_dT\_S** [float] The temperature derivative of temperature of the phase at constant entropy, [K/K]

### dT\_dT\_U()

Method to calculate and return the temperature derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial T}\right)_U$$

#### Returns

**dT\_dT\_U** [float] The temperature derivative of temperature of the phase at constant internal energy, [K/K]

# $dT_dV_A()$

Method to calculate and return the volume derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial V}\right)_A$$

### Returns

**dT\_dV\_A** [float] The volume derivative of temperature of the phase at constant Helmholtz energy, [K/m^3/mol]

# $dT_dV_G()$

Method to calculate and return the volume derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial V}\right)_G$$

 $dT_dV_G$  [float] The volume derivative of temperature of the phase at constant Gibbs energy, [K/m^3/mol]

# $dT_dV_H()$

Method to calculate and return the volume derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial V}\right)_H$$

#### Returns

**dT\_dV\_H** [float] The volume derivative of temperature of the phase at constant enthalpy, [K/m^3/mol]

# $dT_dV_S()$

Method to calculate and return the volume derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial V}\right)_S$$

# Returns

**dT\_dV\_S** [float] The volume derivative of temperature of the phase at constant entropy, [K/m^3/mol]

# $dT_dV_U()$

Method to calculate and return the volume derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial V}\right)_U$$

#### Returns

**dT\_dV\_U** [float] The volume derivative of temperature of the phase at constant internal energy, [K/m^3/mol]

# dT\_drho\_A()

Method to calculate and return the density derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial \rho}\right)_A$$

Returns

**dT\_drho\_A** [float] The density derivative of temperature of the phase at constant Helmholtz energy, [K/mol/m^3]

# dT\_drho\_G()

Method to calculate and return the density derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial \rho}\right)_G$$

# Returns

**dT\_drho\_G** [float] The density derivative of temperature of the phase at constant Gibbs energy, [K/mol/m^3]

# dT\_drho\_H()

Method to calculate and return the density derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial \rho}\right)_{H}$$

### Returns

**dT\_drho\_H** [float] The density derivative of temperature of the phase at constant enthalpy, [K/mol/m^3]

# dT\_drho\_S()

Method to calculate and return the density derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial \rho}\right)_S$$

### Returns

**dT\_drho\_S** [float] The density derivative of temperature of the phase at constant entropy, [K/mol/m^3]

### dT\_drho\_U()

Method to calculate and return the density derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial \rho}\right)_U$$

# Returns

**dT\_drho\_U** [float] The density derivative of temperature of the phase at constant internal energy, [K/mol/m^3]

### dU\_dP()

Method to calculate and return the constant-temperature pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_T = -P\left(\frac{\partial V}{\partial P}\right)_T - V + \left(\frac{\partial H}{\partial P}\right)_T$$

dU\_dP [float] Constant-temperature pressure derivative of internal energy, [J/(mol\*Pa)]

dU\_dP\_T()

Method to calculate and return the constant-temperature pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_T = -P\left(\frac{\partial V}{\partial P}\right)_T - V + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dU\_dP [float] Constant-temperature pressure derivative of internal energy, [J/(mol\*Pa)]

 $dU_dP_V()$ 

Method to calculate and return the constant-volume pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_V = \left(\frac{\partial H}{\partial P}\right)_V - V$$

Returns

dU\_dP\_V [float] Constant-volume pressure derivative of internal energy, [J/(mol\*Pa)]

dU\_dT()

Method to calculate and return the constant-pressure temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_P = -P\left(\frac{\partial V}{\partial T}\right)_P + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

**dU\_dT** [float] Constant-pressure temperature derivative of internal energy, [J/(mol\*K)]

dU\_dT\_P()

Method to calculate and return the constant-pressure temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_P = -P\left(\frac{\partial V}{\partial T}\right)_P + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

 $dU_dT$  [float] Constant-pressure temperature derivative of internal energy, [J/(mol\*K)]

dU\_dT\_V()

Method to calculate and return the constant-volume temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_V = \left(\frac{\partial H}{\partial T}\right)_V - V\left(\frac{\partial P}{\partial T}\right)_V$$

Returns

dU\_dT\_V [float] Constant-volume temperature derivative of internal energy, [J/(mol\*K)]

 $dU_dV_P()$ 

Method to calculate and return the constant-pressure volume derivative of internal energy.

$$\left(\frac{\partial U}{\partial V}\right)_P = \left(\frac{\partial U}{\partial T}\right)_P \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

dU\_dV\_P [float] Constant-pressure volume derivative of internal energy, [J/(m^3)]

# $dU_dV_T()$

Method to calculate and return the constant-temperature volume derivative of internal energy.

$$\left(\frac{\partial U}{\partial V}\right)_T = \left(\frac{\partial U}{\partial P}\right)_T \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

dU\_dV\_T [float] Constant-temperature volume derivative of internal energy, [J/(m^3)]

#### dU\_mass\_dP()

Method to calculate and return the pressure derivative of mass internal energy of the phase at constant temperature.

$$\left(\frac{\partial U_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dU\_mass\_dP** [float] The pressure derivative of mass internal energy of the phase at constant temperature, [J/mol/Pa]

### dU\_mass\_dP\_T()

Method to calculate and return the pressure derivative of mass internal energy of the phase at constant temperature.

$$\left(\frac{\partial U_{\text{mass}}}{\partial P}\right)_{T}$$

# Returns

dU\_mass\_dP\_T [float] The pressure derivative of mass internal energy of the phase at constant temperature, [J/mol/Pa]

# dU\_mass\_dP\_V()

Method to calculate and return the pressure derivative of mass internal energy of the phase at constant volume.

$$\left(\frac{\partial U_{\text{mass}}}{\partial P}\right)_V$$

### Returns

**dU\_mass\_dP\_V** [float] The pressure derivative of mass internal energy of the phase at constant volume, [J/mol/Pa]

# dU\_mass\_dT()

Method to calculate and return the temperature derivative of mass internal energy of the phase at constant pressure.

$$\left(\frac{\partial U_{\text{mass}}}{\partial T}\right)_{H}$$

**dU\_mass\_dT** [float] The temperature derivative of mass internal energy of the phase at constant pressure, [J/mol/K]

# dU\_mass\_dT\_P()

Method to calculate and return the temperature derivative of mass internal energy of the phase at constant pressure.

$$\left(\frac{\partial U_{\text{mass}}}{\partial T}\right)_P$$

### Returns

**dU\_mass\_dT\_P** [float] The temperature derivative of mass internal energy of the phase at constant pressure, [J/mol/K]

#### dU\_mass\_dT\_V()

Method to calculate and return the temperature derivative of mass internal energy of the phase at constant volume.

$$\left(\frac{\partial U_{\text{mass}}}{\partial T}\right)_V$$

# Returns

**dU\_mass\_dT\_V** [float] The temperature derivative of mass internal energy of the phase at constant volume, [J/mol/K]

#### dU\_mass\_dV\_P()

Method to calculate and return the volume derivative of mass internal energy of the phase at constant pressure.

$$\left(\frac{\partial U_{\text{mass}}}{\partial V}\right)_P$$

# Returns

**dU\_mass\_dV\_P** [float] The volume derivative of mass internal energy of the phase at constant pressure, [J/mol/m^3/mol]

# dU\_mass\_dV\_T()

Method to calculate and return the volume derivative of mass internal energy of the phase at constant temperature.

$$\left(\frac{\partial U_{\text{mass}}}{\partial V}\right)_T$$

### Returns

**dU\_mass\_dV\_T** [float] The volume derivative of mass internal energy of the phase at constant temperature, [J/mol/m^3/mol]

# $dV_dP_A()$

Method to calculate and return the pressure derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial P}\right)_A$$

### Returns

**dV\_dP\_A** [float] The pressure derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/Pa]

# $dV_dP_G()$

Method to calculate and return the pressure derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial P}\right)_G$$

### Returns

**dV\_dP\_G** [float] The pressure derivative of volume of the phase at constant Gibbs energy, [m^3/mol/Pa]

#### $dV_dP_H()$

Method to calculate and return the pressure derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial P}\right)_H$$

# Returns

**dV\_dP\_H** [float] The pressure derivative of volume of the phase at constant enthalpy, [m^3/mol/Pa]

# $dV_dP_S()$

Method to calculate and return the pressure derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial P}\right)_S$$

# Returns

**dV\_dP\_S** [float] The pressure derivative of volume of the phase at constant entropy, [m^3/mol/Pa]

# dV\_dP\_U()

Method to calculate and return the pressure derivative of volume of the phase at constant internal energy.

 $\left(\frac{\partial V}{\partial P}\right)_U$ 

Returns

**dV\_dP\_U** [float] The pressure derivative of volume of the phase at constant internal energy, [m^3/mol/Pa]

# $dV_dT_A()$

Method to calculate and return the temperature derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial T}\right)_A$$

### Returns

**dV\_dT\_A** [float] The temperature derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/K]

# dV\_dT\_G()

Method to calculate and return the temperature derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial T}\right)_G$$

#### Returns

**dV\_dT\_G** [float] The temperature derivative of volume of the phase at constant Gibbs energy, [m^3/mol/K]

# dV\_dT\_H()

Method to calculate and return the temperature derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial T}\right)_{H}$$

### Returns

**dV\_dT\_H** [float] The temperature derivative of volume of the phase at constant enthalpy, [m^3/mol/K]

# $dV_dT_S()$

Method to calculate and return the temperature derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial T}\right)_S$$

# Returns

**dV\_dT\_S** [float] The temperature derivative of volume of the phase at constant entropy, [m^3/mol/K]

# dV\_dT\_U()

Method to calculate and return the temperature derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial T}\right)_U$$

 $dV_dT_U$  [float] The temperature derivative of volume of the phase at constant internal energy,  $[m^3/mol/K]$ 

# $dV_dV_A()$

Method to calculate and return the volume derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial V}\right)_A$$

### Returns

**dV\_dV\_A** [float] The volume derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/m^3/mol]

# $dV_dV_G()$

Method to calculate and return the volume derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial V}\right)_G$$

# Returns

**dV\_dV\_G** [float] The volume derivative of volume of the phase at constant Gibbs energy, [m^3/mol/m^3/mol]

# $dV_dV_H()$

Method to calculate and return the volume derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial V}\right)_H$$

#### Returns

**dV\_dV\_H** [float] The volume derivative of volume of the phase at constant enthalpy, [m^3/mol/m^3/mol]

# $dV_dV_S()$

Method to calculate and return the volume derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial V}\right)_S$$

#### Returns

**dV\_dV\_S** [float] The volume derivative of volume of the phase at constant entropy, [m^3/mol/m^3/mol]

### $dV_dV_U()$

Method to calculate and return the volume derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial V}\right)_U$$

### Returns

**dV\_dV\_U** [float] The volume derivative of volume of the phase at constant internal energy, [m^3/mol/m^3/mol]

### dV\_drho\_A()

Method to calculate and return the density derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial\rho}\right)_A$$

#### Returns

**dV\_drho\_A** [float] The density derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/mol/m^3]

### dV\_drho\_G()

Method to calculate and return the density derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial \rho}\right)_G$$

# Returns

**dV\_drho\_G** [float] The density derivative of volume of the phase at constant Gibbs energy, [m^3/mol/mol/m^3]

# dV\_drho\_H()

Method to calculate and return the density derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial \rho}\right)_H$$

# Returns

**dV\_drho\_H** [float] The density derivative of volume of the phase at constant enthalpy, [m^3/mol/mol/m^3]

# dV\_drho\_S()

Method to calculate and return the density derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial \rho}\right)_S$$

Returns

**dV\_drho\_S** [float] The density derivative of volume of the phase at constant entropy, [m^3/mol/mol/m^3]

# dV\_drho\_U()

Method to calculate and return the density derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial \rho}\right)_{U}$$

# Returns

**dV\_drho\_U** [float] The density derivative of volume of the phase at constant internal energy, [m^3/mol/mol/m^3]

# property dipoles

Dipole moments for each component, [debye].

#### Returns

dipoles [list[float]] Dipole moments for each component, [debye].

# drho\_dP\_A()

Method to calculate and return the pressure derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial P}\right)_A$$

#### Returns

**drho\_dP\_A** [float] The pressure derivative of density of the phase at constant Helmholtz energy, [mol/m^3/Pa]

#### drho\_dP\_G()

Method to calculate and return the pressure derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial P}\right)_G$$

#### Returns

**drho\_dP\_G** [float] The pressure derivative of density of the phase at constant Gibbs energy, [mol/m^3/Pa]

# drho\_dP\_H()

Method to calculate and return the pressure derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial\rho}{\partial P}\right)_{H}$$

### Returns

**drho\_dP\_H** [float] The pressure derivative of density of the phase at constant enthalpy, [mol/m^3/Pa]

# drho\_dP\_S()

Method to calculate and return the pressure derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial P}\right)_S$$

### Returns

**drho\_dP\_S** [float] The pressure derivative of density of the phase at constant entropy, [mol/m^3/Pa]

# drho\_dP\_U()

Method to calculate and return the pressure derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial P}\right)_U$$

# Returns

**drho\_dP\_U** [float] The pressure derivative of density of the phase at constant internal energy, [mol/m^3/Pa]

# $drho_dT_A()$

Method to calculate and return the temperature derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial T}\right)_A$$

#### Returns

**drho\_dT\_A** [float] The temperature derivative of density of the phase at constant Helmholtz energy, [mol/m^3/K]

# drho\_dT\_G()

Method to calculate and return the temperature derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial T}\right)_G$$

### Returns

**drho\_dT\_G** [float] The temperature derivative of density of the phase at constant Gibbs energy, [mol/m^3/K]

# drho\_dT\_H()

Method to calculate and return the temperature derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial \rho}{\partial T}\right)_{H}$$

**drho\_dT\_H** [float] The temperature derivative of density of the phase at constant enthalpy, [mol/m^3/K]

# drho\_dT\_S()

Method to calculate and return the temperature derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial T}\right)_S$$

#### Returns

**drho\_dT\_S** [float] The temperature derivative of density of the phase at constant entropy, [mol/m^3/K]

# drho\_dT\_U()

Method to calculate and return the temperature derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial T}\right)_U$$

#### Returns

**drho\_dT\_U** [float] The temperature derivative of density of the phase at constant internal energy, [mol/m^3/K]

# drho\_dV\_A()

Method to calculate and return the volume derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial V}\right)_A$$

# Returns

**drho\_dV\_A** [float] The volume derivative of density of the phase at constant Helmholtz energy, [mol/m^3/m^3/mol]

### drho\_dV\_G()

Method to calculate and return the volume derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial V}\right)_G$$

#### Returns

**drho\_dV\_G** [float] The volume derivative of density of the phase at constant Gibbs energy, [mol/m^3/m^3/mol]

#### drho\_dV\_H()

Method to calculate and return the volume derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial\rho}{\partial V}\right)_{H}$$

**drho\_dV\_H** [float] The volume derivative of density of the phase at constant enthalpy, [mol/m^3/m^3/mol]

# drho\_dV\_S()

Method to calculate and return the volume derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial V}\right)_S$$

### Returns

**drho\_dV\_S** [float] The volume derivative of density of the phase at constant entropy, [mol/m^3/m^3/mol]

# drho\_dV\_U()

Method to calculate and return the volume derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial V}\right)_U$$

# Returns

**drho\_dV\_U** [float] The volume derivative of density of the phase at constant internal energy, [mol/m^3/m^3/mol]

# drho\_drho\_A()

Method to calculate and return the density derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_A$$

Returns

**drho\_drho\_A** [float] The density derivative of density of the phase at constant Helmholtz energy, [mol/m^3/mol/m^3]

# drho\_drho\_G()

Method to calculate and return the density derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_{G}$$

#### Returns

**drho\_drho\_G** [float] The density derivative of density of the phase at constant Gibbs energy, [mol/m^3/mol/m^3]

### drho\_drho\_H()

Method to calculate and return the density derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_{H}$$

### Returns

**drho\_drho\_H** [float] The density derivative of density of the phase at constant enthalpy, [mol/m^3/mol/m^3]

### drho\_drho\_S()

Method to calculate and return the density derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_S$$

#### Returns

**drho\_drho\_S** [float] The density derivative of density of the phase at constant entropy, [mol/m^3/mol/m^3]

# drho\_drho\_U()

Method to calculate and return the density derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_U$$

# Returns

**drho\_drho\_U** [float] The density derivative of density of the phase at constant internal energy, [mol/m^3/mol/m^3]

### property economic\_statuses

Status of each component in in relation to import and export from various regions, [-].

#### Returns

**economic\_statuses** [list[dict]] Status of each component in in relation to import and export from various regions, [-].

# flashed = True

# property formulas

Formulas of each component, [-].

Returns

formulas [list[str]] Formulas of each component, [-].

### property heaviest\_liquid

The liquid-like phase with the highest mass density, [-]

#### Returns

**heaviest\_liquid** [Phase or None] Phase with the highest mass density or None if there are no liquid like phases, [-]

# isentropic\_exponent()

Method to calculate and return the real gas is entropic exponent of the phase, which satisfies the relationship  $PV^k = \text{const.}$ 

$$k = -\frac{V}{P} \frac{C_p}{C_v} \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

**k\_PV** [float] Isentropic exponent of a real fluid, [-]

### isentropic\_exponent\_PT()

Method to calculate and return the real gas isentropic exponent of the phase, which satisfies the relationship  $P^{(1-k)}T^k = \text{const.}$ 

$$k = \frac{1}{1 - \frac{P}{C_p} \left(\frac{\partial V}{\partial T}\right)_P}$$

### Returns

**k\_PT** [float] Isentropic exponent of a real fluid, [-]

### isentropic\_exponent\_PV()

Method to calculate and return the real gas isentropic exponent of the phase, which satisfies the relationship  $PV^k = \text{const.}$ 

$$k = -\frac{V}{P} \frac{C_p}{C_v} \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

k\_PV [float] Isentropic exponent of a real fluid, [-]

# isentropic\_exponent\_TV()

Method to calculate and return the real gas isentropic exponent of the phase, which satisfies the relationship  $TV^{k-1} = \text{const.}$ 

$$k = 1 + \frac{V}{C_v} \left(\frac{\partial P}{\partial T}\right)_V$$

Returns

**k\_TV** [float] Isentropic exponent of a real fluid, [-]

### isobaric\_expansion()

Method to calculate and return the isobatic expansion coefficient of the bulk according to the selected calculation methodology.

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

Returns

beta [float] Isobaric coefficient of a thermal expansion, [1/K]

# isothermal\_bulk\_modulus()

Method to calculate and return the isothermal bulk modulus of the phase.

$$K_T = -V \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

isothermal\_bulk\_modulus [float] Isothermal bulk modulus, [Pa]

# **k**()

Calculate and return the thermal conductivity of the bulk according to the selected thermal conductivity settings in BulkSettings, the settings in *ThermalConductivityGasMixture* and *ThermalConductivityLiquidMixture*, and the configured pure-component settings in *ThermalConductivityGas* and *ThermalConductivityLiquid*.

#### Returns

k [float] Thermal Conductivity of bulk phase calculated with mixing rules, [Pa\*s]

# kappa()

Method to calculate and return the isothermal compressibility of the bulk according to the selected calculation methodology.

$$\kappa = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

### Returns

kappa [float] Isothermal coefficient of compressibility, [1/Pa]

# property legal\_statuses

Status of each component in in relation to import and export rules from various regions, [-].

### Returns

**legal\_statuses** [list[dict]] Status of each component in in relation to import and export rules from various regions, [-].

# property lightest\_liquid

The liquid-like phase with the lowest mass density, [-]

### Returns

**lightest\_liquid** [Phase or None] Phase with the lowest mass density or None if there are no liquid like phases, [-]

# liquid\_bulk = None

# property logPs

Octanol-water partition coefficients for each component, [-].

# Returns

logPs [list[float]] Octanol-water partition coefficients for each component, [-].

# log\_zs()

Method to calculate and return the log of mole fractions specified. These are used in calculating entropy and in many other formulas.

 $\ln z_i$ 

### Returns

log\_zs [list[float]] Log of mole fractions, [-]

# max\_liquid\_phases = 1

# molar\_water\_content(phase=None)

Method to calculate and return the molar water content; this is the g/mol of the fluid which is coming from water, [g/mol].

water content =  $MW_{H2O}w_{H2O}$ 

molar\_water\_content [float] Molar water content, [g/mol]

# property molecular\_diameters

Lennard-Jones molecular diameters for each component, [angstrom].

# Returns

**molecular\_diameters** [list[float]] Lennard-Jones molecular diameters for each component, [angstrom].

### mu()

Calculate and return the viscosity of the bulk according to the selected viscosity settings in BulkSettings, the settings in *ViscosityGasMixture* and *ViscosityLiquidMixture*, and the configured pure-component settings in *ViscosityGas* and *ViscosityLiquid*.

# Returns

mu [float] Viscosity of bulk phase calculated with mixing rules, [Pa\*s]

### property names

Names for each component, [-].

# Returns

names [list[str]] Names for each component, [-].

### nu(phase=None)

Method to calculate and return the kinematic viscosity of the equilibrium state.

$$\nu = \frac{\mu}{\rho}$$

# Returns

nu [float] Kinematic viscosity, [m^2/s]

### property omegas

Acentric factors for each component, [-].

### Returns

omegas [list[float]] Acentric factors for each component, [-].

# property phase

Method to calculate and return a string representing the phase of the mixture. The return string uses 'V' to represent the gas phase, 'L' to represent a liquid phase, and 'S' to represent a solid phase (always in that order).

A state with three liquids, two solids, and a gas would return 'VLLLSS'.

Returns

phase [str] Phase string, [-]

### property phase\_STPs

Standard states ('g', 'l', or 's') for each component, [-].

# Returns

phase\_STPs [list[str]] Standard states ('g', 'l', or 's') for each component, [-].

#### pseudo\_Pc(phase=None)

Method to calculate and return the pseudocritical pressure calculated using Kay's rule (linear mole fractions):

$$P_{c,pseudo} = \sum_{i} z_i P_{c,i}$$

Returns

**pseudo\_Pc** [float] Pseudocritical pressure of the phase, [Pa]

### pseudo\_Tc(phase=None)

Method to calculate and return the pseudocritical temperature calculated using Kay's rule (linear mole fractions):

$$T_{c,pseudo} = \sum_{i} z_i T_{c,i}$$

### Returns

pseudo\_Tc [float] Pseudocritical temperature of the phase, [K]

### pseudo\_Vc(phase=None)

Method to calculate and return the pseudocritical volume calculated using Kay's rule (linear mole fractions):

$$V_{c,pseudo} = \sum_{i} z_i V_{c,i}$$

Returns

pseudo\_Vc [float] Pseudocritical volume of the phase, [m^3/mol]

### pseudo\_Zc(phase=None)

Method to calculate and return the pseudocritical compressibility calculated using Kay's rule (linear mole fractions):

$$Z_{c,pseudo} = \sum_{i} z_i Z_{c,i}$$

Returns

pseudo\_Zc [float] Pseudocritical compressibility of the phase, [-]

# property quality

Method to return the mass vapor fraction of the equilibrium state. If no vapor/gas is present, 0 is always returned. This is normally called the quality.

Returns

quality [float] Vapor mass fraction, [-]

# reacted = False

### rho()

Method to calculate and return the molar density of the phase.

 $\rho = frac1V$ 

Returns

rho [float] Molar density, [mol/m^3]

# rho\_mass(phase=None)

Method to calculate and return mass density of the phase.

$$\rho = \frac{MW}{1000 \cdot VM}$$

Returns

rho\_mass [float] Mass density, [kg/m^3]

### rho\_mass\_liquid\_ref(phase=None)

Method to calculate and return the liquid reference mass density according to the temperature variable *T\_liquid\_volume\_ref* of *thermo.bulk.BulkSettings* and the composition of the phase.

Returns

rho\_mass\_liquid\_ref [float] Liquid mass density at the reference condition, [kg/m^3]

#### property rhocs

Molar densities at the critical point for each component, [mol/m^3].

# Returns

rhocs [list[float]] Molar densities at the critical point for each component, [mol/m^3].

### property rhocs\_mass

Densities at the critical point for each component, [kg/m^3].

### Returns

rhocs\_mass [list[float]] Densities at the critical point for each component, [kg/m^3].

### property rhog\_STPs

Molar gas densities at STP for each component; metastable if normally another state, [mol/m^3].

### Returns

**rhog\_STPs** [list[float]] Molar gas densities at STP for each component; metastable if normally another state, [mol/m^3].

# property rhog\_STPs\_mass

Gas densities at STP for each component; metastable if normally another state, [kg/m^3].

# Returns

**rhog\_STPs\_mass** [list[float]] Gas densities at STP for each component; metastable if normally another state, [kg/m^3].

# property rhol\_60Fs

Liquid molar densities for each component at 60 °F, [mol/m^3].

# Returns

rhol\_60Fs [list[float]] Liquid molar densities for each component at 60 °F, [mol/m^3].

# property rhol\_60Fs\_mass

Liquid mass densities for each component at 60 °F, [kg/m^3].

### Returns

rhol\_60Fs\_mass [list[float]] Liquid mass densities for each component at 60 °F, [kg/m^3].

# property rhol\_STPs

Molar liquid densities at STP for each component, [mol/m^3].

Returns

rhol\_STPs [list[float]] Molar liquid densities at STP for each component, [mol/m^3].

#### property rhol\_STPs\_mass

Liquid densities at STP for each component, [kg/m^3].

#### Returns

**rhol\_STPs\_mass** [list[float]] Liquid densities at STP for each component, [kg/m<sup>3</sup>].

# property rhos\_Tms

Solid molar densities for each component at their respective melting points, [mol/m^3].

#### Returns

**rhos\_Tms** [list[float]] Solid molar densities for each component at their respective melting points, [mol/m^3].

#### property rhos\_Tms\_mass

Solid mass densities for each component at their melting point, [kg/m^3].

#### Returns

**rhos\_Tms\_mass** [list[float]] Solid mass densities for each component at their melting point, [kg/m^3].

# sigma()

Calculate and return the surface tension of the bulk according to the selected surface tension settings in BulkSettings, the settings in SurfaceTensionMixture and the configured pure-component settings in SurfaceTension.

#### Returns

sigma [float] Surface tension of bulk phase calculated with mixing rules, [N/m]

### Notes

A value is only returned if all phases in the bulk are liquids; this property is for a liquid-ideal gas calculation, not the interfacial tension between two liquid phases.

# property sigma\_STPs

Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].

#### Returns

**sigma\_STPs** [list[float]] Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].

### property sigma\_Tbs

Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].

# Returns

**sigma\_Tbs** [list[float]] Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].

# property sigma\_Tms

Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].

# Returns

**sigma\_Tms** [list[float]] Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].

#### property similarity\_variables

Similarity variables for each component, [mol/g].

Returns

similarity\_variables [list[float]] Similarity variables for each component, [mol/g].

# property smiless

SMILES identifiers for each component, [-].

Returns

smiless [list[str]] SMILES identifiers for each component, [-].

### solid\_bulk = None

# property solubility\_parameters

Solubility parameters for each component at 298.15 K, [Pa^0.5].

#### Returns

**solubility\_parameters** [list[float]] Solubility parameters for each component at 298.15 K, [Pa^0.5].

### speed\_of\_sound()

Method to calculate and return the molar speed of sound of the bulk according to the selected calculation methodology.

$$w = \left[-V^2 \left(\frac{\partial P}{\partial V}\right)_T \frac{C_p}{C_v}\right]^{1/2}$$

A similar expression based on molar density is:

$$w = \left[ \left( \frac{\partial P}{\partial \rho} \right)_T \frac{C_p}{C_v} \right]^{1/2}$$

Returns

w [float] Speed of sound for a real gas, [m\*kg^0.5/(s\*mol^0.5)]

# speed\_of\_sound\_mass()

Method to calculate and return the speed of sound of the phase.

$$w = \left[-V^2 \frac{1000}{MW} \left(\frac{\partial P}{\partial V}\right)_T \frac{C_p}{C_v}\right]^{1/2}$$

Returns

w [float] Speed of sound for a real gas, [m/s]

value(name, phase=None)

Method to retrieve a property from a string. This more or less wraps *getattr*, but also allows for the property to be returned for a specific phase if *phase* is provided.

*name* could be a python property like 'Tms' or a callable method like 'H'; and if the property is on a perphase basis like 'betas\_mass', a phase object can be provided as the second argument and only the value for that phase will be returned.

### **Parameters**

**name** [str] String representing the property, [-]

**phase** [thermo.phase.Phase, optional] Phase to retrieve the property for only (if specified), [-]

value [various] Value specified, [various]

# property water\_index

The index of the component water in the components. None if water is not present. Water is recognized by its CAS number.

Returns

water\_index [int] The index of the component water, [-]

# property water\_phase

The liquid-like phase with the highest water mole fraction, [-]

### Returns

**water\_phase** [Phase or None] Phase with the highest water mole fraction or None if there are no liquid like phases with water, [-]

# property water\_phase\_index

The liquid-like phase with the highest mole fraction of water, [-]

# Returns

water\_phase\_index [int] Index into the attribute EquilibriumState.liquids which refers to the liquid-like phase with the highest water mole fraction, [-]

### ws(phase=None)

Method to calculate and return the mass fractions of the phase, [-]

### Returns

ws [list[float]] Mass fractions, [-]

# ws\_no\_water(phase=None)

Method to calculate and return the mass fractions of all species in the phase, normalized to a water-free basis (the mass fraction of water returned is zero).

### Returns

ws\_no\_water [list[float]] Mass fractions on a water free basis, [-]

### zs\_no\_water(phase=None)

Method to calculate and return the mole fractions of all species in the phase, normalized to a water-free basis (the mole fraction of water returned is zero).

### Returns

zs\_no\_water [list[float]] Mole fractions on a water free basis, [-]

# 7.13 Flash Calculations (thermo.flash)

This module contains classes and functions for performing flash calculations.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Main Interfaces
  - Pure Components
  - Vapor-Liquid Systems

- Vapor and Multiple Liquid Systems
- Base Flash Class
- Specific Flash Algorithms

# 7.13.1 Main Interfaces

# **Pure Components**

Bases: thermo.flash.flash\_base.Flash

Class for performing flash calculations on pure-component systems. This class is subtantially more robust than using multicomponent algorithms on pure species. It is also faster. All parameters are also attributes.

The minimum information that is needed in addition to the Phase objects is:

- MW
- · Vapor pressure curve if including liquids
- Sublimation pressure curve if including solids
- · Functioning enthalpy models for each phase

# Parameters

- **constants** [*ChemicalConstantsPackage* object] Package of chemical constants; these are used as boundaries at times, initial guesses other times, and in all cases these properties are accessible as attributes of the resulting *EquilibriumState* object, [-]
- **correlations** [*PropertyCorrelationsPackage*] Package of chemical T-dependent properties; these are used as boundaries at times, for initial guesses other times, and in all cases these properties are accessible as attributes of the resulting *EquilibriumState* object, [-]
- gas [Phase object] A single phase which can represent the gas phase, [-]
- **liquids** [list[*Phase*]] A list of phases for representing the liquid phase; normally only one liquid phase is present for a pure-component system, but multiple liquids are allowed for the really weird cases like having both parahydrogen and orthohydrogen. The liquid phase which calculates a lower Gibbs free energy is always used. [-]
- **settings** [*BulkSettings* object] Object containing settings for calculating bulk and transport properties, [-]

# Notes

The algorithms in this object are mostly from [1] and [2]. They all boil down to newton methods with analytical derivatives. The phase with the lowest Gibbs energy is the most stable if there are multiple solutions.

Phase input combinations which have specific simplifying assumptions (and thus more speed) are:

- a *CEOSLiquid* and a *CEOSGas* with the same (consistent) parameters
- a CEOSGas with the IGMIX eos and a GibbsExcessLiquid
- a IAPWS95Liquid and a IAPWS95Gas
- a CoolPropLiquid and a CoolPropGas

Additional information that can be provided in the *ChemicalConstantsPackage* object and *PropertyCorrelationsPackage* object that may help convergence is:

- Tc, Pc, omega, Tb, and atoms
- Gas heat capacity correlations
- · Liquid molar volume correlations
- · Heat of vaporization correlations

### References

[1], [2]

# **Examples**

Create all the necessary objects using all of the default parameters for decane and do a flash at 300 K and 1 bar:

```
>>> from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CEOSGas,_

_FlashPureVLS
>>> constants, correlations = ChemicalConstantsPackage.from_IDs(['decane'])
>>> eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
>>> liquid = CEOSLiquid(PRMIX, HeatCapacityGases=correlations.HeatCapacityGases,_

___eos_kwargs=eos_kwargs)
>>> gas = CEOSGas(PRMIX, HeatCapacityGases=correlations.HeatCapacityGases, eos_

___kwargs=eos_kwargs)
>>> flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid],_

____solids=[])
>>> print(flasher.flash(T=300, P=1e5))
<EquilibriumState, T=300.0000, P=100000.0000, zs=[1.0], betas=[1.0], phases=[

___<CEOSLiquid, T=300 K, P=100000 Pa>]>
```

Working with steam:

```
>>> from thermo import FlashPureVLS, IAPWS95Liquid, IAPWS95Gas, iapws_constants,_
...iapws_correlations
>>> liquid = IAPWS95Liquid(T=300, P=1e5, zs=[1])
>>> gas = IAPWS95Gas(T=300, P=1e5, zs=[1])
>>> flasher = FlashPureVLS(iapws_constants, iapws_correlations, gas, [liquid], [])
>>> PT = flasher.flash(T=800.0, P=1e7)
>>> PT.rho_mass()
```

(continues on next page)

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```
29.1071839176
>>> print(flasher.flash(T=600, VF=.5))
<EquilibriumState, T=600.0000, P=12344824.3572, zs=[1.0], betas=[0.5, 0.5], phases=[
...<IAPWS95Gas, T=600 K, P=1.23448e+07 Pa>, <IAPWS95Liquid, T=600 K, P=1.23448e+07_
...Pa>]>
>>> print(flasher.flash(T=600.0, H=50802))
<EquilibriumState, T=600.0000, P=10000469.1288, zs=[1.0], betas=[1.0], phases=[
...<IAPWS95Gas, T=600 K, P=1.00005e+07 Pa>]>
>>> print(flasher.flash(P=1e7, S=104.))
<EquilibriumState, T=599.6790, P=1000000.0000, zs=[1.0], betas=[1.0], phases=[
...<IAPWS95Gas, T=599.679 K, P=1e+07 Pa>]>
>>> print(flasher.flash(V=.00061, U=55850))
<EquilibriumState, T=800.5922, P=10144789.0899, zs=[1.0], betas=[1.0], phases=[
...<IAPWS95Gas, T=800.592 K, P=1.01448e+07 Pa>]>
```

### Attributes

- VL\_IG\_hack [bool] Whether or not to trust the saturation curve of the liquid phase; applied automatically to the *GibbsExcessLiquid* phase if there is a single liquid only, [-]
- VL\_EOS\_hacks [bool] Whether or not to trust the saturation curve of the EOS liquid phase; applied automatically to the *CEOSLiquid* phase if there is a single liquid only, [-]
- **TPV\_HSGUA\_guess\_maxiter** [int] Maximum number of iterations to try when converging a shortcut model for flashes with one (T, P, V) spec and one (H, S, G, U, A) spec, [-]
- **TPV\_HSGUA\_guess\_xtol** [float] Convergence tolerance in the iteration variable when converging a shortcut model for flashes with one (T, P, V) spec and one (H, S, G, U, A) spec, [-]
- **TPV\_HSGUA\_maxiter** [int] Maximum number of iterations to try when converging a flashes with one (T, P, V) spec and one (H, S, G, U, A) spec; this is on a per-phase basis, so if there is a liquid and a gas phase, the maximum number of iterations that could end up being tried would be twice this, [-]
- **TPV\_HSGUA\_xtol** [float] Convergence tolerance in the iteration variable dimension when converging a flash with one (T, P, V) spec and one (H, S, G, U, A) spec, [-]
- **TVF\_maxiter** [int] Maximum number of iterations to try when converging a flashes with a temperature and vapor fraction specification, [-]
- **TVF\_xtol** [float] Convergence tolerance in the temperature dimension when converging a flashes with a temperature and vapor fraction specification, [-]
- **PVF\_maxiter** [int] Maximum number of iterations to try when converging a flashes with a pressure and vapor fraction specification, [-]
- **PVF\_xtol** [float] Convergence tolerance in the pressure dimension when converging a flashes with a pressure and vapor fraction specification, [-]
- **TSF\_maxiter** [int] Maximum number of iterations to try when converging a flashes with a temperature and solid fraction specification, [-]
- **TSF\_xtol** [float] Convergence tolerance in the temperature dimension when converging a flashes with a temperature and solid fraction specification, [-]
- **PSF\_maxiter** [int] Maximum number of iterations to try when converging a flashes with a pressure and solid fraction specification, [-]

**PSF\_xtol** [float] Convergence tolerance in the pressure dimension when converging a flashes with a pressure and solid fraction specification, [-]

# Vapor-Liquid Systems

class thermo.flash.FlashVL(constants, correlations, gas, liquid, settings=<thermo.bulk.BulkSettings object>)
Bases: thermo.flash.flash\_base.Flash

Class for performing flash calculations on one and two phase vapor and liquid multicomponent systems. Use *FlashVLN* for systems which can have multiple liquid phases.

The minimum information that is needed in addition to the Phase objects is:

- MWs
- Vapor pressure curve
- · Functioning enthalpy models for each phase

#### Parameters

- **constants** [*ChemicalConstantsPackage* object] Package of chemical constants; these are used as boundaries at times, initial guesses other times, and in all cases these properties are accessible as attributes of the resulting *EquilibriumState* object, [-]
- **correlations** [*PropertyCorrelationsPackage*] Package of chemical T-dependent properties; these are used as boundaries at times, for initial guesses other times, and in all cases these properties are accessible as attributes of the resulting *EquilibriumState* object, [-]
- gas [Phase object] A single phase which can represent the gas phase, [-]
- liquid [Phase] A single phase which can represent the liquid phase, [-]
- **settings** [*BulkSettings* object] Object containing settings for calculating bulk and transport properties, [-]

### Notes

The algorithms in this object are mostly from [1], [2] and [3]. Sequential substitution without acceleration is used by default to converge two-phase systems.

Quasi-newton methods are used by default to converge bubble and dew point calculations.

Flashes with one (T, P, V) spec and one (H, S, G, U, A) spec are solved by a 1D search over PT flashes.

Additional information that can be provided in the *ChemicalConstantsPackage* object and *PropertyCorrelationsPackage* object that may help convergence is:

- Tc, Pc, omega, Tb, and atoms
- · Gas heat capacity correlations
- · Liquid molar volume correlations
- Heat of vaporization correlations

**Warning:** If this flasher is used on systems that can form two or more liquid phases, and the flash specs are in that region, there is no guarantee which solution is returned. Sometimes it is almost random, jumping back and forth and providing nasty discontinuities.

### References

[1], [2], [3]

### **Examples**

For the system methane-ethane-nitrogen with a composition [0.965, 0.018, 0.017], calculate the vapor fraction of the system and equilibrium phase compositions at 110 K and 1 bar. Use the Peng-Robinson equation of state and the chemsep sample interaction parameter database.

```
>>> from thermo import ChemicalConstantsPackage, CEOSGas, CEOSLiquid, PRMIX, FlashVL
>>> from thermo.interaction_parameters import IPDB
>>> constants, properties = ChemicalConstantsPackage.from_IDs(['methane', 'ethane',
\rightarrow 'nitrogen'])
>>> kijs = IPDB.get_ip_asymmetric_matrix('ChemSep PR', constants.CASs, 'kij')
>>> kijs
[[0.0, -0.0059, 0.0289], [-0.0059, 0.0, 0.0533], [0.0289, 0.0533, 0.0]]
>>> eos kwargs = {'Pcs': constants.Pcs. 'Tcs': constants.Tcs. 'omegas': constants.
→omegas, 'kijs': kijs}
>>> gas = CEOSGas(PRMIX, eos_kwargs=eos_kwargs, HeatCapacityGases=properties.
→HeatCapacityGases)
>>> liquid = CEOSLiquid(PRMIX, eos_kwargs=eos_kwargs, HeatCapacityGases=properties.
→HeatCapacityGases)
>>> flasher = FlashVL(constants, properties, liquid=liquid, gas=gas)
>>> zs = [0.965, 0.018, 0.017]
>>> PT = flasher.flash(T=110.0, P=1e5, zs=zs)
>>> PT.VF, PT.gas.zs, PT.liquid0.zs
(0.10365, [0.881788, 2.6758e-05, 0.11818], [0.97462, 0.02007, 0.005298])
```

A few more flashes with the same system to showcase the functionality of the *flash* interface:

```
>>> flasher.flash(P=1e5, VF=1, zs=zs).T
133.6
>>> flasher.flash(T=133, VF=0, zs=zs).P
518367.4
>>> flasher.flash(P=PT.P, H=PT.H(), zs=zs).T
110.0
>>> flasher.flash(P=PT.P, S=PT.S(), zs=zs).T
110.0
>>> flasher.flash(T=PT.T, H=PT.H(), zs=zs).T
110.0
>>> flasher.flash(T=PT.T, S=PT.S(), zs=zs).T
110.0
```

### Attributes

- **PT\_SS\_MAXITER** [int] Maximum number of sequential substitution iterations to try when converging a two-phase solution, [-]
- PT\_SS\_TOL [float] Convergence tolerance in sequential substitution [-]
- **PT\_SS\_POLISH** [bool] When set to True, flashes which are very near a vapor fraction of 0 or 1 are converged to a higher tolerance to ensure the solution is correct; without this, a flash might converge to a vapor fraction of -1e-7 and be called single phase, but with this the correct solution may be found to be 1e-8 and will be correctly returned as two phase.[-]

- PT\_SS\_POLISH\_VF [float] What tolerance to a vapor fraction of 0 or 1; this is an absolute vapor fraction value, [-]
- **PT\_SS\_POLISH\_MAXITER** [int] Maximum number of sequential substitution iterations to try when converging a two-phase solution that has been detected to be very sensitive, with a vapor fraction near 0 or 1 [-]
- **PT\_SS\_POLISH\_TOL** [float] Convergence tolerance in sequential substitution when converging a two-phase solution that has been detected to be very sensitive, with a vapor fraction near 0 or 1 [-]
- **PT\_STABILITY\_MAXITER** [int] Maximum number of iterations to try when converging a stability test, [-]
- PT\_STABILITY\_XTOL [float] Convergence tolerance in the stability test [-]
- **DEW\_BUBBLE\_VF\_K\_COMPOSITION\_INDEPENDENT\_XTOL** [float] Convergence tolerance in Newton solver for bubble, dew, and vapor fraction spec flashes when both the liquid and gas model's K values do not dependent on composition, [-]
- **DEW\_BUBBLE\_QUASI\_NEWTON\_XTOL** [float] Convergence tolerance in quasi-Newton bubble and dew point flashes, [-]
- **DEW\_BUBBLE\_QUASI\_NEWTON\_MAXITER** [int] Maximum number of iterations to use in quasi-Newton bubble and dew point flashes, [-]
- **DEW\_BUBBLE\_NEWTON\_XTOL** [float] Convergence tolerance in Newton bubble and dew point flashes, [-]
- **DEW\_BUBBLE\_NEWTON\_MAXITER** [int] Maximum number of iterations to use in Newton bubble and dew point flashes, [-]
- **TPV\_HSGUA\_BISECT\_XTOL** [float] Tolerance in the iteration variable when converging a flash with one (T, P, V) spec and one (H, S, G, U, A) spec using a bisection-type solver, [-]
- **TPV\_HSGUA\_BISECT\_YTOL** [float] Absolute tolerance in the (H, S, G, U, A) spec when converging a flash with one (T, P, V) spec and one (H, S, G, U, A) spec using a bisection-type solver, [-]
- **TPV\_HSGUA\_BISECT\_YTOL\_ONLY** [bool] When True, the *TPV\_HSGUA\_BISECT\_XTOL* setting is ignored and the flash is considered converged once *TPV\_HSGUA\_BISECT\_YTOL* is satisfied, [-]
- **TPV\_HSGUA\_NEWTON\_XTOL** [float] Tolerance in the iteration variable when converging a flash with one (T, P, V) spec and one (H, S, G, U, A) spec using a full newton solver, [-]
- **TPV\_HSGUA\_NEWTON\_MAXITER** [float] Maximum number of iterations when converging a flash with one (T, P, V) spec and one (H, S, G, U, A) spec using full newton solver, [-]
- **TPV\_HSGUA\_SECANT\_MAXITER** [float] Maximum number of iterations when converging a flash with one (T, P, V) spec and one (H, S, G, U, A) spec using a secant solver, [-]
- **HSGUA\_NEWTON\_ANALYTICAL\_JAC** [bool] Whether or not to calculate the full newton jacobian analytically or numerically; this would need to be set to False if the phase objects used in the flash do not have complete analytical derivatives implemented, [-]

# Vapor and Multiple Liquid Systems

**class** thermo.flash.**FlashVLN**(constants, correlations, liquids, gas, solids=None,

settings=<thermo.bulk.BulkSettings object>)

Bases: thermo.flash.flash\_vl.FlashVL

Class for performing flash calculations on multiphase vapor-liquid systems. This rigorous class does not make any assumptions and will search for up to the maximum amount of liquid phases specified by the user. Vapor and each liquid phase do not need to use a consistent thermodynamic model.

The minimum information that is needed in addition to the Phase objects is:

- MWs
- Vapor pressure curve
- Functioning enthalpy models for each phase

### **Parameters**

- **constants** [*ChemicalConstantsPackage* object] Package of chemical constants; these are used as boundaries at times, initial guesses other times, and in all cases these properties are accessible as attributes of the resulting *EquilibriumState* object, [-]
- **correlations** [*PropertyCorrelationsPackage*] Package of chemical T-dependent properties; these are used as boundaries at times, for initial guesses other times, and in all cases these properties are accessible as attributes of the resulting *EquilibriumState* object, [-]
- gas [Phase object] A single phase which can represent the gas phase, [-]
- **liquids** [list[*Phase*]] A list of phase objects that can represent the liquid phases; if working with a VLL system with a consistent model, specify the same liquid phase twice; the length of this list is the maximum number of liquid phases that will be searched for, [-]
- solids [list[Phase]] Not used, [-]
- **settings** [*BulkSettings* object] Object containing settings for calculating bulk and transport properties, [-]

# Notes

The algorithms in this object are mostly from [1], [2] and [3]. Sequential substitution without acceleration is used by default to converge multiphase systems.

Additional information that can be provided in the *ChemicalConstantsPackage* object and *PropertyCorrelationsPackage* object that may help convergence is:

- Tc, Pc, omega, Tb, and atoms
- Gas heat capacity correlations
- · Liquid molar volume correlations
- · Heat of vaporization correlations

# References

[1], [2], [3]

# **Examples**

A three-phase flash of butanol, water, and ethanol with the SRK EOS without BIPs:

```
>>> from thermo import ChemicalConstantsPackage, CEOSGas, CEOSLiquid, SRKMIX,
→FlashVLN, PropertyCorrelationsPackage, HeatCapacityGas
>>> constants = ChemicalConstantsPackage(Tcs=[563.0, 647.14, 514.0], Pcs=[4414000.0,
\rightarrow 22048320.0, 6137000.0], omegas=[0.59, 0.344, 0.635], MWs=[74.1216, 18.01528, 46.
↔06844], CASs=['71-36-3', '7732-18-5', '64-17-5'])
>>> properties = PropertyCorrelationsPackage(constants=constants,
                                        HeatCapacityGases=[HeatCapacityGas(poly_
→fit=(50.0, 1000.0, [-3.787200194613107e-20, 1.7692887427654656e-16, -3.
→445247207129205e-13, 3.612771874320634e-10, -2.1953250181084466e-07, 7.
→707135849197655e-05, -0.014658388538054169, 1.5642629364740657, -7.
\rightarrow 614560475001724])),
                                        HeatCapacityGas(poly_fit=(50.0, 1000.0, [5.
. . .
→543665000518528e-22, -2.403756749600872e-18, 4.2166477594350336e-15, -3.
→7965208514613565e-12, 1.823547122838406e-09, -4.3747690853614695e-07, 5.
→437938301211039e-05, -0.003220061088723078, 33.32731489750759])),
                                        HeatCapacityGas(poly_fit=(50.0, 1000.0, [-1.
. . .
→162767978165682e-20, 5.4975285700787494e-17, -1.0861242757337942e-13, 1.
→1582703354362728e-10, -7.160627710867427e-08, 2.5392014654765875e-05, -0.
→004732593693568646, 0.5072291035198603, 20.037826650765965])),], )
>>> eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
>>> gas = CEOSGas(SRKMIX, eos_kwargs, HeatCapacityGases=properties.
→HeatCapacityGases)
>>> lig = CEOSLiquid(SRKMIX, eos_kwargs, HeatCapacityGases=properties.
→HeatCapacityGases)
>>> flashN = FlashVLN(constants, properties, liquids=[liq, liq], gas=gas)
>>> res = flashN.flash(T=361, P=1e5, zs=[.25, 0.7, .05])
>>> res.phase_count
3
```

# Attributes

- **SS\_NP\_MAXITER** [int] Maximum number of sequential substitution iterations to try when converging a three or more phase solution, [-]
- **SS\_NP\_TOL** [float] Convergence tolerance in sequential substitution for a three or more phase solution [-]
- **SS\_NP\_TRIVIAL\_TOL** [float] Tolerance at which to quick a three-phase flash because it is converging to the trivial solution, [-]
- **SS\_STAB\_AQUEOUS\_CHECK** [bool] If True, the first three-phase stability check will be on water (if it is present) as it forms a three-phase solution more than any other component, [-]
- **DOUBLE\_CHECK\_2P** [bool] This parameter should be set to True if any issues in the solution are noticed. It can slow down two-phase solution. It ensures that all potential vapor-liquid and liquid-liquid phase pairs are searched for stability, instead of testing first for a vapor-liquid solution and then moving on to a three phase flash if an instability is detected, [-]

# **Base Flash Class**

# class thermo.flash.Flash

Bases: object

Base class for performing flash calculations. All Flash objects need to inherit from this, and common methods can be added to it.

# Methods

flash([zs, T, P, VF, SF, V, H, S, G, U, A,])	Method to perform a flash calculation and return the
	result as an EquilibriumState object.
<i>plot_TP</i> (zs[, Tmin, Tmax, pts, branches,])	Method to create a plot of the phase envelope as can
	be calculated from a series of temperature & vapor
	fraction spec flashes.

flash(zs=None, T=None, P=None, VF=None, SF=None, V=None, H=None, S=None, G=None, U=None, A=None, solution=None, hot\_start=None, retry=False, dest=None)

Method to perform a flash calculation and return the result as an *EquilibriumState* object. This generic interface allows flashes with any combination of valid specifications; if a flash is unimplemented and error will be raised.

# Parameters

- **zs** [list[float], optional] Mole fractions of each component, required unless there is only one component, [-]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- VF [float, optional] Vapor fraction, [-]
- SF [float, optional] Solid fraction, [-]
- V [float, optional] Molar volume of the overall bulk, [m^3/mol]
- H [float, optional] Molar enthalpy of the overall bulk, [J/mol]
- **S** [float, optional] Molar entropy of the overall bulk, [J/(mol\*K)]
- G [float, optional] Molar Gibbs free energy of the overall bulk, [J/mol]
- U [float, optional] Molar internal energy of the overall bulk, [J/mol]
- A [float, optional] Molar Helmholtz energy of the overall bulk, [J/mol]
- **solution** [str or int, optional] When multiple solutions exist, if more than one is found they will be sorted by T (and then P) increasingly; this number will index into the multiple solution array. Negative indexing is supported. 'high' is an alias for 0, and 'low' an alias for -1. Setting this parameter may make a flash slower because in some cases more checks are performed. [-]
- **hot\_start** [*EquilibriumState*] A previously converged flash or initial guessed state from which the flash can begin; this parameter can save time in some cases, [-]
- **retry** [bool] Usually for flashes like UV or PH, there are multiple sets of possible iteration variables. For the UV case, the prefered iteration variable is P, so each iteration a PV solve is done on the phase; but equally the flash can be done iterating on *T*, where a TV solve is done on the phase each iteration. Depending on the tolerances, the flash type, the

thermodynamic consistency of the phase, and other factors, it is possible the flash can fail. If *retry* is set to True, the alternate variable set will be iterated as a backup if the first flash fails. [-]

**dest** [None or *EquilibriumState* or *EquilibriumStream*] What type of object the flash result is set into; leave as None to obtain the normal *EquilibriumState* results, [-]

### Returns

**results** [*EquilibriumState*] Equilibrium object containing the state of the phases after the flash calculation [-]

# Notes

**Warning:** Not all flash specifications have a unique solution. Not all flash specifications will converge, whether from a bad model, bad inputs, or simply a lack of convergence by the implemented algorithms. You are welcome to submit these cases to the author but the library is provided AS IS, with NO SUPPORT.

**Warning:** Convergence of a flash may be impaired by providing *hot\_start*. If reliability is desired, do not use this parameter.

**Warning:** The most likely thermodynamic methods to converge are thermodynamically consistent ones. This means e.g. an ideal liquid and an ideal gas; or an equation of state for both phases. Mixing thermodynamic models increases the possibility of multiple solutions, discontinuities, and other not-fun issues for the algorithms.

# 

Method to create a plot of the phase envelope as can be calculated from a series of temperature & vapor fraction spec flashes. By default vapor fractions of 0 and 1 are plotted; additional vapor fraction specifications can be specified in the *branches* argument as a list.

### **Parameters**

zs [list[float]] Mole fractions of the feed, [-]

Tmin [float, optional] Minimum temperature to begin the plot, [K]

Tmax [float, optional] Maximum temperature to end the plot, [K]

pts [int, optional] The number of points to calculated for each vapor fraction value, [-]

branches [list[float], optional] Extra vapor fraction values to plot, [-]

**ignore\_errors** [bool, optional] Whether to fail on a calculation failure or to ignore the bad point, [-]

values [bool, optional] If True, the calculated values will be returned instead of plotted, [-]

show [bool, optional] If False, the plot will be returned instead of shown, [-]

**hot** [bool, optional] Whether to restart the next flash from the previous flash or not (intended to speed the call when True), [-]

Ts [list[float]] Temperatures, [K]

P\_dews, P\_bubbles, branch\_Ps

# 7.13.2 Specific Flash Algorithms

It is recommended to use the Flash classes, which are designed to have generic interfaces. The implemented specific flash algorithms may be changed in the future, but reading their source code may be helpful for instructive purposes.

# 7.14 Functional Group Identification (thermo.functional\_groups)

This module contains various methods for identifying functional groups in molecules. This functionality requires the RDKit library to work.

For submitting pull requests, please use the GitHub issue tracker.

- Specific molecule matching functions
- Hydrocarbon Groups
- Oxygen Groups
- Nitrogen Groups
- Sulfur Groups
- Silicon Groups
- Boron Groups
- Phosphorus Groups
- Halogen Groups
- Organometalic Groups
- Other Groups
- Utility functions
- Functions using group identification

# 7.14.1 Specific molecule matching functions

FC(F)(F)F', IC(I)(I)I', O=C(CI)CI', O=C(F)F', O=C(O)O',

$$O = C = O', 'O = C = S', 'S = C = S', '[C - ]#[O + ]'])$$

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is organic. The definition of organic vs. inorganic compounds is arabitrary. The rules implemented here are fairly complex.

• If a compound has an C-C bond, a C=C bond, a carbon triple bond, a carbon attatched however to a hydrogen, a carbon in a ring, or an amide group.

- If a compound is in the list of canonical smiles *organic\_smiles*, either the defaults in the library or those provided as an input to the function, the molecule is considered organic.
- If a compound is in the list of canonical smiles *inorganic\_smiles*, either the defaults in the library or those provided as an input to the function, the molecule is considered inorganic.
- If *restrict\_atoms* is provided and atoms are present in the molecule that are restricted, the compound is considered restricted.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

restrict\_atoms [Iterable[str]] Atoms that cannot be found in an organic molecule, [-]

organic\_smiles [Iterable[str]] Smiles that are hardcoded to be organic, [-]

inorganic\_smiles [Iterable[str]] Smiles that are hardcoded to be inorganic, [-]

# Returns

is\_organic [bool] Whether or not the compound is a organic or not, [-].

# **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_organic(MolFromSmiles("CC(C)C(C)C(C)C"))
True
```

### thermo.functional\_groups.is\_inorganic(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is inorganic.

# Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_inorganic [bool] Whether or not the compound is inorganic or not, [-].

# **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_inorganic(MolFromSmiles("0=[Zr].Cl.Cl"))
True
```

# 7.14.2 Hydrocarbon Groups

```
thermo.functional_groups.is_alkane(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an alkane, also refered to as a paraffin. All bonds in the molecule must be single carbon-carbon or carbon-hydrogen.

# **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

### Returns

is\_alkane [bool] Whether or not the compound is an alkane or not, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alkane(MolFromSmiles("CCC"))
True
```

## thermo.functional\_groups.is\_cycloalkane(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a cycloalkane, also refered to as a naphthenes.

**Parameters** 

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_cycloalkane [bool] Whether or not the compound is a cycloalkane or not, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_cycloalkane(MolFromSmiles('C1CCCCCCCC1'))
True
```

## thermo.functional\_groups.is\_branched\_alkane(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a branched alkane, also refered to as an isoparaffin. All bonds in the molecule must be single carbon-carbon or carbon-hydrogen.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_branched\_alkane [bool] Whether or not the compound is a branched alkane or not, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_branched_alkane(MolFromSmiles("CC(C)C(C)C(C)C"))
True
```

#### thermo.functional\_groups.is\_alkene(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an alkene. Alkenes are also refered to as olefins.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_alkene [bool] Whether or not the compound is a alkene or not, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alkene(MolFromSmiles('C=C'))
True
```

## thermo.functional\_groups.is\_alkyne(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an alkyne.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_alkyne [bool] Whether or not the compound is a alkyne or not, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alkyne(MolFromSmiles('CC#C'))
True
```

## thermo.functional\_groups.is\_aromatic(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is aromatic.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_aromatic [bool] Whether or not the compound is aromatic or not, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_aromatic(MolFromSmiles('CC1=CC=CC=C1C'))
True
```

## 7.14.3 Oxygen Groups

```
thermo.functional_groups.is_alcohol(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule any alcohol functional groups.

Parameters

**mol** [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_alcohol [bool] Whether or not the compound is an alcohol, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alcohol(MolFromSmiles('CCO'))
True
```

## thermo.functional\_groups.is\_polyol(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a polyol (more than 1 alcohol functional groups).

Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

**is\_polyol** [bool] Whether or not the compound is a polyol, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_polyol(MolFromSmiles('C(C(C0)0)0'))
True
```

#### thermo.functional\_groups.is\_ketone(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a ketone.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_ketone [bool] Whether or not the compound is a ketone, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_ketone(MolFromSmiles('C1CCC(=0)CC1'))
True
```

## thermo.functional\_groups.is\_aldehyde(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an aldehyde.

## Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_aldehyde [bool] Whether or not the compound is an aldehyde, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_aldehyde(MolFromSmiles('C=0'))
True
```

thermo.functional\_groups.is\_carboxylic\_acid(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carboxylic acid.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_carboxylic\_acid [bool] Whether or not the compound is a carboxylic acid, [-].

## **Examples**

Butyric acid (butter)

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carboxylic_acid(MolFromSmiles('CCCC(=0)0'))
True
```

## thermo.functional\_groups.is\_ether(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an ether.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_ether [bool] Whether or not the compound is an ether, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_ether(MolFromSmiles('CC(C)OC(C)C'))
True
```

## thermo.functional\_groups.is\_phenol(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a phenol.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

**is\_phenol** [bool] Whether or not the compound is a phenol, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_phenol(MolFromSmiles('CC(=0)NC1=CC=C(C=C1)0'))
True
```

## thermo.functional\_groups.is\_ester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an ester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_ester [bool] Whether or not the compound is an ester, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_ester(MolFromSmiles('CCOC(=0)C'))
True
```

## thermo.functional\_groups.is\_anhydride(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an anhydride.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_anhydride [bool] Whether or not the compound is an anhydride, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_anhydride(MolFromSmiles('C1=CC(=0)0C1=0'))
True
```

## thermo.functional\_groups.is\_acyl\_halide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a acyl halide.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_acyl\_halide [bool] Whether or not the compound is a acyl halide, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_acyl_halide(MolFromSmiles('C(CCC(=0)Cl)CC(=0)Cl'))
True
```

## thermo.functional\_groups.is\_carbonate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carbonate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_carbonate [bool] Whether or not the compound is a carbonate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carbonate(MolFromSmiles('C(=0)(0C(C1)(C1)C1)0C(C1)(C1)C1'))
True
```

## thermo.functional\_groups.is\_carboxylate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carboxylate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_carboxylate [bool] Whether or not the compound is a carboxylate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carboxylate(MolFromSmiles('CC(=0)[0-].[Na+]'))
True
```

## thermo.functional\_groups.is\_hydroperoxide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a hydroperoxide.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_hydroperoxide [bool] Whether or not the compound is a hydroperoxide, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_hydroperoxide(MolFromSmiles('CC(C)(C)00'))
True
```

## thermo.functional\_groups.is\_peroxide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a peroxide.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_peroxide [bool] Whether or not the compound is a peroxide, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_peroxide(MolFromSmiles('CC(C)(C)00C(C)(C)C'))
True
```

## thermo.functional\_groups.is\_orthoester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a orthoester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_orthoester [bool] Whether or not the compound is a orthoester, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_orthoester(MolFromSmiles('CCOC(C)(OCC)OCC'))
True
```

## thermo.functional\_groups.is\_methylenedioxy(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a methylenedioxy.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_methylenedioxy [bool] Whether or not the compound is a methylenedioxy, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_methylenedioxy(MolFromSmiles('C10C2=CC=CC=C201'))
True
```

thermo.functional\_groups.is\_orthocarbonate\_ester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a orthocarbonate ester .

### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_orthocarbonate\_ester [bool] Whether or not the compound is a orthocarbonate ester , [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_orthocarbonate_ester (MolFromSmiles('COC(OC)(OC)OC')
True
```

## thermo.functional\_groups.is\_carboxylic\_anhydride(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carboxylic anhydride .

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_carboxylic\_anhydride [bool] Whether or not the compound is a carboxylic anhydride, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carboxylic_anhydride (MolFromSmiles('CCCC(=0)OC(=0)CCC')
True
```

## 7.14.4 Nitrogen Groups

#### thermo.functional\_groups.is\_amide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule has a amide RC(=O)NRR group.

## Parameters

**mol** [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_amide [bool] Whether or not the compound is a amide or not, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_amide(MolFromSmiles('CN(C)C=0'))
True
```

## thermo.functional\_groups.is\_amidine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule has a amidine RC(NR)NR2 group.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_amidine [bool] Whether or not the compound is a amidine or not, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_amidine(MolFromSmiles('C1=CC(=CC=C1C(=N)N)0CCCCC0C2=CC=C(C=C2)C(=N)N'))
True
```

## thermo.functional\_groups.is\_amine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a amine.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_amine [bool] Whether or not the compound is a amine, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_amine(MolFromSmiles('CN'))
True
```

## thermo.functional\_groups.is\_primary\_amine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a primary amine.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_primary\_amine [bool] Whether or not the compound is a primary amine, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_primary_amine(MolFromSmiles('CN'))
True
```

thermo.functional\_groups.is\_secondary\_amine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a secondary amine.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_secondary\_amine [bool] Whether or not the compound is a secondary amine, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_secondary_amine(MolFromSmiles('CNC'))
True
```

## thermo.functional\_groups.is\_tertiary\_amine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a tertiary amine.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_tertiary\_amine [bool] Whether or not the compound is a tertiary amine, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_tertiary_amine(MolFromSmiles('CN(C)C'))
True
```

## thermo.functional\_groups.is\_quat(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a quat.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_quat [bool] Whether or not the compound is a quat, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_quat(MolFromSmiles('CCCCCCCCCCCC[N+](C)(C)CCCCCCCCCCCCCCC.[Cl-]'))
True
```

## thermo.functional\_groups.is\_imine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a imine.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_imine [bool] Whether or not the compound is a imine, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_imine(MolFromSmiles('C1=CC=C(C=C1)C(=N)C2=CC=C2'))
True
```

## thermo.functional\_groups.is\_primary\_ketimine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a primary ketimine.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_primary\_ketimine [bool] Whether or not the compound is a primary ketimine, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_primary_ketimine(MolFromSmiles('C1=CC=C(C=C1)C(=N)C2=CC=CC=C2'))
True
```

#### thermo.functional\_groups.is\_secondary\_ketimine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a secondary ketimine.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_secondary\_ketimine [bool] Whether or not the compound is a secondary ketimine, [-].

thermo.functional\_groups.is\_primary\_aldimine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a primary aldimine.

## Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_primary\_aldimine [bool] Whether or not the compound is a primary aldimine, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_primary_aldimine(MolFromSmiles('CC=N'))
True
```

## thermo.functional\_groups.is\_secondary\_aldimine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a secondary aldimine.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_secondary\_aldimine [bool] Whether or not the compound is a secondary aldimine, [-].

## Examples

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_secondary_aldimine(MolFromSmiles( 'C1=CC=C(C=C1)/C=N\\0'))
True
```

## thermo.functional\_groups.is\_imide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a imide.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_imide [bool] Whether or not the compound is a imide, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_imide(MolFromSmiles('C1=CC=C2C(=C1)C(=0)NC2=0'))
True
```

thermo.functional\_groups.is\_azide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a azide.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_azide [bool] Whether or not the compound is a azide, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_azide(MolFromSmiles('C1=CC=C(C=C1)N=[N+]=[N-]'))
True
```

## thermo.functional\_groups.is\_azo(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a azo.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_azo [bool] Whether or not the compound is a azo, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_azo(MolFromSmiles('C1=CC=C(C=C1)N=NC2=CC=C2'))
True
```

## thermo.functional\_groups.is\_cyanate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a cyanate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_cyanate [bool] Whether or not the compound is a cyanate, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_cyanate(MolFromSmiles('COC#N'))
True
```

## thermo.functional\_groups.is\_isocyanate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a isocyanate.

### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_isocyanate [bool] Whether or not the compound is a isocyanate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_isocyanate(MolFromSmiles('CN=C=0'))
True
```

## thermo.functional\_groups.is\_nitrate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a nitrate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_nitrate [bool] Whether or not the compound is a nitrate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_nitrate(MolFromSmiles('CCCCC0[N+](=0)[0-]'))
True
```

## thermo.functional\_groups.is\_nitrile(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a nitrile.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_nitrile [bool] Whether or not the compound is a nitrile, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_nitrile(MolFromSmiles('CC#N'))
True
```

thermo.functional\_groups.is\_isonitrile(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a isonitrile.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_isonitrile [bool] Whether or not the compound is a isonitrile, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_isonitrile(MolFromSmiles('C[N+]#[C-]'))
True
```

## thermo.functional\_groups.is\_nitrite(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a nitrite.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_nitrite [bool] Whether or not the compound is a nitrite, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_nitrite(MolFromSmiles('CC(C)CCON=0'))
True
```

## thermo.functional\_groups.is\_nitro(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a nitro.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_nitro [bool] Whether or not the compound is a nitro, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_nitro(MolFromSmiles('C[N+](=0)[0-]'))
True
```

## thermo.functional\_groups.is\_nitroso(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a nitroso.

### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_nitroso [bool] Whether or not the compound is a nitroso, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_nitroso(MolFromSmiles('C1=CC=C(C=C1)N=0'))
True
```

## thermo.functional\_groups.is\_oxime(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a oxime.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_oxime [bool] Whether or not the compound is a oxime, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_oxime(MolFromSmiles('CC(=NO)C'))
True
```

## thermo.functional\_groups.is\_pyridyl(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a pyridyl.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_pyridyl [bool] Whether or not the compound is a pyridyl, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_pyridyl(MolFromSmiles('CN1CCC[C@H]1C1=CC=CN=C1'))
True
```

thermo.functional\_groups.is\_carbamate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carbamate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_carbamate [bool] Whether or not the compound is a carbamate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carbamate(MolFromSmiles('CC(C)OC(=0)NC1=CC(=CC=C1)Cl'))
True
```

## 7.14.5 Sulfur Groups

```
thermo.functional_groups.is_mercaptan(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule has a mercaptan R-SH group. This is also called a thiol.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_mercaptan [bool] Whether or not the compound is a mercaptan or not, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_mercaptan(MolFromSmiles("CS"))
True
```

#### thermo.functional\_groups.is\_sulfide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a sulfide. This group excludes disulfides.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_sulfide [bool] Whether or not the compound is a sulfide, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_sulfide(MolFromSmiles('CSC'))
True
```

## thermo.functional\_groups.is\_disulfide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a disulfide.

### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_disulfide [bool] Whether or not the compound is a disulfide, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_disulfide(MolFromSmiles('CSSC'))
True
```

## thermo.functional\_groups.is\_sulfoxide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a sulfoxide.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_sulfoxide [bool] Whether or not the compound is a sulfoxide, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_sulfoxide(MolFromSmiles('CS(=0)C'))
True
```

## thermo.functional\_groups.is\_sulfone(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a sulfone.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_sulfone [bool] Whether or not the compound is a sulfone, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_sulfone(MolFromSmiles('CS(=0)(=0)C'))
True
```

thermo.functional\_groups.is\_sulfinic\_acid(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a sulfinic acid.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_sulfinic\_acid [bool] Whether or not the compound is a sulfinic acid, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_sulfinic_acid(MolFromSmiles('0=S(0)CCN'))
True
```

### thermo.functional\_groups.is\_sulfonic\_acid(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a sulfonic acid.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_sulfonic\_acid [bool] Whether or not the compound is a sulfonic acid, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_sulfonic_acid(MolFromSmiles('OS(=0)(=0)c1ccccc1'))
True
```

#### thermo.functional\_groups.is\_sulfonate\_ester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a sulfonate ester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_sulfonate\_ester [bool] Whether or not the compound is a sulfonate ester, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_sulfonate_ester(MolFromSmiles('COS(=0)(=0)C(F)(F)F'))
True
```

## thermo.functional\_groups.is\_thiocyanate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a thiocyanate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_thiocyanate [bool] Whether or not the compound is a thiocyanate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_thiocyanate(MolFromSmiles('C1=CC=C(C=C1)SC#N'))
True
```

## thermo.functional\_groups.is\_isothiocyanate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a isothiocyanate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_isothiocyanate [bool] Whether or not the compound is a isothiocyanate, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_isothiocyanate(MolFromSmiles('C=CCN=C=S'))
True
```

#### thermo.functional\_groups.is\_thicketone(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a thioketone.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_thicketone [bool] Whether or not the compound is a thicketone, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_thioketone(MolFromSmiles('C1=CC=C(C=C1)C(=S)C2=CC=C2'))
True
```

## thermo.functional\_groups.is\_thial(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a thial.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_thial [bool] Whether or not the compound is a thial, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_thial(MolFromSmiles('CC=S'))
True
```

#### thermo.functional\_groups.is\_carbothioic\_s\_acid(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a Carbothioic S-acid.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_carbothioic\_s\_acid [bool] Whether or not the compound is a Carbothioic S-acid, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carbothioic_s_acid(MolFromSmiles('C1=CC=C(C=C1)C(=0)S'))
True
```

```
thermo.functional_groups.is_carbothioic_o_acid(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a Carbothioic S-acid.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_carbothioic\_o\_acid [bool] Whether or not the compound is a Carbothioic S-acid, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carbothioic_o_acid(MolFromSmiles('OC(=S)c1ccccc10'))
True
```

## thermo.functional\_groups.is\_thiolester(mol)

Given a rdkit. Chem. rdchem. Mol object, returns whether or not the molecule is a thiolester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_thiolester [bool] Whether or not the compound is a thiolester, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_thiolester(MolFromSmiles('CSC(=0)C=C'))
True
```

## thermo.functional\_groups.is\_thionoester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a thionoester.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_thionoester [bool] Whether or not the compound is a thionoester, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_thionoester(MolFromSmiles('CCOC(=S)S'))
True
```

```
thermo.functional_groups.is_carbodithioic_acid(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carbodithioic acid .

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_carbodithioic\_acid [bool] Whether or not the compound is a carbodithioic acid , [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carbodithioic_acid(MolFromSmiles('C1=CC=C(C=C1)C(=S)S'))
True
```

thermo.functional\_groups.is\_carbodithio(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a carbodithio.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_carbodithio [bool] Whether or not the compound is a carbodithio, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_carbodithio(MolFromSmiles('C(=S)(N)SSC(=S)N'))
True
```

## 7.14.6 Silicon Groups

```
thermo.functional_groups.is_siloxane(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a siloxane.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_siloxane [bool] Whether or not the compound is a siloxane, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_siloxane(MolFromSmiles('C[Si]1(0[Si](0[Si](01)(C)C)(C)C)(C)C)C))
True
```

thermo.functional\_groups.is\_silyl\_ether(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule any silyl ether functional groups.

Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_silyl\_ether [bool] Whether or not the compound is an silyl ether, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_silyl_ether(MolFromSmiles('C[Si](C)(C)OS(=0)(=0)C(F)(F)F'))
True
```

## 7.14.7 Boron Groups

#### thermo.functional\_groups.is\_boronic\_acid(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule has any boronic acid functional groups.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_boronic\_acid [bool] Whether or not the compound is an boronic acid, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_boronic_acid(MolFromSmiles('B(C)(0)0'))
True
```

#### thermo.functional\_groups.is\_boronic\_ester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a boronic ester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_boronic\_ester [bool] Whether or not the compound is a boronic ester, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_boronic_ester(MolFromSmiles('B(C)(OC(C)C)OC(C)C'))
True
```

#### thermo.functional\_groups.is\_borinic\_acid(mol)

Given a rdkit. Chem. rdchem. Mol object, returns whether or not the molecule is a borinic acid.

## Parameters

**mol** [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_borinic\_acid [bool] Whether or not the compound is a borinic acid, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_borinic_acid(MolFromSmiles('BO'))
True
```

thermo.functional\_groups.is\_borinic\_ester(mol)

Given a rdkit. Chem. rdchem. Mol object, returns whether or not the molecule is a borinic ester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_borinic\_ester [bool] Whether or not the compound is a borinic ester, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_borinic_ester(MolFromSmiles('B(C1=CC=CC=C1)(C2=CC=C2)OCCN'))
True
```

## 7.14.8 Phosphorus Groups

#### thermo.functional\_groups.is\_phosphine(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a phosphine.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_phosphine [bool] Whether or not the compound is a phosphine, [-].

#### Examples

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_phosphine(MolFromSmiles('CCCPC'))
True
```

thermo.functional\_groups.is\_phosphonic\_acid(mol)

Given a rdkit. Chem. rdchem. Mol object, returns whether or not the molecule is a phosphonic\_acid.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_phosphonic\_acid [bool] Whether or not the compound is a phosphonic\_acid, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_phosphonic_acid(MolFromSmiles('C1=CC=C(C=C1)CP(=0)(0)0'))
True
```

## thermo.functional\_groups.is\_phosphodiester(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a phosphodiester.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_phosphodiester [bool] Whether or not the compound is a phosphodiester, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_phosphodiester(MolFromSmiles('C(COP(=0)(0)OCC(C(=0)0)N)N=C(N)N'))
True
```

## thermo.functional\_groups.is\_phosphate(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a phosphate.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_phosphate [bool] Whether or not the compound is a phosphate, [-].

## **Examples**

## 7.14.9 Halogen Groups

```
thermo.functional_groups.is_haloalkane(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a haloalkane.

## Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_haloalkane [bool] Whether or not the compound is a haloalkane, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_haloalkane(MolFromSmiles('CCCl'))
True
```

## thermo.functional\_groups.is\_fluoroalkane(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a fluoroalkane.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_fluoroalkane [bool] Whether or not the compound is a fluoroalkane, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_fluoroalkane(MolFromSmiles('CF'))
True
```

## thermo.functional\_groups.is\_chloroalkane(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a chloroalkane.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_chloroalkane [bool] Whether or not the compound is a chloroalkane, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_chloroalkane(MolFromSmiles('CCl'))
True
```

#### thermo.functional\_groups.is\_bromoalkane(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a bromoalkane.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_bromoalkane [bool] Whether or not the compound is a bromoalkane, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_bromoalkane(MolFromSmiles('CBr'))
True
```

thermo.functional\_groups.is\_iodoalkane(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is a iodoalkane.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

is\_iodoalkane [bool] Whether or not the compound is a iodoalkane, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_iodoalkane(MolFromSmiles('CI'))
True
```

## 7.14.10 Organometalic Groups

```
thermo.functional_groups.is_alkyllithium(mol)
```

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule any alkyllithium functional groups.

## Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_alkyllithium [bool] Whether or not the compound is an alkyllithium, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alkyllithium(MolFromSmiles('[Li+].[CH3-]'))
True
```

## thermo.functional\_groups.is\_alkylaluminium(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule any alkylaluminium functional groups.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_alkylaluminium [bool] Whether or not the compound is an alkylaluminium, [-].

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alkylaluminium(MolFromSmiles('CC[A1](CC)CC'))
True
```

## thermo.functional\_groups.is\_alkylmagnesium\_halide(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule any alkylmagnesium\_halide functional groups.

## Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

## Returns

is\_alkylmagnesium\_halide [bool] Whether or not the compound is an alkylmagnesium\_halide,

[-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_alkylmagnesium_halide(MolFromSmiles('C1=CC=[C-]C=C1.[Mg+2].[Br-]'))
True
```

## 7.14.11 Other Groups

## thermo.functional\_groups.is\_acid(mol)

Given a *rdkit.Chem.rdchem.Mol* object, returns whether or not the molecule is an acid.

## Parameters

**mol** [rdkit.Chem.rdchem.Mol] Molecule [-]

#### Returns

is\_acid [bool] Whether or not the compound is a acid, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> is_acid(MolFromSmiles('CC(=0)0'))
True
```

## 7.14.12 Utility functions

thermo.functional\_groups.count\_ring\_ring\_attatchments(mol)

Given a *rdkit.Chem.rdchem.Mol* object, count the number of times a ring in the molecule is bonded with another ring in the molecule.

An easy explanation is cubane - each edge of the cube is a ring uniquely bonding with another ring; so this function returns twelve.

#### **Parameters**

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

Returns

ring\_ring\_attatchments [bool] The number of ring-ring bonds, [-].

## **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> count_ring_ring_attatchments(MolFromSmiles('C12C3C4C1C5C2C3C45'))
12
```

Given a *rdkit.Chem.rdchem.Mol* object, count the number of rings in the molecule that are attatched to another ring. if *allow\_neighbors* is True, any bond to another atom that is part of a ring is allowed; if it is False, the rings have to share a wall.

#### Parameters

mol [rdkit.Chem.rdchem.Mol] Molecule [-]

- **allow\_neighbors** [bool] Whether or not to count neighboring rings or just ones sharing a wall, [-]
- atom\_rings [rdkit.Chem.rdchem.RingInfo, optional] Internal parameter, used for performance only

## Returns

rings\_attatched\_to\_rings [bool] The number of rings bonded to other rings, [-].

#### **Examples**

```
>>> from rdkit.Chem import MolFromSmiles
>>> count_rings_attatched_to_rings(MolFromSmiles('C12C3C4C1C5C2C3C45'))
6
```

## 7.14.13 Functions using group identification

thermo.functional\_groups.BVirial\_Tsonopoulos\_extended\_ab(Tc, Pc, dipole, smiles)

Calculates the of *a* and *b* parameters of the Tsonopoulos (extended) second virial coefficient prediction method. These parameters account for polarity. This function uses *rdkit* to identify the component type of the molecule.

#### Parameters

Tc [float] Critical temperature of fluid [K]

Pc [float] Critical pressure of the fluid [Pa]

dipole [float] dipole moment, optional, [Debye]

#### Returns

- a [float] Fit parameter matched to one of the supported chemical classes.
- **b** [float] Fit parameter matched to one of the supported chemical classes.

## Notes

To calculate *a* or *b*, the following rules are used:

For 'simple' or 'normal' fluids:

a = 0b = 0

For 'ketone', 'aldehyde', 'alkyl nitrile', 'ether', 'carboxylic acid', or 'ester' types of chemicals:

$$a = -2.14 \times 10^{-4} \mu_r - 4.308 \times 10^{-21} (\mu_r)^8$$
$$b = 0$$

For 'alkyl halide', 'mercaptan', 'sulfide', or 'disulfide' types of chemicals:

$$a = -2.188 \times 10^{-4} (\mu_r)^4 - 7.831 \times 10^{-21} (\mu_r)^8$$

b = 0

For 'alkanol' types of chemicals (except methanol):

$$a = 0.0878$$

$$b = 0.00908 + 0.0006957\mu_r$$

For methanol:

$$a = 0.0878$$
  
 $b = 0.0525$ 

For water:

a = -0.0109

$$b = 0$$

If required, the form of dipole moment used in the calculation of some types of *a* and *b* values is as follows:

$$\mu_r = 100000 \frac{\mu^2 (Pc/101325.0)}{Tc^2}$$

## References

[1], [2]

## 7.15 Heat Capacity (thermo.heat\_capacity)

This module contains implementations of *TDependentProperty* representing liquid, vapor, and solid heat capacity. A variety of estimation and data methods are available as included in the *chemicals* library. Additionally liquid, vapor, and solid mixture heat capacity predictor objects are implemented subclassing *MixtureProperty*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Pure Liquid Heat Capacity
- Pure Gas Heat Capacity
- Pure Solid Heat Capacity
- Mixture Liquid Heat Capacity
- Mixture Gas Heat Capacity
- Mixture Solid Heat Capacity

## 7.15.1 Pure Liquid Heat Capacity

class thermo.heat\_capacity.HeatCapacityLiquid(CASRN=", MW=None, similarity\_variable=None,

Tc=None, omega=None, Cpgm=None, extrapolation='linear', \*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with liquid heat capacity as a function of temperature. Consists of seven coefficient-based methods, two constant methods, one tabular source, two CSP methods based on gas heat capacity, one simple estimator, and the external library CoolProp.

## Parameters

CASRN [str, optional] The CAS number of the chemical

MW [float, optional] Molecular weight, [g/mol]

similarity\_variable [float, optional] similarity variable, n\_atoms/MW, [mol/g]

Tc [float, optional] Critical temperature, [K]

omega [float, optional] Acentric factor, [-]

- **Cpgm** [float or callable, optional] Idea-gas molar heat capacity at T or callable for the same, [J/mol/K]
- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]

**method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

#### See also:

chemicals.heat\_capacity.Zabransky\_quasi\_polynomial chemicals.heat\_capacity.Zabransky\_cubic chemicals.heat\_capacity.Rowlinson\_Poling chemicals.heat\_capacity.Rowlinson\_Bondi chemicals.heat\_capacity.Dadgostar\_Shaw chemicals.heat\_capacity.Shomate

#### Notes

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the list stored in *heat\_capacity\_liquid\_methods*.

# ZABRANSKY\_SPLINE, ZABRANSKY\_QUASIPOLYNOMIAL, ZABRANSKY\_SPLINE\_C, and ZABRANSKY\_QUASIPOLYNOMIAL\_C:

Rigorous expressions developed in [1] following critical evaluation of the available data. The spline methods use the form described in Zabransky\_cubic over short ranges with varying coefficients to obtain a wider range. The quasi-polynomial methods use the form described in Zabransky\_quasi\_polynomial, more suitable for extrapolation, and over then entire range. Respectively, there is data available for 588, 146, 51, and 26 chemicals. 'C' denotes constant- pressure data available from more precise experiments. The others are heat capacity values averaged over a temperature changed.

#### ZABRANSKY\_SPLINE\_SAT and ZABRANSKY\_QUASIPOLYNOMIAL\_SAT:

Rigorous expressions developed in [1] following critical evaluation of the available data. The spline method use the form described in Zabransky\_cubic over short ranges with varying coefficients to obtain a wider range. The quasi-polynomial method use the form described in Zabransky\_quasi\_polynomial, more suitable for extrapolation, and over their entire range. Respectively, there is data available for 203, and 16 chemicals. Note that these methods are for the saturation curve!

#### VDI\_TABULAR:

Tabular data up to the critical point available in [5]. Note that this data is along the saturation curve.

#### **ROWLINSON\_POLING:**

CSP method described in Rowlinson\_Poling. Requires a ideal gas heat capacity value at the same temperature as it is to be calculated.

#### **ROWLINSON\_BONDI**:

CSP method described in Rowlinson\_Bondi. Requires a ideal gas heat capacity value at the same temperature as it is to be calculated.

## COOLPROP:

CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [3]. Very slow.

## DADGOSTAR\_SHAW:

A basic estimation method using the *similarity variable* concept; requires only molecular structure, so is very convenient. See Dadgostar\_Shaw for details.

#### POLING\_CONST:

Constant values in [2] at 298.15 K; available for 245 liquids.

## CRCSTD:

Constant values tabulated in [4] at 298.15 K; data is available for 433 liquids.

WEBBOOK\_SHOMATE: Shomate form coefficients from [6] for ~200 compounds.

#### References

[1], [2], [3], [4], [5], [6]

#### **Examples**

#### **Methods**

calculate(T, method)	Method to calculate heat capacity of a liquid at tem-
	perature $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

## calculate(T, method)

Method to calculate heat capacity of a liquid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature at which to calculate heat capacity, [K]

method [str] Name of the method to use

#### Returns

Cp [float] Heat capacity of the liquid at T, [J/mol/K]

## name = 'Liquid heat capacity'

#### property\_max = 10000.0

Maximum valid of Heat capacity; arbitrarily set. For fluids very near the critical point, this value can be obscenely high.

## property\_min = 1

Allow very low heat capacities; arbitrarily set; liquid heat capacity should always be somewhat substantial.

```
ranked_methods = ['ZABRANSKY_SPLINE', 'ZABRANSKY_QUASIPOLYNOMIAL',
```

'ZABRANSKY\_SPLINE\_C', 'ZABRANSKY\_QUASIPOLYNOMIAL\_C', 'ZABRANSKY\_SPLINE\_SAT',

```
'ZABRANSKY_QUASIPOLYNOMIAL_SAT', 'WEBBOOK_SHOMATE', 'VDI_TABULAR', 'COOLPROP'
```

'DADGOSTAR\_SHAW', 'ROWLINSON\_POLING', 'ROWLINSON\_BONDI', 'POLING\_CONST', 'CRCSTD'] Default rankings of the available methods.

#### test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods.

For the CSP method Rowlinson\_Poling, the model is considered valid for all temperatures. The simple method Dadgostar\_Shaw is considered valid for all temperatures. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### Parameters

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

units = 'J/mol/K'

```
thermo.heat_capacity.heat_capacity_liquid_methods = ['ZABRANSKY_SPLINE',
'ZABRANSKY_QUASIPOLYNOMIAL', 'ZABRANSKY_SPLINE_C', 'ZABRANSKY_QUASIPOLYNOMIAL_C',
'ZABRANSKY_SPLINE_SAT', 'ZABRANSKY_QUASIPOLYNOMIAL_SAT', 'WEBBOOK_SHOMATE',
'VDI_TABULAR', 'ROWLINSON_POLING', 'ROWLINSON_BONDI', 'COOLPROP', 'DADGOSTAR_SHAW',
'POLING_CONST', 'CRCSTD']
```

Holds all methods available for the HeatCapacityLiquid class, for use in iterating over them.

## 7.15.2 Pure Gas Heat Capacity

```
class thermo.heat_capacity.HeatCapacityGas(CASRN=", MW=None, similarity_variable=None,
```

*extrapolation='linear', iscyclic\_aliphatic=False, \*\*kwargs*) Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with gas heat capacity as a function of temperature. Consists of three coefficient-based methods, two constant methods, one tabular source, one simple estimator, one group-contribution estimator, one component specific method, and the external library CoolProp.

#### Parameters

CASRN [str, optional] The CAS number of the chemical

MW [float, optional] Molecular weight, [g/mol]

similarity\_variable [float, optional] similarity variable, n\_atoms/MW, [mol/g]

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

## See also:

chemicals.heat\_capacity.TRCCp

chemicals.heat\_capacity.Shomate

chemicals.heat\_capacity.Lastovka\_Shaw

chemicals.heat\_capacity.Rowlinson\_Poling

chemicals.heat\_capacity.Rowlinson\_Bondi

#### thermo.joback.Joback

#### Notes

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the list stored in *heat\_capacity\_gas\_methods*.

- **TRCIG:** A rigorous expression derived in [1] for modeling gas heat capacity. Coefficients for 1961 chemicals are available.
- POLING\_POLY: Simple polynomials in [2] not suitable for extrapolation. Data is available for 308 chemicals.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [3]. The heat capacity and enthalpy are implemented analytically and fairly fast; the entropy integral has no analytical integral and so is numerical. CoolProp's amazing coefficient collection is used directly in Python.
- LASTOVKA\_SHAW: A basic estimation method using the *similarity variable* concept; requires only molecular structure, so is very convenient. See Lastovka\_Shaw for details.
- **CRCSTD:** Constant values tabulated in [4] at 298.15 K; data is available for 533 gases.

POLING\_CONST: Constant values in [2] at 298.15 K; available for 348 gases.

**VDI\_TABULAR:** Tabular data up to the critical point available in [5]. Note that this data is along the saturation curve.

WEBBOOK\_SHOMATE: Shomate form coefficients from [6] for ~700 compounds.

JOBACK: An estimation method for organic substances in [7]

#### References

## [1], [2], [3], [4], [5], [6], [7]

#### Examples

```
>>> CpGas = HeatCapacityGas(CASRN='142-82-5', MW=100.2, similarity_variable=0.2295)
>>> CpGas(700)
317.244
```

## **Methods**

calculate(T, method)	Method to calculate surface tension of a liquid at tem-
	perature $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to test the validity of a specified method for
	a given temperature.

## calculate(T, method)

Method to calculate surface tension of a liquid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

## **Parameters**

**T** [float] Temperature at which to calculate heat capacity, [K]

method [str] Method name to use

## Returns

**Cp** [float] Calculated heat capacity, [J/mol/K]

name = 'gas heat capacity'

## property\_max = 10000.0

Maximum valid of Heat capacity; arbitrarily set. For fluids very near the critical point, this value can be obscenely high.

## property\_min = 0

Heat capacities have a minimum value of 0 at 0 K.

```
ranked_methods = ['TRCIG', 'WEBBOOK_SHOMATE', 'POLING_POLY', 'COOLPROP', 'JOBACK',
'LASTOVKA_SHAW', 'CRCSTD', 'POLING_CONST', 'VDI_TABULAR']
    Default rankings of the available methods.
```

## test\_method\_validity(T, method)

Method to test the validity of a specified method for a given temperature.

'TRC' and 'Poling' both have minimum and maimum temperatures. The constant temperatures in POL-ING\_CONST and CRCSTD are considered valid for 50 degrees around their specified temperatures. Lastovka\_Shaw is considered valid for the whole range of temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

## **Parameters**

**T** [float] Temperature at which to determine the validity of the method, [K]

method [str] Name of the method to test

## Returns

validity [bool] Whether or not a specifid method is valid

## units = 'J/mol/K'

thermo.heat\_capacity.heat\_capacity\_gas\_methods = ['COOLPROP', 'TRCIG', 'WEBBOOK\_SHOMATE', 'POLING\_POLY', 'LASTOVKA\_SHAW', 'CRCSTD', 'POLING\_CONST', 'JOBACK', 'VDI\_TABULAR']

Holds all methods available for the *HeatCapacityGas* class, for use in iterating over them.

# 7.15.3 Pure Solid Heat Capacity

```
class thermo.heat_capacity.HeatCapacitySolid(CASRN=", similarity variable=None, MW=None,
```

extrapolation='linear', \*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with solid heat capacity as a function of temperature. Consists of two temperature-dependent expressions, one constant value source, and one simple estimator.

## **Parameters**

**similarity\_variable** [float, optional] similarity variable, n\_atoms/MW, [mol/g]

MW [float, optional] Molecular weight, [g/mol]

CASRN [str, optional] The CAS number of the chemical

- **load\_data** [bool, optional] If False, do not load property coefficients from data sources in files [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

## See also:

chemicals.heat\_capacity.Lastovka\_solid

chemicals.heat\_capacity.Shomate

## Notes

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the list stored in *heat\_capacity\_solid\_methods*.

**PERRY151:** Simple polynomials with valous exponents selected for each expression. Coefficients are in units of calories/mol/K. The full expression is:

$$Cp = a + bT + c/T^2 + dT^2$$

Data is available for 284 solids, from [2].

CRCSTD: Values tabulated in [1] at 298.15 K; data is available for 529 solids.

**LASTOVKA\_S:** A basic estimation method using the *similarity variable* concept; requires only molecular structure, so is very convenient. See Lastovka\_solid for details.

**WEBBOOK\_SHOMATE:** Shomate form coefficients from [3] for ~300 compounds.

#### References

[1], [2], [3]

#### **Examples**

```
>>> CpSolid = HeatCapacitySolid(CASRN='142-82-5', MW=100.2, similarity_variable=0.

→2295)
>>> CpSolid(200)
131.205824
```

## **Methods**

calculate(T, method)	Method to calculate heat capacity of a solid at tem-
	perature $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

## calculate(T, method)

Method to calculate heat capacity of a solid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

## Parameters

T [float] Temperature at which to calculate heat capacity, [K]

**method** [str] Name of the method to use

#### Returns

Cp [float] Heat capacity of the solid at T, [J/mol/K]

## name = 'solid heat capacity'

## property\_max = 10000.0

Maximum value of Heat capacity; arbitrarily set.

## property\_min = 0

Heat capacities have a minimum value of 0 at 0 K.

## ranked\_methods = ['WEBBOOK\_SHOMATE', 'PERRY151', 'CRCSTD', 'LASTOVKA\_S']

Default rankings of the available methods.

## test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures. For the Lastovka\_solid method, it is considered valid under 10000K.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

## **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

#### Returns

validity [bool] Whether or not a method is valid

## units = 'J/mol/K'

# thermo.heat\_capacity.heat\_capacity\_solid\_methods = ['WEBBOOK\_SHOMATE', 'PERRY151', 'CRCSTD', 'LASTOVKA\_S']

Holds all methods available for the HeatCapacitySolid class, for use in iterating over them.

## 7.15.4 Mixture Liquid Heat Capacity

class thermo.heat\_capacity.HeatCapacityLiquidMixture(MWs=[], CASs=[], HeatCapacityLiquids=[])
Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with liquid heat capacity of a mixture as a function of temperature, pressure, and composition. Consists only of mole weighted averaging, and the Laliberte method for aqueous electrolyte solutions.

## Parameters

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

CASs [str, optional] The CAS numbers of all species in the mixture

**HeatCapacityLiquids** [list[HeatCapacityLiquid], optional] HeatCapacityLiquid objects created for all species in the mixture [-]

## Notes

To iterate over all methods, use the list stored in *heat\_capacity\_liquid\_mixture\_methods*.

LALIBERTE: Electrolyte model equation with coefficients; see thermo.electrochem. Laliberte\_heat\_capacity for more details.

LINEAR: Mixing rule described in mixing\_simple.

## **Methods**

calculate(T, P, zs, ws, method)	Method to calculate heat capacity of a liquid mixture at temperature <i>T</i> , pressure <i>P</i> , mole fractions <i>zs</i> and weight fractions <i>ws</i> with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for the given conditions.

## Tmax

Maximum temperature at which no method can calculate the heat capacity above.

## Tmin

Minimum temperature at which no method can calculate the heat capacity under.

```
calculate(T, P, zs, ws, method)
```

Method to calculate heat capacity of a liquid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

## Parameters

- T [float] Temperature at which to calculate the property, [K]
- **P** [float] Pressure at which to calculate the property, [Pa]
- **zs** [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

#### Returns

Cplm [float] Molar heat capacity of the liquid mixture at the given conditions, [J/mol]

```
name = 'Liquid heat capacity'
```

## property\_max = 10000.0

Maximum valid of Heat capacity; arbitrarily set. For fluids very near the critical point, this value can be obscenely high.

## property\_min = 1

Allow very low heat capacities; arbitrarily set; liquid heat capacity should always be somewhat substantial.

```
ranked_methods = ['LALIBERTE', 'LINEAR']
```

## test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

## Parameters

T [float] Temperature at which to check method validity, [K]

**P** [float] Pressure at which to check method validity, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

## Returns

validity [bool] Whether or not a specifid method is valid

```
units = 'J/mol'
```

```
thermo.heat_capacity.heat_capacity_liquid_mixture_methods = ['LALIBERTE', 'LINEAR']
Holds all methods available for the HeatCapacityLiquidMixture class, for use in iterating over them.
```

# 7.15.5 Mixture Gas Heat Capacity

```
class thermo.heat_capacity.HeatCapacityGasMixture(CASs=[], HeatCapacityGases=[], MWs=[])
Bases: thermo.utils.mixture_property.MixtureProperty
```

Class for dealing with the gas heat capacity of a mixture as a function of temperature, pressure, and composition. Consists only of mole weighted averaging.

## Parameters

CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]

**HeatCapacityGases** [list[HeatCapacityGas], optional] HeatCapacityGas objects created for all species in the mixture [-]

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

## Notes

To iterate over all methods, use the list stored in heat\_capacity\_gas\_mixture\_methods.

LINEAR: Mixing rule described in mixing\_simple.

## **Methods**

calculate(T, P, zs, ws, method)	Method to calculate heat capacity of a gas mixture at temperature $T$ , pressure $P$ , mole fractions $zs$ and weight fractions $ws$ with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for the given conditions.

## Tmax

Maximum temperature at which no method can calculate the heat capacity above.

#### Tmin

Minimum temperature at which no method can calculate the heat capacity under.

## calculate(T, P, zs, ws, method)

Method to calculate heat capacity of a gas mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

## Parameters

T [float] Temperature at which to calculate the property, [K]

**P** [float] Pressure at which to calculate the property, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

## Returns

Cpgm [float] Molar heat capacity of the gas mixture at the given conditions, [J/mol]

## name = 'Gas heat capacity'

## property\_max = 10000.0

Maximum valid of Heat capacity; arbitrarily set. For fluids very near the critical point, this value can be obscenely high.

## property\_min = 0

Heat capacities have a minimum value of 0 at 0 K.

## ranked\_methods = ['LINEAR']

## test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

#### **Parameters**

- T [float] Temperature at which to check method validity, [K]
- **P** [float] Pressure at which to check method validity, [Pa]

**zs** [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

Returns

validity [bool] Whether or not a specifid method is valid

units = 'J/mol'

thermo.heat\_capacity.heat\_capacity\_gas\_mixture\_methods = ['LINEAR']

Holds all methods available for the HeatCapacityGasMixture class, for use in iterating over them.

# 7.15.6 Mixture Solid Heat Capacity

```
class thermo.heat_capacity.HeatCapacitySolidMixture(CASs=[], HeatCapacitySolids=[], MWs=[])
Bases: thermo.utils.mixture_property.MixtureProperty
```

Class for dealing with solid heat capacity of a mixture as a function of temperature, pressure, and composition. Consists only of mole weighted averaging.

## Parameters

CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]

**HeatCapacitySolids** [list[HeatCapacitySolid], optional] HeatCapacitySolid objects created for all species in the mixture [-]

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

## Notes

To iterate over all methods, use the list stored in heat\_capacity\_solid\_mixture\_methods.

LINEAR: Mixing rule described in mixing\_simple.

## Methods

calculate(T, P, zs, ws, method)	Method to calculate heat capacity of a solid mixture
	at temperature T, pressure P, mole fractions zs and
	weight fractions ws with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for
	the given conditions.

#### Tmax

Maximum temperature at which no method can calculate the heat capacity above.

## Tmin

Minimum temperature at which no method can calculate the heat capacity under.

## calculate(T, P, zs, ws, method)

Method to calculate heat capacity of a solid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

#### **Parameters**

- **T** [float] Temperature at which to calculate the property, [K]
- **P** [float] Pressure at which to calculate the property, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

## Returns

Cpsm [float] Molar heat capacity of the solid mixture at the given conditions, [J/mol]

#### name = 'Solid heat capacity'

## property\_max = 10000.0

Maximum value of Heat capacity; arbitrarily set.

#### property\_min = 0

Heat capacities have a minimum value of 0 at 0 K.

#### ranked\_methods = ['LINEAR']

## test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

## Parameters

- T [float] Temperature at which to check method validity, [K]
- P [float] Pressure at which to check method validity, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

## units = 'J/mol'

## thermo.heat\_capacity.heat\_capacity\_solid\_mixture\_methods = ['LINEAR']

Holds all methods available for the HeatCapacitySolidMixture class, for use in iterating over them.

# 7.16 Interfacial/Surface Tension (thermo.interface)

This module contains implementations of *TDependentProperty* representing liquid-air surface tension. A variety of estimation and data methods are available as included in the *chemicals* library. Additionally a liquid mixture surface tension predictor objects are implemented subclassing *MixtureProperty*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Pure Liquid Surface Tension
- Mixture Liquid Heat Capacity

# 7.16.1 Pure Liquid Surface Tension

**class** thermo.interface.**SurfaceTension**(*MW*=*None*, *Tb*=*None*, *Tc*=*None*, *Vc*=*None*, *Zc*=*None*, *Zc*=*None*,

omega=None, StielPolar=None, Hvap\_Tb=None, CASRN=",

Vml=None, Cpl=None, extrapolation='DIPPR106\_AB', \*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with surface tension as a function of temperature. Consists of three coefficient-based methods and four data sources, one source of tabular information, five corresponding-states estimators, and one substance-specific method.

## Parameters

**Tb** [float, optional] Boiling point, [K]

MW [float, optional] Molecular weight, [g/mol]

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

Vc [float, optional] Critical volume, [m^3/mol]

Zc [float, optional] Critical compressibility

omega [float, optional] Acentric factor, [-]

StielPolar [float, optional] Stiel polar factor

Hvap\_Tb [float] Mass enthalpy of vaporization at the normal boiling point [kg/m^3]

CASRN [str, optional] The CAS number of the chemical

- Vml [float or callable, optional] Liquid molar volume at a given temperature and pressure or callable for the same, [m<sup>3</sup>/mol]
- **Cpl** [float or callable, optional] Molar heat capacity of the fluid at a pressure and temperature or or callable for the same, [J/mol/K]
- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

## See also:

chemicals.interface.REFPROP\_sigma

chemicals.interface.Somayajulu

chemicals.interface.Jasper

chemicals.interface.Brock\_Bird

chemicals.interface.Sastri\_Rao

## chemicals.interface.Pitzer

chemicals.interface.Zuo\_Stenby

- chemicals.interface.Miqueu
- chemicals.interface.Aleem

chemicals.interface.sigma\_IAPWS

## Notes

To iterate over all methods, use the list stored in *surface\_tension\_methods*.

- \*IAPWS: The IAPWS formulation for water, REFPROP\_sigma
- **STREFPROP:** The REFPROP coefficient-based method, documented in the function REFPROP\_sigma for 115 fluids from [5].
- **SOMAYAJULU and SOMAYAJULU2:** The Somayajulu coefficient-based method, documented in the function Somayajulu. Both methods have data for 64 fluids. The first data set if from [1], and the second from [2]. The later, revised coefficients should be used prefered.
- **JASPER:** Fit with a single temperature coefficient from Jaspen (1972) as documented in the function Jasper. Data for 522 fluids is available, as shown in [4] but originally in [3].
- BROCK\_BIRD: CSP method documented in Brock\_Bird. Most popular estimation method; from 1955.
- SASTRI\_RAO: CSP method documented in Sastri\_Rao. Second most popular estimation method; from 1995.
- PITZER: CSP method documented in Pitzer\_sigma; from 1958.

**ZUO\_STENBY:** CSP method documented in Zuo\_Stenby; from 1997.

MIQUEU: CSP method documented in Miqueu.

ALEEM: CSP method documented in Aleem.

VDI\_TABULAR: Tabular data in [6] along the saturation curve; interpolation is as set by the user or the default.

## References

[1], [2], [3], [4], [5], [6]

## **Methods**

calculate(T, method)	Method to calculate surface tension of a liquid at tem	
	perature $T$ with a given method.	
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.	

#### calculate(T, method)

Method to calculate surface tension of a liquid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

## Parameters

T [float] Temperature at which to calculate surface tension, [K]

method [str] Name of the method to use

#### Returns

sigma [float] Surface tension of the liquid at T, [N/m]

name = 'Surface tension'

## property\_max = 4.0

Maximum valid value of surface tension. Set to roughly twice that of cobalt at its melting point.

## property\_min = 0

Mimimum valid value of surface tension. This occurs at the critical point exactly.

```
ranked_methods = ['IAPWS', 'REFPROP', 'SOMAYAJULU2', 'SOMAYAJULU', 'VDI_PPDS',
'VDI_TABULAR', 'JASPER', 'MIQUEU', 'BROCK_BIRD', 'SASTRI_RAO', 'PITZER',
'ZUO_STENBY', 'Aleem']
```

Default rankings of the available methods.

## test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For CSP methods, the models are considered valid from 0 K to the critical point. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### Parameters

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

#### Returns

validity [bool] Whether or not a method is valid

units = 'N/m'

```
thermo.interface.surface_tension_methods = ['IAPWS', 'REFPROP', 'SOMAYAJULU2',
'SOMAYAJULU', 'VDI_PPDS', 'VDI_TABULAR', 'JASPER', 'MIQUEU', 'BROCK_BIRD', 'SASTRI_RAO',
'PITZER', 'ZUO_STENBY', 'Aleem']
```

Holds all methods available for the SurfaceTension class, for use in iterating over them.

# 7.16.2 Mixture Liquid Heat Capacity

## class thermo.interface.SurfaceTensionMixture(MWs=[], Tbs=[], Tcs=[], CASs=[], SurfaceTensions=[], VolumeLiquids=[], \*\*kwargs)

Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with surface tension of a mixture as a function of temperature, pressure, and composition. Consists of two mixing rules specific to surface tension, and mole weighted averaging.

Prefered method is Winterfeld\_Scriven\_Davis which requires mole fractions, pure component surface tensions, and the molar density of each pure component. Diguilio\_Teja is of similar accuracy, but requires the surface tensions of pure components at their boiling points, as well as boiling points and critical points and mole fractions. An ideal mixing rule based on mole fractions, **LINEAR**, is also available and is still relatively accurate.

## Parameters

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

Tbs [list[float], optional] Boiling points of all species in the mixture, [K]

Tcs [list[float], optional] Critical temperatures of all species in the mixture, [K]

CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]

**SurfaceTensions** [list[SurfaceTension], optional] SurfaceTension objects created for all species in the mixture [-]

- **VolumeLiquids** [list[VolumeLiquid], optional] VolumeLiquid objects created for all species in the mixture [-]
- **correct\_pressure\_pure** [bool, optional] Whether to try to use the better pressure-corrected pure component models or to use only the T-only dependent pure species models, [-]

## See also:

chemicals.interface.Winterfeld\_Scriven\_Davis
chemicals.interface.Diguilio\_Teja

## Notes

To iterate over all methods, use the list stored in *surface\_tension\_mixture\_methods*.

WINTERFELDSCRIVENDAVIS: Mixing rule described in Winterfeld\_Scriven\_Davis.

**DIGUILIOTEJA:** Mixing rule described in Diguilio\_Teja.

LINEAR: Mixing rule described in mixing\_simple.

## References

[1]

## Methods

calculate(T, P, zs, ws, method)	Method to calculate surface tension of a liquid mix-
	ture at temperature $T$ , pressure $P$ , mole fractions $zs$
	and weight fractions ws with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for
	the given conditions.

## Tmax

Maximum temperature at which no method can calculate the property above.

Tmin

Minimum temperature at which no method can calculate the property under.

## calculate(T, P, zs, ws, method)

Method to calculate surface tension of a liquid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

## Parameters

T [float] Temperature at which to calculate the property, [K]

P [float] Pressure at which to calculate the property, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

## Returns

sigma [float] Surface tension of the liquid at given conditions, [N/m]

```
name = 'Surface tension'
```

## property\_max = 4.0

Maximum valid value of surface tension. Set to roughly twice that of cobalt at its melting point.

## property\_min = 0

Mimimum valid value of surface tension. This occurs at the critical point exactly.

```
ranked_methods = ['Winterfeld, Scriven, and Davis (1978)', 'Diguilio and Teja
(1988)', 'LINEAR']
```

## test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

## Parameters

T [float] Temperature at which to check method validity, [K]

P [float] Pressure at which to check method validity, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

Returns

validity [bool] Whether or not a specifid method is valid

units = 'N/m'

# thermo.interface.surface\_tension\_mixture\_methods = ['Winterfeld, Scriven, and Davis (1978)', 'Diguilio and Teja (1988)', 'LINEAR']

Holds all methods available for the SurfaceTensionMixture class, for use in iterating over them.

# 7.17 Interaction Parameters (thermo.interaction\_parameters)

This module contains a small database of interaction parameters. Only two data sets are currently included, both from ChemSep. If you would like to add parameters to this project please make a referenced compilation of values and submit them on GitHub.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

## class thermo.interaction\_parameters.InteractionParameterDB

Basic database framework for interaction parameters.

## Methods

<pre>get_ip_asymmetric_matrix(name, CASs, ip[,</pre>	Get a table of interaction parameters from a specified
T])	source for the specified parameters.
<pre>get_ip_automatic(CASs, ip_type, ip)</pre>	Get an interaction parameter for the first table con-
	taining the value.
<pre>get_ip_specific(name, CASs, ip)</pre>	Get an interaction parameter from a table.
	continues on next page

	1 10
<pre>get_ip_symmetric_matrix(name, CASs, ip[, T])</pre>	Get a table of interaction parameters from a specified
	source for the specified parameters.
<pre>get_tables_with_type(ip_type)</pre>	Get a list of tables which have a type of a parameter.
<pre>has_ip_specific(name, CASs, ip)</pre>	Check if a bip exists in a table.
load_json(file, name)	Load a json file from disk containing interaction co-
	efficients.
validate_table(name)	Basic method which checks that all CAS numbers are
	valid, and that all elements of the data have non-nan
	values.

Table 75 – continued from previous page

## get\_ip\_asymmetric\_matrix(name, CASs, ip, T=298.15)

Get a table of interaction parameters from a specified source for the specified parameters.

## Parameters

name [str] Name of the data table, [-]

CASs [Iterable[str]] CAS numbers; they do not need to be sorted, [-]

ip [str] Name of the parameter to retrieve, [-]

T [float, optional] Temperature of the system, [-]

## Returns

values [list[list[float]]] Interaction parameters specified by *ip*, [-]

## **Examples**

## get\_ip\_automatic(CASs, ip\_type, ip)

Get an interaction parameter for the first table containing the value.

## Parameters

CASs [Iterable[str]] CAS numbers; they do not need to be sorted, [-]

ip\_type [str] Name of the parameter type, [-]

ip [str] Name of the parameter to retrieve, [-]

## Returns

value [float] Interaction parameter specified by ip, [-]

## **Examples**

## get\_ip\_specific(name, CASs, ip)

Get an interaction parameter from a table. If the specified parameter is missing, the default *missing* value as defined in the data file is returned instead.

## **Parameters**

name [str] Name of the data table, [-]

CASs [Iterable[str]] CAS numbers; they do not need to be sorted, [-]

ip [str] Name of the parameter to retrieve, [-]

## Returns

value [float] Interaction parameter specified by ip, [-]

## **Examples**

Check if nitrogen-ethane as a PR BIP:

```
>>> from thermo.interaction_parameters import IPDB
>>> IPDB.get_ip_specific('ChemSep PR', ['7727-37-9', '74-84-0'], 'kij')
0.0533
```

## get\_ip\_symmetric\_matrix(name, CASs, ip, T=298.15)

Get a table of interaction parameters from a specified source for the specified parameters. This method assumes symmetric parameters for speed.

## Parameters

name [str] Name of the data table, [-]

CASs [Iterable[str]] CAS numbers; they do not need to be sorted, [-]

ip [str] Name of the parameter to retrieve, [-]

T [float, optional] Temperature of the system, [-]

## Returns

values [list[float]]] Interaction parameters specified by *ip*, [-]

## **Examples**

```
>>> from thermo.interaction_parameters import IPDB
>>> IPDB.get_ip_symmetric_matrix(name='ChemSep PR', CASs=['7727-37-9', '74-84-0
\[intersection], ip='kij')
[[0.0, 0.0533, 0.0878], [0.0533, 0.0, 0.0011], [0.0878, 0.0011, 0.0]]
```

#### get\_tables\_with\_type(ip\_type)

Get a list of tables which have a type of a parameter.

Parameters

ip\_type [str] Name of the parameter type, [-]

Returns

table\_names [list[str]] Interaction parameter tables including ip, [-]

## **Examples**

```
>>> from thermo.interaction_parameters import IPDB
>>> IPDB.get_tables_with_type('PR kij')
['ChemSep PR']
```

## has\_ip\_specific(name, CASs, ip)

Check if a bip exists in a table.

## **Parameters**

name [str] Name of the data table, [-]

CASs [Iterable[str]] CAS numbers; they do not need to be sorted, [-]

ip [str] Name of the parameter to retrieve, [-]

### Returns

present [bool] Whether or not the data is included in the table, [-]

#### **Examples**

Check if nitrogen-ethane as a PR BIP:

```
>>> from thermo.interaction_parameters import IPDB
>>> IPDB.has_ip_specific('ChemSep PR', ['7727-37-9', '74-84-0'], 'kij')
True
```

#### load\_json(file, name)

Load a json file from disk containing interaction coefficients.

The format for the file is as follows:

A data key containing a dictionary with a key:

- *CAS1 CAS2* [str] The CAS numbers of both components, sorted from small to high as integers; they should have the '-' symbols still in them and have a single space between them; if these are ternary or higher parameters, follow the same format for the other CAS numbers, [-]
- values [dict[str][various]] All of the values listed in the metadata element *necessary keys*; they are None if missing.

A metadata key containing:

- symmetric [bool] Whether or not the interaction coefficients are missing.
- *source* [str] Where the data came from.
- *components* [int] The number of components each interaction parameter is for; 2 for binary, 3 for ternary, etc.
- necessary keys [list[str]] Which elements are required in the data.

- *P dependent* [bool] Whether or not the interaction parameters are pressure dependent.
- *missing* [dict[str][float]] Values which are missing are returned with these values
- type [One of 'PR kij', 'SRK kij', etc; used to group data but not] tied into anything else.
- *T dependent* [bool] Whether or not the data is T-dependent.

## **Parameters**

file [str] Path to json file on disk which contains interaction coefficients, [-]

name [str] Name that the data read should be referred to by, [-]

## validate\_table(name)

Basic method which checks that all CAS numbers are valid, and that all elements of the data have non-nan values. Raises an exception if any of the data is missing or is a nan value.

#### thermo.interaction\_parameters.IPDB =

#### <thermo.interaction\_parameters.InteractionParameterDB object>

Basic database framework for interaction parameters.

Exmple database with NRTL and PR values from ChemSep. This is lazy-loaded, access it as *thermo.interaction\_parameters.IPDB*.

## class thermo.interaction\_parameters.ScalarParameterDB

Basic database framework for scalar parameters of various thermodynamic models. The following keys are used:

#### **Peng-Robinson**

Twu Volume-translated Peng-Robinson: TwuPRL, TwuPRM, TwuPRN, TwuPRc

Volume-translated Peng-Robinson: PRc

Peng-Robinson-Stryjek-Vera: PRSVkappa1

Peng-Robinson-Stryjek-Vera 2: PRSV2kappa1, PRSV2kappa2, PRSV2kappa3

## SRK

Twu Volume-translated Peng-Robinson: TwuSRKL, TwuSRKM, TwuSRKN, TwuSRKC

Volume-translated Peng-Robinson: SRKc

Refinery Soave-Redlich-Kwong: APISRKS1, APISRKS2

MSRK: MSRKM, MSRKN, MSRKc

Predictive Soave-Redlich-Kwong: MCSRKC1, MCSRKC2, MCSRKC3

## **Excess Gibbs Energy Models**

Regular Solution: RegularSolutionV, RegularSolutionSP

## **Methods**

<pre>get_parameter_automatic(CAS, parameter)</pre>	Get an interaction parameter for the first table con- taining the value.
<pre>get_parameter_specific(name, CAS, parame- ter)</pre>	Get a parameter from a table.
get_parameter_vector(name, CASs, parameter)	Get a list of parameters from a specified source for the specified parameter.
<pre>get_tables_with_type(parameter)</pre>	Get a list of tables which have a parameter.
<pre>has_parameter_specific(name, CAS, parame- ter)</pre>	Check if a parameter exists in a table.

load\_json

#### SPDB

Example scalar parameters for models. This is lazy-loaded, access it as *thermo.interaction\_parameters.SPDB*.

# 7.18 Legal and Economic Chemical Data (thermo.law)

## thermo.law.economic\_status(CASRN, method=None, get\_methods=False) Look up the economic status of a chemical.

This API is considered experimental, and is expected to be removed in a future release in favor of a more complete object-oriented interface.

thermo.law.legal\_status(CASRN, method=None, get\_methods=False, CASi=None)

Looks up the legal status of a chemical according to either a specifc method or with all methods.

Returns either the status as a string for a specified method, or the status of the chemical in all available data sources, in the format {source: status}.

Parameters

```
CASRN [string] CASRN [-]
```

#### Returns

status [str or dict] Legal status information [-]

**methods** [list, only returned if get\_methods == True] List of methods which can be used to obtain legal status with the given inputs

## **Other Parameters**

- **method** [string, optional] A string for the method name to use, as defined by constants in legal\_status\_methods
- **get\_methods** [bool, optional] If True, function will determine which methods can be used to obtain the legal status for the desired chemical, and will return methods instead of the status

CASi [int, optional] CASRN as an integer, used internally [-]

## Notes

Supported methods are:

- **DSL**: Canada Domestic Substance List, [1]. As extracted on Feb 11, 2015 from a html list. This list is updated continuously, so this version will always be somewhat old. Strictly speaking, there are multiple lists but they are all bundled together here. A chemical may be 'Listed', or be on the 'Non-Domestic Substances List (NDSL)', or be on the list of substances with 'Significant New Activity (SNAc)', or be on the DSL but with a 'Ministerial Condition pertaining to this substance', or have been removed from the DSL, or have had a Ministerial prohibition for the substance.
- **TSCA**: USA EPA Toxic Substances Control Act Chemical Inventory, [2]. This list is as extracted on 2016-01. It is believed this list is updated on a periodic basis (> 6 month). A chemical may simply be 'Listed', or may have certain flags attached to it. All these flags are described in the dict TSCA\_flags.
- **EINECS**: European INventory of Existing Commercial chemical Substances, [3]. As extracted from a spreadsheet dynamically generated at [1]. This list was obtained March 2015; a more recent revision already exists.
- NLP: No Longer Polymers, a list of chemicals with special regulatory exemptions in EINECS. Also described at [3].
- SPIN: Substances Prepared in Nordic Countries. Also a boolean data type. Retrieved 2015-03 from [4].

Other methods which could be added are:

- Australia: AICS Australian Inventory of Chemical Substances
- China: Inventory of Existing Chemical Substances Produced or Imported in China (IECSC)
- Europe: REACH List of Registered Substances
- India: List of Hazardous Chemicals
- Japan: ENCS: Inventory of existing and new chemical substances
- Korea: Existing Chemicals Inventory (KECI)
- Mexico: INSQ National Inventory of Chemical Substances in Mexico
- New Zealand: Inventory of Chemicals (NZIoC)
- Philippines: PICCS Philippines Inventory of Chemicals and Chemical Substances

#### References

[1], [2], [3], [4]

## **Examples**

## thermo.law.load\_economic\_data()

thermo.law.load\_law\_data()

# 7.19 NRTL Gibbs Excess Model (thermo.nrtl)

This module contains a class *NRTL* for performing activity coefficient calculations with the NRTL model. An older, functional calculation for activity coefficients only is also present, *NRTL\_gammas*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- NRTL Class
- NRTL Functional Calculations
- NRTL Regression Calculations

# 7.19.1 NRTL Class

class thermo.nrtl.NRTL(T, xs, tau\_coeffs=None, alpha\_coeffs=None, ABEFGHCD=None, tau\_as=None, tau\_bs=None, tau\_es=None, tau\_fs=None, tau\_gs=None, tau\_hs=None, alpha\_cs=None, alpha\_ds=None)

Bases: thermo.activity.GibbsExcess

Class for representing an a liquid with excess gibbs energy represented by the NRTL equation. This model is capable of representing VL and LL behavior. [1] and [2] are good references on this model.

$$g^{E} = RT \sum_{i} x_{i} \frac{\sum_{j} \tau_{ji} G_{ji} x_{j}}{\sum_{j} G_{ji} x_{j}}$$
$$G_{ij} = \exp(-\alpha_{ij} \tau_{ij})$$
$$\alpha_{ij} = c_{ij} + d_{ij}T$$
$$\tau_{ij} = A_{ij} + \frac{B_{ij}}{T} + E_{ij} \ln T + F_{ij}T + \frac{G_{ij}}{T^{2}} + H_{ij}T^{2}$$

#### **Parameters**

- T [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]

- **tau\_coeffs** [list[list[float]]], optional] NRTL parameters, indexed by [i][j] and then each value is a 6 element list with parameters [*a*, *b*, *e*, *f*, *g*, *h*]; either (*tau\_coeffs* and *alpha\_coeffs*) or *ABEFGHCD* are required, [-]
- alpha\_coeffs [list[float]], optional] NRTL alpha parameters, []
- **ABEFGHCD** [tuple[list[list[float]], 8], optional] Contains the following. One of (*tau\_coeffs* and *alpha\_coeffs*) or *ABEFGHCD* or some of the *tau* or *alpha* parameters are required, [-]
- tau\_as [list[list[float]], optional] a parameters used in calculating NRTL.taus, [-]
- tau\_bs [list[list[float]], optional] b parameters used in calculating NRTL.taus, [K]
- tau\_es [list[list[float]], optional] e parameters used in calculating NRTL.taus, [-]
- tau\_fs [list[list[float]], optional] f paraemeters used in calculating NRTL.taus, [1/K]
- tau\_gs [list[list[float]], optional] e parameters used in calculating NRTL.taus, [K^2]
- tau\_hs [list[list[float]], optional] f parameters used in calculating NRTL.taus, [1/K^2]
- alpha\_cs [list[list[float]], optional] c parameters used in calculating NRTL.alphas, [-]
- alpha\_ds [list[list[float]], optional] d paraemeters used in calculating NRTL.alphas, [1/K]

## Notes

In addition to the methods presented here, the methods of its base class thermo.activity.GibbsExcess are available as well.

## References

[1], [2]

#### **Examples**

The DDBST has published numerous problems showing this model a simple binary system, Example P05.01b in [2], shows how to use parameters from the DDBST which are in units of calorie and need the gas constant as a multiplier:

```
>>> from scipy.constants import calorie, R
>>> N = 2
>>> T = 70.0 + 273.15
>>> xs = [0.252, 0.748]
>>> tausA = tausE = tausF = tausG = tausH = alphaD = [[0.0]*N for i in range(N)]
>>> tausB = [[0, -121.2691/R*calorie], [1337.8574/R*calorie, 0]]
>>> alphaC = [[0, 0.2974],[.2974, 0]]
>>> ABEFGHCD = (tausA, tausB, tausE, tausF, tausG, tausH, alphaC, alphaD)
>>> GE = NRTL(T=T, xs=xs, ABEFGHCD=ABEFGHCD)
>>> GE.gammas()
[1.93605165145, 1.15366304520]
>>> GE
NRTL(T=343.15, xs=[0.252, 0.748], tau_bs=[[0, -61.0249799309399], [673.
→2359767282798, 0]], alpha_cs=[[0, 0.2974], [0.2974, 0]])
>>> GE_GE(), GE_dGE_dT(), GE_d2GE_dT2()
(780.053057219, 0.5743500022, -0.003584843605528)
```

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```
>>> GE.HE(), GE.SE(), GE.dHE_dT(), GE.dSE_dT()
(582.964853938, -0.57435000227, 1.230139083237, 0.0035848436055)
```

The solution given by the DDBST has the same values [1.936, 1.154], and can be found here: http://chemthermo.ddbst.com/Problems\_Solutions/Mathcad\_Files/P05.01b%20VLE%20Behavior%20of% 20Ethanol%20-%20Water%20Using%20NRTL.xps

## Attributes

- T [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]

## Methods

	Calculate and return the excess Gibbs energy of a liq-
	uid phase represented by the NRTL model.
Gs()	Calculates and return the <i>G</i> terms in the NRTL model
05()	for a specified temperature.
alphac()	<u> </u>
alphas()	Calculates and return the <i>alpha</i> terms in the NRTL
	model for a specified temperature.
d2GE_dT2()	Calculate and return the second tempreature deriva-
	tive of excess Gibbs energy of a liquid phase repre-
	sented by the NRTL model.
d2GE_dTdxs()	Calculate and return the temperature derivative of
	mole fraction derivatives of excess Gibbs energy of
	a liquid represented by the NRTL model.
d2GE_dxixjs()	Calculate and return the second mole fraction deriva-
	tives of excess Gibbs energy of a liquid represented
	by the NRTL model.
d2Gs_dT2()	Calculates and return the second temperature deriva-
	tive of G terms in the NRTL model for a specified
	temperature.
d2taus_dT2()	Calculate and return the second temperature deriva-
	tive of the tau terms for the NRTL model for a spec-
	ified temperature.
d3Gs_dT3()	Calculates and return the third temperature derivative
	of G terms in the NRTL model for a specified tem-
	perature.
d3taus_dT3()	Calculate and return the third temperature derivative
	of the <i>tau</i> terms for the NRTL model for a specified
	temperature.
dGE_dT()	Calculate and return the first tempreature derivative
	of excess Gibbs energy of a liquid phase represented
	by the NRTL model.
dGE_dxs()	Calculate and return the mole fraction derivatives of
~	excess Gibbs energy of a liquid represented by the
	NRTL model.
dGs_dT()	Calculates and return the first temperature derivative
~	of G terms in the NRTL model for a specified tem-
	perature.
	continues on next page

Table 11 continued norm previous page	
dtaus_dT()	Calculate and return the temperature derivative of the
	tau terms for the NRTL model for a specified temper-
	ature.
taus()	Calculate and return the <i>tau</i> terms for the NRTL
	model for a specified temperature.
<i>to_T_xs</i> (T, xs)	Method to construct a new NRTL instance at temper-
	ature T, and mole fractions xs with the same param-
	eters as the existing object.

Table	77 - continued from	previous page
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## **to\_T\_xs**(*T*, *xs*)

Method to construct a new NRTL instance at temperature T, and mole fractions xs with the same parameters as the existing object.

#### **Parameters**

T [float] Temperature, [K]

xs [list[float]] Mole fractions of each component, [-]

## Returns

obj [NRTL] New NRTL object at the specified conditions [-]

## Notes

If the new temperature is the same temperature as the existing temperature, if the *tau*, *Gs*, or *alphas* terms or their derivatives have been calculated, they will be set to the new object as well.

## taus()

Calculate and return the tau terms for the NRTL model for a specified temperature.

$$\tau_{ij} = A_{ij} + \frac{B_{ij}}{T} + E_{ij} \ln T + F_{ij}T + \frac{G_{ij}}{T^2} + H_{ij}T^2$$

Returns

taus [list[list[float]]] tau terms, asymmetric matrix [-]

## Notes

These tau ij values (and the coefficients) are NOT symmetric.

## dtaus\_dT()

Calculate and return the temperature derivative of the *tau* terms for the NRTL model for a specified temperature.

$$\frac{\partial \tau_{ij}}{\partial T}_{P,x_i} = -\frac{B_{ij}}{T^2} + \frac{E_{ij}}{T} + F_{ij} - \frac{2G_{ij}}{T^3} + 2H_{ij}T$$

Returns

**dtaus\_dT** [list[list[float]]] First temperature derivative of tau terms, asymmetric matrix [1/K]

## d2taus\_dT2()

Calculate and return the second temperature derivative of the *tau* terms for the NRTL model for a specified temperature.

$$\frac{\partial^2 \tau_{ij}}{\partial T^2}_{P,x_i} = \frac{2B_{ij}}{T^3} - \frac{E_{ij}}{T^2} + \frac{6G_{ij}}{T^4} + 2H_{ij}$$

#### Returns

**d2taus\_dT2** [list[list[float]]] Second temperature derivative of tau terms, asymmetric matrix [1/K^2]

d3taus\_dT3()

Calculate and return the third temperature derivative of the *tau* terms for the NRTL model for a specified temperature.

$$\frac{\partial^3 \tau_{ij}}{\partial T^3}_{P,x_i} = -\frac{6B_{ij}}{T^4} + \frac{2E_{ij}}{T^3} - \frac{24G_{ij}}{T^5}$$

#### Returns

**d3taus\_dT3** [list[list[float]]] Third temperature derivative of tau terms, asymmetric matrix [1/K^3]

## alphas()

Calculates and return the *alpha* terms in the NRTL model for a specified temperature.

$$\alpha_{ij} = c_{ij} + d_{ij}T$$

#### Returns

alphas [list[list[float]]] alpha terms, possibly asymmetric matrix [-]

#### Notes

alpha values (and therefore *cij* and *dij* are normally symmetrical; but this is not strictly required.

Some sources suggest the c term should be fit to a given system; but the d term should be fit for an entire chemical family to avoid overfitting.

Recommended values for *cij* according to one source are:

0.30 Nonpolar substances with nonpolar substances; low deviation from ideality. 0.20 Hydrocarbons that are saturated interacting with polar liquids that do not associate, or systems that for multiple liquid phases which are immiscible 0.47 Strongly self associative systems, interacting with non-polar substances

alpha\_coeffs should be a list[list[cij, dij]] so a 3d array

## Gs()

Calculates and return the G terms in the NRTL model for a specified temperature.

$$G_{ij} = \exp(-\alpha_{ij}\tau_{ij})$$

#### Returns

**Gs** [list[list[float]]] G terms, asymmetric matrix [-]

## dGs\_dT()

Calculates and return the first temperature derivative of G terms in the NRTL model for a specified temperature.

$$\frac{\partial G_{ij}}{\partial T} = \left(-\alpha(T)\frac{d}{dT}\tau(T) - \tau(T)\frac{d}{dT}\alpha(T)\right)e^{-\alpha(T)\tau(T)}$$

Returns

dGs\_dT [list[list[float]]] Temperature derivative of G terms, asymmetric matrix [1/K]

## Notes

Derived with SymPy:

```
>>> from sympy import *
>>> T = symbols('T')
>>> alpha, tau = symbols('alpha, tau', cls=Function)
>>> diff(exp(-alpha(T)*tau(T)), T)
```

## $d2Gs_dT2()$

Calculates and return the second temperature derivative of G terms in the NRTL model for a specified temperature.

$$\frac{\partial^2 G_{ij}}{\partial T^2} = \left( \left( \alpha(T) \frac{d}{dT} \tau(T) + \tau(T) \frac{d}{dT} \alpha(T) \right)^2 - \alpha(T) \frac{d^2}{dT^2} \tau(T) - 2 \frac{d}{dT} \alpha(T) \frac{d}{dT} \tau(T) \right) e^{-\alpha(T)\tau(T)} dT$$

Returns

**d2Gs\_dT2** [list[list[float]]] Second temperature derivative of G terms, asymmetric matrix [1/K^2]

## Notes

Derived with SymPy:

```
>>> from sympy import *
>>> T = symbols('T')
>>> alpha, tau = symbols('alpha, tau', cls=Function)
>>> diff(exp(-alpha(T)*tau(T)), T, 2)
```

## d3Gs\_dT3()

Calculates and return the third temperature derivative of *G* terms in the NRTL model for a specified temperature.

$$\frac{\partial^3 G_{ij}}{\partial T^3} = \left(\alpha(T)\frac{d}{dT}\tau(T) + \tau(T)\frac{d}{dT}\alpha(T)\right)^3 + \left(3\alpha(T)\frac{d}{dT}\tau(T) + 3\tau(T)\frac{d}{dT}\alpha(T)\right)\left(\alpha(T)\frac{d^2}{dT^2}\tau(T) + 2\frac{d}{dT}\alpha(T)\frac{d}{dT}\tau(T)\right)^3 + \left(3\alpha(T)\frac{d}{dT}\tau(T) + 3\tau(T)\frac{d}{dT}\alpha(T)\right)\left(\alpha(T)\frac{d}{dT}\tau(T) + 2\frac{d}{dT}\alpha(T)\frac{d}{dT}\tau(T)\right)^3 + \left(3\alpha(T)\frac{d}{dT}\tau(T) + 3\tau(T)\frac{d}{dT}\alpha(T)\right)\left(\alpha(T)\frac{d}{dT}\tau(T) + 2\frac{d}{dT}\alpha(T)\frac{d}{dT}\tau(T)\right)^3 + \left(3\alpha(T)\frac{d}{dT}\tau(T) + 3\tau(T)\frac{d}{dT}\tau(T)\right)^3 + \left(3\alpha(T)\frac{d}{dT}\tau(T)\right)^3 + \left(3\alpha(T)\frac{d}{dT}\tau(T)\right)$$

Returns

**d3Gs\_dT3** [list[list[float]]] Third temperature derivative of G terms, asymmetric matrix [1/K^3]

## Notes

Derived with SymPy:

```
>>> from sympy import *
>>> T = symbols('T')
>>> alpha, tau = symbols('alpha, tau', cls=Function)
>>> diff(exp(-alpha(T)*tau(T)), T, 3)
```

GE()

Calculate and return the excess Gibbs energy of a liquid phase represented by the NRTL model.

$$g^E = RT \sum_i x_i \frac{\sum_j \tau_{ji} G_{ji} x_j}{\sum_j G_{ji} x_j}$$

#### Returns

GE [float] Excess Gibbs energy, [J/mol]

## $dGE_dT()$

Calculate and return the first tempreature derivative of excess Gibbs energy of a liquid phase represented by the NRTL model.

Returns

**dGE\_dT** [float] First temperature derivative of excess Gibbs energy, [J/(mol\*K)]

## $d2GE_dT2()$

Calculate and return the second tempreature derivative of excess Gibbs energy of a liquid phase represented by the NRTL model.

#### Returns

d2GE\_dT2 [float] Second temperature derivative of excess Gibbs energy, [J/(mol\*K^2)]

## dGE\_dxs()

Calculate and return the mole fraction derivatives of excess Gibbs energy of a liquid represented by the NRTL model.

$$\frac{\partial g^E}{\partial x_i}$$

## Returns

dGE\_dxs [list[float]] Mole fraction derivatives of excess Gibbs energy, [J/mol]

## d2GE\_dxixjs()

Calculate and return the second mole fraction derivatives of excess Gibbs energy of a liquid represented by the NRTL model.

$$\frac{\partial^2 g^E}{\partial x_i \partial x_j} = RT \left[ + \frac{G_{ij} \tau_{ij}}{\sum_m x_m G_{mj}} + \frac{G_{ji} \tau_{jiij}}{\sum_m x_m G_{mi}} - \frac{(\sum_m x_m G_{mj} \tau_{mj})G_{ij}}{(\sum_m x_m G_{mj})^2} - \frac{(\sum_m x_m G_{mi} \tau_{mi})G_{ji}}{(\sum_m x_m G_{mi})^2} \sum_k \left( \frac{2x_k (\sum_m x_m \tau_{mi}) G_{ji}}{(\sum_m x_m T_{mi})^2} - \frac{(\sum_m x_m G_{mi} \tau_{mi})G_{ji}}{(\sum_m x_m G_{mi})^2} \right) \right]$$

## Returns

**d2GE\_dxixjs** [list[list[float]]] Second mole fraction derivatives of excess Gibbs energy, [J/mol]

## d2GE\_dTdxs()

Calculate and return the temperature derivative of mole fraction derivatives of excess Gibbs energy of a liquid represented by the NRTL model.

$$\frac{\partial^2 g^E}{\partial x_i \partial T} = R \left[ -T \left( \sum_j \left( -\frac{x_j (G_{ij} \frac{\partial \tau_{ij}}{\partial T} + \tau_{ij} \frac{\partial G_{ij}}{\partial T})}{\sum_k x_k G_{kj}} + \frac{x_j G_{ij} \tau_{ij} (\sum_k x_k \frac{\partial G_{kj}}{\partial T})}{(\sum_k x_k G_{kj})^2} + \frac{x_j \frac{\partial G_{ij}}{\partial T} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})^2} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})} + \frac{x_j G_{ij} (\sum_k x_k G_{kj} \tau_{kj})}{(\sum_k x_k G_{kj} \tau_{kj})})} +$$

## Returns

-

**d2GE\_dTdxs** [list[float]] Temperature derivative of mole fraction derivatives of excess Gibbs energy, [J/(mol\*K)]

# 7.19.2 NRTL Functional Calculations

## thermo.nrtl.NRTL\_gammas(xs, taus, alphas)

Calculates the activity coefficients of each species in a mixture using the Non-Random Two-Liquid (NRTL) method, given their mole fractions, dimensionless interaction parameters, and nonrandomness constants. Those are normally correlated with temperature in some form, and need to be calculated separately.

$$\ln(\gamma_i) = \frac{\sum_{j=1}^n x_j \tau_{ji} G_{ji}}{\sum_{k=1}^n x_k G_{ki}} + \sum_{j=1}^n \frac{x_j G_{ij}}{\sum_{k=1}^n x_k G_{kj}} \left( \tau_{ij} - \frac{\sum_{m=1}^n x_m \tau_{mj} G_{mj}}{\sum_{k=1}^n x_k G_{kj}} \right)$$
$$G_{ij} = \exp\left(-\alpha_{ij} \tau_{ij}\right)$$

#### **Parameters**

xs [list[float]] Liquid mole fractions of each species, [-]

- **taus** [list[list[float]]] Dimensionless interaction parameters of each compound with each other, [-]
- **alphas** [list[list[float]]] Nonrandomness constants of each compound interacting with each other, [-]

## Returns

gammas [list[float]] Activity coefficient for each species in the liquid mixture, [-]

#### Notes

This model needs N^2 parameters.

One common temperature dependence of the nonrandomness constants is:

$$\alpha_{ij} = c_{ij} + d_{ij}T$$

Most correlations for the interaction parameters include some of the terms shown in the following form:

$$\tau_{ij} = A_{ij} + \frac{B_{ij}}{T} + \frac{C_{ij}}{T^2} + D_{ij}\ln(T) + E_{ij}T^{F_{ij}}$$

The original form of this model used the temperature dependence of taus in the form (values can be found in the literature, often with units of calories/mol):

$$\tau_{ij} = \frac{b_{ij}}{RT}$$

For this model to produce ideal acitivty coefficients (gammas = 1), all interaction parameters should be 0; the value of alpha does not impact the calculation when that is the case.

#### References

[1], [2]

## **Examples**

Ethanol-water example, at 343.15 K and 1 MPa:

```
>>> NRTL_gammas(xs=[0.252, 0.748], taus=[[0, -0.178], [1.963, 0]],
... alphas=[[0, 0.2974],[.2974, 0]])
[1.9363183763514304, 1.1537609663170014]
```

## 7.19.3 NRTL Regression Calculations

## thermo.nrtl.NRTL\_gammas\_binaries(xs, tau12, tau21, alpha12, alpha21, gammas=None)

Calculates activity coefficients at fixed *tau* and *alpha* values for a binary system at a series of mole fractions. This is used for regression of *tau* and *alpha* parameters. This function is highly optimized, and operates on multiple points at a time.

$$\ln \gamma_1 = x_2^2 \left[ \tau_{21} \left( \frac{G_{21}}{x_1 + x_2 G_{21}} \right)^2 + \frac{\tau_{12} G_{12}}{(x_2 + x_1 G_{12})^2} \right]$$
$$\ln \gamma_2 = x_1^2 \left[ \tau_{12} \left( \frac{G_{12}}{x_2 + x_1 G_{12}} \right)^2 + \frac{\tau_{21} G_{21}}{(x_1 + x_2 G_{21})^2} \right]$$
$$G_{ij} = \exp(-\alpha_{ij} \tau_{ij})$$

#### Parameters

- xs [list[float]] Liquid mole fractions of each species in the format x0\_0, x1\_0, (component 1 point1, component 2 point 1), x0\_1, x1\_1, (component 1 point2, component 2 point 2), ... [-]
- tau12 [float] tau parameter for 12, [-]
- tau21 [float] tau parameter for 21, [-]
- alpha12 [float] alpha parameter for 12, [-]
- alpha21 [float] alpha parameter for 21, [-]
- **gammas** [list[float], optional] Array to store the activity coefficient for each species in the liquid mixture, indexed the same as *xs*; can be omitted or provided for slightly better performance [-]

## Returns

**gammas** [list[float]] Activity coefficient for each species in the liquid mixture, indexed the same as *xs*, [-]

## **Examples**

```
>>> NRTL_gammas_binaries([.1, .9, 0.3, 0.7, .85, .15], 0.1759, 0.7991, .2, .3)
[2.121421, 1.011342, 1.52177, 1.09773, 1.016062, 1.841391]
```

# 7.20 Legacy Mixtures (thermo.mixture)

class thermo.mixture.Mixture(IDs=None, zs=None, ws=None, Vfls=None, Vfgs=None, T=None, P=None, VF=None, H=None, Hm=None, S=None, Sm=None, pkg=None, Vf TP=(None, None))

Bases: object

Creates a Mixture object which contains basic information such as molecular weight and the structure of the species, as well as thermodynamic and transport properties as a function of two of the variables temperature, pressure, vapor fraction, enthalpy, or entropy.

The components of the mixture must be specified by specifying the names of the chemicals; the composition can be specified by providing any one of the following parameters:

- · Mass fractions ws
- Mole fractions zs
- Liquid volume fractions (based on pure component densities) Vfls
- Gas volume fractions (based on pure component densities) Vfgs

If volume fractions are provided, by default the pure component volumes are calculated at the specified T and P. To use another reference temperature and pressure specify it as a tuple for the argument  $Vf_TP$ .

If no thermodynamic conditions are specified, or if only one of T and P are specified without another thermodynamic variable as well, the T and P 298.15 K and/or 101325 Pa will be set instead of the missing variables.

#### Parameters

- **IDs** [list, optional] List of chemical identifiers names, CAS numbers, SMILES or InChi strings can all be recognized and may be mixed [-]
- zs [list or dict, optional] Mole fractions of all components in the mixture [-]
- ws [list or dict, optional] Mass fractions of all components in the mixture [-]
- **Vfls** [list or dict, optional] Volume fractions of all components as a hypothetical liquid phase based on pure component densities [-]
- **Vfgs** [list, or dict optional] Volume fractions of all components as a hypothetical gas phase based on pure component densities [-]
- T [float, optional] Temperature of the mixture (default 298.15 K), [K]
- **P** [float, optional] Pressure of the mixture (default 101325 Pa) [Pa]
- VF [float, optional] Vapor fraction (mole basis) of the mixture, [-]

Hm [float, optional] Molar enthalpy of the mixture, [J/mol]

H [float, optional] Mass enthalpy of the mixture, [J/kg]

Sm [float, optional] Molar entropy of the mixture, [J/mol/K]

S [float, optional] Mass entropy of the mixture, [J/kg/K]

- pkg [object] The thermodynamic property package to use for flash calculations; one of the caloric packages in thermo.property\_package; defaults to the ideal model [-]
- Vf\_TP [tuple(2, float), optional] The (T, P) at which the volume fractions are specified to be at, [K] and [Pa]

## Notes

**Warning:** The Mixture class is not designed for high-performance or the ability to use different thermodynamic models. It is especially limited in its multiphase support and the ability to solve with specifications other than temperature and pressure. It is impossible to change constant properties such as a compound's critical temperature in this interface.

It is recommended to switch over to the *thermo.flash* interface which solves those problems and is better positioned to grow. That interface also requires users to be responsible for their chemical constants and pure component correlations; while default values can easily be loaded for most compounds, the user is ultimately responsible for them.

## **Examples**

Creating Mixture objects:

For mixtures with large numbers of components, it may be confusing to enter the composition separate from the names of the chemicals. For that case, the syntax using dictionaries as follows is supported with any composition specification:

```
comp = OrderedDict([('methane', 0.96522),
>>>
                           ('nitrogen', 0.00259),
. . .
                           ('carbon dioxide', 0.00596),
. . .
                           ('ethane', 0.01819),
. . .
                           ('propane', 0.0046),
. . .
                           ('isobutane', 0.00098),
. . .
                           ('butane', 0.00101),
. . .
                           ('2-methylbutane', 0.00047),
. . .
                           ('pentane', 0.00032),
. . .
                           ('hexane', 0.00066)])
. . .
>>> m = Mixture(zs=comp)
```

## Attributes

MW [float] Mole-weighted average molecular weight all chemicals in the mixture, [g/mol]

IDs [list of str] Names of all the species in the mixture as given in the input, [-]

names [list of str] Names of all the species in the mixture, [-]

CASs [list of str] CAS numbers of all species in the mixture, [-]

MWs [list of float] Molecular weights of all chemicals in the mixture, [g/mol]

Tms [list of float] Melting temperatures of all chemicals in the mixture, [K]

- **Tbs** [list of float] Boiling temperatures of all chemicals in the mixture, [K]
- Tcs [list of float] Critical temperatures of all chemicals in the mixture, [K]
- Pcs [list of float] Critical pressures of all chemicals in the mixture, [Pa]
- Vcs [list of float] Critical volumes of all chemicals in the mixture, [m^3/mol]
- Zcs [list of float] Critical compressibilities of all chemicals in the mixture, [-]
- **rhocs** [list of float] Critical densities of all chemicals in the mixture, [kg/m<sup>3</sup>]
- **rhocms** [list of float] Critical molar densities of all chemicals in the mixture, [mol/m^3]
- omegas [list of float] Acentric factors of all chemicals in the mixture, [-]
- **StielPolars** [list of float] Stiel Polar factors of all chemicals in the mixture, see chemicals. acentric.Stiel\_polar\_factor for the definition, [-]
- Tts [list of float] Triple temperatures of all chemicals in the mixture, [K]
- Pts [list of float] Triple pressures of all chemicals in the mixture, [Pa]
- Hfuss [list of float] Enthalpy of fusions of all chemicals in the mixture, [J/kg]
- Hfusms [list of float] Molar enthalpy of fusions of all chemicals in the mixture, [J/mol]
- Hsubs [list of float] Enthalpy of sublimations of all chemicals in the mixture, [J/kg]
- Hsubms [list of float] Molar enthalpy of sublimations of all chemicals in the mixture, [J/mol]
- Hfms [list of float] Molar enthalpy of formations of all chemicals in the mixture, [J/mol]
- Hfs [list of float] Enthalpy of formations of all chemicals in the mixture, [J/kg]
- **Gfms** [list of float] Molar Gibbs free energies of formation of all chemicals in the mixture, [J/mol]
- **Gfs** [list of float] Gibbs free energies of formation of all chemicals in the mixture, [J/kg]
- Sfms [list of float] Molar entropy of formation of all chemicals in the mixture, [J/mol/K]
- Sfs [list of float] Entropy of formation of all chemicals in the mixture, [J/kg/K]
- **S0ms** [list of float] Standard absolute entropies of all chemicals in the mixture, [J/mol/K]
- S0s [list of float] Standard absolute entropies of all chemicals in the mixture, [J/kg/K]
- Hcms [list of float] Molar higher heats of combustions of all chemicals in the mixture, [J/mol]
- Hcs [list of float] Higher heats of combustions of all chemicals in the mixture, [J/kg]
- Hcms\_lower [list of float] Molar lower heats of combustions of all chemicals in the mixture, [J/mol]
- Hcs\_lower [list of float] Higher lower of combustions of all chemicals in the mixture, [J/kg]
- Tflashs [list of float] Flash points of all chemicals in the mixture, [K]
- Tautoignitions [list of float] Autoignition points of all chemicals in the mixture, [K]
- **LFLs** [list of float] Lower flammability limits of the gases in an atmosphere at STP, mole fractions, [-]
- **UFLs** [list of float] Upper flammability limit of the gases in an atmosphere at STP, mole fractions, [-]
- **TWAs** [list of list of tuple(quantity, unit)] Time-Weighted Average limits on worker exposure to dangerous chemicals.

- **STELs** [list of tuple(quantity, unit)] Short-term Exposure limits on worker exposure to dangerous chemicals.
- Ceilings [list of tuple(quantity, unit)] Ceiling limits on worker exposure to dangerous chemicals.
- Skins [list of bool] Whether or not each of the chemicals can be absorbed through the skin.
- **Carcinogens** [list of str or dict] Carcinogen status information for each chemical in the mixture.
- **Chemicals** [list of Chemical instances] Chemical instances used in calculating mixture properties, [-]
- **dipoles** [list of float] Dipole moments of all chemicals in the mixture in debye, [3.33564095198e-30 ampere\*second^2]
- **Stockmayers** [list of float] Lennard-Jones depth of potential-energy minimum over k for all chemicals in the mixture, [K]
- **molecular\_diameters** [list of float] Lennard-Jones molecular diameters of all chemicals in the mixture, [angstrom]
- **GWPs** [list of float] Global warming potentials (default 100-year outlook) (impact/mass chemical)/(impact/mass CO2) of all chemicals in the mixture, [-]
- **ODPs** [list of float] Ozone Depletion potentials (impact/mass chemical)/(impact/mass CFC-11), of all chemicals in the mixture, [-]
- **logPs** [list of float] Octanol-water partition coefficients of all chemicals in the mixture, [-]
- **Psat\_298s** [list of float] Vapor pressure of the chemicals in the mixture at 298.15 K, [Pa]
- **phase\_STPs** [list of str] Phase of the chemicals in the mixture at 298.15 K and 101325 Pa; one of 's', 'l', 'g', or 'l/g'.
- Vml\_Tbs [list of float] Molar volumes of the chemicals in the mixture as liquids at their normal boiling points, [m^3/mol]
- Vml\_Tms [list of float] Molar volumes of the chemicals in the mixture as liquids at their melting points, [m^3/mol]
- Vml\_STPs [list of float] Molar volume of the chemicals in the mixture as liquids at 298.15 K and 101325 Pa, [m<sup>3</sup>/mol]
- **rhoml\_STPs** [list of float] Molar densities of the chemicals in the mixture as liquids at 298.15 K and 101325 Pa, [mol/m^3]
- Vmg\_STPs [list of float] Molar volume of the chemicals in the mixture as gases at 298.15 K and 101325 Pa, [m<sup>3</sup>/mol]
- Vms\_Tms [list of float] Molar volumes of solid phase at the melting point [m^3/mol]
- **rhos\_Tms** [list of float] Mass densities of solid phase at the melting point [kg/m^3]
- **Hvap\_Tbms** [list of float] Molar enthalpies of vaporization of the chemicals in the mixture at their normal boiling points, [J/mol]
- **Hvap\_Tbs** [list of float] Mass enthalpies of vaporization of the chemicals in the mixture at their normal boiling points, [J/kg]
- **alpha** Thermal diffusivity of the mixture at its current temperature, pressure, and phase in units of [m^2/s].
- **alphag** Thermal diffusivity of the gas phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .

- **alphags** Pure component thermal diffusivities of the chemicals in the mixture in the gas phase at the current temperature and pressure, in units of [m<sup>2</sup>/s].
- **alphal** Thermal diffusivity of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- **alphals** Pure component thermal diffusivities of the chemicals in the mixture in the liquid phase at the current temperature and pressure, in units of [m^2/s].
- A Helmholtz energy of the mixture at its current state, in units of [J/kg].

Am Helmholtz energy of the mixture at its current state, in units of [J/mol].

- atom\_fractions Dictionary of atomic fractions for each atom in the mixture.
- atom\_fractionss List of dictionaries of atomic fractions for all chemicals in the mixture.
- atomss List of dictionaries of atom counts for all chemicals in the mixture.
- **Bvirial** Second virial coefficient of the gas phase of the mixture at its current temperature, pressure, and composition in units of [mol/m^3].

charges Charges for all chemicals in the mixture, [faraday].

- Cp Mass heat capacity of the mixture at its current phase and temperature, in units of [J/kg/K].
- *Cpg* Gas-phase heat capacity of the mixture at its current temperature , and composition in units of [J/kg/K].
- *Cpgm* Gas-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- *Cpgms* Gas-phase ideal gas heat capacity of the chemicals at its current temperature, in units of [J/mol/K].
- *Cpgs* Gas-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].
- **Cp1** Liquid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/kg/K].
- **Cplm** Liquid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- *Cplms* Liquid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/mol/K].
- *Cpls* Liquid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].
- *Cpm* Molar heat capacity of the mixture at its current phase and temperature, in units of [J/mol/K].
- **Cps** Solid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/kg/K].
- **Cpsm** Solid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- *Cpsms* Solid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/mol/K].
- *Cpss* Solid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].

- *Cvg* Gas-phase ideal-gas contant-volume heat capacity of the mixture at its current temperature, in units of [J/kg/K].
- *Cvgm* Gas-phase ideal-gas contant-volume heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- *Cvgms* Gas-phase pure component ideal-gas contant-volume heat capacities of the chemicals in the mixture at its current temperature, in units of [J/mol/K].
- *Cvgs* Gas-phase pure component ideal-gas contant-volume heat capacities of the chemicals in the mixture at its current temperature, in units of [J/kg/K].
- economic\_statuses List of dictionaries of the economic status for all chemicals in the mixture.
- eos Equation of state object held by the mixture.
- formulas Chemical formulas for all chemicals in the mixture.
- *Hvapms* Pure component enthalpies of vaporization of the chemicals in the mixture at its current temperature, in units of [J/mol].
- *Hvaps* Enthalpy of vaporization of the chemicals in the mixture at its current temperature, in units of [J/kg].
- InChI\_Keys InChI keys for all chemicals in the mixture.
- **InChIs** InChI strings for all chemicals in the mixture.
- *isentropic\_exponent* Gas-phase ideal-gas isentropic exponent of the mixture at its current temperature, [dimensionless].
- *isentropic\_exponents* Gas-phase pure component ideal-gas isentropic exponent of the chemicals in the mixture at its current temperature, [dimensionless].
- *isobaric\_expansion* Isobaric (constant-pressure) expansion of the mixture at its current phase, temperature, and pressure in units of [1/K].
- *isobaric\_expansion\_g* Isobaric (constant-pressure) expansion of the gas phase of the mixture at its current temperature and pressure, in units of [1/K].
- *isobaric\_expansion\_gs* Pure component isobaric (constant-pressure) expansions of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [1/K].
- *isobaric\_expansion\_1* Isobaric (constant-pressure) expansion of the liquid phase of the mixture at its current temperature and pressure, in units of [1/K].
- *isobaric\_expansion\_1s* Pure component isobaric (constant-pressure) expansions of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [1/K].
- **IUPAC\_names** IUPAC names for all chemicals in the mixture.
- JT Joule Thomson coefficient of the mixture at its current phase, temperature, and pressure in units of [K/Pa].
- *JTg* Joule Thomson coefficient of the gas phase of the mixture if one exists at its current temperature and pressure, in units of [K/Pa].
- *JTgs* Pure component Joule Thomson coefficients of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [K/Pa].
- **JT1** Joule Thomson coefficient of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [K/Pa].

- *JT1s* Pure component Joule Thomson coefficients of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [K/Pa].
- **k** Thermal conductivity of the mixture at its current phase, temperature, and pressure in units of [W/m/K].
- *kg* Thermal conductivity of the mixture in the gas phase at its current temperature, pressure, and composition in units of [Pa\*s].
- *kgs* Pure component thermal conductivies of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [W/m/K].
- **k1** Thermal conductivity of the mixture in the liquid phase at its current temperature, pressure, and composition in units of [Pa\*s].
- **kls** Pure component thermal conductivities of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [W/m/K].
- *legal\_statuses* List of dictionaries of the legal status for all chemicals in the mixture.
- **mass\_fractions** Dictionary of mass fractions for each atom in the mixture.
- mass\_fractionss List of dictionaries of mass fractions for all chemicals in the mixture.
- mu Viscosity of the mixture at its current phase, temperature, and pressure in units of [Pa\*s].
- *mug* Viscosity of the mixture in the gas phase at its current temperature, pressure, and composition in units of [Pa\*s].
- *mugs* Pure component viscosities of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [Pa\*s].
- **mul** Viscosity of the mixture in the liquid phase at its current temperature, pressure, and composition in units of [Pa\*s].
- *muls* Pure component viscosities of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [Pa\*s].
- *nu* Kinematic viscosity of the mixture at its current temperature, pressure, and phase in units of  $[m^2/s]$ .
- *nug* Kinematic viscosity of the gas phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .
- *nugs* Pure component kinematic viscosities of the gas phase of the chemicals in the mixture at its current temperature and pressure, in units of  $[m^2/s]$ .
- **nul** Kinematic viscosity of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- **nuls** Pure component kinematic viscosities of the liquid phase of the chemicals in the mixture at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- *permittivites* Pure component relative permittivities of the chemicals in the mixture at its current temperature, [dimensionless].
- *Pr* Prandtl number of the mixture at its current temperature, pressure, and phase; [dimension-less].
- *Prg* Prandtl number of the gas phase of the mixture if one exists at its current temperature and pressure, [dimensionless].
- **Prgs** Pure component Prandtl numbers of the gas phase of the chemicals in the mixture at its current temperature and pressure, [dimensionless].

- **Pr1** Prandtl number of the liquid phase of the mixture if one exists at its current temperature and pressure, [dimensionless].
- **Prls** Pure component Prandtl numbers of the liquid phase of the chemicals in the mixture at its current temperature and pressure, [dimensionless].
- **Psats** Pure component vapor pressures of the chemicals in the mixture at its current temperature, in units of [Pa].
- **PSRK\_groups** List of dictionaries of PSRK subgroup: count groups for each chemical in the mixture.
- PubChems PubChem Component ID numbers for all chemicals in the mixture.
- *rho* Mass density of the mixture at its current phase and temperature and pressure, in units of [kg/m^3].
- *rhog* Gas-phase mass density of the mixture at its current temperature, pressure, and composition in units of [kg/m^3].
- **rhogm** Molar density of the mixture in the gas phase at the current temperature, pressure, and composition in units of [mol/m^3].
- **rhogms** Pure component molar densities of the chemicals in the gas phase at the current temperature and pressure, in units of [mol/m^3].
- *rhogm\_STP* Molar density of the mixture in the gas phase at 298.15 K and 101.325 kPa, and the current composition, in units of [mol/m<sup>3</sup>].
- **rhogs** Pure-component gas-phase mass densities of the chemicals in the mixture at its current temperature and pressure, in units of [kg/m^3].
- *rhog\_STP* Gas-phase mass density of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [kg/m<sup>3</sup>].
- **rhol** Liquid-phase mass density of the mixture at its current temperature, pressure, and composition in units of [kg/m^3].
- **rholm** Molar density of the mixture in the liquid phase at the current temperature, pressure, and composition in units of [mol/m^3].
- **rholms** Pure component molar densities of the chemicals in the mixture in the liquid phase at the current temperature and pressure, in units of [mol/m^3].
- *rholm\_STP* Molar density of the mixture in the liquid phase at 298.15 K and 101.325 kPa, and the current composition, in units of [mol/m^3].
- **rhols** Pure-component liquid-phase mass density of the chemicals in the mixture at its current temperature and pressure, in units of [kg/m^3].
- **rho1\_STP** Liquid-phase mass density of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [kg/m<sup>3</sup>].
- *rhom* Molar density of the mixture at its current phase and temperature and pressure, in units of [mol/m^3].
- **rhosms** Pure component molar densities of the chemicals in the solid phase at the current temperature and pressure, in units of [mol/m^3].
- **rhoss** Pure component solid-phase mass density of the chemicals in the mixture at its current temperature, in units of [kg/m^3].
- ringss List of ring counts for all chemicals in the mixture.

- **sigma** Surface tension of the mixture at its current temperature and composition, in units of [N/m].
- *sigmas* Pure component surface tensions of the chemicals in the mixture at its current temperature, in units of [N/m].
- smiless SMILES strings for all chemicals in the mixture.
- *solubility\_parameters* Pure component solubility parameters of the chemicals in the mixture at its current temperature and pressure, in units of [Pa^0.5].
- synonymss Lists of synonyms for all chemicals in the mixture.
- **U** Internal energy of the mixture at its current state, in units of [J/kg].
- Um Internal energy of the mixture at its current state, in units of [J/mol].
- **UNIFAC\_Dortmund\_groups** List of dictionaries of Dortmund UNIFAC subgroup: count groups for each chemcial in the mixture.
- **UNIFAC\_groups** List of dictionaries of UNIFAC subgroup: count groups for each chemical in the mixture.
- Vm Molar volume of the mixture at its current phase and temperature and pressure, in units of [m^3/mol].
- *Vmg* Gas-phase molar volume of the mixture at its current temperature, pressure, and composition in units of [m<sup>3</sup>/mol].
- *Vmgs* Pure component gas-phase molar volumes of the chemicals in the mixture at its current temperature and pressure, in units of [m^3/mol].
- *Vmg\_STP* Gas-phase molar volume of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [m^3/mol].
- Vml Liquid-phase molar volume of the mixture at its current temperature, pressure, and composition in units of [m^3/mol].
- *Vmls* Pure component liquid-phase molar volumes of the chemicals in the mixture at its current temperature and pressure, in units of [m^3/mol].
- Vml\_STP Liquid-phase molar volume of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [m<sup>3</sup>/mol].
- *Vmss* Pure component solid-phase molar volumes of the chemicals in the mixture at its current temperature, in units of [m^3/mol].
- *Z* Compressibility factor of the mixture at its current phase and temperature and pressure, [dimensionless].
- *Zg* Compressibility factor of the mixture in the gas phase at the current temperature, pressure, and composition, [dimensionless].
- *Zgs* Pure component compressibility factors of the chemicals in the mixture in the gas phase at the current temperature and pressure, [dimensionless].
- *Zg\_STP* Gas-phase compressibility factor of the mixture at 298.15 K and 101.325 kPa, and the current composition, [dimensionless].
- Z1 Compressibility factor of the mixture in the liquid phase at the current temperature, pressure, and composition, [dimensionless].
- **Z1s** Pure component compressibility factors of the chemicals in the liquid phase at the current temperature and pressure, [dimensionless].

- **Z1\_STP** Liquid-phase compressibility factor of the mixture at 298.15 K and 101.325 kPa, and the current composition, [dimensionless].
- **Zss** Pure component compressibility factors of the chemicals in the mixture in the solid phase at the current temperature and pressure, [dimensionless].

## Methods

<pre>Hc_volumetric_g([T, P])</pre>	Standard higher molar heat of combustion of the mix-
	ture, in units of $[J/m^3]$ at the specified T and P in the
	gas phase.
<pre>Hc_volumetric_g_lower([T, P])</pre>	Standard lower molar heat of combustion of the mix-
	ture, in units of $[J/m^3]$ at the specified T and P in
	the gas phase.
Vfgs([T, P])	Volume fractions of all species in a hypothetical pure-
	gas phase at the current or specified temperature and
	pressure.
Vfls([T, P])	Volume fractions of all species in a hypothetical pure-
	liquid phase at the current or specified temperature
	and pressure.
draw_2d([Hs])	Interface for drawing a 2D image of all the molecules
	in the mixture.
<pre>set_chemical_TP([T, P])</pre>	Basic method to change all chemical instances to be
	at the T and P specified.
<pre>set_chemical_constants()</pre>	Basic method which retrieves and sets constants of
	chemicals to be accessible as lists from a Mixture ob-
	ject.

Bond	
Capillary	
Grashof	
Jakob	
Peclet_heat	
Reynolds	
Weber	
compound_index	
eos_pures	
flash_caloric	
properties	
set_Chemical_property_objects	
set_TP_sources	
set_constant_sources	
set_constants	
set_eos	
set_property_package	

## property A

Helmholtz energy of the mixture at its current state, in units of [J/kg].

This property requires that the property package of the mixture found a solution to the given state variables. It also depends on the molar volume of the mixture at its current conditions.

### property API

API gravity of the hypothetical liquid phase of the mixture, [degrees]. The reference condition is water at 15.6 °C ( $60 \text{ }^{\circ}\text{F}$ ) and 1 atm (rho=999.016 kg/m^3, standardized).

### **Examples**

```
>>> Mixture(['hexane', 'decane'], ws=[0.5, 0.5]).API
71.34707841728181
```

### property Am

Helmholtz energy of the mixture at its current state, in units of [J/mol].

This property requires that the property package of the mixture found a solution to the given state variables. It also depends on the molar volume of the mixture at its current conditions.

Bond(L=None)

### property Bvirial

Second virial coefficient of the gas phase of the mixture at its current temperature, pressure, and composition in units of [mol/m^3].

This property uses the object-oriented interface *thermo.volume.VolumeGasMixture*, converting its result with thermo.utils.B\_from\_Z.

## **Examples**

```
>>> Mixture(['hexane'], ws=[1], T=300, P=1E5).Bvirial
-0.001486976173801296
```

### Capillary(V=None)

### property Cp

Mass heat capacity of the mixture at its current phase and temperature, in units of [J/kg/K].

## **Examples**

```
>>> w = Mixture(['water'], ws=[1])
>>> w.Cp, w.phase
(4180.597021827336, 'l')
>>> Pd = Mixture(['palladium'], ws=[1])
>>> Pd.Cp, Pd.phase
(234.26767209171211, 's')
```

### property Cpg

Gas-phase heat capacity of the mixture at its current temperature , and composition in units of [J/kg/K]. For calculation of this property at other temperatures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface thermo.heat\_capacity. HeatCapacityGasMixture; each Mixture instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

```
>>> Mixture(['oxygen', 'nitrogen'], ws=[.4, .6], T=350, P=1E6).Cpg
995.8911053614883
```

## property Cpgm

Gas-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K]. For calculation of this property at other temperatures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface thermo.heat\_capacity. HeatCapacityGasMixture; each Mixture instance creates one to actually perform the calculations.

#### **Examples**

```
>>> Mixture(['oxygen', 'nitrogen'], ws=[.4, .6], T=350, P=1E6).Cpgm
29.361044582498046
```

### property Cpgms

Gas-phase ideal gas heat capacity of the chemicals at its current temperature, in units of [J/mol/K].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cpgms
[89.55804092586159, 111.70390334788907]
```

#### property Cpgs

Gas-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cpgs
[1146.5360555565146, 1212.3488046342566]
```

### property Cpl

Liquid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/kg/K]. For calculation of this property at other temperatures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity*. *HeatCapacityLiquidMixture*; each Mixture instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

### **Examples**

```
>>> Mixture(['water', 'sodium chloride'], ws=[.9, .1], T=301.5).Cpl
3735.4604049449786
```

#### property Cplm

Liquid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K]. For calculation of this property at other temperatures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.heat\_capacity*. *HeatCapacityLiquidMixture*; each Mixture instance creates one to actually perform the calculations.

```
>>> Mixture(['toluene', 'decane'], ws=[.9, .1], T=300).Cplm
168.29127923518843
```

## property Cplms

Liquid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/mol/K].

## **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cplms
[140.9113971170526, 163.62584810669068]
```

### property Cpls

Liquid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cpls
[1803.9697581961016, 1775.869915141704]
```

#### property Cpm

Molar heat capacity of the mixture at its current phase and temperature, in units of [J/mol/K]. Available only if single phase.

#### **Examples**

```
>>> Mixture(['ethylbenzene'], ws=[1], T=550, P=3E6).Cpm
294.18449553310046
```

#### property Cps

Solid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/kg/K]. For calculation of this property at other temperatures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface thermo.heat\_capacity. HeatCapacitySolidMixture; each Mixture instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

### **Examples**

```
>>> Mixture(['silver', 'platinum'], ws=[0.95, 0.05]).Cps
229.55166388430328
```

#### property Cpsm

Solid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K]. For calculation of this property at other temperatures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface thermo.heat\_capacity. HeatCapacitySolidMixture; each Mixture instance creates one to actually perform the calculations.

```
>>> Mixture(['silver', 'platinum'], ws=[0.95, 0.05]).Cpsm
25.32745796347474
```

## property Cpsms

Solid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/mol/K].

## Examples

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cpsms
[109.77384365511931, 135.22614707678474]
```

### property Cpss

Solid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cpss
[1405.341925822248, 1467.6412627521154]
```

#### property Cvg

Gas-phase ideal-gas contant-volume heat capacity of the mixture at its current temperature, in units of [J/kg/K]. Subtracts R from the ideal-gas heat capacity; does not include pressure-compensation from an equation of state.

#### **Examples**

```
>>> Mixture(['water'], ws=[1], T=520).Cvg
1506.1471795798861
```

#### property Cvgm

Gas-phase ideal-gas contant-volume heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K]. Subtracts R from the ideal-gas heat capacity; does not include pressure-compensation from an equation of state.

#### **Examples**

```
>>> Mixture(['water'], ws=[1], T=520).Cvgm
27.13366316134193
```

#### property Cvgms

Gas-phase pure component ideal-gas contant-volume heat capacities of the chemicals in the mixture at its current temperature, in units of [J/mol/K]. Subtracts R from the ideal-gas heat capacities; does not include pressure-compensation from an equation of state.

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cvgms
[81.2435811258616, 103.38944354788907]
```

## property Cvgs

Gas-phase pure component ideal-gas contant-volume heat capacities of the chemicals in the mixture at its current temperature, in units of [J/kg/K]. Subtracts R from the ideal-gas heat capacity; does not include pressure-compensation from an equation of state.

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Cvgs
[1040.093040003431, 1122.1100117398266]
```

### Grashof(Tw=None, L=None)

## H = None

## property Hc

Standard higher heat of combustion of the mixture, in units of [J/kg].

This property depends on the bulk composition only.

### property Hc\_lower

Standard lower heat of combustion of the mixture, in units of [J/kg].

This property depends on the bulk composition only.

### Hc\_volumetric\_g(T=288.7055555555555, P=101325.0)

Standard higher molar heat of combustion of the mixture, in units of  $[J/m^3]$  at the specified *T* and *P* in the gas phase.

This property depends on the bulk composition only.

### Parameters

T [float, optional] Reference temperature, [K]

P [float, optional] Reference pressure, [Pa]

#### Returns

Hc\_volumetric\_g [float, optional] Higher heat of combustion on a volumetric basis, [J/m^3]

#### **Hc\_volumetric\_g\_lower**(*T*=288.705555555555, *P*=101325.0)

Standard lower molar heat of combustion of the mixture, in units of  $[J/m^3]$  at the specified T and P in the gas phase.

This property depends on the bulk composition only.

#### Parameters

T [float, optional] Reference temperature, [K]

**P** [float, optional] Reference pressure, [Pa]

#### Returns

Hc\_volumetric\_g [float, optional] Lower heat of combustion on a volumetric basis, [J/m^3]

#### property Hcm

Standard higher molar heat of combustion of the mixture, in units of [J/mol].

This property depends on the bulk composition only.

### property Hcm\_lower

Standard lower molar heat of combustion of the mixture, in units of [J/mol].

This property depends on the bulk composition only.

#### Hm = None

### property Hvapms

Pure component enthalpies of vaporization of the chemicals in the mixture at its current temperature, in units of [J/mol].

## **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Hvapms
[32639.806783391632, 36851.7902195611]
```

## property Hvaps

Enthalpy of vaporization of the chemicals in the mixture at its current temperature, in units of [J/kg].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Hvaps
[417859.9144942896, 399961.16950519773]
```

### property IUPAC\_names

IUPAC names for all chemicals in the mixture.

### **Examples**

```
>>> Mixture(['1-hexene', '1-nonene'], zs=[.7, .3]).IUPAC_names
['hex-1-ene', 'non-1-ene']
```

## property InChI\_Keys

InChI keys for all chemicals in the mixture.

## **Examples**

```
>>> Mixture(['1-nonene'], zs=[1]).InChI_Keys
['JRZJOMJEPLMPRA-UHFFFAOYSA-N']
```

#### property InChIs

InChI strings for all chemicals in the mixture.

```
>>> Mixture(['methane', 'ethane', 'propane', 'butane'],
... zs=[0.25, 0.25, 0.25, 0.25]).InChIs
['CH4/h1H4', 'C2H6/c1-2/h1-2H3', 'C3H8/c1-3-2/h3H2,1-2H3', 'C4H10/c1-3-4-2/h3-
-4H2,1-2H3']
```

### property JT

Joule Thomson coefficient of the mixture at its current phase, temperature, and pressure in units of [K/Pa]. Available only if single phase.

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[T\left(\frac{\partial V}{\partial T}\right)_{P} - V\right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

#### **Examples**

```
>>> Mixture(['water'], ws=[1]).JT
-2.2150394958666412e-07
```

#### property JTg

Joule Thomson coefficient of the gas phase of the mixture if one exists at its current temperature and pressure, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[T\left(\frac{\partial V}{\partial T}\right)_{P} - V\right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

### **Examples**

>>> Mixture(['dodecane'], ws=[1], T=400, P=1000).JTg
5.4089897835384913e-05

### property JTgs

Pure component Joule Thomson coefficients of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[ T \left(\frac{\partial V}{\partial T}\right)_{P} - V \right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

## **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).JTgs
[6.0940046688790938e-05, 4.1290005523287549e-05]
```

#### property JT1

Joule Thomson coefficient of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[ T \left(\frac{\partial V}{\partial T}\right)_{P} - V \right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

```
>>> Mixture(['dodecane'], ws=[1], T=400).JTL
-3.193910574559279e-07
```

#### property JTls

Pure component Joule Thomson coefficients of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [K/Pa].

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[T\left(\frac{\partial V}{\partial T}\right)_{P} - V\right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

## **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).JTls
[-3.8633730709853161e-07, -3.464395792560331e-07]
```

#### Jakob(Tw=None)

### property PSRK\_groups

List of dictionaries of PSRK subgroup: count groups for each chemical in the mixture. Uses the PSRK subgroups, as determined by DDBST's online service.

### **Examples**

```
>>> Mixture(['1-pentanol', 'decane'], ws=[0.5, 0.5]).PSRK_groups
[{1: 1, 2: 4, 14: 1}, {1: 2, 2: 8}]
```

#### $P_default = 101325.0$

### property Parachor

Parachor of the mixture at its current temperature and pressure, in units of [N^0.25\*m^2.75/mol].

$$P = \frac{\sigma^{0.25} MW}{\rho_L - \rho_V}$$

Calculated based on surface tension, density of the liquid and gas phase, and molecular weight. For uses of this property, see thermo.utils.Parachor.

### **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).Parachor
4.233407085050756e-05
```

#### property Parachors

Pure component Parachor parameters of the chemicals in the mixture at its current temperature and pressure, in units of  $[N^{0.25*}m^{2.75/mol}]$ .

$$P = \frac{\sigma^{0.25} MW}{\rho_L - \rho_V}$$

Calculated based on surface tension, density of the liquid and gas phase, and molecular weight. For uses of this property, see thermo.utils.Parachor.

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).Parachors
[3.67956160000855504e-05, 4.82947303150274e-05]
```

### property Pbubble

Bubble point pressure of the mixture at its current temperature and composition, in units of [Pa].

This property requires that the property package of the mixture found a solution to the given state variables.

#### property Pdew

Dew point pressure of the mixture at its current temperature and composition, in units of [Pa].

This property requires that the property package of the mixture found a solution to the given state variables.

```
Peclet_heat(V=None, D=None)
```

#### property Pr

Prandtl number of the mixture at its current temperature, pressure, and phase; [dimensionless]. Available only if single phase.

$$Pr = \frac{C_p \mu}{k}$$

#### **Examples**

```
>>> Mixture(['acetone'], ws=[1]).Pr
4.183039103542711
```

#### property Prg

Prandtl number of the gas phase of the mixture if one exists at its current temperature and pressure, [dimensionless].

$$Pr = \frac{C_p \mu}{k}$$

#### **Examples**

```
>>> Mixture(['NH3'], ws=[1]).Prg
0.8472637319330079
```

#### property Prgs

Pure component Prandtl numbers of the gas phase of the chemicals in the mixture at its current temperature and pressure, [dimensionless].

$$Pr = \frac{C_p \mu}{k}$$

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).Prgs
[0.7810364900059606, 0.784358381123896]
```

### property Prl

Prandtl number of the liquid phase of the mixture if one exists at its current temperature and pressure, [dimensionless].

$$Pr = \frac{C_p \mu}{k}$$

### **Examples**

```
>>> Mixture(['nitrogen'], ws=[1], T=70).Prl
2.782821450148889
```

#### property Prls

Pure component Prandtl numbers of the liquid phase of the chemicals in the mixture at its current temperature and pressure, [dimensionless].

$$Pr = \frac{C_p \mu}{k}$$

#### **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).Prls
[6.13542244155373, 5.034355147908088]
```

#### property Psats

Pure component vapor pressures of the chemicals in the mixture at its current temperature, in units of [Pa].

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Psats
[32029.25774454549, 10724.419010511821]
```

## property PubChems

PubChem Component ID numbers for all chemicals in the mixture.

## **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5]).PubChems
[241, 1140]
```

## property R\_specific

Specific gas constant of the mixture, in units of [J/kg/K].

```
>>> Mixture(['N2', '02'], zs=[0.79, .21]).R_specific
288.1928437986195
```

**Reynolds**(*V*=*None*, *D*=*None*)

#### property SG

Specific gravity of the mixture, [dimensionless].

For gas-phase conditions, this is calculated at 15.6  $^{\circ}$ C (60  $^{\circ}$ F) and 1 atm for the mixture and the reference fluid, air. For liquid and solid phase conditions, this is calculated based on a reference fluid of water at 4 $^{\circ}$ C at 1 atm, but the with the liquid or solid mixture's density at the currently specified conditions.

### **Examples**

>>> Mixture('MTBE').SG
0.7428160596603596

#### property SGg

Specific gravity of a hypothetical gas phase of the mixture, . [dimensionless]. The reference condition is air at 15.6 °C (60 °F) and 1 atm (rho=1.223 kg/m^3). The definition for gases uses the compressibility factor of the reference gas and the mixture both at the reference conditions, not the conditions of the mixture.

### **Examples**

>>> Mixture('argon').SGg
1.3800407778218216

#### property SGl

Specific gravity of a hypothetical liquid phase of the mixture at the specified temperature and pressure, [dimensionless]. The reference condition is water at 4 °C and 1 atm (rho=999.017 kg/m^3). For liquids, SG is defined that the reference chemical's T and P are fixed, but the chemical itself varies with the specified T and P.

### **Examples**

```
>>> Mixture('water', ws=[1], T=365).SGl
0.9650065522428539
```

#### property SGs

Specific gravity of a hypothetical solid phase of the mixture at the specified temperature and pressure, [dimensionless]. The reference condition is water at 4 °C and 1 atm (rho=999.017 kg/m^3). The SG varries with temperature and pressure but only very slightly.

#### $T_default = 298.15$

#### property Tbubble

Bubble point temperature of the mixture at its current pressure and composition, in units of [K].

This property requires that the property package of the mixture found a solution to the given state variables.

### property Tdew

Dew point temperature of the mixture at its current pressure and composition, in units of [K].

This property requires that the property package of the mixture found a solution to the given state variables.

### property U

Internal energy of the mixture at its current state, in units of [J/kg].

This property requires that the property package of the mixture found a solution to the given state variables. It also depends on the molar volume of the mixture at its current conditions.

## property UNIFAC\_Dortmund\_groups

List of dictionaries of Dortmund UNIFAC subgroup: count groups for each chemcial in the mixture. Uses the Dortmund UNIFAC subgroups, as determined by DDBST's online service.

## **Examples**

```
>>> Mixture(['1-pentanol', 'decane'], ws=[0.5, 0.5]).UNIFAC_Dortmund_groups
[{1: 1, 2: 4, 14: 1}, {1: 2, 2: 8}]
```

## property UNIFAC\_Qs

UNIFAC Q (normalized Van der Waals area) values, dimensionless. Used in the UNIFAC model.

## **Examples**

```
>>> Mixture(['o-xylene', 'decane'], zs=[.5, .5]).UNIFAC_Qs
[3.536, 6.016]
```

## property UNIFAC\_Rs

UNIFAC R (normalized Van der Waals volume) values, dimensionless. Used in the UNIFAC model.

## Examples

```
>>> Mixture(['o-xylene', 'm-xylene'], zs=[.5, .5]).UNIFAC_Rs
[4.6578, 4.6578]
```

## property UNIFAC\_groups

List of dictionaries of UNIFAC subgroup: count groups for each chemical in the mixture. Uses the original UNIFAC subgroups, as determined by DDBST's online service.

## **Examples**

```
>>> Mixture(['1-pentanol', 'decane'], ws=[0.5, 0.5]).UNIFAC_groups
[{1: 1, 2: 4, 14: 1}, {1: 2, 2: 8}]
```

## property Um

Internal energy of the mixture at its current state, in units of [J/mol].

This property requires that the property package of the mixture found a solution to the given state variables. It also depends on the molar volume of the mixture at its current conditions.

## V\_over\_F = None

#### property Van\_der\_Waals\_areas

List of unnormalized Van der Waals areas of all the chemicals in the mixture, in units of [m<sup>2</sup>/mol].

### **Examples**

```
>>> Mixture(['1-pentanol', 'decane'], ws=[0.5, 0.5]).Van_der_Waals_areas
[1052000.0, 1504000.0]
```

### property Van\_der\_Waals\_volumes

List of unnormalized Van der Waals volumes of all the chemicals in the mixture, in units of [m^3/mol].

### **Examples**

```
>>> Mixture(['1-pentanol', 'decane'], ws=[0.5, 0.5]).Van_der_Waals_volumes
[6.9762279e-05, 0.00010918455800000001]
```

#### **Vfgs**(*T*=*None*, *P*=*None*)

Volume fractions of all species in a hypothetical pure-gas phase at the current or specified temperature and pressure. If temperature or pressure are specified, the non-specified property is assumed to be that of the mixture. Note this is a method, not a property. Volume fractions are calculated based on **pure species volumes only**.

#### **Examples**

```
>>> Mixture(['sulfur hexafluoride', 'methane'], zs=[.2, .9], T=315).Vfgs()
[0.18062059238682632, 0.8193794076131737]
```

```
>>> S = Mixture(['sulfur hexafluoride', 'methane'], zs=[.1, .9])
>>> S.Vfgs(P=1E2)
[0.0999987466608421, 0.9000012533391578]
```

#### Vfls(T=None, P=None)

Volume fractions of all species in a hypothetical pure-liquid phase at the current or specified temperature and pressure. If temperature or pressure are specified, the non-specified property is assumed to be that of the mixture. Note this is a method, not a property. Volume fractions are calculated based on **pure species volumes only**.

#### Examples

```
>>> Mixture(['hexane', 'pentane'], zs=[.5, .5], T=315).Vfls()
[0.5299671144566751, 0.47003288554332484]
```

```
>>> S = Mixture(['hexane', 'decane'], zs=[0.25, 0.75])
>>> S.Vfls(298.16, 101326)
[0.18301434895886864, 0.8169856510411313]
```

#### property Vm

Molar volume of the mixture at its current phase and temperature and pressure, in units of [m<sup>3</sup>/mol]. Available only if single phase.

```
>>> Mixture(['ethylbenzene'], ws=[1], T=550, P=3E6).Vm
0.00017758024401627633
```

## property Vmg

Gas-phase molar volume of the mixture at its current temperature, pressure, and composition in units of [m^3/mol]. For calculation of this property at other temperatures or pressures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume*. *VolumeGasMixture*; each Mixture instance creates one to actually perform the calculations.

### **Examples**

```
>>> Mixture(['hexane'], ws=[1], T=300, P=2E5).Vmg
0.010888694235142216
```

## property Vmg\_STP

Gas-phase molar volume of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [m^3/mol].

#### **Examples**

```
>>> Mixture(['nitrogen'], ws=[1]).Vmg_STP
0.02445443688838904
```

#### property Vmgs

Pure component gas-phase molar volumes of the chemicals in the mixture at its current temperature and pressure, in units of [m^3/mol].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Vmgs
[0.024929001982294974, 0.024150186467130488]
```

#### property Vml

Liquid-phase molar volume of the mixture at its current temperature, pressure, and composition in units of [m^3/mol]. For calculation of this property at other temperatures or pressures or compositions, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume*. *VolumeLiquidMixture*; each Mixture instance creates one to actually perform the calculations.

## **Examples**

```
>>> Mixture(['cyclobutane'], ws=[1], T=225).Vml
7.42395423425395e-05
```

## property Vml\_STP

Liquid-phase molar volume of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of  $[m^3/mol]$ .

```
>>> Mixture(['cyclobutane'], ws=[1]).Vml_STP
8.143327329133706e-05
```

## property Vmls

Pure component liquid-phase molar volumes of the chemicals in the mixture at its current temperature and pressure, in units of  $[m^3/mol]$ .

## **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Vmls
[9.188896727673715e-05, 0.00010946199496993461]
```

## Vms = None

#### property Vmss

Pure component solid-phase molar volumes of the chemicals in the mixture at its current temperature, in units of  $[m^3/mol]$ .

## **Examples**

```
>>> Mixture(['iron'], ws=[1], T=320).Vmss
[7.09593392630242e-06]
```

Weber(V=None, D=None)

#### property Z

Compressibility factor of the mixture at its current phase and temperature and pressure, [dimensionless]. Available only if single phase.

#### **Examples**

```
>>> Mixture(['MTBE'], ws=[1], T=900, P=1E-2).Z
0.99999999999056374
```

## property Zg

Compressibility factor of the mixture in the gas phase at the current temperature, pressure, and composition, [dimensionless].

Utilizes the object oriented interface and thermo.volume.VolumeGasMixture to perform the actual calculation of molar volume.

```
>>> Mixture(['hexane'], ws=[1], T=300, P=1E5).Zg
0.94038593768888885
```

## property Zg\_STP

Gas-phase compressibility factor of the mixture at 298.15 K and 101.325 kPa, and the current composition, [dimensionless].

## Examples

```
>>> Mixture(['nitrogen'], ws=[1]).Zg_STP
0.9995520809691023
```

### property Zgs

Pure component compressibility factors of the chemicals in the mixture in the gas phase at the current temperature and pressure, [dimensionless].

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Zgs
[0.9493743379816593, 0.9197146081359057]
```

#### property Zl

Compressibility factor of the mixture in the liquid phase at the current temperature, pressure, and composition, [dimensionless].

Utilizes the object oriented interface and *thermo.volume.VolumeLiquidMixture* to perform the actual calculation of molar volume.

## **Examples**

```
>>> Mixture(['water'], ws=[1]).Zl
0.0007385375470263454
```

#### property Z1\_STP

Liquid-phase compressibility factor of the mixture at 298.15 K and 101.325 kPa, and the current composition, [dimensionless].

### **Examples**

```
>>> Mixture(['cyclobutane'], ws=[1]).Zl_STP
0.0033285083663950068
```

### property Zls

Pure component compressibility factors of the chemicals in the liquid phase at the current temperature and pressure, [dimensionless].

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).Zls
[0.0034994191720201235, 0.004168655010037687]
```

### property Zss

Pure component compressibility factors of the chemicals in the mixture in the solid phase at the current temperature and pressure, [dimensionless].

## **Examples**

```
>>> Mixture(['palladium'], ws=[1]).Zss
[0.00036248477437931853]
```

### property alpha

Thermal diffusivity of the mixture at its current temperature, pressure, and phase in units of  $[m^2/s]$ . Available only if single phase.

$$\alpha = \frac{k}{\rho C p}$$

#### **Examples**

```
>>> Mixture(['furfural'], ws=[1]).alpha
8.696537158635412e-08
```

#### property alphag

Thermal diffusivity of the gas phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

#### **Examples**

```
>>> Mixture(['ammonia'], ws=[1]).alphag
1.6968517002221566e-05
```

#### property alphags

Pure component thermal diffusivities of the chemicals in the mixture in the gas phase at the current temperature and pressure, in units of  $[m^2/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).alphags
[3.3028044028118324e-06, 2.4412958544059014e-06]
```

## property alphal

Thermal diffusivity of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

## **Examples**

```
>>> Mixture(['nitrogen'], ws=[1], T=70).alphal
9.444949636299626e-08
```

#### property alphals

Pure component thermal diffusivities of the chemicals in the mixture in the liquid phase at the current temperature and pressure, in units of  $[m^2/s]$ .

$$\alpha = \frac{k}{\rho C p}$$

## **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).alphals
[8.732683564481583e-08, 7.57355434073289e-08]
```

### property atom\_fractions

Dictionary of atomic fractions for each atom in the mixture.

#### **Examples**

```
>>> Mixture(['CO2', 'O2'], zs=[0.5, 0.5]).atom_fractions
{'C': 0.2, 'O': 0.8}
```

## property atom\_fractionss

List of dictionaries of atomic fractions for all chemicals in the mixture.

### **Examples**

```
>>> Mixture(['oxygen', 'nitrogen'], zs=[.5, .5]).atom_fractionss
[{'0': 1.0}, {'N': 1.0}]
```

## property atoms

Mole-averaged dictionary of atom counts for all atoms of the chemicals in the mixture.

```
>>> Mixture(['nitrogen', 'oxygen'], zs=[.01, .99]).atoms
{'0': 1.98, 'N': 0.02}
```

## property atomss

List of dictionaries of atom counts for all chemicals in the mixture.

## **Examples**

```
>>> Mixture(['nitrogen', 'oxygen'], zs=[.01, .99]).atomss
[{'N': 2}, {'O': 2}]
```

### autoflash = True

### property charge\_balance

Charge imbalance of the mixture, in units of [faraday]. Mixtures meeting the electroneutrality condition will have an imbalance of 0.

### **Examples**

```
>>> Mixture(['Na+', 'Cl-', 'water'], zs=[.01, .01, .98]).charge_balance
0.0
```

### property charges

Charges for all chemicals in the mixture, [faraday].

## Examples

```
>>> Mixture(['water', 'sodium ion', 'chloride ion'], zs=[.9, .05, .05]).charges
[0, 1, -1]
```

compound\_index(CAS)

#### conductivity = None

### property constants

Returns a :obj: thermo.chemical\_package.ChemicalConstantsPackage instance with constants from the mixture, [-].

#### draw\_2d(Hs=False)

Interface for drawing a 2D image of all the molecules in the mixture. Requires an HTML5 browser, and the libraries RDKit and IPython. An exception is raised if either of these libraries is absent.

#### Parameters

Hs [bool] Whether or not to show hydrogen

Mixture(['natural gas']).draw\_2d()

## property economic\_statuses

List of dictionaries of the economic status for all chemicals in the mixture.

## Examples

```
>>> Mixture(['o-xylene', 'm-xylene'], zs=[.5, .5]).economic_statuses
[["US public: {'Manufactured': 0.0, 'Imported': 0.0, 'Exported': 0.0}",
    u'100,000 - 1,000,000 tonnes per annum',
    'OECD HPV Chemicals'],
["US public: {'Manufactured': 39.805, 'Imported': 0.0, 'Exported': 0.0}",
    u'100,000 - 1,000,000 tonnes per annum',
    'OECD HPV Chemicals']]
```

### property eos

Equation of state object held by the mixture. See : obj:thermo.eos\_mix for a full listing.

## eos\_in\_a\_box = []

eos\_pures(eos=<class 'thermo.eos.PR'>, T=None, P=None)

flash\_caloric(T=None, P=None, VF=None, Hm=None, Sm=None, H=None, S=None)

### flashed = True

### property formulas

Chemical formulas for all chemicals in the mixture.

## Examples

```
>>> Mixture(['ethanol', 'trichloroethylene', 'furfuryl alcohol'],
... ws=[0.5, 0.2, 0.3]).formulas
['C2H60', 'C2HCl3', 'C5H602']
```

### property isentropic\_exponent

Gas-phase ideal-gas isentropic exponent of the mixture at its current temperature, [dimensionless]. Does not include pressure-compensation from an equation of state.

## Examples

```
>>> Mixture(['hydrogen'], ws=[1]).isentropic_exponent
1.405237786321222
```

### property isentropic\_exponents

Gas-phase pure component ideal-gas isentropic exponent of the chemicals in the mixture at its current temperature, [dimensionless].

Does not include pressure-compensation from an equation of state.

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).isentropic_exponents
[1.1023398979313739, 1.080418846592871]
```

### property isobaric\_expansion

Isobaric (constant-pressure) expansion of the mixture at its current phase, temperature, and pressure in units of [1/K]. Available only if single phase.

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

### **Examples**

```
>>> Mixture(['water'], ws=[1], T=647.1, P=22048320.0).isobaric_expansion
0.34074205839222449
```

#### property isobaric\_expansion\_g

Isobaric (constant-pressure) expansion of the gas phase of the mixture at its current temperature and pressure, in units of [1/K]. Available only if single phase.

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

#### **Examples**

```
>>> Mixture(['argon'], ws=[1], T=647.1, P=22048320.0).isobaric_expansion_g
0.0015661100323025273
```

### property isobaric\_expansion\_gs

Pure component isobaric (constant-pressure) expansions of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [1/K].

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_F$$

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).isobaric_expansion_gs
[0.0038091518363900499, 0.0043556759306508453]
```

#### property isobaric\_expansion\_1

Isobaric (constant-pressure) expansion of the liquid phase of the mixture at its current temperature and pressure, in units of [1/K]. Available only if single phase.

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_F$$

```
>>> Mixture(['argon'], ws=[1], T=647.1, P=22048320.0).isobaric_expansion_1
0.001859152875154442
```

### property isobaric\_expansion\_ls

Pure component isobaric (constant-pressure) expansions of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [1/K].

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).isobaric_expansion_ls
[0.0012736035771253886, 0.0011234157437069571]
```

#### property k

Thermal conductivity of the mixture at its current phase, temperature, and pressure in units of [W/m/K]. Available only if single phase.

#### **Examples**

```
>>> Mixture(['ethanol'], ws=[1], T=300).kl
0.16313594741877802
```

## property kg

Thermal conductivity of the mixture in the gas phase at its current temperature, pressure, and composition in units of [Pa\*s].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.thermal\_conductivity*. *ThermalConductivityGasMixture*; each Mixture instance creates one to actually perform the calculations.

#### **Examples**

```
>>> Mixture(['water'], ws=[1], T=500).kg
0.036035173297862676
```

#### property kgs

Pure component thermal conductivies of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [W/m/K].

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).kgs
[0.011865404482987936, 0.010981336502491088]
```

## property kl

Thermal conductivity of the mixture in the liquid phase at its current temperature, pressure, and composition in units of [Pa\*s].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface thermo.thermal\_conductivity. ThermalConductivityLiquidMixture; each Mixture instance creates one to actually perform the calculations.

### **Examples**

```
>>> Mixture(['water'], ws=[1], T=320).kl
0.6369957248212118
```

### property kls

Pure component thermal conductivities of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [W/m/K].

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).kls
[0.13391538485205587, 0.12429339088930591]
```

### ks = None

### property legal\_statuses

List of dictionaries of the legal status for all chemicals in the mixture.

## **Examples**

```
>>> Mixture(['oxygen', 'nitrogen'], zs=[.5, .5]).legal_statuses
[{'DSL': 'LISTED',
    'NLP': 'UNLISTED',
    'SPIN': 'LISTED',
    'TSCA': 'LISTED'},
    {'DSL': 'LISTED',
    'NLP': 'UNLISTED',
    'SPIN': 'LISTED',
    'SPIN': 'LISTED',
    'SPIN': 'LISTED',
    'SPIN': 'LISTED',
```

## property mass\_fractions

Dictionary of mass fractions for each atom in the mixture.

```
>>> Mixture(['CO2', 'O2'], zs=[0.5, 0.5]).mass_fractions
{'C': 0.15801826905745822, 'O': 0.8419817309425419}
```

### property mass\_fractionss

List of dictionaries of mass fractions for all chemicals in the mixture.

### **Examples**

```
>>> Mixture(['oxygen', 'nitrogen'], zs=[.5, .5]).mass_fractionss
[{'0': 1.0}, {'N': 1.0}]
```

#### property mu

Viscosity of the mixture at its current phase, temperature, and pressure in units of [Pa\*s]. Available only if single phase.

#### **Examples**

```
>>> Mixture(['ethanol'], ws=[1], T=400).mu
1.1853097849748213e-05
```

#### property mug

Viscosity of the mixture in the gas phase at its current temperature, pressure, and composition in units of [Pa\*s].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.viscosity.ViscosityGasMixture*; each Mixture instance creates one to actually perform the calculations.

### **Examples**

```
>>> Mixture(['water'], ws=[1], T=500).mug
1.7298722343367148e-05
```

#### property mugs

Pure component viscosities of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [Pa\*s].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).mugs
[8.082880451060605e-06, 7.442602145854158e-06]
```

#### property mul

Viscosity of the mixture in the liquid phase at its current temperature, pressure, and composition in units of [Pa\*s].

For calculation of this property at other temperatures and pressures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.viscosity*. *ViscosityLiquidMixture*; each Mixture instance creates one to actually perform the calculations.

```
>>> Mixture(['water'], ws=[1], T=320).mul
0.0005767262693751547
```

### property muls

Pure component viscosities of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [Pa\*s].

## **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).muls
[0.00045545522798131764, 0.00043274394349114754]
```

#### property nu

Kinematic viscosity of the mixture at its current temperature, pressure, and phase in units of [m<sup>2</sup>/s]. Available only if single phase.

$$\nu = \frac{\mu}{\rho}$$

### **Examples**

```
>>> Mixture(['argon'], ws=[1]).nu
1.3842643382482236e-05
```

### property nug

Kinematic viscosity of the gas phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\nu = \frac{\mu}{\rho}$$

### **Examples**

```
>>> Mixture(['methane'], ws=[1], T=115).nug
2.5118460023343146e-06
```

#### property nugs

Pure component kinematic viscosities of the gas phase of the chemicals in the mixture at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\nu = \frac{\mu}{\rho}$$

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).nugs
[5.357870271650772e-07, 3.8127962283230277e-07]
```

## property nul

Kinematic viscosity of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\nu = \frac{\mu}{\rho}$$

## Examples

```
>>> Mixture(['methane'], ws=[1], T=110).nul
2.858088468937333e-07
```

#### property nuls

Pure component kinematic viscosities of the liquid phase of the chemicals in the mixture at its current temperature and pressure, in units of  $[m^2/s]$ .

$$\nu = \frac{\mu}{\rho}$$

### **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).nuls
[5.357870271650772e-07, 3.8127962283230277e-07]
```

#### property permittivites

Pure component relative permittivities of the chemicals in the mixture at its current temperature, [dimensionless].

#### Examples

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).permittivites
[2.23133472, 1.8508128]
```

### phase = None

properties(copy\_pures=True, copy\_mixtures=True)

### property\_package\_constants = None

#### property rho

Mass density of the mixture at its current phase and temperature and pressure, in units of [kg/m^3]. Available only if single phase.

```
>>> Mixture(['decane'], ws=[1], T=550, P=2E6).rho
498.67008448640604
```

## property rhog

Gas-phase mass density of the mixture at its current temperature, pressure, and composition in units of [kg/m^3]. For calculation of this property at other temperatures, pressures, or compositions or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume*. *VolumeGasMixture*; each Mixture instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

### **Examples**

```
>>> Mixture(['hexane'], ws=[1], T=300, P=2E5).rhog
7.914447603999089
```

### property rhog\_STP

Gas-phase mass density of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [kg/m^3].

## **Examples**

```
>>> Mixture(['nitrogen'], ws=[1]).rhog_STP
1.145534453639403
```

### property rhogm

Molar density of the mixture in the gas phase at the current temperature, pressure, and composition in units of [mol/m^3].

Utilizes the object oriented interface and thermo.volume.VolumeGasMixture to perform the actual calculation of molar volume.

## **Examples**

```
>>> Mixture(['water'], ws=[1], T=500).rhogm
24.467426039789093
```

## property rhogm\_STP

Molar density of the mixture in the gas phase at 298.15 K and 101.325 kPa, and the current composition, in units of [mol/m^3].

```
>>> Mixture(['nitrogen'], ws=[1]).rhogm_STP
40.892374850585895
```

## property rhogms

Pure component molar densities of the chemicals in the gas phase at the current temperature and pressure, in units of [mol/m^3].

## **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).rhogms
[40.11392035309789, 41.407547778608084]
```

## property rhogs

Pure-component gas-phase mass densities of the chemicals in the mixture at its current temperature and pressure, in units of [kg/m^3].

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).rhogs
[3.1333721283939258, 3.8152260283954584]
```

#### property rhol

Liquid-phase mass density of the mixture at its current temperature, pressure, and composition in units of [kg/m^3]. For calculation of this property at other temperatures, pressures, compositions or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.volume*. *VolumeLiquidMixture*; each Mixture instance creates one to actually perform the calculations. Note that that interface provides output in molar units.

### **Examples**

```
>>> Mixture(['o-xylene'], ws=[1], T=297).rhol
876.9946785618097
```

#### property rhol\_STP

Liquid-phase mass density of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [kg/m^3].

## **Examples**

```
>>> Mixture(['cyclobutane'], ws=[1]).rhol_STP
688.9851989526821
```

#### property rholm

Molar density of the mixture in the liquid phase at the current temperature, pressure, and composition in units of [mol/m^3].

Utilizes the object oriented interface and *thermo.volume.VolumeLiquidMixture* to perform the actual calculation of molar volume.

```
>>> Mixture(['water'], ws=[1], T=300).rholm
55317.352773503124
```

## property rholm\_STP

Molar density of the mixture in the liquid phase at 298.15 K and 101.325 kPa, and the current composition, in units of [mol/m^3].

## **Examples**

```
>>> Mixture(['water'], ws=[1]).rholm_STP
55344.59086372442
```

### property rholms

Pure component molar densities of the chemicals in the mixture in the liquid phase at the current temperature and pressure, in units of [mol/m^3].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).rholms
[10882.699301520635, 9135.590853014008]
```

#### property rhols

Pure-component liquid-phase mass density of the chemicals in the mixture at its current temperature and pressure, in units of [kg/m^3].

#### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).rhols
[850.0676666084917, 841.7389069631628]
```

#### property rhom

Molar density of the mixture at its current phase and temperature and pressure, in units of [mol/m<sup>3</sup>]. Available only if single phase.

#### **Examples**

```
>>> Mixture(['1-hexanol'], ws=[1]).rhom
7983.414573003429
```

## rhos = None

#### property rhosms

Pure component molar densities of the chemicals in the solid phase at the current temperature and pressure, in units of [mol/m^3].

```
>>> Mixture(['iron'], ws=[1], T=320).rhosms
[140925.7767033753]
```

## property rhoss

Pure component solid-phase mass density of the chemicals in the mixture at its current temperature, in units of [kg/m^3].

## **Examples**

```
>>> Mixture(['iron'], ws=[1], T=320).rhoss
[7869.999999999994]
```

## property ringss

List of ring counts for all chemicals in the mixture.

#### **Examples**

```
>>> Mixture(['Docetaxel', 'Paclitaxel'], zs=[.5, .5]).ringss
[6, 7]
```

### set\_Chemical\_property\_objects()

### set\_TP\_sources()

#### set\_chemical\_TP(T=None, P=None)

Basic method to change all chemical instances to be at the T and P specified. If they are not specified, the the values of the mixture will be used. This is not necessary for using the Mixture instance unless values specified to chemicals are required.

## set\_chemical\_constants()

Basic method which retrieves and sets constants of chemicals to be accessible as lists from a Mixture object. This gets called automatically on the instantiation of a new Mixture instance.

#### set\_constant\_sources()

#### set\_constants()

set\_eos(T, P, eos=<class 'thermo.eos\_mix.PRMIX'>)

#### set\_property\_package(pkg=None)

#### property sigma

Surface tension of the mixture at its current temperature and composition, in units of [N/m].

For calculation of this property at other temperatures, or specifying manually the method used to calculate it, and more - see the object oriented interface *thermo.interface.SurfaceTensionMixture*; each Mixture instance creates one to actually perform the calculations.

```
>>> Mixture(['water'], ws=[1], T=300, P=1E5).sigma
0.07176932405246211
```

## property sigmas

Pure component surface tensions of the chemicals in the mixture at its current temperature, in units of [N/m].

## Examples

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5], T=320).sigmas
[0.02533469712937521, 0.025254723406585546]
```

### property similarity\_variables

Similarity variables for all chemicals in the mixture, see chemicals.elements.similarity\_variable for the definition, [mol/g]

### **Examples**

```
>>> Mixture(['benzene', 'toluene'], ws=[0.5, 0.5]).similarity_variables
[0.15362587797189262, 0.16279853724428964]
```

#### property smiless

SMILES strings for all chemicals in the mixture.

#### **Examples**

>>> Mixture(['methane', 'ethane', 'propane', 'butane'], ... zs=[0.25, 0.25, 0.25, 0.25]).smiless ['C', 'CC', 'CCC', 'CCCC']

#### property solubility\_parameters

Pure component solubility parameters of the chemicals in the mixture at its current temperature and pressure, in units of [Pa^0.5].

$$\delta = \sqrt{\frac{\Delta H_{vap} - RT}{V_m}}$$

### **Examples**

```
>>> Mixture(['benzene', 'hexane'], ws=[0.5, 0.5], T=320).solubility_parameters
[18062.51359608708, 14244.12852702228]
```

#### property speed\_of\_sound

Bulk speed of sound of the mixture at its current temperature, [m/s].

```
>>> Mixture(['toluene'], P=1E5, VF=0.5, ws=[1]).speed_of_sound
478.99527258140211
```

## property speed\_of\_sound\_g

Gas-phase speed of sound of the mixture at its current temperature, [m/s].

### **Examples**

```
>>> Mixture(['nitrogen'], ws=[1]).speed_of_sound_g
351.77445481641661
```

### property speed\_of\_sound\_1

Liquid-phase speed of sound of the mixture at its current temperature, [m/s].

## **Examples**

```
>>> Mixture(['toluene'], P=1E5, T=300, ws=[1]).speed_of_sound_1
1116.0852487852942
```

### property synonymss

Lists of synonyms for all chemicals in the mixture.

### **Examples**

### xs = None

ys = None

# 7.21 Permittivity/Dielectric Constant (thermo.permittivity)

This module contains implementations of *TDependentProperty* representing liquid permittivity. A variety of estimation and data methods are available as included in the *chemicals* library.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

• Pure Liquid Permittivity

# 7.21.1 Pure Liquid Permittivity

class thermo.permittivity.PermittivityLiquid(CASRN=", extrapolation='linear', \*\*kwargs)
Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with liquid permittivity as a function of temperature. Consists of one temperature-dependent simple expression, one constant value source, and IAPWS.

### Parameters

CASRN [str, optional] The CAS number of the chemical

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

### Notes

To iterate over all methods, use the list stored in *permittivity\_methods*.

**CRC:** Simple polynomials for calculating permittivity over a specified temperature range only. The full expression is:

$$\epsilon_r = A + BT + CT^2 + DT^3$$

Not all chemicals use all terms; in fact, few do. Data is available for 759 liquids, from [1].

- **CRC\_CONSTANT:** Constant permittivity values at specified temperatures only. Data is from [1], and is available for 1303 liquids.
- IAPWS: The IAPWS model for water permittivity as a liquid.

#### References

#### [1]

### Attributes

Tmax Maximum temperature (K) at which the current method can calculate the property.

*Tmin* Minimum temperature (K) at which the current method can calculate the property.

### **Methods**

calculate(T, method)	Method to calculate permittivity of a liquid at tem-
	perature $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

#### property Tmax

Maximum temperature (K) at which the current method can calculate the property.

### property Tmin

Minimum temperature (K) at which the current method can calculate the property.

#### calculate(T, method)

Method to calculate permittivity of a liquid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature at which to calculate relative permittivity, [K]

method [str] Name of the method to use

Returns

epsilon [float] Relative permittivity of the liquid at T, [-]

#### name = 'liquid relative permittivity'

### property\_max = 1000.0

Maximum valid of permittivity; highest in the data available is ~240.

#### property\_min = 1.0

Relative permittivity must always be larger than 1; nothing is better than a vacuum.

ranked\_methods = ['IAPWS', 'CRC', 'CRC\_CONSTANT']
Default rankings of the available methods.

#### test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

### **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

## units = '-'

thermo.permittivity.permittivity\_methods = ['CRC', 'CRC\_CONSTANT', 'IAPWS']

Holds all methods available for the *PermittivityLiquid* class, for use in iterating over them.

# 7.22 Phase Models (thermo.phases)

```
• Base Class
```

- Ideal Gas Equation of State
- Cubic Equations of State
  - Gas Phases
  - Liquid Phases

- Activity Based Liquids
- Fundamental Equations of State
- CoolProp Wrapper

The phases subpackage exposes classes that represent the state of single phase mixture, including the composition, temperature, pressure, enthalpy, and entropy. Phase objects are immutable and know nothing about bulk properties or transport properties. The goal is for each phase to be able to compute all of its thermodynamic properties, including volume-based ones. Use settings to handle different assumptions.

# 7.22.1 Base Class

### class thermo.phases.Phase

Bases: object

*Phase* is the base class for all phase objects in *thermo*. Each sub-class implements a number of core properties; many other properties can be calculated from them.

Among those properties are H, S, Cp, dP\_dT, dP\_dV, d2P\_dT2, d2P\_dV2, and d2P\_dTdV.

An additional set of properties that can be implemented and that enable more functionality are  $dH_dP$ ,  $dS_dT$ ,  $dS_dP$ ,  $d2H_dT2$ ,  $d2H_dP2$ ,  $d2S_dP2$ ,  $dH_dT_V$ ,  $dH_dP_V$ ,  $dH_dV_T$ ,  $dH_dV_P$ ,  $dS_dT_V$ ,  $dS_dP_V$ ,  $d2H_dTdP$ ,  $d2H_dT2_V$ ,  $d2P_dTdP$ ,  $d2P_dVdP$ ,  $d2P_dVdT_TP$ ,  $d2P_dT2_PV$ .

Some models may re-implement properties which would normally be calculated by this *Phase* base class because they have more explicit, faster ways of calculating the property.

When a phase object is the result of a Flash calculation, the resulting phase objects have a reference to a *ChemicalConstantsPackage* object and all of its properties can be accessed from from the resulting phase objects as well.

A *ChemicalConstantsPackage* object can also be manually set to the attribute *constants* to enable access to those properties. This includes mass-based properties, which are not accessible from Phase objects without a reference to the constants.

### Attributes

CASs CAS registration numbers for each component, [-].

Carcinogens Status of each component in cancer causing registries, [-].

Ceilings Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

*GWPs* Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

Gfgs Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

Gfgs\_mass Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

Hcs Higher standard molar heats of combustion for each component, [J/mol].

Hcs\_lower Lower standard molar heats of combustion for each component, [J/mol].

Hcs\_lower\_mass Lower standard heats of combustion for each component, [J/kg].

Hcs\_mass Higher standard heats of combustion for each component, [J/kg].

Hf\_STPs Standard state molar enthalpies of formation for each component, [J/mol].

Hf\_STPs\_mass Standard state mass enthalpies of formation for each component, [J/kg].

- **Hfgs** Ideal gas standard molar enthalpies of formation for each component, [J/mol].
- *Hfgs\_mass* Ideal gas standard enthalpies of formation for each component, [J/kg].
- Hfus\_Tms Molar heats of fusion for each component at their respective melting points, [J/mol].
- Hfus\_Tms\_mass Heats of fusion for each component at their respective melting points, [J/kg].
- Hsub\_Tts Heats of sublimation for each component at their respective triple points, [J/mol].
- Hsub\_Tts\_mass Heats of sublimation for each component at their respective triple points, [J/kg].
- Hvap\_298s Molar heats of vaporization for each component at 298.15 K, [J/mol].
- Hvap\_298s\_mass Heats of vaporization for each component at 298.15 K, [J/kg].
- *Hvap\_Tbs* Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].
- Hvap\_Tbs\_mass Heats of vaporization for each component at their respective normal boiling points, [J/kg].
- InChI\_Keys InChI Keys for each component, [-].
- InChIs InChI strings for each component, [-].
- LFLs Lower flammability limits for each component, [-].
- MWs Similatiry variables for each component, [g/mol].
- **ODPs** Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].
- PSRK\_groups PSRK subgroup: count groups for each component, [-].
- Parachors Parachors for each component, [N^0.25\*m^2.75/mol].
- **Pcs** Critical pressures for each component, [Pa].
- Psat\_298s Vapor pressures for each component at 298.15 K, [Pa].
- *Pts* Triple point pressures for each component, [Pa].
- PubChems Pubchem IDs for each component, [-].
- **RI\_Ts** Temperatures at which the refractive indexes were reported for each component, [K].
- **RIs** Refractive indexes for each component, [-].
- **S0gs** Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].
- **S0gs\_mass** Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].
- **STELs** Short term exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].
- *Sfgs* Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].
- Sfgs\_mass Ideal gas standard entropies of formation for each component, [J/(kg\*K)].
- Skins Whether each compound can be absorbed through the skin or not, [-].
- StielPolars Stiel polar factors for each component, [-].
- *Stockmayers* Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].
- **TWAs** Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

Tautoignitions Autoignition temperatures for each component, [K].

*Tbs* Boiling temperatures for each component, [K].

Tcs Critical temperatures for each component, [K].

Tflashs Flash point temperatures for each component, [K].

Tms Melting temperatures for each component, [K].

*Tts* Triple point temperatures for each component, [K].

UFLs Upper flammability limits for each component, [-].

UNIFAC\_Dortmund\_groups UNIFAC\_Dortmund\_group: count groups for each component, [-].

UNIFAC\_Qs UNIFAC Q parameters for each component, [-].

**UNIFAC\_Rs** UNIFAC *R* parameters for each component, [-].

UNIFAC\_groups UNIFAC\_group: count groups for each component, [-].

**VF** Method to return the vapor fraction of the phase.

Van\_der\_Waals\_areas Unnormalized Van der Waals areas for each component, [m^2/mol].

Van\_der\_Waals\_volumes Unnormalized Van der Waals volumes for each component, [m^3/mol].

Vcs Critical molar volumes for each component, [m^3/mol].

- Vmg\_STPs Gas molar volumes for each component at STP; metastable if normally another state, [m^3/mol].
- Vml\_60Fs Liquid molar volumes for each component at 60 °F, [m^3/mol].

*Vml\_STPs* Liquid molar volumes for each component at STP, [m^3/mol].

Vml\_Tms Liquid molar volumes for each component at their respective melting points, [m^3/mol].

Vms\_Tms Solid molar volumes for each component at their respective melting points, [m^3/mol].

Zcs Critical compressibilities for each component, [-].

atomss Breakdown of each component into its elements and their counts, as a dict, [-].

beta Method to return the phase fraction of this phase.

beta\_mass Method to return the mass phase fraction of this phase.

beta\_volume Method to return the volumetric phase fraction of this phase.

charges Charge number (valence) for each component, [-].

conductivities Electrical conductivities for each component, [S/m].

*conductivity\_Ts* Temperatures at which the electrical conductivities for each component were measured, [K].

dipoles Dipole moments for each component, [debye].

*economic\_statuses* Status of each component in in relation to import and export from various regions, [-].

force\_phase

formulas Formulas of each component, [-].

- legal\_statuses Status of each component in in relation to import and export rules from various regions, [-].
- logPs Octanol-water partition coefficients for each component, [-].
- molecular\_diameters Lennard-Jones molecular diameters for each component, [angstrom].
- names Names for each component, [-].
- omegas Acentric factors for each component, [-].
- phase\_STPs Standard states ('g', 'l', or 's') for each component, [-].
- rhocs Molar densities at the critical point for each component, [mol/m^3].
- *rhocs\_mass* Densities at the critical point for each component, [kg/m^3].
- *rhog\_STPs* Molar gas densities at STP for each component; metastable if normally another state, [mol/m^3].
- *rhog\_STPs\_mass* Gas densities at STP for each component; metastable if normally another state, [kg/m^3].
- *rhol\_60Fs* Liquid molar densities for each component at 60 °F, [mol/m^3].
- rhol\_60Fs\_mass Liquid mass densities for each component at 60 °F, [kg/m^3].
- *rhol\_STPs* Molar liquid densities at STP for each component, [mol/m^3].
- rhol\_STPs\_mass Liquid densities at STP for each component, [kg/m^3].
- *rhos\_Tms* Solid molar densities for each component at their respective melting points, [mol/m^3].
- rhos\_Tms\_mass Solid mass densities for each component at their melting point, [kg/m^3].
- sigma\_STPs Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].
- *sigma\_Tbs* Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].
- sigma\_Tms Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].

similarity\_variables Similarity variables for each component, [mol/g].

smiless SMILES identifiers for each component, [-].

solubility\_parameters Solubility parameters for each component at 298.15 K, [Pa^0.5].

## Methods

A()	Method to calculate and return the Helmholtz energy
	of the phase.
API()	Method to calculate and return the API of the phase.
A_dep()	Method to calculate and return the departure
	Helmholtz energy of the phase.
A_formation_ideal_gas()	Method to calculate and return the ideal-gas
	Helmholtz energy of formation of the phase (as if
	the phase was an ideal gas).
A_ideal_gas()	Method to calculate and return the ideal-gas
	Helmholtz energy of the phase.
	continues on port page

Table 80 – c	ontinued from previous page
A_mass()	Method to calculate and return mass Helmholtz en-
	ergy of the phase.
A_reactive()	Method to calculate and return the Helmholtz free en-
_ 0	ergy of the phase on a reactive basis.
<i>Cp()</i>	Method to calculate and return the constant-pressure
CP()	heat capacity of the phase.
Cp_Cv_ratio()	Method to calculate and return the Cp/Cv ratio of the
$cp_cv_latio()$	
(n (w matio ideal acc()	phase. Method to calculate and return the ratio of the ideal-
Cp_Cv_ratio_ideal_gas()	
	gas heat capacity to its constant-volume heat capac-
	ity.
Cp_ideal_gas()	Method to calculate and return the ideal-gas heat ca-
	pacity of the phase.
Cp_mass()	Method to calculate and return mass constant pres-
	sure heat capacity of the phase.
Cpig_integrals_over_T_pure()	Method to calculate and return the integrals of the
	ideal-gas heat capacities divided by temperature of
	every component in the phase from a temperature of
	<i>Phase.T_REF_IG</i> to the system temperature.
<pre>Cpig_integrals_pure()</pre>	Method to calculate and return the integrals of the
	ideal-gas heat capacities of every component in the
	phase from a temperature of <i>Phase</i> . T_REF_IG to the
	system temperature.
Cpigs_pure()	Method to calculate and return the ideal-gas heat ca-
	pacities of every component in the phase.
<i>Cv</i> ()	Method to calculate and return the constant-volume
	heat capacity $Cv$ of the phase.
Cv_dep()	Method to calculate and return the difference between
	the actual $Cv$ and the ideal-gas constant volume heat
	capacity $C_v^{ig}$ of the phase.
Cv_ideal_gas()	Method to calculate and return the ideal-gas constant
cv_iucui_gub()	volume heat capacity of the phase.
Cv_mass()	Method to calculate and return mass constant volume
(v_mass()	heat capacity of the phase.
60	
G()	Method to calculate and return the Gibbs free energy
C dow()	of the phase.
G_dep()	Method to calculate and return the departure Gibbs
	free energy of the phase.
G_dep_phi_consistency()	Method to calculate and return a consistency check
	between departure Gibbs free energy, and the fugac-
	ity coefficients.
<pre>G_formation_ideal_gas()</pre>	Method to calculate and return the ideal-gas Gibbs
	free energy of formation of the phase (as if the phase
	was an ideal gas).
G_ideal_gas()	Method to calculate and return the ideal-gas Gibbs
	free energy of the phase.
	Method to calculate and return mass Gibbs energy of
G_mass()	
G_mass()	the phase.
G_mass() G_min()	the phase. Method to calculate and return the Gibbs free energy

Table 80 – continu	ued from previous page
G_min_criteria()	Method to calculate and return the Gibbs energy cri-
	teria required for comparing phase stability.
G_reactive()	Method to calculate and return the Gibbs free energy
	of the phase on a reactive basis.
H()	Method to calculate and return the enthalpy of the
	phase.
H_C_ratio()	Method to calculate and return the atomic ratio of hy-
	drogen atoms to carbon atoms, based on the current
	composition of the phase.
H_C_ratio_mass()	Method to calculate and return the mass ratio of hy-
<u>11_0_14010_mabb()</u>	drogen atoms to carbon atoms, based on the current
	composition of the phase.
H_dep_phi_consistency()	Method to calculate and return a consistency check
n_ucp_pni_consistency()	between departure enthalpy, and the fugacity coeffi-
	cients' temperature derivatives.
H_formation_ideal_gas()	Method to calculate and return the ideal-gas enthalpy
II_IOIIMACIOII_IUEAI_YAS()	of formation of the phase (as if the phase was an ideal
II Grow which	gas).
H_from_phi()	Method to calculate and return the enthalpy of the
	fluid as calculated from the ideal-gas enthalpy and the
	the fugacity coefficients' temperature derivatives.
H_ideal_gas()	Method to calculate and return the ideal-gas enthalpy
	of the phase.
H_mass()	Method to calculate and return mass enthalpy of the
	phase.
H_phi_consistency()	Method to calculate and return a consistency check
	between ideal gas enthalpy behavior, and the fugacity
	coefficients and their temperature derivatives.
H_reactive()	Method to calculate and return the enthalpy of the
	phase on a reactive basis, using the <i>Hfs</i> values of the
	phase.
Hc()	Method to calculate and return the molar ideal-gas
	higher heat of combustion of the object, [J/mol]
Hc_lower()	Method to calculate and return the molar ideal-gas
	lower heat of combustion of the object, [J/mol]
<pre>Hc_lower_mass()</pre>	Method to calculate and return the mass ideal-gas
	lower heat of combustion of the object, [J/mol]
Hc_lower_normal()	Method to calculate and return the volumetric ideal-
~	gas lower heat of combustion of the object using the
	normal gas volume, [J/m^3]
<pre>Hc_lower_standard()</pre>	Method to calculate and return the volumetric ideal-
	gas lower heat of combustion of the object using the
	standard gas volume, [J/m^3]
Hc_mass()	Method to calculate and return the mass ideal-gas
11C_11105()	higher heat of combustion of the object, [J/mol]
Hc_normal()	Method to calculate and return the volumetric ideal-
iic_iioi mai()	gas higher heat of combustion of the object using the
	normal gas volume, [J/m^3]
II. standard()	
Hc_standard()	Method to calculate and return the volumetric ideal-
Hc_standard()	

	continued from previous page
<pre>Joule_Thomson()</pre>	Method to calculate and return the Joule-Thomson
	coefficient of the phase.
MW()	Method to calculate and return molecular weight of
	the phase.
MW_inv()	Method to calculate and return inverse of molecular
	weight of the phase.
PIP()	Method to calculate and return the phase identifica-
	tion parameter of the phase.
P_max_at_V(V)	Dummy method.
P_transitions()	Dummy method.
Pmc()	Method to calculate and return the mechanical criti-
()	cal pressure of the phase.
<i>S</i> ()	Method to calculate and return the entropy of the
5()	phase.
SG()	Method to calculate and return the standard liquid
500	specific gravity of the phase, using constant liquid
	pure component densities not calculated by the phase
<b>66</b>	object, at 60 °F.
SG_gas()	Method to calculate and return the specific gravity of
	the phase with respect to a gas reference density.
S_dep_phi_consistency()	Method to calculate and return a consistency check
	between ideal gas entropy behavior, and the fugacity
	coefficients and their temperature derivatives.
<pre>S_formation_ideal_gas()</pre>	Method to calculate and return the ideal-gas entropy
	of formation of the phase (as if the phase was an idea
	gas).
S_from_phi()	Method to calculate and return the entropy of the fluid
	as calculated from the ideal-gas entropy and the the
	fugacity coefficients' temperature derivatives.
S_ideal_gas()	Method to calculate and return the ideal-gas entropy
	of the phase.
S_mass()	Method to calculate and return mass entropy of the
	phase.
<pre>S_phi_consistency()</pre>	Method to calculate and return a consistency check
	between ideal gas entropy behavior, and the fugacity
	coefficients and their temperature derivatives.
S_reactive()	Method to calculate and return the entropy of the
	phase on a reactive basis, using the Sfs values of the
	phase of a reactive basis, using the 5/3 values of the
T_max_at_V(V)	Method to calculate the maximum temperature the
$1_{\text{max}_{a} \leq V(V)}$	
	phase can create at a constant volume, if one exists returns None otherwise.
Tmc()	Method to calculate and return the mechanical critic
**()	cal temperature of the phase.
U()	Method to calculate and return the internal energy of
	the phase.
U_dep()	Method to calculate and return the departure international
	energy of the phase.
	Method to calculate and return the ideal-gas interna
U_formation_ideal_gas()	$\varphi$
<pre>U_formation_ideal_gas()</pre>	energy of formation of the phase (as if the phase was

U_ideal_gas()	continued from previous page Method to calculate and return the ideal-gas interna
0_1uea1_gas()	-
II maga()	energy of the phase.
U_mass()	Method to calculate and return mass internal energy
	of the phase.
U_reactive()	Method to calculate and return the internal energy o
	the phase on a reactive basis.
V()	Method to return the molar volume of the phase.
V_dep()	Method to calculate and return the departure (from ideal gas behavior) molar volume of the phase.
V_from_phi()	Method to calculate and return the molar volume of
	the fluid as calculated from the pressure derivative
	of fugacity coefficients.
V_gas()	Method to calculate and return the ideal-gas mola
	volume of the phase at the chosen reference tempera
	ture and pressure, according to the temperature vari
	able $T_{gas_ref}$ and pressure variable $P_{gas_ref}$ of
	the thermo.bulk.BulkSettings.
V_gas_normal()	Method to calculate and return the ideal-gas mo
v_gas_norman()	lar volume of the phase at the normal temperatur
	and pressure, according to the temperature variable
	$T_normal$ and pressure variable $P_normal$ of the
	thermo.bulk.BulkSettings.
V_gas_standard()	Method to calculate and return the ideal-gas mo
	lar volume of the phase at the standard temperatur
	and pressure, according to the temperature variabl
	<i>T_standard</i> and pressure variable <i>P_standard</i> of th
	thermo.bulk.BulkSettings.
V_ideal_gas()	Method to calculate and return the ideal-gas mola
	volume of the phase.
V_iter([force])	Method to calculate and return the volume of th
	phase in a way suitable for a TV resolution to con
	verge on the same pressure.
V_liquid_ref()	Method to calculate and return the liquid refer
- 0	ence molar volume according to the temperatur
	variable T_liquid_volume_ref of thermo.bulk
	BulkSettings and the composition of the phase.
V_mass()	Method to calculate and return the specific volume of
	the phase.
V_phi_consistency()	Method to calculate and return a consistency chec
	between molar volume, and the fugacity coefficients
	pressures derivatives.
Vfgs()	Method to calculate and return the ideal-gas volum
	fractions of the components of the phase.
Vfls()	Method to calculate and return the ideal-liquid vol
V113()	-
	ume fractions of the components of the phase
	using the standard liquid densities at the tem
	perature variable <i>T_liquid_volume_ref</i> of thermo
	bulk.BulkSettings and the composition of th
	phase.
Vmc()	Method to calculate and return the mechanical critical volume of the phase.

Tahle	80	- continued	from	nrevious	nad
Table	00	- continueu	IIOIII	previous	page

Table 80 – continue	d from previous page
Wobbe_index()	Method to calculate and return the molar Wobbe in-
	dex of the object, [J/mol].
<pre>Wobbe_index_lower()</pre>	Method to calculate and return the molar lower
V	Wobbe index of the
<pre>Wobbe_index_lower_mass()</pre>	Method to calculate and return the lower mass Wobbe
~	index of the object, [J/kg].
<pre>Wobbe_index_lower_normal()</pre>	Method to calculate and return the volumetric normal
	lower Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_lower_standard()</pre>	Method to calculate and return the volumetric stan-
	dard lower Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_mass()</pre>	Method to calculate and return the mass Wobbe index
V	of the object, [J/kg].
<pre>Wobbe_index_normal()</pre>	Method to calculate and return the volumetric normal
V	Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_standard()</pre>	Method to calculate and return the volumetric stan-
V	dard Wobbe index of the object, [J/m^3].
Z()	Method to calculate and return the compressibility
	factor of the phase.
Zmc()	Method to calculate and return the mechanical criti-
	cal compressibility of the phase.
activities()	Method to calculate and return the activities of each
V	component in the phase [-].
as_json()	Method to create a JSON-friendly serialization of the
_3	phase which can be stored, and reloaded later.
<pre>atom_fractions()</pre>	Method to calculate and return the atomic composi-
_ ~	tion of the phase; returns a dictionary of atom frac-
	tion (by count), containing only those elements who
	are present.
<pre>atom_mass_fractions()</pre>	Method to calculate and return the atomic mass frac-
	tions of the phase; returns a dictionary of atom frac-
	tion (by mass), containing only those elements who
	are present.
<pre>chemical_potential()</pre>	Method to calculate and return the chemical poten-
	tials of each component in the phase [-].
d2P_dT2()	Method to calculate and return the second tempera-
	ture derivative of pressure of the phase.
$d2P_dTdV()$	Method to calculate and return the second derivative
	of pressure with respect to temperature and volume
	of the phase.
d2P_dTdrho()	Method to calculate and return the temperature
	derivative and then molar density derivative of the
	pressure of the phase.
d2P_dV2()	Method to calculate and return the second volume
-	derivative of pressure of the phase.
d2P_dVdT()	Method to calculate and return the second derivative
~	of pressure with respect to temperature and volume
	of the phase.
d2P_drho2()	Method to calculate and return the second molar den-
	sity derivative of pressure of the phase.

Table 80 – continued from previous page

Tabl	e 80 – continued from previous page
d2T_dP2()	Method to calculate and return the constant-volume
	second pressure derivative of temperature of the
	phase.
d2T_dP2_V()	Method to calculate and return the constant-volume
	second pressure derivative of temperature of the
	phase.
d2T_dPdV()	Method to calculate and return the derivative of pres-
	sure and then the derivative of volume of temperature
	of the phase.
d2T_dPdrho()	Method to calculate and return the pressure derivative
	and then molar density derivative of the temperature
	of the phase.
d2T_dV2()	Method to calculate and return the constant-pressure
	second volume derivative of temperature of the
	phase.
d2T_dV2_P()	Method to calculate and return the constant-pressure
~	second volume derivative of temperature of the
	phase.
d2T_dVdP()	Method to calculate and return the derivative of pres-
	sure and then the derivative of volume of temperature
	of the phase.
d2T_drho2()	Method to calculate and return the second molar den-
	sity derivative of temperature of the phase.
d2V_dP2()	Method to calculate and return the constant-
	temperature pressure derivative of volume of the
	phase.
d2V_dP2_T()	Method to calculate and return the constant-
	temperature pressure derivative of volume of the
	phase.
d2V_dPdT()	Method to calculate and return the derivative of pres-
	sure and then the derivative of temperature of volume
	of the phase.
d2V_dT2()	Method to calculate and return the constant-pressure
	second temperature derivative of volume of the
	phase.
d2V_dT2_P()	Method to calculate and return the constant-pressure
	second temperature derivative of volume of the
	phase.
d2V_dTdP()	Method to calculate and return the derivative of pres-
	sure and then the derivative of temperature of volume
	of the phase.
d2rho_dP2()	Method to calculate and return the second pressure
	derivative of molar density of the phase.
d2rho_dPdT()	Method to calculate and return the pressure derivative
	and then temperature derivative of the molar density
	of the phase.
d2rho_dT2()	Method to calculate and return the second tempera-
	ture derivative of molar density of the phase.
dA_dP()	Method to calculate and return the constant-
~	temperature pressure derivative of Helmholtz
	energy.
	continues on next page

Table 80 – c	ontinued from previous page
$dA_dP_T()$	Method to calculate and return the constant-
	temperature pressure derivative of Helmholtz
	energy.
$dA_dP_V()$	Method to calculate and return the constant-volume
	pressure derivative of Helmholtz energy.
$dA_dT()$	Method to calculate and return the constant-pressure
	temperature derivative of Helmholtz energy.
dA_dT_P()	Method to calculate and return the constant-pressure
	temperature derivative of Helmholtz energy.
dA_dT_V()	Method to calculate and return the constant-volume
	temperature derivative of Helmholtz energy.
$dA_dV_P()$	Method to calculate and return the constant-pressure
	volume derivative of Helmholtz energy.
$dA_dV_T()$	Method to calculate and return the constant-
	temperature volume derivative of Helmholtz energy.
dA_mass_dP([prop])	Method to calculate and return the pressure derivative
··· • • ···	of mass Helmholtz energy of the phase at constant
	temperature.
dA_mass_dP_T([prop])	Method to calculate and return the pressure derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
dA_mass_dP_V([prop])	Method to calculate and return the pressure derivative
	of mass Helmholtz energy of the phase at constant
	volume.
dA_mass_dT([prop])	Method to calculate and return the temperature
	derivative of mass Helmholtz energy of the phase at
	constant pressure.
dA_mass_dT_P([prop])	Method to calculate and return the temperature
	derivative of mass Helmholtz energy of the phase at
	constant pressure.
dA_mass_dT_V([prop])	Method to calculate and return the temperature
	derivative of mass Helmholtz energy of the phase at
	constant volume.
dA_mass_dV_P([prop])	Method to calculate and return the volume derivative
	of mass Helmholtz energy of the phase at constant
	pressure.
dA_mass_dV_T([prop])	Method to calculate and return the volume derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
dCpigs_dT_pure()	Method to calculate and return the first temperature
	derivative of ideal-gas heat capacities of every com-
	ponent in the phase.
dCv_dP_T()	Method to calculate the pressure derivative of Cv,
	constant volume heat capacity, at constant tempera-
	ture.
dCv_dT_P()	Method to calculate the temperature derivative of Cv,
	constant volume heat capacity, at constant pressure.
dCv_mass_dP_T([prop])	Method to calculate and return the pressure derivative
	of mass Constant-volume heat capacity of the phase
	at constant temperature.
	continues on next page

Table 80 - c	ontinued from previous page
dCv_mass_dT_P([prop])	Method to calculate and return the temperature
	derivative of mass Constant-volume heat capacity of
	the phase at constant pressure.
$dG_dP()$	Method to calculate and return the constant-
	temperature pressure derivative of Gibbs free
	energy.
$dG_dP_T()$	Method to calculate and return the constant-
	temperature pressure derivative of Gibbs free
	energy.
$dG_dP_V()$	Method to calculate and return the constant-volume
	pressure derivative of Gibbs free energy.
$dG_dT()$	Method to calculate and return the constant-pressure
	-
	temperature derivative of Gibbs free energy.
$dG_dT_P()$	Method to calculate and return the constant-pressure
	temperature derivative of Gibbs free energy.
$dG_dT_V()$	Method to calculate and return the constant-volume
	temperature derivative of Gibbs free energy.
$dG_dV_P()$	Method to calculate and return the constant-pressure
	volume derivative of Gibbs free energy.
$dG_dV_T()$	Method to calculate and return the constant-
	temperature volume derivative of Gibbs free energy.
dG_mass_dP([prop])	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dG_mass_dP_T([prop])	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dG_mass_dP_V([prop])	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	volume.
dG_mass_dT([prop])	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant pressure.
dG_mass_dT_P([prop])	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant pressure.
dG_mass_dT_V([prop])	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant volume.
dG_mass_dV_P([prop])	Method to calculate and return the volume derivative
	of mass Gibbs free energy of the phase at constant
	pressure.
dG_mass_dV_T([prop])	Method to calculate and return the volume derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
$dH_dP_T()$	Method to calculate and return the pressure derivative
	of enthalpy of the phase at constant pressure.
dH_dT_P()	Method to calculate and return the temperature
**	derivative of enthalpy of the phase at constant pres-
	sure.
	continues on next page

Table 90 continued from p .

Table 80 - cont	tinued from previous page
dH_dns()	Method to calculate and return the mole number
	derivative of the enthalpy of the phase.
dH_mass_dP([prop])	Method to calculate and return the pressure deriva-
	tive of mass enthalpy of the phase at constant tem-
	perature.
dH_mass_dP_T([prop])	Method to calculate and return the pressure deriva-
	tive of mass enthalpy of the phase at constant tem-
	perature.
dH_mass_dP_V([prop])	Method to calculate and return the pressure derivative
	of mass enthalpy of the phase at constant volume.
dH_mass_dT([prop])	Method to calculate and return the temperature
	derivative of mass enthalpy of the phase at constant
	pressure.
<i>dH_mass_dT_P</i> ([prop])	Method to calculate and return the temperature
un_mass_u1_r([ptop])	-
	derivative of mass enthalpy of the phase at constant
	pressure.
<i>dH_mass_dT_V</i> ([prop])	Method to calculate and return the temperature
	derivative of mass enthalpy of the phase at constant
	volume.
dH_mass_dV_P([prop])	Method to calculate and return the volume derivative
	of mass enthalpy of the phase at constant pressure.
dH_mass_dV_T([prop])	Method to calculate and return the volume derivative
	of mass enthalpy of the phase at constant tempera-
	ture.
<i>dP_dP_A</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of pressure of the phase at constant Helmholtz energy.
<i>dP_dP_G</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of pressure of the phase at constant Gibbs energy.
<i>dP_dP_H</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of pressure of the phase at constant enthalpy.
<i>dP_dP_S</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of pressure of the phase at constant entropy.
$dP_dP_T()$	Method to calculate and return the pressure derivative
	of pressure of the phase at constant temperature.
<i>dP_dP_U</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of pressure of the phase at constant internal energy.
$dP_dP_V()$	Method to calculate and return the pressure derivative
V	of pressure of the phase at constant volume.
$dP_dT()$	Method to calculate and return the first temperature
	derivative of pressure of the phase.
<i>dP_dT_A</i> ([property, differentiate_by,])	Method to calculate and return the temperature
;,,,,,;,,)	derivative of pressure of the phase at constant
	Helmholtz energy.
<i>dP_dT_G</i> ([property, differentiate_by,])	Method to calculate and return the temperature
"_"_"_"([property, amerendate_by,])	derivative of pressure of the phase at constant Gibbs
<i>dP_dT_H</i> ([property, differentiate_by,])	energy.           Method to calculate and return the temperature
ar_ar_n([property, unterentiate_by,])	
	derivative of pressure of the phase at constant en-
	thalpy.
	continues on next page

Table 80 – continu	led from previous page
$dP_dT_P()$	Method to calculate and return the temperature
	derivative of temperature of the phase at constant
	pressure.
<i>dP_dT_S</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of pressure of the phase at constant en-
	tropy.
<i>dP_dT_U</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of pressure of the phase at constant internal
	energy.
$dP_dV()$	Method to calculate and return the first volume
	derivative of pressure of the phase.
<i>dP_dV_A</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
ur_uv_n([property, unceentate_by,])	of pressure of the phase at constant Helmholtz energy.
<i>dP_dV_G</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
dr_dv_G([property, differentiate_by,])	
dD du u(faragente differentiate has 1)	of pressure of the phase at constant Gibbs energy.
<i>dP_dV_H</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of pressure of the phase at constant enthalpy.
$dP_dV_P()$	Method to calculate and return the volume derivative
	of pressure of the phase at constant pressure.
<i>dP_dV_S</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of pressure of the phase at constant entropy.
<i>dP_dV_U</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of pressure of the phase at constant internal energy.
dP_drho()	Method to calculate and return the molar density
	derivative of pressure of the phase.
<i>dP_drho_A</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of pressure of the phase at constant Helmholtz energy.
<i>dP_drho_G</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of pressure of the phase at constant Gibbs energy.
<i>dP_drho_H</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of pressure of the phase at constant enthalpy.
<i>dP_drho_S</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of pressure of the phase at constant entropy.
<i>dP_drho_U</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of pressure of the phase at constant internal energy.
$dS_dP_T()$	Method to calculate and return the pressure derivative
	of entropy of the phase at constant pressure.
dS_dV_P()	Method to calculate and return the volume derivative
	of entropy of the phase at constant pressure.
$dS_dV_T()$	Method to calculate and return the volume derivative
us_uv_1()	
	of entropy of the phase at constant temperature.
dS_dns()	Method to calculate and return the mole number
	derivative of the entropy of the phase.
dS_mass_dP([prop])	Method to calculate and return the pressure derivative
	of mass entropy of the phase at constant temperature.
dS_mass_dP_T([prop])	Method to calculate and return the pressure derivative
	of mass entropy of the phase at constant temperature.
dS_mass_dP_V([prop])	Method to calculate and return the pressure derivative
	of mass entropy of the phase at constant volume.
	continues on next page

Table 80 – continued from previous page

	inued from previous page
dS_mass_dT([prop])	Method to calculate and return the temperature
	derivative of mass entropy of the phase at constant
	pressure.
dS_mass_dT_P([prop])	Method to calculate and return the temperature
	derivative of mass entropy of the phase at constant
	pressure.
dS_mass_dT_V([prop])	Method to calculate and return the temperature
	derivative of mass entropy of the phase at constant volume.
dS_mass_dV_P([prop])	Method to calculate and return the volume derivative
	of mass entropy of the phase at constant pressure.
dS_mass_dV_T([prop])	Method to calculate and return the volume derivative
	of mass entropy of the phase at constant temperature.
$dT_dP()$	Method to calculate and return the constant-volume
	pressure derivative of temperature of the phase.
<i>dT_dP_A</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of temperature of the phase at constant Helmholtz en-
	ergy.
<i>dT_dP_G</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of temperature of the phase at constant Gibbs energy.
<i>dT_dP_H</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of temperature of the phase at constant enthalpy.
<i>dT_dP_S</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of temperature of the phase at constant entropy.
$dT_dP_T()$	Method to calculate and return the pressure derivative
	of temperature of the phase at constant temperature.
<i>dT_dP_U</i> ([property, differentiate_by,])	Method to calculate and return the pressure deriva-
	tive of temperature of the phase at constant internal
	energy.
$dT_dP_V()$	Method to calculate and return the constant-volume
	pressure derivative of temperature of the phase.
<i>dT_dT_A</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of temperature of the phase at constant
	Helmholtz energy.
<i>dT_dT_G</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of temperature of the phase at constant
	Gibbs energy.
<i>dT_dT_H</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of temperature of the phase at constant en-
	thalpy.
dT_dT_P()	Method to calculate and return the temperature
	derivative of temperature of the phase at constant
	pressure.
<i>dT_dT_S</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of temperature of the phase at constant en-
	tropy.
<i>dT_dT_U</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of temperature of the phase at constant in- ternal energy.

Method to calculate and return the temperature derivative of temperature of the phase at constant vol- ume.
uiiiv,
Method to calculate and return the constant-pressure
volume derivative of temperature of the phase.
Method to calculate and return the volume derivative
of temperature of the phase at constant Helmholtz en-
ergy.
Method to calculate and return the volume derivative
of temperature of the phase at constant Gibbs energy.
Method to calculate and return the volume derivative
of temperature of the phase at constant enthalpy.
Method to calculate and return the constant-pressure
volume derivative of temperature of the phase.
Method to calculate and return the volume derivative
of temperature of the phase at constant entropy.
Method to calculate and return the volume derivative
of temperature of the phase at constant temperature.
Method to calculate and return the volume derivative
of temperature of the phase at constant internal en-
ergy. Method to calculate and return the molar density
derivative of temperature of the phase.
Method to calculate and return the density derivative
of temperature of the phase at constant Helmholtz en-
ergy. Method to calculate and return the density derivative
•
of temperature of the phase at constant Gibbs energy.
Method to calculate and return the density derivative
of temperature of the phase at constant enthalpy.
Method to calculate and return the density derivative
of temperature of the phase at constant entropy.
Method to calculate and return the density derivative
of temperature of the phase at constant internal en-
ergy.
Method to calculate and return the constant-
temperature pressure derivative of internal energy.
Method to calculate and return the constant-
temperature pressure derivative of internal energy.
Method to calculate and return the constant-volume
pressure derivative of internal energy.
Method to calculate and return the constant-pressure
temperature derivative of internal energy.
Method to calculate and return the constant-pressure
temperature derivative of internal energy.
Method to calculate and return the constant-volume
temperature derivative of internal energy.
Method to calculate and return the constant-pressure
volume derivative of internal energy.
Method to calculate and return the constant- temperature volume derivative of internal energy.

Table 80 – continued from previous page

Table 80 – continu	ed from previous page
dU_mass_dP([prop])	Method to calculate and return the pressure deriva-
	tive of mass internal energy of the phase at constant
	temperature.
dU_mass_dP_T([prop])	Method to calculate and return the pressure deriva-
	tive of mass internal energy of the phase at constant
	temperature.
dU_mass_dP_V([prop])	Method to calculate and return the pressure deriva-
do_mass_dr_v([prop])	tive of mass internal energy of the phase at constant
	volume.
dU_mass_dT([prop])	Method to calculate and return the temperature
	derivative of mass internal energy of the phase at con-
	stant pressure.
dU_mass_dT_P([prop])	Method to calculate and return the temperature
	derivative of mass internal energy of the phase at con-
	stant pressure.
dU_mass_dT_V([prop])	Method to calculate and return the temperature
	derivative of mass internal energy of the phase at con-
	stant volume.
dU_mass_dV_P([prop])	Method to calculate and return the volume derivative
	of mass internal energy of the phase at constant pres-
	sure.
dU_mass_dV_T([prop])	Method to calculate and return the volume derivative
	of mass internal energy of the phase at constant tem-
	perature.
$dV_dP()$	Method to calculate and return the constant-
	temperature pressure derivative of volume of the
	phase.
<i>dV_dP_A</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of volume of the phase at constant Helmholtz energy.
<i>dV_dP_G</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of volume of the phase at constant Gibbs energy.
<i>dV_dP_H</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of volume of the phase at constant enthalpy.
<i>dV_dP_S</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of volume of the phase at constant entropy.
$dV_dP_T()$	Method to calculate and return the constant-
	temperature pressure derivative of volume of the
	phase.
<i>dV_dP_U</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
uv_ur_o([property; unrefenduate_oy;])	of volume of the phase at constant internal energy.
$dV_dP_V()$	Method to calculate and return the volume derivative
$av_aP_v()$	
	of pressure of the phase at constant volume.
$dV_dT()$	Method to calculate and return the constant-pressure
	temperature derivative of volume of the phase.
<i>dV_dT_A</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of volume of the phase at constant
	Helmholtz energy.
<i>dV_dT_G</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of volume of the phase at constant Gibbs
	energy.
	continues on next page

Table 80 - continue	ed from previous page
<i>dV_dT_H</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of volume of the phase at constant en-
	thalpy.
$dV_dT_P()$	Method to calculate and return the constant-pressure
	temperature derivative of volume of the phase.
<i>dV_dT_S</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of volume of the phase at constant entropy.
<i>dV_dT_U</i> ([property, differentiate_by,])	Method to calculate and return the temperature
av_ur_o([property, unrerentatio_oy,])	derivative of volume of the phase at constant inter-
	nal energy.
$dV_dT_V()$	Method to calculate and return the temperature
	1
	derivative of volume of the phase at constant volume.
<i>dV_dV_A</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of volume of the phase at constant Helmholtz energy.
<i>dV_dV_G</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of volume of the phase at constant Gibbs energy.
<i>dV_dV_H</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of volume of the phase at constant enthalpy.
$dV_dV_P()$	Method to calculate and return the volume derivative
	of volume of the phase at constant pressure.
<i>dV_dV_S</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of volume of the phase at constant entropy.
dV_dV_T()	Method to calculate and return the volume derivative
	of volume of the phase at constant temperature.
<i>dV_dV_U</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
av_av_o([property, amerentiate_by,])	of volume of the phase at constant internal energy.
dV_dns()	Method to calculate and return the mole number
du deles A([energentes d:ff-mantists here ])	derivatives of the molar volume <i>V</i> of the phase.
<i>dV_drho_A</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of volume of the phase at constant Helmholtz energy.
<i>dV_drho_G</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of volume of the phase at constant Gibbs energy.
<i>dV_drho_H</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of volume of the phase at constant enthalpy.
<i>dV_drho_S</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of volume of the phase at constant entropy.
<i>dV_drho_U</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of volume of the phase at constant internal energy.
dZ_dP()	Method to calculate and return the pressure derivative
	of compressibility of the phase.
$dZ_dT()$	Method to calculate and return the temperature
uz_u1()	derivative of compressibility of the phase.
$dZ_{dV}()$	Method to calculate and return the volume derivative
az_av()	
	of compressibility of the phase.
dZ_dns()	Method to calculate and return the mole number
	derivatives of the compressibility factor $Z$ of the
	phase.
$dZ_dzs()$	Method to calculate and return the mole fraction
uz_uzs()	
uz_uzs()	derivatives of the compressibility factor $Z$ of the
	derivatives of the compressibility factor $Z$ of the phase.

Table 80 – continued from previous page

	inued from previous page
dfugacities_dP()	Method to calculate and return the pressure derivative
	of the fugacities of the components in the phase.
dfugacities_dT()	Method to calculate and return the temperature
	derivative of fugacities of the phase.
dfugacities_dns()	Method to calculate and return the mole number
	derivative of the fugacities of the components in the
	phase.
dfugacity_dP()	Method to calculate and return the pressure deriva-
	tive of fugacity of the phase; provided the phase is 1
	component.
dfugacity_dT()	Method to calculate and return the temperature
	derivative of fugacity of the phase; provided the
	phase is 1 component.
<pre>disobaric_expansion_dP()</pre>	Method to calculate and return the pressure derivative
	of isobatic expansion coefficient of the phase.
<pre>disobaric_expansion_dT()</pre>	Method to calculate and return the temperature
	derivative of isobatic expansion coefficient of the
	phase.
<pre>disothermal_compressibility_dT()</pre>	Method to calculate and return the temperature
	derivative of isothermal compressibility of the phase.
dkappa_dT()	Method to calculate and return the temperature
	derivative of isothermal compressibility of the phase
<pre>dlnfugacities_dns()</pre>	Method to calculate and return the mole number
	derivative of the log of fugacities of the components
	in the phase.
dlnfugacities_dzs()	Method to calculate and return the mole fraction
	derivative of the log of fugacities of the components
	in the phase.
dlnphis_dP()	Method to calculate and return the pressure derivative
	of the log of fugacity coefficients of each component
	in the phase.
dlnphis_dT()	Method to calculate and return the temperature
	derivative of the log of fugacity coefficients of each
	component in the phase.
<pre>dphis_dP() dphis_dT()</pre>	Method to calculate and return the pressure derivative
	of fugacity coefficients of the phase.
	Method to calculate and return the temperature
	derivative of fugacity coefficients of the phase.
dphis_dzs()	Method to calculate and return the molar composition
	derivative of fugacity coefficients of the phase.
drho_dP()	Method to calculate and return the pressure derivative
	of molar density of the phase.
<i>drho_dP_A</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of density of the phase at constant Helmholtz energy.
<i>drho_dP_G</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of density of the phase at constant Gibbs energy.
<i>drho_dP_H</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of density of the phase at constant enthalpy.
<i>drho_dP_S</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative of density of the phase at constant entropy.

	ied from previous page
<i>drho_dP_U</i> ([property, differentiate_by,])	Method to calculate and return the pressure derivative
	of density of the phase at constant internal energy.
drho_dT()	Method to calculate and return the temperature
~	derivative of molar density of the phase.
<i>drho_dT_A</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of density of the phase at constant
	Helmholtz energy.
<i>drho_dT_G</i> ([property, differentiate_by,])	Method to calculate and return the temperature
uno_u1_0([property, unceentrate_by,])	derivative of density of the phase at constant Gibbs
<i>drho_dT_H</i> ([property, differentiate_by,])	energy. Method to calculate and return the temperature
<i>umo_u1_n</i> ([property, unerentiate_by,])	-
	derivative of density of the phase at constant en-
	thalpy.
<i>drho_dT_S</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of density of the phase at constant entropy.
<i>drho_dT_U</i> ([property, differentiate_by,])	Method to calculate and return the temperature
	derivative of density of the phase at constant internal
	energy.
drho_dT_V()	Method to calculate and return the temperature
	derivative of molar density of the phase at constant
	volume.
<i>drho_dV_A</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of density of the phase at constant Helmholtz energy.
<i>drho_dV_G</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of density of the phase at constant Gibbs energy.
<i>drho_dV_H</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of density of the phase at constant enthalpy.
<i>drho_dV_S</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
	of density of the phase at constant entropy.
drho_dV_T()	Method to calculate and return the volume derivative
	of molar density of the phase.
<i>drho_dV_U</i> ([property, differentiate_by,])	Method to calculate and return the volume derivative
uno_uv_o([property; unerenduce_oy;])	of density of the phase at constant internal energy.
<i>drho_drho_A</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
armo_armo_A([property, amerentiate_by,])	of density of the phase at constant Helmholtz energy.
debe debe ((forementer differentiate bar 1)	
<i>drho_drho_G</i> ([property, differentiate_by,])	Method to calculate and return the density derivative
	of density of the phase at constant Gibbs energy.
<pre>drho_drho_H([property, differentiate_by,])</pre>	Method to calculate and return the density derivative
	of density of the phase at constant enthalpy.
<pre>drho_drho_S([property, differentiate_by,])</pre>	Method to calculate and return the density derivative
	of density of the phase at constant entropy.
<pre>drho_drho_U([property, differentiate_by,])</pre>	Method to calculate and return the density derivative
	of density of the phase at constant internal energy.
drho_mass_dP()	Method to calculate the mass density derivative with
	respect to pressure, at constant temperature.
drho_mass_dT()	Method to calculate the mass density derivative with
<u> </u>	respect to temperature, at constant pressure.
dspeed_of_sound_dP_T()	Method to calculate the pressure derivative of speed
dspeed_of_sound_dP_T()	Method to calculate the pressure derivative of speed of sound at constant temperature in molar units.
	Method to calculate the pressure derivative of speed

Table 80 – continued from previous page

Table 80 – co	ontinued from previous page
<pre>from_json(json_repr)</pre>	Method to create a phase from a JSON serialization
	of another phase.
<pre>fugacities()</pre>	Method to calculate and return the fugacities of the
5	phase.
<pre>fugacities_at_zs(zs)</pre>	Method to directly calculate the figacities at a differ-
_ugue_e=e=_uee(20)	ent composition than the current phase.
<pre>fugacities_lowest_Gibbs()</pre>	Method to calculate and return the fugacities of the
14gacitics_10wcst_01003()	phase.
<pre>fugacity()</pre>	Method to calculate and return the fugacity of the
iugacity()	phase; provided the phase is 1 component.
gammas()	Method to calculate and return the activity coeffi-
yanmas()	
<i>i</i>	cients of the phase, [-].
<pre>isentropic_exponent()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship $PV^k = \text{const.}$
<pre>isentropic_exponent_PT()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship $P(1, k) = k$
	$P^{(1-k)}T^k = \text{const.}$
<pre>isentropic_exponent_PV()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$PV^k = \text{const.}$
<pre>isentropic_exponent_TV()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$TV^{k-1} = \text{const.}$
<pre>isobaric_expansion()</pre>	Method to calculate and return the isobatic expansion
• • •	coefficient of the phase.
<pre>isothermal_bulk_modulus()</pre>	Method to calculate and return the isothermal bulk
	modulus of the phase.
<pre>isothermal_compressibility()</pre>	Method to calculate and return the isothermal com-
	pressibility of the phase.
kappa()	Method to calculate and return the isothermal com-
	pressibility of the phase.
<pre>lnfugacities()</pre>	Method to calculate and return the log of fugacities
	of the phase.
lnphi()	Method to calculate and return the log of fugacity co-
	efficient of the phase; provided the phase is 1 compo-
	nent.
lnphis()	Method to calculate and return the log of fugacity co-
	efficients of each component in the phase.
<pre>lnphis_G_min()</pre>	Method to calculate and return the log fugacity coef-
	ficients of the phase.
<pre>lnphis_at_zs(zs)</pre>	Method to directly calculate the log fugacity coef-
	ficients at a different composition than the current
	phase.
log_zs()	Method to calculate and return the log of mole frac-
109_23()	tions specified.
model hach (ligners share)	
<pre>model_hash([ignore_phase])</pre>	Method to compute a hash of a phase.
<pre>molar_water_content()</pre>	Method to calculate and return the molar water con-
	tent; this is the g/mol of the fluid which is coming
	from water, [g/mol].
	continues on next page

Table 80 – continued from previous page

mu()	- continued from previous page
ma()	
phi()	Method to calculate and return the fugacity coeffi-
	cient of the phase; provided the phase is 1 compo-
	nent.
phis()	Method to calculate and return the fugacity coeffi-
F()	cients of the phase.
pseudo_Pc()	Method to calculate and return the pseudocritical
pocaao_re()	pressure calculated using Kay's rule (linear mole
	fractions):
pseudo_Tc()	Method to calculate and return the pseudocritica
pocaao_re()	temperature calculated using Kay's rule (linear mole
	fractions):
pseudo_Vc()	Method to calculate and return the pseudocritical vol-
pseudo_ve()	ume calculated using Kay's rule (linear mole frac-
	tions):
pseudo_Zc()	Method to calculate and return the pseudocritica
pseudo_zc()	compressibility calculated using Kay's rule (linear
	mole fractions):
<b>rh</b> o()	Method to calculate and return the molar density of
rho()	•
	the phase. Method to calculate and return mass density of the
<pre>rho_mass()</pre>	•
abo man limit a CO	phase.
<pre>rho_mass_liquid_ref()</pre>	Method to calculate and return the liquid refer
	ence mass density according to the temperature
	variable <i>T_liquid_volume_ref</i> of thermo.bulk.
	BulkSettings and the composition of the phase.
sigma()	Calculate and return the surface tension of the phase
<pre>speed_of_sound()</pre>	Method to calculate and return the molar speed of
	sound of the phase.
<pre>speed_of_sound_mass()</pre>	Method to calculate and return the speed of sound of
	the phase.
state_hash()	Basic method to calculate a hash of the state of the
	phase and its model parameters.
to(zs[, T, P, V])	Method to create a new Phase object with the same
	constants as the existing Phase but at different condi-
	tions.
to_ <i>TP_zs</i> (T, P, zs)	Method to create a new Phase object with the same
	constants as the existing Phase but at a different $T$ and
	Р.
value(name)	Method to retrieve a property from a string.
ws()	Method to calculate and return the mass fractions o
	the phase, [-]
<pre>ws_no_water()</pre>	Method to calculate and return the mass fractions o
	all species in the phase, normalized to a water-free
	basis (the mass fraction of water returned is zero).
<pre>zs_no_water()</pre>	Method to calculate and return the mole fractions o
	all species in the phase, normalized to a water-free
	basis (the mole fraction of water returned is zero).

# Table 80 – continued from previous page

# **A**()

Method to calculate and return the Helmholtz energy of the phase.

A = U - TS

#### Returns

A [float] Helmholtz energy, [J/mol]

### API()

Method to calculate and return the API of the phase.

API gravity = 
$$\frac{141.5}{\text{SG}} - 131.5$$

## Returns

API [float] API of the fluid [-]

### A\_dep()

Method to calculate and return the departure Helmholtz energy of the phase.

$$A_{dep} = U_{dep} - TS_{dep}$$

### Returns

A\_dep [float] Departure Helmholtz energy, [J/mol]

#### A\_formation\_ideal\_gas()

Method to calculate and return the ideal-gas Helmholtz energy of formation of the phase (as if the phase was an ideal gas).

$$A_{reactive}^{ig} = U_{reactive}^{ig} - T_{ref}^{ig} S_{reactive}^{ig}$$

Returns

**A\_formation\_ideal\_gas** [float] Helmholtz energy of formation of the phase on a reactive basis as an ideal gas, [J/(mol)]

## A\_ideal\_gas()

Method to calculate and return the ideal-gas Helmholtz energy of the phase.

$$A^{ig} = U^{ig} - TS^{ig}$$

### Returns

A\_ideal\_gas [float] Ideal gas Helmholtz free energy, [J/(mol)]

# A\_mass()

Method to calculate and return mass Helmholtz energy of the phase.

$$A_{mass} = \frac{1000A_{molar}}{MW}$$

Returns

A\_mass [float] Mass Helmholtz energy, [J/(kg)]

## A\_reactive()

Method to calculate and return the Helmholtz free energy of the phase on a reactive basis.

 $A_{reactive} = U_{reactive} - TS_{reactive}$ 

A\_reactive [float] Helmholtz free energy of the phase on a reactive basis, [J/(mol)]

## property CASs

CAS registration numbers for each component, [-].

Returns

CASs [list[str]] CAS registration numbers for each component, [-].

## property Carcinogens

Status of each component in cancer causing registries, [-].

Returns

Carcinogens [list[dict]] Status of each component in cancer causing registries, [-].

### property Ceilings

Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

## Returns

**Ceilings** [list[tuple[(float, str)]]] Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

## Cp()

Method to calculate and return the constant-pressure heat capacity of the phase.

#### Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

### Cp\_Cv\_ratio()

Method to calculate and return the Cp/Cv ratio of the phase.

 $\frac{C_p}{C_v}$ 

#### Returns

Cp\_Cv\_ratio [float] Cp/Cv ratio, [-]

## Cp\_Cv\_ratio\_ideal\_gas()

Method to calculate and return the ratio of the ideal-gas heat capacity to its constant-volume heat capacity.

$$\frac{C_p^{ig}}{C_v^{ig}}$$

#### Returns

**Cp\_Cv\_ratio\_ideal\_gas** [float] Cp/Cv for the phase as an ideal gas, [-]

#### Cp\_ideal\_gas()

Method to calculate and return the ideal-gas heat capacity of the phase.

$$C_p^{ig} = \sum_i z_i C_{p,i}^{ig}$$

#### Returns

**Cp** [float] Ideal gas heat capacity, [J/(mol\*K)]

Cp\_mass()

Method to calculate and return mass constant pressure heat capacity of the phase.

$$Cp_{mass} = \frac{1000Cp_{molar}}{MW}$$

Cp\_mass [float] Mass heat capacity, [J/(kg\*K)]

## Cpgs\_poly\_fit = False

### Cpig\_integrals\_over\_T\_pure()

Method to calculate and return the integrals of the ideal-gas heat capacities divided by temperature of every component in the phase from a temperature of *Phase*. *T\_REF\_IG* to the system temperature. This method is powered by the *HeatCapacityGases* objects, except when all components have the same heat capacity form and a fast implementation has been written for it (currently only polynomials).

$$\Delta S^{ig} = \int_{T_{ref}}^{T} \frac{C_p^{ig}}{T} dT$$

#### Returns

**dS\_ig** [list[float]] Integrals of ideal gas heat capacity over temperature from the reference temperature to the system temperature, [J/(mol)]

### Cpig\_integrals\_pure()

Method to calculate and return the integrals of the ideal-gas heat capacities of every component in the phase from a temperature of *Phase.T\_REF\_IG* to the system temperature. This method is powered by the *HeatCapacityGases* objects, except when all components have the same heat capacity form and a fast implementation has been written for it (currently only polynomials).

$$\Delta H^{ig} = \int_{T_{ref}}^{T} C_p^{ig} dT$$

#### Returns

**dH\_ig** [list[float]] Integrals of ideal gas heat capacity from the reference temperature to the system temperature, [J/(mol)]

### Cpigs\_pure()

Method to calculate and return the ideal-gas heat capacities of every component in the phase. This method is powered by the *HeatCapacityGases* objects, except when all components have the same heat capacity form and a fast implementation has been written for it (currently only polynomials).

#### Returns

**Cp\_ig** [list[float]] Molar ideal gas heat capacities, [J/(mol\*K)]

**Cv**()

Method to calculate and return the constant-volume heat capacity Cv of the phase.

$$C_v = T \left(\frac{\partial P}{\partial T}\right)_V^2 / \left(\frac{\partial P}{\partial V}\right)_T + Cp$$

### Returns

Cv [float] Constant volume molar heat capacity, [J/(mol\*K)]

### Cv\_dep()

Method to calculate and return the difference between the actual Cv and the ideal-gas constant volume heat capacity  $C_v^{ig}$  of the phase.

$$C_v^{dep} = C_v - C_v^{ig}$$

Returns

Cv\_dep [float] Departure ideal gas constant volume heat capacity, [J/(mol\*K)]

#### Cv\_ideal\_gas()

Method to calculate and return the ideal-gas constant volume heat capacity of the phase.

$$C_v^{ig} = \sum_i z_i C_{p,i}^{ig} - R$$

#### Returns

Cv [float] Ideal gas constant volume heat capacity, [J/(mol\*K)]

## Cv\_mass()

Method to calculate and return mass constant volume heat capacity of the phase.

$$Cv_{mass} = \frac{1000Cv_{molar}}{MW}$$

## Returns

Cv\_mass [float] Mass constant volume heat capacity, [J/(kg\*K)]

## **G**()

Method to calculate and return the Gibbs free energy of the phase.

$$G = H - TS$$

Returns

G [float] Gibbs free energy, [J/mol]

### property GWPs

Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

#### Returns

**GWPs** [list[float]] Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

## G\_dep()

Method to calculate and return the departure Gibbs free energy of the phase.

$$G_{dep} = H_{dep} - TS_{dep}$$

## Returns

G\_dep [float] Departure Gibbs free energy, [J/mol]

## G\_dep\_phi\_consistency()

Method to calculate and return a consistency check between departure Gibbs free energy, and the fugacity coefficients.

$$G_{dep}^{\rm from \, phi} = RT \sum_{i} z_i \phi_i$$

Returns

error [float] Relative consistency error  $|1 - G_{dep}^{\text{from phi}}/G_{dep}^{\text{implemented}}|$ , [-]

### G\_formation\_ideal\_gas()

Method to calculate and return the ideal-gas Gibbs free energy of formation of the phase (as if the phase was an ideal gas).

$$G_{reactive}^{ig} = H_{reactive}^{ig} - T_{ref}^{ig} S_{reactive}^{ig}$$

**G\_formation\_ideal\_gas** [float] Gibbs free energy of formation of the phase on a reactive basis as an ideal gas, [J/(mol)]

### G\_ideal\_gas()

Method to calculate and return the ideal-gas Gibbs free energy of the phase.

$$G^{ig} = H^{ig} - TS^{ig}$$

#### Returns

**G\_ideal\_gas** [float] Ideal gas free energy, [J/(mol)]

## G\_mass()

Method to calculate and return mass Gibbs energy of the phase.

$$G_{mass} = \frac{1000G_{molar}}{MW}$$

Returns

G\_mass [float] Mass Gibbs energy, [J/(kg)]

### G\_min()

Method to calculate and return the Gibbs free energy of the phase.

$$G = H - TS$$

#### Returns

G [float] Gibbs free energy, [J/mol]

#### G\_min\_criteria()

Method to calculate and return the Gibbs energy criteria required for comparing phase stability. This calculation can be faster than calculating the full Gibbs energy. For this comparison to work, all phases must use the ideal gas basis.

$$G^{\text{criteria}} = G^{dep} + RT \sum_{i} z_i \ln z_i$$

Returns

G\_crit [float] Gibbs free energy like criteria [J/mol]

#### G\_reactive()

Method to calculate and return the Gibbs free energy of the phase on a reactive basis.

$$G_{reactive} = H_{reactive} - TS_{reactive}$$

Returns

G\_reactive [float] Gibbs free energy of the phase on a reactive basis, [J/(mol)]

#### property Gfgs

Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

#### Returns

**Gfgs** [list[float]] Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

#### property Gfgs\_mass

Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

**Gfgs\_mass** [list[float]] Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

### H()

Method to calculate and return the enthalpy of the phase. The reference state for most subclasses is an ideal-gas enthalpy of zero at 298.15 K and 101325 Pa.

#### Returns

H [float] Molar enthalpy, [J/(mol)]

## H\_C\_ratio()

Method to calculate and return the atomic ratio of hydrogen atoms to carbon atoms, based on the current composition of the phase.

### Returns

H\_C\_ratio [float] H/C ratio on a molar basis, [-]

## Notes

None is returned if no species are present that have carbon atoms.

#### H\_C\_ratio\_mass()

Method to calculate and return the mass ratio of hydrogen atoms to carbon atoms, based on the current composition of the phase.

#### Returns

H\_C\_ratio\_mass [float] H/C ratio on a mass basis, [-]

#### **Notes**

None is returned if no species are present that have carbon atoms.

#### H\_dep\_phi\_consistency()

Method to calculate and return a consistency check between departure enthalpy, and the fugacity coefficients' temperature derivatives.

$$H_{dep}^{\text{from phi}} = -RT^2 \sum_{i} z_i \frac{\partial \ln \phi_i}{\partial T}$$

Returns

error [float] Relative consistency error  $|1 - H_{dep}^{\text{from phi}}/H_{dep}^{\text{implemented}}|$ , [-]

#### H\_formation\_ideal\_gas()

Method to calculate and return the ideal-gas enthalpy of formation of the phase (as if the phase was an ideal gas).

$$H_{reactive}^{ig} = \sum_{i} z_i H_{f,i}$$

#### Returns

**H\_formation\_ideal\_gas** [float] Enthalpy of formation of the phase on a reactive basis as an ideal gas, [J/mol]

# H\_from\_phi()

Method to calculate and return the enthalpy of the fluid as calculated from the ideal-gas enthalpy and the the fugacity coefficients' temperature derivatives.

$$H^{\text{from phi}} = H^{ig} - RT^2 \sum_{i} z_i \frac{\partial \ln \phi_i}{\partial T}$$

### Returns

H [float] Enthalpy as calculated from fugacity coefficient temperature derivatives [J/mol]

### H\_ideal\_gas()

Method to calculate and return the ideal-gas enthalpy of the phase.

$$H^{ig} = \sum_{i} z_i H_i^{ig}$$

### Returns

**H** [float] Ideal gas enthalpy, [J/(mol)]

#### H\_mass()

Method to calculate and return mass enthalpy of the phase.

$$H_{mass} = \frac{1000H_{molar}}{MW}$$

Returns

H\_mass [float] Mass enthalpy, [J/kg]

#### H\_phi\_consistency()

Method to calculate and return a consistency check between ideal gas enthalpy behavior, and the fugacity coefficients and their temperature derivatives.

$$H^{\text{from phi}} = H^{ig} - RT^2 \sum_i z_i \frac{\partial \ln \phi_i}{\partial T}$$

#### Returns

**error** [float] Relative consistency error  $|1 - H^{\text{from phi}}/H^{\text{implemented}}|$ , [-]

#### H\_reactive()

Method to calculate and return the enthalpy of the phase on a reactive basis, using the *Hfs* values of the phase.

$$H_{reactive} = H + \sum_{i} z_i H_{f,i}$$

#### Returns

H\_reactive [float] Enthalpy of the phase on a reactive basis, [J/mol]

Hc()

Method to calculate and return the molar ideal-gas higher heat of combustion of the object, [J/mol]

#### Returns

Hc [float] Molar higher heat of combustion, [J/(mol)]

## Hc\_lower()

Method to calculate and return the molar ideal-gas lower heat of combustion of the object, [J/mol]

Returns

Hc\_lower [float] Molar lower heat of combustion, [J/(mol)]

#### Hc\_lower\_mass()

Method to calculate and return the mass ideal-gas lower heat of combustion of the object, [J/mol]

#### Returns

**Hc\_lower\_mass** [float] Mass lower heat of combustion, [J/(kg)]

### Hc\_lower\_normal()

Method to calculate and return the volumetric ideal-gas lower heat of combustion of the object using the normal gas volume, [J/m^3]

Returns

Hc\_lower\_normal [float] Volumetric (normal) lower heat of combustion, [J/(m^3)]

#### Hc\_lower\_standard()

Method to calculate and return the volumetric ideal-gas lower heat of combustion of the object using the standard gas volume, [J/m^3]

#### Returns

Hc\_lower\_standard [float] Volumetric (standard) lower heat of combustion, [J/(m^3)]

## Hc\_mass()

Method to calculate and return the mass ideal-gas higher heat of combustion of the object, [J/mol]

#### Returns

Hc\_mass [float] Mass higher heat of combustion, [J/(kg)]

### Hc\_normal()

Method to calculate and return the volumetric ideal-gas higher heat of combustion of the object using the normal gas volume, [J/m^3]

### Returns

Hc\_normal [float] Volumetric (normal) higher heat of combustion, [J/(m^3)]

### Hc\_standard()

Method to calculate and return the volumetric ideal-gas higher heat of combustion of the object using the standard gas volume, [J/m^3]

#### Returns

Hc\_normal [float] Volumetric (standard) higher heat of combustion, [J/(m^3)]

### property Hcs

Higher standard molar heats of combustion for each component, [J/mol].

#### Returns

Hcs [list[float]] Higher standard molar heats of combustion for each component, [J/mol].

## property Hcs\_lower

Lower standard molar heats of combustion for each component, [J/mol].

## Returns

**Hcs\_lower** [list[float]] Lower standard molar heats of combustion for each component, [J/mol].

## property Hcs\_lower\_mass

Lower standard heats of combustion for each component, [J/kg].

#### Returns

**Hcs\_lower\_mass** [list[float]] Lower standard heats of combustion for each component, [J/kg].

### property Hcs\_mass

Higher standard heats of combustion for each component, [J/kg].

Returns

**Hcs\_mass** [list[float]] Higher standard heats of combustion for each component, [J/kg].

#### property Hf\_STPs

Standard state molar enthalpies of formation for each component, [J/mol].

### Returns

**Hf\_STPs** [list[float]] Standard state molar enthalpies of formation for each component, [J/mol].

## property Hf\_STPs\_mass

Standard state mass enthalpies of formation for each component, [J/kg].

#### Returns

**Hf\_STPs\_mass** [list[float]] Standard state mass enthalpies of formation for each component, [J/kg].

## property Hfgs

Ideal gas standard molar enthalpies of formation for each component, [J/mol].

### Returns

**Hfgs** [list[float]] Ideal gas standard molar enthalpies of formation for each component, [J/mol].

## property Hfgs\_mass

Ideal gas standard enthalpies of formation for each component, [J/kg].

#### Returns

Hfgs\_mass [list[float]] Ideal gas standard enthalpies of formation for each component, [J/kg].

#### property Hfus\_Tms

Molar heats of fusion for each component at their respective melting points, [J/mol].

#### Returns

**Hfus\_Tms** [list[float]] Molar heats of fusion for each component at their respective melting points, [J/mol].

#### property Hfus\_Tms\_mass

Heats of fusion for each component at their respective melting points, [J/kg].

#### Returns

**Hfus\_Tms\_mass** [list[float]] Heats of fusion for each component at their respective melting points, [J/kg].

## property Hsub\_Tts

Heats of sublimation for each component at their respective triple points, [J/mol].

### Returns

**Hsub\_Tts** [list[float]] Heats of sublimation for each component at their respective triple points, [J/mol].

#### property Hsub\_Tts\_mass

Heats of sublimation for each component at their respective triple points, [J/kg].

### Returns

Hsub\_Tts\_mass [list[float]] Heats of sublimation for each component at their respective triple points, [J/kg].

## property Hvap\_298s

Molar heats of vaporization for each component at 298.15 K, [J/mol].

### Returns

Hvap\_298s [list[float]] Molar heats of vaporization for each component at 298.15 K, [J/mol].

## property Hvap\_298s\_mass

Heats of vaporization for each component at 298.15 K, [J/kg].

### Returns

Hvap\_298s\_mass [list[float]] Heats of vaporization for each component at 298.15 K, [J/kg].

### property Hvap\_Tbs

Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].

#### Returns

**Hvap\_Tbs** [list[float]] Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].

## property Hvap\_Tbs\_mass

Heats of vaporization for each component at their respective normal boiling points, [J/kg].

## Returns

**Hvap\_Tbs\_mass** [list[float]] Heats of vaporization for each component at their respective normal boiling points, [J/kg].

### INCOMPRESSIBLE\_CONST = 1e+30

## property InChI\_Keys

InChI Keys for each component, [-].

## Returns

InChI\_Keys [list[str]] InChI Keys for each component, [-].

## property InChIs

InChI strings for each component, [-].

## Returns

InChIs [list[str]] InChI strings for each component, [-].

## Joule\_Thomson()

Method to calculate and return the Joule-Thomson coefficient of the phase.

$$\mu_{JT} = \left(\frac{\partial T}{\partial P}\right)_{H} = \frac{1}{C_{p}} \left[T\left(\frac{\partial V}{\partial T}\right)_{P} - V\right] = \frac{V}{C_{p}} \left(\beta T - 1\right)$$

Returns

**mu\_JT** [float] Joule-Thomson coefficient [K/Pa]

### property LFLs

Lower flammability limits for each component, [-].

LFLs [list[float]] Lower flammability limits for each component, [-].

## LOG\_P\_REF\_IG = 11.52608845149651

### MW()

Method to calculate and return molecular weight of the phase.

$$\mathbf{MW} = \sum_i z_i \mathbf{MW}_i$$

Returns

MW [float] Molecular weight, [g/mol]

#### MW\_inv()

Method to calculate and return inverse of molecular weight of the phase.

$$\frac{1}{\mathbf{MW}} = \frac{1}{\sum_{i} z_i \mathbf{MW}_i}$$

Returns

MW\_inv [float] Inverse of molecular weight, [mol/g]

### property MWs

Similatiry variables for each component, [g/mol].

#### Returns

MWs [list[float]] Similatiry variables for each component, [g/mol].

## property ODPs

Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

#### Returns

**ODPs** [list[float]] Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

### PIP()

Method to calculate and return the phase identification parameter of the phase.

$$\Pi = V \left[ \frac{\frac{\partial^2 P}{\partial V \partial T}}{\frac{\partial P}{\partial T}} - \frac{\frac{\partial^2 P}{\partial V^2}}{\frac{\partial P}{\partial V}} \right]$$

Returns

**PIP** [float] Phase identification parameter, [-]

# property PSRK\_groups

PSRK subgroup: count groups for each component, [-].

Returns

PSRK\_groups [list[dict]] PSRK subgroup: count groups for each component, [-].

 $P_MIN_FIXED = 0.01$ 

 $P_{REF_{IG}} = 101325.0$ 

P\_REF\_IG\_INV = 9.869232667160129e-06

## $P_max_at_V(V)$

Dummy method. The idea behind this method, which is implemented by some subclasses, is to calculate the maximum pressure the phase can create at a constant volume, if one exists; returns None otherwise. This method, as a dummy method, always returns None.

## Parameters

V [float] Constant molar volume, [m^3/mol]

### Returns

P [float] Maximum possible isochoric pressure, [Pa]

## P\_transitions()

Dummy method. The idea behind this method is to calculate any pressures (at constant temperature) which cause the phase properties to become discontinuous.

### Returns

P\_transitions [list[float]] Transition pressures, [Pa]

#### property Parachors

Parachors for each component, [N^0.25\*m^2.75/mol].

### Returns

Parachors [list[float]] Parachors for each component, [N^0.25\*m^2.75/mol].

#### property Pcs

Critical pressures for each component, [Pa].

### Returns

Pcs [list[float]] Critical pressures for each component, [Pa].

#### Pmc()

Method to calculate and return the mechanical critical pressure of the phase.

#### Returns

Pmc [float] Mechanical critical pressure, [Pa]

### property Psat\_298s

Vapor pressures for each component at 298.15 K, [Pa].

### Returns

Psat\_298s [list[float]] Vapor pressures for each component at 298.15 K, [Pa].

# Psats\_poly\_fit = False

## property Pts

Triple point pressures for each component, [Pa].

## Returns

Pts [list[float]] Triple point pressures for each component, [Pa].

### property PubChems

Pubchem IDs for each component, [-].

## Returns

PubChems [list[int]] Pubchem IDs for each component, [-].

### R = 8.31446261815324

R2 = 69.13028862866763

## property RI\_Ts

Temperatures at which the refractive indexes were reported for each component, [K].

### Returns

**RI\_Ts** [list[float]] Temperatures at which the refractive indexes were reported for each component, [K].

## property RIs

Refractive indexes for each component, [-].

### Returns

RIs [list[float]] Refractive indexes for each component, [-].

## $R_{inv} = 0.12027235504272604$

### **S**()

Method to calculate and return the entropy of the phase. The reference state for most subclasses is an ideal-gas entropy of zero at 298.15 K and 101325 Pa.

## Returns

**S** [float] Molar entropy, [J/(mol\*K)]

## property S0gs

Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].

## Returns

**S0gs** [list[float]] Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].

# property S0gs\_mass

Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].

## Returns

**S0gs\_mass** [list[float]] Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].

# SG()

Method to calculate and return the standard liquid specific gravity of the phase, using constant liquid pure component densities not calculated by the phase object, at 60 °F.

## Returns

SG [float] Specific gravity of the liquid, [-]

## Notes

The reference density of water is from the IAPWS-95 standard - 999.0170824078306 kg/m^3.

## SG\_gas()

Method to calculate and return the specific gravity of the phase with respect to a gas reference density.

### Returns

SG\_gas [float] Specific gravity of the gas, [-]

#### Notes

The reference molecular weight of air used is 28.9586 g/mol.

## property STELs

Short term exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

#### Returns

**STELs** [list[tuple[(float, str)]]] Short term exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

# S\_dep\_phi\_consistency()

Method to calculate and return a consistency check between ideal gas entropy behavior, and the fugacity coefficients and their temperature derivatives.

$$S_{dep}^{\text{from phi}} = -\sum_{i} z_{i} R \left( \ln \phi_{i} + T \frac{\partial \ln \phi_{i}}{\partial T} \right)$$

Returns

error [float] Relative consistency error  $|1 - S_{dep}^{\text{from phi}}/S_{dep}^{\text{implemented}}|$ , [-]

## S\_formation\_ideal\_gas()

Method to calculate and return the ideal-gas entropy of formation of the phase (as if the phase was an ideal gas).

$$S_{reactive}^{ig} = \sum_{i} z_i S_{f,i}$$

Returns

**S\_formation\_ideal\_gas** [float] Entropy of formation of the phase on a reactive basis as an ideal gas, [J/(mol\*K)]

### S\_from\_phi()

Method to calculate and return the entropy of the fluid as calculated from the ideal-gas entropy and the the fugacity coefficients' temperature derivatives.

$$S = S^{ig} - \sum_{i} z_i R \left( \ln \phi_i + T \frac{\partial \ln \phi_i}{\partial T} \right)$$

Returns

S [float] Entropy as calculated from fugacity coefficient temperature derivatives [J/(mol\*K)]

S\_ideal\_gas()

Method to calculate and return the ideal-gas entropy of the phase.

$$S^{ig} = \sum_{i} z_i S_i^{ig} - R \ln\left(\frac{P}{P_{ref}}\right) - R \sum_{i} z_i \ln(z_i)$$

### Returns

**S** [float] Ideal gas molar entropy, [J/(mol\*K)]

S\_mass()

Method to calculate and return mass entropy of the phase.

$$S_{mass} = \frac{1000S_{molar}}{MW}$$

**S\_mass** [float] Mass enthalpy, [J/(kg\*K)]

# S\_phi\_consistency()

Method to calculate and return a consistency check between ideal gas entropy behavior, and the fugacity coefficients and their temperature derivatives.

$$S = S^{ig} - \sum_{i} z_i R \left( \ln \phi_i + T \frac{\partial \ln \phi_i}{\partial T} \right)$$

Returns

**error** [float] Relative consistency error  $|1 - S^{\text{from phi}}/S^{\text{implemented}}|$ , [-]

# S\_reactive()

Method to calculate and return the entropy of the phase on a reactive basis, using the Sfs values of the phase.

$$S_{reactive} = S + \sum_{i} z_i S_{f,i}$$

Returns

**S\_reactive** [float] Entropy of the phase on a reactive basis, [J/(mol\*K)]

### property Sfgs

Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

## Returns

**Sfgs** [list[float]] Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

## property Sfgs\_mass

Ideal gas standard entropies of formation for each component, [J/(kg\*K)].

#### Returns

**Sfgs\_mass** [list[float]] Ideal gas standard entropies of formation for each component, [J/(kg\*K)].

### property Skins

Whether each compound can be absorbed through the skin or not, [-].

### Returns

Skins [list[bool]] Whether each compound can be absorbed through the skin or not, [-].

# property StielPolars

Stiel polar factors for each component, [-].

Returns

StielPolars [list[float]] Stiel polar factors for each component, [-].

# property Stockmayers

Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].

Returns

**Stockmayers** [list[float]] Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].

## property TWAs

Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

**TWAs** [list[tuple[(float, str)]]] Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m<sup>3</sup>), [various].

- $T_MAX_FIXED = 10000.0$
- $T_MIN_FIXED = 0.001$
- $T_MIN_FLASH = 1e-300$
- $T_REF_IG = 298.15$

### T\_REF\_IG\_INV = 0.0033540164346805303

The numerical inverse of *T\_REF\_IG*, stored to save a division.

## $T_max_at_V(V)$

Method to calculate the maximum temperature the phase can create at a constant volume, if one exists; returns None otherwise.

### **Parameters**

V [float] Constant molar volume, [m^3/mol]

Pmax [float] Maximum possible isochoric pressure, if already known [Pa]

## Returns

T [float] Maximum possible temperature, [K]

#### property Tautoignitions

Autoignition temperatures for each component, [K].

### Returns

Tautoignitions [list[float]] Autoignition temperatures for each component, [K].

### property Tbs

Boiling temperatures for each component, [K].

## Returns

**Tbs** [list[float]] Boiling temperatures for each component, [K].

### property Tcs

Critical temperatures for each component, [K].

### Returns

Tcs [list[float]] Critical temperatures for each component, [K].

# property Tflashs

Flash point temperatures for each component, [K].

### Returns

Tflashs [list[float]] Flash point temperatures for each component, [K].

### Tmc()

Method to calculate and return the mechanical critical temperature of the phase.

#### Returns

Tmc [float] Mechanical critical temperature, [K]

### property Tms

Melting temperatures for each component, [K].

Tms [list[float]] Melting temperatures for each component, [K].

# property Tts

Triple point temperatures for each component, [K].

# Returns

**Tts** [list[float]] Triple point temperatures for each component, [K].

# **U**()

Method to calculate and return the internal energy of the phase.

$$U = H - PV$$

# Returns

U [float] Internal energy, [J/mol]

# property UFLs

Upper flammability limits for each component, [-].

### Returns

UFLs [list[float]] Upper flammability limits for each component, [-].

## property UNIFAC\_Dortmund\_groups

UNIFAC\_Dortmund\_group: count groups for each component, [-].

### Returns

**UNIFAC\_Dortmund\_groups** [list[dict]] UNIFAC\_Dortmund\_group: count groups for each component, [-].

# property UNIFAC\_Qs

UNIFAC Q parameters for each component, [-].

#### Returns

UNIFAC\_Qs [list[float]] UNIFAC Q parameters for each component, [-].

## property UNIFAC\_Rs

UNIFAC *R* parameters for each component, [-].

### Returns

UNIFAC\_Rs [list[float]] UNIFAC R parameters for each component, [-].

# property UNIFAC\_groups

UNIFAC\_group: count groups for each component, [-].

#### Returns

UNIFAC\_groups [list[dict]] UNIFAC\_group: count groups for each component, [-].

# U\_dep()

Method to calculate and return the departure internal energy of the phase.

$$U_{dep} = H_{dep} - PV_{dep}$$

# Returns

U\_dep [float] Departure internal energy, [J/mol]

### U\_formation\_ideal\_gas()

Method to calculate and return the ideal-gas internal energy of formation of the phase (as if the phase was an ideal gas).

$$U_{reactive}^{ig} = H_{reactive}^{ig} - P_{ref}^{ig} V^{ig}$$

Returns

**U\_formation\_ideal\_gas** [float] Internal energy of formation of the phase on a reactive basis as an ideal gas, [J/(mol)]

### U\_ideal\_gas()

Method to calculate and return the ideal-gas internal energy of the phase.

$$U^{ig} = H^{ig} - PV^{ig}$$

#### Returns

U\_ideal\_gas [float] Ideal gas internal energy, [J/(mol)]

### U\_mass()

Method to calculate and return mass internal energy of the phase.

$$U_{mass} = \frac{1000U_{molar}}{MW}$$

Returns

U\_mass [float] Mass internal energy, [J/(kg)]

### U\_reactive()

Method to calculate and return the internal energy of the phase on a reactive basis.

$$U_{reactive} = H_{reactive} - PV$$

Returns

U\_reactive [float] Internal energy of the phase on a reactive basis, [J/(mol)]

**V**()

Method to return the molar volume of the phase.

#### Returns

V [float] Molar volume, [m^3/mol]

#### property VF

Method to return the vapor fraction of the phase. If no vapor/gas is present, 0 is always returned. This method is only available when the phase is linked to an EquilibriumState.

Returns

VF [float] Vapor fraction, [-]

#### V\_MAX\_FIXED = 100000000.0

# $V_MIN_FIXED = 1e-09$

V\_dep()

Method to calculate and return the departure (from ideal gas behavior) molar volume of the phase.

$$V_{dep} = V - \frac{RT}{P}$$

Returns

V\_dep [float] Departure molar volume, [m^3/mol]

### V\_from\_phi()

Method to calculate and return the molar volume of the fluid as calculated from the pressure derivatives of fugacity coefficients.

$$V^{\text{from phi P der}} = \left( \left( \sum_{i} z_{i} \frac{\partial \ln \phi_{i}}{\partial P} \right) P + 1 \right) RT/P$$

Returns

V [float] Molar volume, [m^3/mol]

V\_gas()

Method to calculate and return the ideal-gas molar volume of the phase at the chosen reference temperature and pressure, according to the temperature variable  $T\_gas\_ref$  and pressure variable  $P\_gas\_ref$  of the thermo.bulk.BulkSettings.

$$V^{ig} = \frac{RT_{ref}}{P_{ref}}$$

### Returns

 $V_{gas}$  [float] Ideal gas molar volume at the reference temperature and pressure, [m<sup>3</sup>/mol]

# V\_gas\_normal()

Method to calculate and return the ideal-gas molar volume of the phase at the normal temperature and pressure, according to the temperature variable *T\_normal* and pressure variable *P\_normal* of the *thermo*. *bulk*.*BulkSettings*.

$$V^{ig} = \frac{RT_{norm}}{P_{norm}}$$

### Returns

V\_gas\_normal [float] Ideal gas molar volume at normal temperature and pressure, [m^3/mol]

### V\_gas\_standard()

Method to calculate and return the ideal-gas molar volume of the phase at the standard temperature and pressure, according to the temperature variable *T\_standard* and pressure variable *P\_standard* of the *thermo*. *bulk.BulkSettings*.

$$V^{ig} = \frac{RT_{std}}{P_{std}}$$

#### Returns

V\_gas\_standard [float] Ideal gas molar volume at standard temperature and pressure, [m^3/mol]

# V\_ideal\_gas()

Method to calculate and return the ideal-gas molar volume of the phase.

$$V^{ig} = \frac{RT}{P}$$

#### Returns

V [float] Ideal gas molar volume, [m^3/mol]

### V\_iter(force=False)

Method to calculate and return the volume of the phase in a way suitable for a TV resolution to converge on the same pressure. This often means the return value of this method is an mpmath *mpf*. This dummy method simply returns the implemented V method.

### Returns

V [float or mpf] Molar volume, [m^3/mol]

### V\_liquid\_ref()

Method to calculate and return the liquid reference molar volume according to the temperature variable *T\_liquid\_volume\_ref* of *thermo.bulk.BulkSettings* and the composition of the phase.

$$V = \sum_{i} z_i V_i$$

### Returns

V\_liquid\_ref [float] Liquid molar volume at the reference condition, [m^3/mol]

### V\_mass()

Method to calculate and return the specific volume of the phase.

$$V_{mass} = \frac{1000 \cdot VM}{MW}$$

#### Returns

V\_mass [float] Specific volume of the phase, [m^3/kg]

#### V\_phi\_consistency()

Method to calculate and return a consistency check between molar volume, and the fugacity coefficients' pressures derivatives.

$$V^{\text{from phi P der}} = \left( \left( \sum_{i} z_i \frac{\partial \ln \phi_i}{\partial P} \right) P + 1 \right) RT/P$$

Returns

error [float] Relative consistency error  $|1 - V^{\text{from phi P der}}/V^{\text{implemented}}|$ , [-]

# property Van\_der\_Waals\_areas

Unnormalized Van der Waals areas for each component, [m^2/mol].

#### Returns

Van\_der\_Waals\_areas [list[float]] Unnormalized Van der Waals areas for each component, [m^2/mol].

# property Van\_der\_Waals\_volumes

Unnormalized Van der Waals volumes for each component, [m^3/mol].

# Returns

Van\_der\_Waals\_volumes [list[float]] Unnormalized Van der Waals volumes for each component, [m^3/mol].

#### property Vcs

Critical molar volumes for each component, [m<sup>3</sup>/mol].

#### Returns

Vcs [list[float]] Critical molar volumes for each component, [m^3/mol].

# Vfgs()

Method to calculate and return the ideal-gas volume fractions of the components of the phase. This is the same as the mole fractions.

# Returns

Vfgs [list[float]] Ideal-gas volume fractions of the components of the phase, [-]

# Vfls()

Method to calculate and return the ideal-liquid volume fractions of the components of the phase, using the standard liquid densities at the temperature variable *T\_liquid\_volume\_ref* of thermo.bulk. BulkSettings and the composition of the phase.

### Returns

Vfls [list[float]] Ideal-liquid volume fractions of the components of the phase, [-]

# Vmc()

Method to calculate and return the mechanical critical volume of the phase.

# Returns

**Vmc** [float] Mechanical critical volume, [m<sup>3</sup>/mol]

# property Vmg\_STPs

Gas molar volumes for each component at STP; metastable if normally another state, [m^3/mol].

### Returns

Vmg\_STPs [list[float]] Gas molar volumes for each component at STP; metastable if normally another state, [m<sup>3</sup>/mol].

## property Vml\_60Fs

Liquid molar volumes for each component at 60 °F, [m^3/mol].

### Returns

Vml\_60Fs [list[float]] Liquid molar volumes for each component at 60 °F, [m^3/mol].

# property Vml\_STPs

Liquid molar volumes for each component at STP, [m^3/mol].

### Returns

Vml\_STPs [list[float]] Liquid molar volumes for each component at STP, [m^3/mol].

### property Vml\_Tms

Liquid molar volumes for each component at their respective melting points, [m^3/mol].

### Returns

**Vml\_Tms** [list[float]] Liquid molar volumes for each component at their respective melting points, [m^3/mol].

# property Vms\_Tms

Solid molar volumes for each component at their respective melting points, [m^3/mol].

# Returns

**Vms\_Tms** [list[float]] Solid molar volumes for each component at their respective melting points, [m^3/mol].

#### Wobbe\_index()

Method to calculate and return the molar Wobbe index of the object, [J/mol].

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{\text{SG}}}$$

Returns

Wobbe\_index\_lower()

Method to calculate and return the molar lower Wobbe index of the object, [J/mol].

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

Returns

Wobbe\_index\_lower [float] Molar lower Wobbe index, [J/(mol)]

# Wobbe\_index\_lower\_mass()

Method to calculate and return the lower mass Wobbe index of the object, [J/kg].

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

Returns

Wobbe\_index\_lower\_mass [float] Mass lower Wobbe index, [J/(kg)]

### Wobbe\_index\_lower\_normal()

Method to calculate and return the volumetric normal lower Wobbe index of the object, [J/m<sup>3</sup>]. The normal gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{SG}}$$

Returns

Wobbe\_index\_lower\_normal [float] Volumetric normal lower Wobbe index, [J/(m^3)]

### Wobbe\_index\_lower\_standard()

Method to calculate and return the volumetric standard lower Wobbe index of the object, [J/m^3]. The standard gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{lower}}{\sqrt{\mathrm{SG}}}$$

#### Returns

Wobbe\_index\_lower\_standard [float] Volumetric standard lower Wobbe index, [J/(m^3)]

## Wobbe\_index\_mass()

Method to calculate and return the mass Wobbe index of the object, [J/kg].

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{\text{SG}}}$$

Returns

Wobbe\_index\_mass [float] Mass Wobbe index, [J/(kg)]

### Wobbe\_index\_normal()

Method to calculate and return the volumetric normal Wobbe index of the object, [J/m^3]. The normal gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{SG}}$$

Returns

## Wobbe\_index\_standard()

Method to calculate and return the volumetric standard Wobbe index of the object, [J/m^3]. The standard gas volume is used in this calculation.

$$I_W = \frac{H_{comb}^{higher}}{\sqrt{SG}}$$

### Returns

Wobbe\_index\_standard [float] Volumetric standard Wobbe index, [J/(m^3)]

### Z()

Method to calculate and return the compressibility factor of the phase.

$$Z = \frac{PV}{RT}$$

### Returns

Z [float] Compressibility factor, [-]

## property Zcs

Critical compressibilities for each component, [-].

## Returns

Zcs [list[float]] Critical compressibilities for each component, [-].

### Zmc()

Method to calculate and return the mechanical critical compressibility of the phase.

# Returns

Zmc [float] Mechanical critical compressibility, [-]

# **\_\_\_eq\_\_**(*other*)

Return self==value.

# \_\_hash\_\_()

Method to calculate and return a hash representing the exact state of the object.

#### Returns

hash [int] Hash of the object, [-]

# activities()

Method to calculate and return the activities of each component in the phase [-].

$$a_i(T, P, x; f_i^0) = \frac{f_i(T, P, x)}{f_i^0(T, P_i^0)}$$

Returns

activities [list[float]] Activities, [-]

## as\_json()

Method to create a JSON-friendly serialization of the phase which can be stored, and reloaded later.

Returns

json\_repr [dict] JSON-friendly representation, [-]

## Examples

```
>>> import json
>>> from thermo import IAPWS95Liquid
>>> phase = IAPWS95Liquid(T=300, P=1e5, zs=[1])
>>> new_phase = Phase.from_json(json.loads(json.dumps(phase.as_json())))
>>> assert phase == new_phase
```

# atom\_fractions()

Method to calculate and return the atomic composition of the phase; returns a dictionary of atom fraction (by count), containing only those elements who are present.

### Returns

atom\_fractions [dict[str: float]] Atom fractions, [-]

## atom\_mass\_fractions()

Method to calculate and return the atomic mass fractions of the phase; returns a dictionary of atom fraction (by mass), containing only those elements who are present.

### Returns

atom\_mass\_fractions [dict[str: float]] Atom mass fractions, [-]

### property atomss

Breakdown of each component into its elements and their counts, as a dict, [-].

# Returns

atomss [list[dict]] Breakdown of each component into its elements and their counts, as a dict,

[-].

# property beta

Method to return the phase fraction of this phase. This method is only available when the phase is linked to an EquilibriumState.

## Returns

beta [float] Phase fraction on a molar basis, [-]

### property beta\_mass

Method to return the mass phase fraction of this phase. This method is only available when the phase is linked to an EquilibriumState.

### Returns

beta\_mass [float] Phase fraction on a mass basis, [-]

### property beta\_volume

Method to return the volumetric phase fraction of this phase. This method is only available when the phase is linked to an EquilibriumState.

#### Returns

beta\_volume [float] Phase fraction on a volumetric basis, [-]

#### property charges

Charge number (valence) for each component, [-].

Returns

charges [list[float]] Charge number (valence) for each component, [-].

## chemical\_potential()

Method to calculate and return the chemical potentials of each component in the phase [-]. For a pure substance, this is the molar Gibbs energy on a reactive basis.

 $\frac{\partial G}{\partial n_i}_{T,P,N_{i\neq i}}$ 

#### Returns

chemical\_potential [list[float]] Chemical potentials, [J/mol]

### composition\_independent = False

# property conductivities

Electrical conductivities for each component, [S/m].

Returns

conductivities [list[float]] Electrical conductivities for each component, [S/m].

### property conductivity\_Ts

Temperatures at which the electrical conductivities for each component were measured, [K].

#### Returns

**conductivity\_Ts** [list[float]] Temperatures at which the electrical conductivities for each component were measured, [K].

# $d2P_dT2()$

Method to calculate and return the second temperature derivative of pressure of the phase.

#### Returns

d2P\_dT2 [float] Second temperature derivative of pressure, [Pa/K^2]

## d2P\_dTdV()

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the phase.

### Returns

**d2P\_dTdV** [float] Second volume derivative of pressure, [mol\*Pa^2/(J\*K)]

### d2P\_dTdrho()

Method to calculate and return the temperature derivative and then molar density derivative of the pressure of the phase.

$$\frac{\partial^2 P}{\partial T \partial \rho} = -V^2 \left(\frac{\partial^2 P}{\partial T \partial V}\right)$$

### Returns

**d2P\_dTdrho** [float] Temperature derivative and then molar density derivative of the pressure, [Pa\*m^3/(K\*mol)]

# d2P\_dV2()

Method to calculate and return the second volume derivative of pressure of the phase.

Returns

d2P\_dV2 [float] Second volume derivative of pressure, [Pa\*mol^2/m^6]

# d2P\_dVdT()

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the phase. This is an alias of  $d2P_dTdV$ .

$$\frac{\partial^2 P}{\partial V \partial T}$$

Returns

### d2P\_drho2()

Method to calculate and return the second molar density derivative of pressure of the phase.

$$\frac{\partial^2 P}{\partial \rho^2} = -V^2 \left( -V^2 \left( \frac{\partial^2 P}{\partial V^2} \right)_T - 2V \left( \frac{\partial P}{\partial V} \right)_T \right)$$

Returns

**d2P\_drho2** [float] Second molar density derivative of pressure, [Pa\*m^6/mol^2]

# d2T\_dP2()

Method to calculate and return the constant-volume second pressure derivative of temperature of the phase.

$$\left(\frac{\partial^2 T}{\partial P^2}\right)_V = -\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial T}{\partial P}\right)_V^3$$

Returns

**d2T\_dP2** [float] Constant-volume second pressure derivative of temperature, [K/Pa^2]

#### d2T\_dP2\_V()

Method to calculate and return the constant-volume second pressure derivative of temperature of the phase.

$$\left(\frac{\partial^2 T}{\partial P^2}\right)_V = -\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial T}{\partial P}\right)_V^3$$

Returns

d2T\_dP2 [float] Constant-volume second pressure derivative of temperature, [K/Pa^2]

# d2T\_dPdV()

Method to calculate and return the derivative of pressure and then the derivative of volume of temperature of the phase.

$$\left(\frac{\partial^2 T}{\partial P \partial V}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V\right] \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

#### Returns

**d2T\_dPdV** [float] Derivative of pressure and then the derivative of volume of temperature, [K\*mol/(Pa\*m^3)]

#### d2T\_dPdrho()

Method to calculate and return the pressure derivative and then molar density derivative of the temperature of the phase.

$$\frac{\partial^2 T}{\partial P \partial \rho} = -V^2 \left( \frac{\partial^2 T}{\partial P \partial V} \right)$$

Returns

**d2T\_dPdrho** [float] Pressure derivative and then molar density derivative of the temperature, [K\*m^3/(Pa\*mol)]

d2T\_dV2()

Method to calculate and return the constant-pressure second volume derivative of temperature of the phase.

$$\left(\frac{\partial^2 T}{\partial V^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial V^2}\right)_T \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T\partial V}\right)\right] \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T\partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T\partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} - \left(\frac{\partial^2 P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right]$$

Returns

**d2T\_dV2** [float] Constant-pressure second volume derivative of temperature, [K\*mol^2/m^6]

# d2T\_dV2\_P()

Method to calculate and return the constant-pressure second volume derivative of temperature of the phase.

$$\left(\frac{\partial^2 T}{\partial V^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial V^2}\right)_T \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T \partial V}\right)\right] \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V^{-2} - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V^{-2}\right] \left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T \partial V}\right)_V^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right)_V^{-2} + \left(\frac{\partial^2 P}{\partial V}\right)_V^{-2} + \left(\frac{\partial^$$

Returns

**d2T\_dV2** [float] Constant-pressure second volume derivative of temperature, [K\*mol^2/m^6]

# d2T\_dVdP()

Method to calculate and return the derivative of pressure and then the derivative of volume of temperature of the phase.

$$\left(\frac{\partial^2 T}{\partial P \partial V}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial T}\right)_V - \left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial^2 P}{\partial T^2}\right)_V\right] \left(\frac{\partial P}{\partial T}\right)_V^{-3}$$

Returns

**d2T\_dPdV** [float] Derivative of pressure and then the derivative of volume of temperature, [K\*mol/(Pa\*m^3)]

### d2T\_drho2()

Method to calculate and return the second molar density derivative of temperature of the phase.

$$\frac{\partial^2 T}{\partial \rho^2} = -V^2 \left( -V^2 \left( \frac{\partial^2 T}{\partial V^2} \right)_P - 2V \left( \frac{\partial T}{\partial V} \right)_P \right)$$

Returns

**d2T\_drho2** [float] Second molar density derivative of temperature, [K\*m^6/mol^2]

d2V\_dP2()

Method to calculate and return the constant-temperature pressure derivative of volume of the phase.

$$\left(\frac{\partial^2 V}{\partial P^2}\right)_T = -\frac{\left(\frac{\partial^2 P}{\partial V^2}\right)_T}{\left(\frac{\partial P}{\partial V}\right)_T^3}$$

Returns

**d2V\_dP2** [float] Constant-temperature pressure derivative of volume, [m^3/(mol\*Pa^2)]

#### d2V\_dP2\_T()

Method to calculate and return the constant-temperature pressure derivative of volume of the phase.

$$\left(\frac{\partial^2 V}{\partial P^2}\right)_T = -\frac{\left(\frac{\partial^2 P}{\partial V^2}\right)_T}{\left(\frac{\partial P}{\partial V}\right)_T^3}$$

d2V\_dP2 [float] Constant-temperature pressure derivative of volume, [m^3/(mol\*Pa^2)]

### d2V\_dPdT()

Method to calculate and return the derivative of pressure and then the derivative of temperature of volume of the phase.

$$\left(\frac{\partial^2 V}{\partial T \partial P}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right] \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

### Returns

**d2V\_dPdT** [float] Derivative of pressure and then the derivative of temperature of volume, [m^3/(mol\*K\*Pa)]

#### d2V\_dT2()

Method to calculate and return the constant-pressure second temperature derivative of volume of the phase.

$$\left(\frac{\partial^2 V}{\partial T^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial T \partial V}\right)\right] \left(\frac{\partial P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right]$$

Returns

**d2V\_dT2** [float] Constant-pressure second temperature derivative of volume, [m^3/(mol\*K^2)]

## d2V\_dT2\_P()

Method to calculate and return the constant-pressure second temperature derivative of volume of the phase.

$$\left(\frac{\partial^2 V}{\partial T^2}\right)_P = -\left[\left(\frac{\partial^2 P}{\partial T^2}\right)_V \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial T \partial V}\right)\right] \left(\frac{\partial P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right] \left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T^{-2} - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right] \left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T^{-2} - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T^{-2}\right] \left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left[\left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left(\frac{\partial^2 P}{\partial V}\right)_T^{-2} + \left(\frac$$

Returns

**d2V\_dT2** [float] Constant-pressure second temperature derivative of volume, [m^3/(mol\*K^2)]

### d2V\_dTdP()

Method to calculate and return the derivative of pressure and then the derivative of temperature of volume of the phase.

$$\left(\frac{\partial^2 V}{\partial T \partial P}\right) = -\left[\left(\frac{\partial^2 P}{\partial T \partial V}\right) \left(\frac{\partial P}{\partial V}\right)_T - \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial^2 P}{\partial V^2}\right)_T\right] \left(\frac{\partial P}{\partial V}\right)_T^{-3}$$

Returns

 $\label{eq:linear} \begin{array}{l} d2V\_dPdT \quad \mbox{[float] Derivative of pressure and then the derivative of temperature of volume, \\ & \mbox{[m^3/(mol^*K^*Pa)]} \end{array}$ 

#### d2rho\_dP2()

Method to calculate and return the second pressure derivative of molar density of the phase.

$$\frac{\partial^2 \rho}{\partial P^2} = -\frac{1}{V^2} \left( \frac{\partial^2 V}{\partial P^2} \right)_T + \frac{2}{V^3} \left( \frac{\partial V}{\partial P} \right)_T^2$$

Returns

d2rho\_dP2 [float] Second pressure derivative of molar density, [mol^2/(Pa\*m^6)]

## d2rho\_dPdT()

Method to calculate and return the pressure derivative and then temperature derivative of the molar density of the phase.

$$\frac{\partial^2 \rho}{\partial P \partial T} = -\frac{1}{V^2} \left( \frac{\partial^2 V}{\partial P \partial T} \right) + \frac{2}{V^3} \left( \frac{\partial V}{\partial T} \right)_P \left( \frac{\partial V}{\partial P} \right)_T$$

#### Returns

**d2rho\_dPdT** [float] Pressure derivative and then temperature derivative of the molar density, [mol/(m^3\*K\*Pa)]

#### d2rho\_dT2()

Method to calculate and return the second temperature derivative of molar density of the phase.

$$\frac{\partial^2 \rho}{\partial T^2} = -\frac{1}{V^2} \left( \frac{\partial^2 V}{\partial T^2} \right)_P + \frac{2}{V^3} \left( \frac{\partial V}{\partial T} \right)_T^2$$

### Returns

**d2rho\_dT2** [float] Second temperature derivative of molar density, [mol^2/(K\*m^6)]

#### $dA_dP()$

Method to calculate and return the constant-temperature pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial U}{\partial P}\right)_T$$

### Returns

dA\_dP [float] Constant-temperature pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

 $dA_dP_T()$ 

Method to calculate and return the constant-temperature pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial U}{\partial P}\right)_T$$

Returns

dA\_dP [float] Constant-temperature pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

 $dA_dP_V()$ 

Method to calculate and return the constant-volume pressure derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial P}\right)_{V} = \left(\frac{\partial H}{\partial P}\right)_{V} - V - S\left(\frac{\partial T}{\partial P}\right)_{V} - T\left(\frac{\partial S}{\partial P}\right)_{V}$$

Returns

dA\_dP\_V [float] Constant-volume pressure derivative of Helmholtz energy, [J/(mol\*Pa)]

 $dA_dT()$ 

Method to calculate and return the constant-pressure temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial U}{\partial T}\right)_P$$

Returns

dA\_dT [float] Constant-pressure temperature derivative of Helmholtz energy, [J/(mol\*K)]

## dA\_dT\_P()

Method to calculate and return the constant-pressure temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial U}{\partial T}\right)_P$$

Returns

dA\_dT [float] Constant-pressure temperature derivative of Helmholtz energy, [J/(mol\*K)]

 $dA_dT_V()$ 

Method to calculate and return the constant-volume temperature derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial T}\right)_{V} = \left(\frac{\partial H}{\partial T}\right)_{V} - V\left(\frac{\partial P}{\partial T}\right)_{V} - T\left(\frac{\partial S}{\partial T}\right)_{V} - S$$

Returns

 $dA_dT_V$  [float] Constant-volume temperature derivative of Helmholtz energy, [J/(mol\*K)]

 $dA_dV_P()$ 

Method to calculate and return the constant-pressure volume derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial V}\right)_P = \left(\frac{\partial A}{\partial T}\right)_P \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

dA\_dV\_P [float] Constant-pressure volume derivative of Helmholtz energy, [J/(m^3)]

 $dA_dV_T()$ 

Method to calculate and return the constant-temperature volume derivative of Helmholtz energy.

$$\left(\frac{\partial A}{\partial V}\right)_T = \left(\frac{\partial A}{\partial P}\right)_T \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

dA\_dV\_T [float] Constant-temperature volume derivative of Helmholtz energy, [J/(m^3)]

 $dA_mass_dP(prop='dA_dP')$ 

Method to calculate and return the pressure derivative of mass Helmholtz energy of the phase at constant temperature.

$$\left(\frac{\partial A_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dA\_mass\_dP** [float] The pressure derivative of mass Helmholtz energy of the phase at constant temperature, [J/mol/Pa]

 $dA_mass_dP_T(prop='dA_dP_T')$ 

Method to calculate and return the pressure derivative of mass Helmholtz energy of the phase at constant temperature.

$$\left(\frac{\partial A_{\text{mass}}}{\partial P}\right)_T$$

**dA\_mass\_dP\_T** [float] The pressure derivative of mass Helmholtz energy of the phase at constant temperature, [J/mol/Pa]

## $dA_mass_dP_V(prop='dA_dP_V')$

Method to calculate and return the pressure derivative of mass Helmholtz energy of the phase at constant volume.

$$\left(\frac{\partial A_{\text{mass}}}{\partial P}\right)_V$$

#### Returns

**dA\_mass\_dP\_V** [float] The pressure derivative of mass Helmholtz energy of the phase at constant volume, [J/mol/Pa]

#### $dA_mass_dT(prop='dA_dT')$

Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at constant pressure.

$$\left(\frac{\partial A_{\text{mass}}}{\partial T}\right)_P$$

# Returns

**dA\_mass\_dT** [float] The temperature derivative of mass Helmholtz energy of the phase at constant pressure, [J/mol/K]

#### $dA_mass_dT_P(prop='dA_dT_P')$

Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at constant pressure.

$$\left(\frac{\partial A_{\text{mass}}}{\partial T}\right)_P$$

Returns

**dA\_mass\_dT\_P** [float] The temperature derivative of mass Helmholtz energy of the phase at constant pressure, [J/mol/K]

 $dA_mass_dT_V(prop='dA_dT_V')$ 

Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at constant volume.

$$\left(\frac{\partial A_{\text{mass}}}{\partial T}\right)_V$$

## Returns

**dA\_mass\_dT\_V** [float] The temperature derivative of mass Helmholtz energy of the phase at constant volume, [J/mol/K]

 $dA_mass_dV_P(prop='dA_dV_P')$ 

Method to calculate and return the volume derivative of mass Helmholtz energy of the phase at constant pressure.

$$\left(\frac{\partial A_{\text{mass}}}{\partial V}\right)_P$$

## Returns

**dA\_mass\_dV\_P** [float] The volume derivative of mass Helmholtz energy of the phase at constant pressure, [J/mol/m^3/mol]

### $dA_mass_dV_T(prop='dA_dV_T')$

Method to calculate and return the volume derivative of mass Helmholtz energy of the phase at constant temperature.

$$\left(\frac{\partial A_{\text{mass}}}{\partial V}\right)_T$$

#### Returns

**dA\_mass\_dV\_T** [float] The volume derivative of mass Helmholtz energy of the phase at constant temperature, [J/mol/m^3/mol]

## dCpigs\_dT\_pure()

Method to calculate and return the first temperature derivative of ideal-gas heat capacities of every component in the phase. This method is powered by the *HeatCapacityGases* objects, except when all components have the same heat capacity form and a fast implementation has been written for it (currently only polynomials).

$$\frac{\partial C_p^{ig}}{\partial T}$$

#### Returns

**dCp\_ig\_dT** [list[float]] First temperature derivatives of molar ideal gas heat capacities, [J/(mol\*K^2)]

# $dCv_dP_T()$

Method to calculate the pressure derivative of Cv, constant volume heat capacity, at constant temperature.

$$\left(\frac{\partial C_v}{\partial P}\right)_T = -T \,\mathrm{dPdT}_{\mathrm{V}}\left(P\right) \frac{d}{dP} \,\mathrm{dVdT}_{\mathrm{P}}\left(P\right) - T \,\mathrm{dVdT}_{\mathrm{P}}\left(P\right) \frac{d}{dP} \,\mathrm{dPdT}_{\mathrm{V}}\left(P\right) + \frac{d}{dP} \,\mathrm{Cp}\left(P\right)$$

## Returns

dCv\_dP\_T [float] Pressure derivative of constant volume heat capacity at constant temperature, [J/mol/K/Pa]

### Notes

Requires d2V\_dTdP, d2P\_dTdP, and d2H\_dTdP.

### dCv\_dT\_P()

Method to calculate the temperature derivative of Cv, constant volume heat capacity, at constant pressure.

$$\left(\frac{\partial C_{v}}{\partial T}\right)_{P} = -\frac{T \operatorname{dPdT_{V}}^{2}(T) \frac{d}{dT} \operatorname{dPdV_{T}}(T)}{\operatorname{dPdV_{T}}^{2}(T)} + \frac{2T \operatorname{dPdT_{V}}(T) \frac{d}{dT} \operatorname{dPdT_{V}}(T)}{\operatorname{dPdV_{T}}(T)} + \frac{\operatorname{dPdT_{V}}^{2}(T)}{\operatorname{dPdV_{T}}(T)} + \frac{d}{dT} \operatorname{Cp}(T)$$

Returns

**dCv\_dT\_P** [float] Temperature derivative of constant volume heat capacity at constant pressure, [J/mol/K^2]

### Notes

Requires *d2P\_dT2\_PV*, *d2P\_dVdT\_TP*, and *d2H\_dT2*.

#### $dCv_mass_dP_T(prop='dCv_dP_T')$

Method to calculate and return the pressure derivative of mass Constant-volume heat capacity of the phase at constant temperature.

$$\left(\frac{\partial Cv_{\text{mass}}}{\partial P}\right)_{T}$$

### Returns

**dCv\_mass\_dP\_T** [float] The pressure derivative of mass Constant-volume heat capacity of the phase at constant temperature, [J/(mol\*K)/Pa]

## $dCv_mass_dT_P(prop='dCv_dT_P')$

Method to calculate and return the temperature derivative of mass Constant-volume heat capacity of the phase at constant pressure.

$$\left(\frac{\partial Cv_{\text{mass}}}{\partial T}\right)_P$$

Returns

 $dCv_mass_dT_P$  [float] The temperature derivative of mass Constant-volume heat capacity of the phase at constant pressure,  $[J/(mol^*K)/K]$ 

dG\_dP()

Method to calculate and return the constant-temperature pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dG\_dP [float] Constant-temperature pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

# $dG_dP_T()$

Method to calculate and return the constant-temperature pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_T = -T\left(\frac{\partial S}{\partial P}\right)_T + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dG\_dP [float] Constant-temperature pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

# $dG_dP_V()$

Method to calculate and return the constant-volume pressure derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial P}\right)_{V} = -T\left(\frac{\partial S}{\partial P}\right)_{V} - S\left(\frac{\partial T}{\partial P}\right)_{V} + \left(\frac{\partial H}{\partial P}\right)_{V}$$

Returns

dG\_dP\_V [float] Constant-volume pressure derivative of Gibbs free energy, [J/(mol\*Pa)]

 $dG_dT()$ 

Method to calculate and return the constant-pressure temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

**dG\_dT** [float] Constant-pressure temperature derivative of Gibbs free energy, [J/(mol\*K)]

 $dG_dT_P()$ 

Method to calculate and return the constant-pressure temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_P = -T\left(\frac{\partial S}{\partial T}\right)_P - S + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

dG\_dT [float] Constant-pressure temperature derivative of Gibbs free energy, [J/(mol\*K)]

dG\_dT\_V()

Method to calculate and return the constant-volume temperature derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial T}\right)_V = -T\left(\frac{\partial S}{\partial T}\right)_V - S + \left(\frac{\partial H}{\partial T}\right)_V$$

Returns

 $dG_dT_V$  [float] Constant-volume temperature derivative of Gibbs free energy,  $[J/(mol^*K)]$ 

 $dG_dV_P()$ 

Method to calculate and return the constant-pressure volume derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial V}\right)_P = \left(\frac{\partial G}{\partial T}\right)_P \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

dG\_dV\_P [float] Constant-pressure volume derivative of Gibbs free energy, [J/(m^3)]

 $dG_dV_T()$ 

Method to calculate and return the constant-temperature volume derivative of Gibbs free energy.

$$\left(\frac{\partial G}{\partial V}\right)_T = \left(\frac{\partial G}{\partial P}\right)_T \left(\frac{\partial P}{\partial V}\right)_T$$

dG\_dV\_T [float] Constant-temperature volume derivative of Gibbs free energy, [J/(m^3)]

### $dG_mass_dP(prop='dG_dP')$

Method to calculate and return the pressure derivative of mass Gibbs free energy of the phase at constant temperature.

$$\left(\frac{\partial G_{\text{mass}}}{\partial P}\right)_T$$

### Returns

**dG\_mass\_dP** [float] The pressure derivative of mass Gibbs free energy of the phase at constant temperature, [J/mol/Pa]

### $dG_mass_dP_T(prop='dG_dP_T')$

Method to calculate and return the pressure derivative of mass Gibbs free energy of the phase at constant temperature.

$$\left(\frac{\partial G_{\text{mass}}}{\partial P}\right)_T$$

# Returns

**dG\_mass\_dP\_T** [float] The pressure derivative of mass Gibbs free energy of the phase at constant temperature, [J/mol/Pa]

### $dG_mass_dP_V(prop='dG_dP_V')$

Method to calculate and return the pressure derivative of mass Gibbs free energy of the phase at constant volume.

$$\left(\frac{\partial G_{\text{mass}}}{\partial P}\right)_V$$

Returns

**dG\_mass\_dP\_V** [float] The pressure derivative of mass Gibbs free energy of the phase at constant volume, [J/mol/Pa]

$$dG_mass_dT(prop='dG_dT')$$

Method to calculate and return the temperature derivative of mass Gibbs free energy of the phase at constant pressure.

$$\left(\frac{\partial G_{\text{mass}}}{\partial T}\right)_P$$

Returns

**dG\_mass\_dT** [float] The temperature derivative of mass Gibbs free energy of the phase at constant pressure, [J/mol/K]

 $dG_mass_dT_P(prop='dG_dT_P')$ 

Method to calculate and return the temperature derivative of mass Gibbs free energy of the phase at constant pressure.

$$\left(\frac{\partial G_{\text{mass}}}{\partial T}\right)_P$$

## Returns

**dG\_mass\_dT\_P** [float] The temperature derivative of mass Gibbs free energy of the phase at constant pressure, [J/mol/K]

## $dG_mass_dT_V(prop='dG_dT_V')$

Method to calculate and return the temperature derivative of mass Gibbs free energy of the phase at constant volume.

$$\left(\frac{\partial G_{\text{mass}}}{\partial T}\right)_V$$

### Returns

**dG\_mass\_dT\_V** [float] The temperature derivative of mass Gibbs free energy of the phase at constant volume, [J/mol/K]

### $dG_mass_dV_P(prop='dG_dV_P')$

Method to calculate and return the volume derivative of mass Gibbs free energy of the phase at constant pressure.

$$\left(\frac{\partial G_{\text{mass}}}{\partial V}\right)_P$$

#### Returns

**dG\_mass\_dV\_P** [float] The volume derivative of mass Gibbs free energy of the phase at constant pressure, [J/mol/m^3/mol]

### $dG_mass_dV_T(prop='dG_dV_T')$

Method to calculate and return the volume derivative of mass Gibbs free energy of the phase at constant temperature.

$$\left(\frac{\partial G_{\text{mass}}}{\partial V}\right)_T$$

### Returns

**dG\_mass\_dV\_T** [float] The volume derivative of mass Gibbs free energy of the phase at constant temperature, [J/mol/m^3/mol]

# $dH_dP_T()$

Method to calculate and return the pressure derivative of enthalpy of the phase at constant pressure.

#### Returns

**dH\_dP\_T** [float] Pressure derivative of enthalpy, [J/(mol\*Pa)]

## $dH_dT_P()$

Method to calculate and return the temperature derivative of enthalpy of the phase at constant pressure.

#### Returns

**dH\_dT\_P** [float] Temperature derivative of enthalpy, [J/(mol\*K)]

dH\_dns()

Method to calculate and return the mole number derivative of the enthalpy of the phase.

$$\frac{\partial H}{\partial n_i}$$

### Returns

dH\_dns [list[float]] Mole number derivatives of the enthalpy of the phase, [J/mol^2]

### dH\_mass\_dP(prop='dH\_dP')

Method to calculate and return the pressure derivative of mass enthalpy of the phase at constant temperature.

$$\left(\frac{\partial H_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dH\_mass\_dP** [float] The pressure derivative of mass enthalpy of the phase at constant temperature, [J/mol/Pa]

### $dH_mass_dP_T(prop='dH_dP_T')$

Method to calculate and return the pressure derivative of mass enthalpy of the phase at constant temperature.

$$\left(\frac{\partial H_{\rm mass}}{\partial P}\right)_{T}$$

#### Returns

**dH\_mass\_dP\_T** [float] The pressure derivative of mass enthalpy of the phase at constant temperature, [J/mol/Pa]

 $dH_mass_dP_V(prop='dH_dP_V')$ 

Method to calculate and return the pressure derivative of mass enthalpy of the phase at constant volume.

$$\left(\frac{\partial H_{\text{mass}}}{\partial P}\right)_V$$

### Returns

**dH\_mass\_dP\_V** [float] The pressure derivative of mass enthalpy of the phase at constant volume, [J/mol/Pa]

## $dH_mass_dT(prop='dH_dT')$

Method to calculate and return the temperature derivative of mass enthalpy of the phase at constant pressure.

$$\left(\frac{\partial H_{\text{mass}}}{\partial T}\right)_{P}$$

**dH\_mass\_dT** [float] The temperature derivative of mass enthalpy of the phase at constant pressure, [J/mol/K]

 $dH_mass_dT_P(prop='dH_dT_P')$ 

Method to calculate and return the temperature derivative of mass enthalpy of the phase at constant pressure.

$$\left(\frac{\partial H_{\text{mass}}}{\partial T}\right)_P$$

#### Returns

**dH\_mass\_dT\_P** [float] The temperature derivative of mass enthalpy of the phase at constant pressure, [J/mol/K]

# $dH_mass_dT_V(prop='dH_dT_V')$

Method to calculate and return the temperature derivative of mass enthalpy of the phase at constant volume.

$$\left(\frac{\partial H_{\text{mass}}}{\partial T}\right)_V$$

## Returns

**dH\_mass\_dT\_V** [float] The temperature derivative of mass enthalpy of the phase at constant volume, [J/mol/K]

dH\_mass\_dV\_P( $prop='dH_dV_P'$ ) Method to calculate and return the volume derivative of mass enthalpy of the phase at constant pressure.

$$\left(\frac{\partial H_{\text{mass}}}{\partial V}\right)_P$$

Returns

**dH\_mass\_dV\_P** [float] The volume derivative of mass enthalpy of the phase at constant pressure, [J/mol/m^3/mol]

 $dH_mass_dV_T(prop='dH_dV_T')$ 

Method to calculate and return the volume derivative of mass enthalpy of the phase at constant temperature.

$$\left(\frac{\partial H_{\text{mass}}}{\partial V}\right)_T$$

### Returns

**dH\_mass\_dV\_T** [float] The volume derivative of mass enthalpy of the phase at constant temperature, [J/mol/m^3/mol]

**dP\_dP\_A**(*property='P'*, *differentiate\_by='P'*, *at\_constant='A'*) Method to calculate and return the pressure derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial P}\right)_A$$

### Returns

**dP\_dP\_A** [float] The pressure derivative of pressure of the phase at constant Helmholtz energy, [Pa/Pa]

dP\_dP\_G(*property='P'*, *differentiate\_by='P'*, *at\_constant='G'*) Method to calculate and return the pressure derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial P}\right)_G$$

# Returns

**dP\_dP\_G** [float] The pressure derivative of pressure of the phase at constant Gibbs energy, [Pa/Pa]

dP\_dP\_H(*property='P'*, *differentiate\_by='P'*, *at\_constant='H'*) Method to calculate and return the pressure derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial P}\right)_H$$

#### Returns

**dP\_dP\_H** [float] The pressure derivative of pressure of the phase at constant enthalpy, [Pa/Pa]

dP\_dP\_S(*property='P'*, *differentiate\_by='P'*, *at\_constant='S'*) Method to calculate and return the pressure derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial P}\right)_S$$

#### Returns

dP\_dP\_S [float] The pressure derivative of pressure of the phase at constant entropy, [Pa/Pa]

## $dP_dP_T()$

Method to calculate and return the pressure derivative of pressure of the phase at constant temperature.

Returns

dP\_dP\_T [float] Pressure derivative of pressure of the phase at constant temperature, [-]

**dP\_dP\_U**(*property='P'*, *differentiate\_by='P'*, *at\_constant='U'*)

Method to calculate and return the pressure derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial P}\right)_U$$

**dP\_dP\_U** [float] The pressure derivative of pressure of the phase at constant internal energy, [Pa/Pa]

#### $dP_dP_V()$

Method to calculate and return the pressure derivative of pressure of the phase at constant volume.

Returns

dP\_dP\_V [float] Pressure derivative of pressure of the phase at constant volume, [-]

#### $dP_dT()$

Method to calculate and return the first temperature derivative of pressure of the phase.

### Returns

**dP\_dT** [float] First temperature derivative of pressure, [Pa/K]

**dP\_dT\_A**(*property='P'*, *differentiate\_by='T'*, *at\_constant='A'*)

Method to calculate and return the temperature derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial T}\right)_A$$

# Returns

**dP\_dT\_A** [float] The temperature derivative of pressure of the phase at constant Helmholtz energy, [Pa/K]

dP\_dT\_G(*property='P'*, *differentiate\_by='T'*, *at\_constant='G'*) Method to calculate and return the temperature derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial T}\right)_{G}$$

### Returns

**dP\_dT\_G** [float] The temperature derivative of pressure of the phase at constant Gibbs energy, [Pa/K]

**dP\_dT\_H**(*property='P'*, *differentiate\_by='T'*, *at\_constant='H'*) Method to calculate and return the temperature derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial T}\right)_H$$

### Returns

**dP\_dT\_H** [float] The temperature derivative of pressure of the phase at constant enthalpy, [Pa/K]

### $dP_dT_P()$

Method to calculate and return the temperature derivative of temperature of the phase at constant pressure.

Returns

dP\_dT\_P [float] Temperature derivative of temperature, [-]

**dP\_dT\_S**(*property='P'*, *differentiate\_by='T'*, *at\_constant='S'*)

Method to calculate and return the temperature derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial T}\right)_S$$

### Returns

**dP\_dT\_S** [float] The temperature derivative of pressure of the phase at constant entropy, [Pa/K]

**dP\_dT\_U**(*property='P'*, *differentiate\_by='T'*, *at\_constant='U'*)

Method to calculate and return the temperature derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial T}\right)_U$$

### Returns

**dP\_dT\_U** [float] The temperature derivative of pressure of the phase at constant internal energy, [Pa/K]

 $dP_dV()$ 

Method to calculate and return the first volume derivative of pressure of the phase.

Returns

**dP\_dV** [float] First volume derivative of pressure, [Pa\*mol/m^3]

**dP\_dV\_A**(property='P', differentiate\_by='V', at\_constant='A')

Method to calculate and return the volume derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial V}\right)_A$$

#### Returns

**dP\_dV\_A** [float] The volume derivative of pressure of the phase at constant Helmholtz energy, [Pa/m^3/mol]

**dP\_dV\_G**(*property='P'*, *differentiate\_by='V'*, *at\_constant='G'*) Method to calculate and return the volume derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial V}\right)_G$$

**dP\_dV\_G** [float] The volume derivative of pressure of the phase at constant Gibbs energy, [Pa/m^3/mol]

dP\_dV\_H(*property='P'*, *differentiate\_by='V'*, *at\_constant='H'*) Method to calculate and return the volume derivative of pressure of the phase at constant enthalpy.

 $\left(\frac{\partial P}{\partial V}\right)_H$ 

### Returns

**dP\_dV\_H** [float] The volume derivative of pressure of the phase at constant enthalpy, [Pa/m^3/mol]

#### $dP_dV_P()$

Method to calculate and return the volume derivative of pressure of the phase at constant pressure.

#### Returns

**dP\_dV\_P** [float] Volume derivative of pressure of the phase at constant pressure, [Pa\*mol/m^3]

**dP\_dV\_S**(*property='P'*, *differentiate\_by='V'*, *at\_constant='S'*) Method to calculate and return the volume derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial V}\right)_S$$

## Returns

**dP\_dV\_S** [float] The volume derivative of pressure of the phase at constant entropy, [Pa/m^3/mol]

**dP\_dV\_U**(*property='P'*, *differentiate\_by='V'*, *at\_constant='U'*) Method to calculate and return the volume derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial V}\right)_U$$

#### Returns

**dP\_dV\_U** [float] The volume derivative of pressure of the phase at constant internal energy, [Pa/m^3/mol]

# dP\_drho()

Method to calculate and return the molar density derivative of pressure of the phase.

$$\frac{\partial P}{\partial \rho} = -V^2 \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

dP\_drho [float] Molar density derivative of pressure, [Pa\*m^3/mol]

**dP\_drho\_A**(*property='P'*, *differentiate\_by='rho'*, *at\_constant='A'*) Method to calculate and return the density derivative of pressure of the phase at constant Helmholtz energy.

$$\left(\frac{\partial P}{\partial \rho}\right)_A$$

#### Returns

**dP\_drho\_A** [float] The density derivative of pressure of the phase at constant Helmholtz energy, [Pa/mol/m^3]

**dP\_drho\_G**(*property='P'*, *differentiate\_by='rho'*, *at\_constant='G'*) Method to calculate and return the density derivative of pressure of the phase at constant Gibbs energy.

$$\left(\frac{\partial P}{\partial \rho}\right)_G$$

### Returns

**dP\_drho\_G** [float] The density derivative of pressure of the phase at constant Gibbs energy, [Pa/mol/m^3]

**dP\_drho\_H**(*property='P'*, *differentiate\_by='rho'*, *at\_constant='H'*) Method to calculate and return the density derivative of pressure of the phase at constant enthalpy.

$$\left(\frac{\partial P}{\partial \rho}\right)_{H}$$

#### Returns

**dP\_drho\_H** [float] The density derivative of pressure of the phase at constant enthalpy, [Pa/mol/m^3]

dP\_drho\_S(property='P', differentiate\_by='rho', at\_constant='S') Method to calculate and return the density derivative of pressure of the phase at constant entropy.

$$\left(\frac{\partial P}{\partial \rho}\right)_S$$

### Returns

**dP\_drho\_S** [float] The density derivative of pressure of the phase at constant entropy, [Pa/mol/m^3]

**dP\_drho\_U**(*property='P'*, *differentiate\_by='rho'*, *at\_constant='U'*) Method to calculate and return the density derivative of pressure of the phase at constant internal energy.

$$\left(\frac{\partial P}{\partial \rho}\right)_{l}$$

Returns

**dP\_drho\_U** [float] The density derivative of pressure of the phase at constant internal energy, [Pa/mol/m^3]

# dS\_dP\_T()

Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.

#### Returns

**dS\_dP\_T** [float] Pressure derivative of entropy, [J/(mol\*K\*Pa)]

# dS\_dV\_P()

Method to calculate and return the volume derivative of entropy of the phase at constant pressure.

#### Returns

**dS\_dV\_P** [float] Volume derivative of entropy, [J/(K\*m^3)]

### $dS_dV_T()$

Method to calculate and return the volume derivative of entropy of the phase at constant temperature.

#### Returns

$$dS_dV_T$$
 [float] Volume derivative of entropy, [J/(K\*m^3)]

### dS\_dns()

Method to calculate and return the mole number derivative of the entropy of the phase.

$$\frac{\partial S}{\partial n_i}$$

#### Returns

dS\_dns [list[float]] Mole number derivatives of the entropy of the phase, [J/(mol^2\*K)]

### $dS_mass_dP(prop='dS_dP')$

Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.

$$\left(\frac{\partial S_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dS\_mass\_dP** [float] The pressure derivative of mass entropy of the phase at constant temperature, [J/(mol\*K)/Pa]

### $dS_mass_dP_T(prop='dS_dP_T')$

Method to calculate and return the pressure derivative of mass entropy of the phase at constant temperature.

$$\left(\frac{\partial S_{\text{mass}}}{\partial P}\right)_T$$

#### Returns

**dS\_mass\_dP\_T** [float] The pressure derivative of mass entropy of the phase at constant temperature, [J/(mol\*K)/Pa]

### $dS_mass_dP_V(prop='dS_dP_V')$

Method to calculate and return the pressure derivative of mass entropy of the phase at constant volume.

$$\left(\frac{\partial S_{\text{mass}}}{\partial P}\right)_V$$

dS\_mass\_dP\_V [float] The pressure derivative of mass entropy of the phase at constant volume, [J/(mol\*K)/Pa]

## $dS_mass_dT(prop='dS_dT')$

Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.

$$\left(\frac{\partial S_{\text{mass}}}{\partial T}\right)_P$$

#### Returns

**dS\_mass\_dT** [float] The temperature derivative of mass entropy of the phase at constant pressure, [J/(mol\*K)/K]

# $dS_mass_dT_P(prop='dS_dT_P')$

Method to calculate and return the temperature derivative of mass entropy of the phase at constant pressure.

$$\left(\frac{\partial S_{\text{mass}}}{\partial T}\right)_P$$

## Returns

**dS\_mass\_dT\_P** [float] The temperature derivative of mass entropy of the phase at constant pressure, [J/(mol\*K)/K]

 $dS_mass_dT_V(prop='dS_dT_V')$ 

Method to calculate and return the temperature derivative of mass entropy of the phase at constant volume.

$$\left(\frac{\partial S_{\text{mass}}}{\partial T}\right)_V$$

#### Returns

 $dS_mass_dT_V$  [float] The temperature derivative of mass entropy of the phase at constant volume,  $[J/(mol^*K)/K]$ 

$$dS_mass_dV_P(prop='dS_dV_P')$$

Method to calculate and return the volume derivative of mass entropy of the phase at constant pressure.

$$\left(\frac{\partial S_{\text{mass}}}{\partial V}\right)_P$$

### Returns

**dS\_mass\_dV\_P** [float] The volume derivative of mass entropy of the phase at constant pressure, [J/(mol\*K)/m^3/mol]

 $dS_mass_dV_T(prop='dS_dV_T')$ 

Method to calculate and return the volume derivative of mass entropy of the phase at constant temperature.

$$\left(\frac{\partial S_{\text{mass}}}{\partial V}\right)_T$$

### Returns

**dS\_mass\_dV\_T** [float] The volume derivative of mass entropy of the phase at constant temperature, [J/(mol\*K)/m^3/mol]

### dT\_dP()

Method to calculate and return the constant-volume pressure derivative of temperature of the phase.

$$\left(\frac{\partial T}{\partial P}\right)_V = \frac{1}{\left(\frac{\partial P}{\partial T}\right)_V}$$

Returns

dT\_dP [float] Constant-volume pressure derivative of temperature, [K/Pa]

**dT\_dP\_A**(*property='T'*, *differentiate\_by='P'*, *at\_constant='A'*)

Method to calculate and return the pressure derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial P}\right)_A$$

# Returns

**dT\_dP\_A** [float] The pressure derivative of temperature of the phase at constant Helmholtz energy, [K/Pa]

**dT\_dP\_G**(*property='T'*, *differentiate\_by='P'*, *at\_constant='G'*) Method to calculate and return the pressure derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial P}\right)_{G}$$

### Returns

**dT\_dP\_G** [float] The pressure derivative of temperature of the phase at constant Gibbs energy, [K/Pa]

**dT\_dP\_H**(*property='T'*, *differentiate\_by='P'*, *at\_constant='H'*) Method to calculate and return the pressure derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial P}\right)_H$$

### Returns

**dT\_dP\_H** [float] The pressure derivative of temperature of the phase at constant enthalpy, [K/Pa]

**dT\_dP\_S**(*property='T'*, *differentiate\_by='P'*, *at\_constant='S'*) Mathed to calculate and actume the pressure domination of temperature of the phase

Method to calculate and return the pressure derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial P}\right)_S$$

Returns

**dT\_dP\_S** [float] The pressure derivative of temperature of the phase at constant entropy, [K/Pa]

## $dT_dP_T()$

Method to calculate and return the pressure derivative of temperature of the phase at constant temperature.

#### Returns

**dT\_dP\_T** [float] Pressure derivative of temperature of the phase at constant temperature, [K/Pa]

### **dT\_dP\_U**(*property='T'*, *differentiate\_by='P'*, *at\_constant='U'*)

Method to calculate and return the pressure derivative of temperature of the phase at constant internal energy.

 $\left(\frac{\partial T}{\partial P}\right)_U$ 

#### Returns

**dT\_dP\_U** [float] The pressure derivative of temperature of the phase at constant internal energy, [K/Pa]

### $dT_dP_V()$

Method to calculate and return the constant-volume pressure derivative of temperature of the phase.

$$\left(\frac{\partial T}{\partial P}\right)_V = \frac{1}{\left(\frac{\partial P}{\partial T}\right)_V}$$

Returns

dT\_dP [float] Constant-volume pressure derivative of temperature, [K/Pa]

Method to calculate and return the temperature derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial T}\right)_A$$

#### Returns

**dT\_dT\_A** [float] The temperature derivative of temperature of the phase at constant Helmholtz energy, [K/K]

# **dT\_dT\_G**(*property='T'*, *differentiate\_by='T'*, *at\_constant='G'*)

Method to calculate and return the temperature derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial T}\right)_G$$

**dT\_dT\_G** [float] The temperature derivative of temperature of the phase at constant Gibbs energy, [K/K]

**dT\_dT\_H**(*property='T'*, *differentiate\_by='T'*, *at\_constant='H'*)

Method to calculate and return the temperature derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial T}\right)_{H}$$

#### Returns

**dT\_dT\_H** [float] The temperature derivative of temperature of the phase at constant enthalpy, [K/K]

## dT\_dT\_P()

Method to calculate and return the temperature derivative of temperature of the phase at constant pressure.

#### Returns

dT\_dT\_P [float] Temperature derivative of temperature of the phase at constant pressure, [-]

Method to calculate and return the temperature derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial T}\right)_S$$

### Returns

**dT\_dT\_S** [float] The temperature derivative of temperature of the phase at constant entropy, [K/K]

## **dT\_dT\_U**(*property='T'*, *differentiate\_by='T'*, *at\_constant='U'*)

Method to calculate and return the temperature derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial T}\right)_U$$

### Returns

**dT\_dT\_U** [float] The temperature derivative of temperature of the phase at constant internal energy, [K/K]

# dT\_dT\_V()

Method to calculate and return the temperature derivative of temperature of the phase at constant volume.

Returns

dT\_dT\_V [float] Temperature derivative of temperature of the phase at constant volume, [-]

dT\_dV()

Method to calculate and return the constant-pressure volume derivative of temperature of the phase.

$$\left(\frac{\partial T}{\partial V}\right)_P = \frac{1}{\left(\frac{\partial V}{\partial T}\right)_P}$$

Returns

dT\_dV [float] Constant-pressure volume derivative of temperature, [K\*m^3/(m^3)]

**dT\_dV\_A**(*property='T'*, *differentiate\_by='V'*, *at\_constant='A'*)

Method to calculate and return the volume derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial V}\right)_A$$

#### Returns

**dT\_dV\_A** [float] The volume derivative of temperature of the phase at constant Helmholtz energy, [K/m^3/mol]

 $dT_dV_G(property='T', differentiate_by='V', at_constant='G')$ Method to calculate and return the volume derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial V}\right)_G$$

### Returns

**dT\_dV\_G** [float] The volume derivative of temperature of the phase at constant Gibbs energy, [K/m^3/mol]

dT\_dV\_H(*property='T'*, *differentiate\_by='V'*, *at\_constant='H'*) Method to calculate and return the volume derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial V}\right)_H$$

### Returns

**dT\_dV\_H** [float] The volume derivative of temperature of the phase at constant enthalpy, [K/m^3/mol]

# $dT_dV_P()$

Method to calculate and return the constant-pressure volume derivative of temperature of the phase.

$$\left(\frac{\partial T}{\partial V}\right)_P = \frac{1}{\left(\frac{\partial V}{\partial T}\right)_P}$$

Returns

**dT\_dV** [float] Constant-pressure volume derivative of temperature, [K\*m^3/(m^3)]

**dT\_dV\_S**(*property='T'*, *differentiate\_by='V'*, *at\_constant='S'*)

Method to calculate and return the volume derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial V}\right)_S$$

### Returns

**dT\_dV\_S** [float] The volume derivative of temperature of the phase at constant entropy, [K/m^3/mol]

### dT\_dV\_T()

Method to calculate and return the volume derivative of temperature of the phase at constant temperature.

#### Returns

**dT\_dV\_T** [float] Pressure derivative of temperature of the phase at constant temperature, [K\*mol/m^3]

#### $dT_dV_U(property='T', differentiate_by='V', at_constant='U')$

Method to calculate and return the volume derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial V}\right)_U$$

### Returns

**dT\_dV\_U** [float] The volume derivative of temperature of the phase at constant internal energy, [K/m^3/mol]

## dT\_drho()

Method to calculate and return the molar density derivative of temperature of the phase.

$$\frac{\partial T}{\partial \rho} = -V^2 \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

dT\_drho [float] Molar density derivative of temperature, [K\*m^3/mol]

### **dT\_drho\_A**(*property='T'*, *differentiate\_by='rho'*, *at\_constant='A'*)

Method to calculate and return the density derivative of temperature of the phase at constant Helmholtz energy.

$$\left(\frac{\partial T}{\partial\rho}\right)_A$$

### Returns

**dT\_drho\_A** [float] The density derivative of temperature of the phase at constant Helmholtz energy, [K/mol/m^3]

### **dT\_drho\_G**(*property='T'*, *differentiate\_by='rho'*, *at\_constant='G'*)

Method to calculate and return the density derivative of temperature of the phase at constant Gibbs energy.

$$\left(\frac{\partial T}{\partial \rho}\right)_G$$

**dT\_drho\_G** [float] The density derivative of temperature of the phase at constant Gibbs energy, [K/mol/m^3]

**dT\_drho\_H**(*property='T'*, *differentiate\_by='rho'*, *at\_constant='H'*) Method to calculate and return the density derivative of temperature of the phase at constant enthalpy.

$$\left(\frac{\partial T}{\partial\rho}\right)_{H}$$

#### Returns

**dT\_drho\_H** [float] The density derivative of temperature of the phase at constant enthalpy, [K/mol/m^3]

**dT\_drho\_S**(*property='T'*, *differentiate\_by='rho'*, *at\_constant='S'*) Method to calculate and return the density derivative of temperature of the phase at constant entropy.

$$\left(\frac{\partial T}{\partial \rho}\right)_S$$

# Returns

**dT\_drho\_S** [float] The density derivative of temperature of the phase at constant entropy, [K/mol/m^3]

**dT\_drho\_U**(*property='T'*, *differentiate\_by='rho'*, *at\_constant='U'*) Method to calculate and return the density derivative of temperature of the phase at constant internal energy.

$$\left(\frac{\partial T}{\partial \rho}\right)_U$$

Returns

**dT\_drho\_U** [float] The density derivative of temperature of the phase at constant internal energy, [K/mol/m^3]

dU\_dP()

Method to calculate and return the constant-temperature pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_T = -P\left(\frac{\partial V}{\partial P}\right)_T - V + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dU\_dP [float] Constant-temperature pressure derivative of internal energy, [J/(mol\*Pa)]

# dU\_dP\_T()

Method to calculate and return the constant-temperature pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_T = -P\left(\frac{\partial V}{\partial P}\right)_T - V + \left(\frac{\partial H}{\partial P}\right)_T$$

Returns

dU\_dP [float] Constant-temperature pressure derivative of internal energy, [J/(mol\*Pa)]

dU\_dP\_V()

Method to calculate and return the constant-volume pressure derivative of internal energy.

$$\left(\frac{\partial U}{\partial P}\right)_V = \left(\frac{\partial H}{\partial P}\right)_V - V$$

Returns

dU\_dP\_V [float] Constant-volume pressure derivative of internal energy, [J/(mol\*Pa)]

dU\_dT()

Method to calculate and return the constant-pressure temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_P = -P\left(\frac{\partial V}{\partial T}\right)_P + \left(\frac{\partial H}{\partial T}\right)_P$$

Returns

 $dU_dT$  [float] Constant-pressure temperature derivative of internal energy, [J/(mol\*K)]

 $dU_dT_P()$ 

Method to calculate and return the constant-pressure temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_{P} = -P\left(\frac{\partial V}{\partial T}\right)_{P} + \left(\frac{\partial H}{\partial T}\right)_{P}$$

Returns

dU\_dT [float] Constant-pressure temperature derivative of internal energy, [J/(mol\*K)]

 $dU_dT_V()$ 

Method to calculate and return the constant-volume temperature derivative of internal energy.

$$\left(\frac{\partial U}{\partial T}\right)_V = \left(\frac{\partial H}{\partial T}\right)_V - V\left(\frac{\partial P}{\partial T}\right)_V$$

Returns

dU\_dT\_V [float] Constant-volume temperature derivative of internal energy, [J/(mol\*K)]

 $dU_dV_P()$ 

Method to calculate and return the constant-pressure volume derivative of internal energy.

$$\left(\frac{\partial U}{\partial V}\right)_P = \left(\frac{\partial U}{\partial T}\right)_P \left(\frac{\partial T}{\partial V}\right)_P$$

Returns

dU\_dV\_P [float] Constant-pressure volume derivative of internal energy, [J/(m^3)]

 $dU_dV_T()$ 

Method to calculate and return the constant-temperature volume derivative of internal energy.

$$\left(\frac{\partial U}{\partial V}\right)_T = \left(\frac{\partial U}{\partial P}\right)_T \left(\frac{\partial P}{\partial V}\right)_T$$

dU\_dV\_T [float] Constant-temperature volume derivative of internal energy, [J/(m^3)]

# dU\_mass\_dP(prop='dU\_dP')

Method to calculate and return the pressure derivative of mass internal energy of the phase at constant temperature.

$$\left(\frac{\partial U_{\text{mass}}}{\partial P}\right)_T$$

# Returns

**dU\_mass\_dP** [float] The pressure derivative of mass internal energy of the phase at constant temperature, [J/mol/Pa]

# $dU_mass_dP_T(prop='dU_dP_T')$

Method to calculate and return the pressure derivative of mass internal energy of the phase at constant temperature.

$$\left(\frac{\partial U_{\text{mass}}}{\partial P}\right)_{T}$$

# Returns

dU\_mass\_dP\_T [float] The pressure derivative of mass internal energy of the phase at constant temperature, [J/mol/Pa]

# $dU_mass_dP_V(prop='dU_dP_V')$

Method to calculate and return the pressure derivative of mass internal energy of the phase at constant volume.

$$\left(\frac{\partial U_{\text{mass}}}{\partial P}\right)_V$$

# Returns

**dU\_mass\_dP\_V** [float] The pressure derivative of mass internal energy of the phase at constant volume, [J/mol/Pa]

$$dU_mass_dT(prop='dU_dT')$$

Method to calculate and return the temperature derivative of mass internal energy of the phase at constant pressure.

$$\left(\frac{\partial U_{\text{mass}}}{\partial T}\right)_P$$

Returns

**dU\_mass\_dT** [float] The temperature derivative of mass internal energy of the phase at constant pressure, [J/mol/K]

 $dU_mass_dT_P(prop='dU_dT_P')$ 

Method to calculate and return the temperature derivative of mass internal energy of the phase at constant pressure.

$$\left(\frac{\partial U_{\text{mass}}}{\partial T}\right)_P$$

Returns

**dU\_mass\_dT\_P** [float] The temperature derivative of mass internal energy of the phase at constant pressure, [J/mol/K]

# $dU_mass_dT_V(prop='dU_dT_V')$

Method to calculate and return the temperature derivative of mass internal energy of the phase at constant volume.

$$\left(\frac{\partial U_{\text{mass}}}{\partial T}\right)_V$$

#### Returns

**dU\_mass\_dT\_V** [float] The temperature derivative of mass internal energy of the phase at constant volume, [J/mol/K]

# $dU_mass_dV_P(prop='dU_dV_P')$

Method to calculate and return the volume derivative of mass internal energy of the phase at constant pressure.

$$\left(\frac{\partial U_{\text{mass}}}{\partial V}\right)_P$$

## Returns

**dU\_mass\_dV\_P** [float] The volume derivative of mass internal energy of the phase at constant pressure, [J/mol/m^3/mol]

## $dU_mass_dV_T(prop='dU_dV_T')$

Method to calculate and return the volume derivative of mass internal energy of the phase at constant temperature.

$$\left(\frac{\partial U_{\text{mass}}}{\partial V}\right)_T$$

## Returns

**dU\_mass\_dV\_T** [float] The volume derivative of mass internal energy of the phase at constant temperature, [J/mol/m^3/mol]

 $dV_dP()$ 

Method to calculate and return the constant-temperature pressure derivative of volume of the phase.

$$\left(\frac{\partial V}{\partial P}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial T}{\partial P}\right)_V$$

dV\_dP [float] Constant-temperature pressure derivative of volume, [m^3/(mol\*Pa)]

**dV\_dP\_A**(*property='V'*, *differentiate\_by='P'*, *at\_constant='A'*) Method to calculate and return the pressure derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial P}\right)_A$$

# Returns

**dV\_dP\_A** [float] The pressure derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/Pa]

**dV\_dP\_G**(*property='V'*, *differentiate\_by='P'*, *at\_constant='G'*) Method to calculate and return the pressure derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial P}\right)_G$$

## Returns

**dV\_dP\_G** [float] The pressure derivative of volume of the phase at constant Gibbs energy, [m^3/mol/Pa]

 $dV_dP_H(property='V', differentiate_by='P', at_constant='H')$ Method to calculate and return the pressure derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial P}\right)_{H}$$

#### Returns

**dV\_dP\_H** [float] The pressure derivative of volume of the phase at constant enthalpy, [m^3/mol/Pa]

**dV\_dP\_S**(*property='V'*, *differentiate\_by='P'*, *at\_constant='S'*) Method to calculate and return the pressure derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial P}\right)_S$$

# Returns

**dV\_dP\_S** [float] The pressure derivative of volume of the phase at constant entropy, [m^3/mol/Pa]

# $dV_dP_T()$

Method to calculate and return the constant-temperature pressure derivative of volume of the phase.

$$\left(\frac{\partial V}{\partial P}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial T}{\partial P}\right)_V$$

dV\_dP [float] Constant-temperature pressure derivative of volume, [m^3/(mol\*Pa)]

**dV\_dP\_U**(*property='V'*, *differentiate\_by='P'*, *at\_constant='U'*) Method to calculate and return the pressure derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial P}\right)_{U}$$

# Returns

**dV\_dP\_U** [float] The pressure derivative of volume of the phase at constant internal energy, [m^3/mol/Pa]

# $dV_dP_V()$

Method to calculate and return the volume derivative of pressure of the phase at constant volume.

#### Returns

**dV\_dP\_V** [float] Pressure derivative of volume of the phase at constant pressure, [m^3/(mol\*Pa)]

# dV\_dT()

Method to calculate and return the constant-pressure temperature derivative of volume of the phase.

$$\left(\frac{\partial V}{\partial T}\right)_P = \frac{-\left(\frac{\partial P}{\partial T}\right)_V}{\left(\frac{\partial P}{\partial V}\right)_T}$$

#### Returns

dV\_dT [float] Constant-pressure temperature derivative of volume, [m^3/(mol\*K)]

# **dV\_dT\_A**(*property='V'*, *differentiate\_by='T'*, *at\_constant='A'*)

Method to calculate and return the temperature derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial T}\right)_A$$

# Returns

**dV\_dT\_A** [float] The temperature derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/K]

**dV\_dT\_G**(*property='V'*, *differentiate\_by='T'*, *at\_constant='G'*)

Method to calculate and return the temperature derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial T}\right)_G$$

## Returns

**dV\_dT\_G** [float] The temperature derivative of volume of the phase at constant Gibbs energy, [m^3/mol/K]

dV\_dT\_H(*property='V'*, *differentiate\_by='T'*, *at\_constant='H'*) Method to calculate and return the temperature derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial T}\right)_H$$

# Returns

**dV\_dT\_H** [float] The temperature derivative of volume of the phase at constant enthalpy, [m^3/mol/K]

## $dV_dT_P()$

Method to calculate and return the constant-pressure temperature derivative of volume of the phase.

$$\left(\frac{\partial V}{\partial T}\right)_P = \frac{-\left(\frac{\partial P}{\partial T}\right)_V}{\left(\frac{\partial P}{\partial V}\right)_T}$$

Returns

**dV\_dT\_S**(*property='V'*, *differentiate\_by='T'*, *at\_constant='S'*) Method to calculate and return the temperature derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial T}\right)_S$$

## Returns

**dV\_dT\_S** [float] The temperature derivative of volume of the phase at constant entropy, [m^3/mol/K]

 $dV_dT_U(property='V', differentiate_by='T', at_constant='U')$ Method to calculate and return the temperature derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial T}\right)_U$$

#### Returns

**dV\_dT\_U** [float] The temperature derivative of volume of the phase at constant internal energy, [m^3/mol/K]

# $dV_dT_V()$

Method to calculate and return the temperature derivative of volume of the phase at constant volume.

# Returns

**dV\_dT\_V** [float] Temperature derivative of volume of the phase at constant volume, [m^3/(mol\*K)]

# **dV\_dV\_A**(*property='V'*, *differentiate\_by='V'*, *at\_constant='A'*)

Method to calculate and return the volume derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial V}\right)_A$$

**dV\_dV\_A** [float] The volume derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/m^3/mol]

 $dV_dV_G(property='V', differentiate_by='V', at_constant='G')$ Method to calculate and return the volume derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial V}\right)_G$$

#### Returns

 $dV_dV_G$  [float] The volume derivative of volume of the phase at constant Gibbs energy, [m^3/mol/m^3/mol]

**dV\_dV\_H**(*property='V'*, *differentiate\_by='V'*, *at\_constant='H'*) Method to calculate and return the volume derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial V}\right)_H$$

#### Returns

**dV\_dV\_H** [float] The volume derivative of volume of the phase at constant enthalpy, [m^3/mol/m^3/mol]

# $dV_dV_P()$

Method to calculate and return the volume derivative of volume of the phase at constant pressure.

#### Returns

dV\_dV\_P [float] Volume derivative of volume of the phase at constant pressure, [-]

```
dV_dV_S(property='V', differentiate_by='V', at_constant='S')
Method to calculate and return the volume derivative of volume of the phase at constant entropy.
```

$$\left(\frac{\partial V}{\partial V}\right)_S$$

## Returns

**dV\_dV\_S** [float] The volume derivative of volume of the phase at constant entropy, [m^3/mol/m^3/mol]

## $dV_dV_T()$

Method to calculate and return the volume derivative of volume of the phase at constant temperature.

#### Returns

dV\_dV\_T [float] Volume derivative of volume of the phase at constant temperature, [-]

 $dV_dV_U$ (property='V', differentiate\_by='V', at\_constant='U') Method to calculate and return the volume derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial V}\right)_U$$

# Returns

**dV\_dV\_U** [float] The volume derivative of volume of the phase at constant internal energy, [m^3/mol/m^3/mol]

# dV\_dns()

Method to calculate and return the mole number derivatives of the molar volume V of the phase.

$$\frac{\partial V}{\partial n_i}$$

#### Returns

dV\_dns [list[float]] Mole number derivatives of the molar volume of the phase, [m^3]

**dV\_drho\_A**(*property='V'*, *differentiate\_by='rho'*, *at\_constant='A'*) Method to calculate and return the density derivative of volume of the phase at constant Helmholtz energy.

$$\left(\frac{\partial V}{\partial \rho}\right)_A$$

## Returns

**dV\_drho\_A** [float] The density derivative of volume of the phase at constant Helmholtz energy, [m^3/mol/mol/m^3]

**dV\_drho\_G**(*property='V'*, *differentiate\_by='rho'*, *at\_constant='G'*) Method to calculate and return the density derivative of volume of the phase at constant Gibbs energy.

$$\left(\frac{\partial V}{\partial \rho}\right)_G$$

#### Returns

**dV\_drho\_G** [float] The density derivative of volume of the phase at constant Gibbs energy, [m^3/mol/mol/m^3]

**dV\_drho\_H**(*property='V'*, *differentiate\_by='rho'*, *at\_constant='H'*) Method to calculate and return the density derivative of volume of the phase at constant enthalpy.

$$\left(\frac{\partial V}{\partial \rho}\right)_{H}$$

Returns

**dV\_drho\_H** [float] The density derivative of volume of the phase at constant enthalpy, [m^3/mol/mol/m^3]

**dV\_drho\_S**(*property='V'*, *differentiate\_by='rho'*, *at\_constant='S'*)

Method to calculate and return the density derivative of volume of the phase at constant entropy.

$$\left(\frac{\partial V}{\partial \rho}\right)_S$$

## Returns

**dV\_drho\_S** [float] The density derivative of volume of the phase at constant entropy, [m^3/mol/mol/m^3]

**dV\_drho\_U**(*property='V'*, *differentiate\_by='rho'*, *at\_constant='U'*) Method to calculate and return the density derivative of volume of the phase at constant internal energy.

$$\left(\frac{\partial V}{\partial \rho}\right)_U$$

# Returns

**dV\_drho\_U** [float] The density derivative of volume of the phase at constant internal energy, [m^3/mol/mol/m^3]

## $dZ_dP()$

Method to calculate and return the pressure derivative of compressibility of the phase.

$$\frac{\partial Z}{\partial P} = \frac{V + P\left(\frac{\partial V}{\partial P}\right)_T}{RT}$$

Returns

dZ\_dP [float] Pressure derivative of compressibility, [1/Pa]

 $dZ_dT()$ 

Method to calculate and return the temperature derivative of compressibility of the phase.

$$\frac{\partial Z}{\partial P} = P \frac{\left(\frac{\partial V}{\partial T}\right)_P - \frac{-V}{T}}{RT}$$

Returns

dZ\_dT [float] Temperature derivative of compressibility, [1/K]

 $dZ_dV()$ 

Method to calculate and return the volume derivative of compressibility of the phase.

$$\frac{\partial Z}{\partial V} = \frac{P - \rho \left(\frac{\partial P}{\partial \rho}\right)_T}{RT}$$

Returns

**dZ\_dV** [float] Volume derivative of compressibility, [mol/(m^3)]

dZ\_dns()

Method to calculate and return the mole number derivatives of the compressibility factor Z of the phase.

 $\frac{\partial Z}{\partial n_i}$ 

**dZ\_dns** [list[float]] Mole number derivatives of the compressibility factor of the phase, [1/mol]

dZ\_dzs()

Method to calculate and return the mole fraction derivatives of the compressibility factor Z of the phase.

$$\frac{\partial Z}{\partial z_i}$$

#### Returns

**dZ\_dzs** [list[float]] Mole fraction derivatives of the compressibility factor of the phase, [-]

#### dfugacities\_dP()

Method to calculate and return the pressure derivative of the fugacities of the components in the phase.

$$\frac{\partial f_i}{\partial P} = z_i \left( P \frac{\partial \phi_i}{\partial P} + \phi_i \right)$$

#### Returns

**dfugacities\_dP** [list[float]] Pressure derivative of fugacities of all components in the phase, [-]

# Notes

For models without pressure dependence of fugacity, the returned result may not be exactly zero due to inaccuracy in floating point results; results are likely on the order of 1e-14 or lower in that case.

## dfugacities\_dT()

Method to calculate and return the temperature derivative of fugacities of the phase.

$$\frac{\partial f_i}{\partial T} = P z_i \frac{\partial \ln \phi_i}{\partial T}$$

# Returns

**dfugacities\_dT** [list[float]] Temperature derivative of fugacities of all components in the phase, [Pa/K]

# dfugacities\_dns()

Method to calculate and return the mole number derivative of the fugacities of the components in the phase.

if i != j:

$$\frac{\partial f_i}{\partial n_j} = P\phi_i z_i \left(\frac{\partial \ln \phi_i}{\partial n_j} - 1\right)$$

if i == j:

$$\frac{\partial f_i}{\partial n_j} = P\phi_i z_i \left(\frac{\partial \ln \phi_i}{\partial n_j} - 1\right) + P\phi_i$$

#### Returns

**dfugacities\_dns** [list[list[float]]] Mole number derivatives of the fugacities of all components in the phase, [Pa/mol]

## dfugacity\_dP()

Method to calculate and return the pressure derivative of fugacity of the phase; provided the phase is 1 component.

**dfugacity\_dP** [list[float]] Fugacity first pressure derivative, [-]

## dfugacity\_dT()

Method to calculate and return the temperature derivative of fugacity of the phase; provided the phase is 1 component.

Returns

**dfugacity dT** [list[float]] Fugacity first temperature derivative, [Pa/K]

# property dipoles

Dipole moments for each component, [debye].

Returns

**dipoles** [list[float]] Dipole moments for each component, [debye].

#### disobaric\_expansion\_dP()

Method to calculate and return the pressure derivative of isobatic expansion coefficient of the phase.

$$\frac{\partial \beta}{\partial P} = \frac{1}{V} \left( \left( \frac{\partial^2 V}{\partial T \partial P} \right) - \frac{\left( \frac{\partial V}{\partial T} \right)_P \left( \frac{\partial V}{\partial P} \right)_T}{V} \right)$$

Returns

dbeta\_dP [float] Pressure derivative of isobaric coefficient of a thermal expansion, [1/(K\*Pa)]

#### disobaric\_expansion\_dT()

Method to calculate and return the temperature derivative of isobatic expansion coefficient of the phase.

$$\frac{\partial \beta}{\partial T} = \frac{1}{V} \left( \left( \frac{\partial^2 V}{\partial T^2} \right)_P - \left( \frac{\partial V}{\partial T} \right)_P^2 / V \right)$$

Returns

**dbeta dT** [float] Temperature derivative of isobaric coefficient of a thermal expansion, [1/K^2]

# disothermal\_compressibility\_dT()

Method to calculate and return the temperature derivative of isothermal compressibility of the phase. 、

$$\frac{\partial \kappa}{\partial T} = -\frac{\left(\frac{\partial^2 V}{\partial P \partial T}\right)}{V} + \frac{\left(\frac{\partial V}{\partial P}\right)_T \left(\frac{\partial V}{\partial T}\right)_P}{V^2}$$

Returns

**dkappa dT** [float] First temperature derivative of isothermal coefficient of compressibility,  $[1/(Pa^{*}K)]$ 

#### $dkappa_dT()$

Method to calculate and return the temperature derivative of isothermal compressibility of the phase. `

/ 0

$$\frac{\partial \kappa}{\partial T} = -\frac{\left(\frac{\partial^2 V}{\partial P \partial T}\right)}{V} + \frac{\left(\frac{\partial V}{\partial P}\right)_T \left(\frac{\partial V}{\partial T}\right)_P}{V^2}$$

Returns

**dkappa\_dT** [float] First temperature derivative of isothermal coefficient of compressibility, [1/(Pa\*K)]

#### dlnfugacities\_dns()

Method to calculate and return the mole number derivative of the log of fugacities of the components in the phase.

$$\frac{\partial \ln f_i}{\partial n_j} = \frac{1}{f_i} \frac{\partial f_i}{\partial n_j}$$

Returns

**dlnfugacities\_dns** [list[float]]] Mole number derivatives of the log of fugacities of all components in the phase, [log(Pa)/mol]

# dlnfugacities\_dzs()

Method to calculate and return the mole fraction derivative of the log of fugacities of the components in the phase.

$$\frac{\partial \ln f_i}{\partial z_j} = \frac{1}{f_i} \frac{\partial f_i}{\partial z_j}$$

#### Returns

**dlnfugacities\_dzs** [list[list[float]]] Mole fraction derivatives of the log of fugacities of all components in the phase, [log(Pa)]

# dlnphis\_dP()

Method to calculate and return the pressure derivative of the log of fugacity coefficients of each component in the phase.

#### Returns

dlnphis\_dP [list[float]] First pressure derivative of log fugacity coefficients, [1/Pa]

# dlnphis\_dT()

Method to calculate and return the temperature derivative of the log of fugacity coefficients of each component in the phase.

#### Returns

dlnphis\_dT [list[float]] First temperature derivative of log fugacity coefficients, [1/K]

#### dphis\_dP()

Method to calculate and return the pressure derivative of fugacity coefficients of the phase.

$$\frac{\partial \phi_i}{\partial P} = \phi_i \frac{\partial \ln \phi_i}{\partial P}$$

#### Returns

**dphis\_dP** [list[float]] Pressure derivative of fugacity coefficients of all components in the phase, [1/Pa]

# dphis\_dT()

Method to calculate and return the temperature derivative of fugacity coefficients of the phase.

$$\frac{\partial \phi_i}{\partial T} = \phi_i \frac{\partial \ln \phi_i}{\partial T}$$

# Returns

**dphis\_dT** [list[float]] Temperature derivative of fugacity coefficients of all components in the phase, [1/K]

# dphis\_dzs()

Method to calculate and return the molar composition derivative of fugacity coefficients of the phase.

$$\frac{\partial \phi_i}{\partial z_j} = \phi_i \frac{\partial \ln \phi_i}{\partial z_j}$$

## Returns

**dphis\_dzs** [list[list[float]]] Molar derivative of fugacity coefficients of all components in the phase, [-]

drho\_dP()

Method to calculate and return the pressure derivative of molar density of the phase.

$$\frac{\partial \rho}{\partial P} = -\frac{1}{V^2} \left( \frac{\partial V}{\partial P} \right)_T$$

#### Returns

drho\_dP [float] Pressure derivative of Molar density, [mol/(Pa\*m^3)]

**drho\_dP\_A**(*property='rho'*, *differentiate\_by='P'*, *at\_constant='A'*) Method to calculate and return the pressure derivative of density of the phase at constant Helmholtz energy.

# $\left(\frac{\partial\rho}{\partial P}\right)_A$

#### Returns

**drho\_dP\_A** [float] The pressure derivative of density of the phase at constant Helmholtz energy, [mol/m^3/Pa]

**drho\_dP\_G**(*property='rho'*, *differentiate\_by='P'*, *at\_constant='G'*) Method to calculate and return the pressure derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial P}\right)_{G}$$

# Returns

**drho\_dP\_G** [float] The pressure derivative of density of the phase at constant Gibbs energy, [mol/m^3/Pa]

**drho\_dP\_H**(*property='rho'*, *differentiate\_by='P'*, *at\_constant='H'*) Method to calculate and return the pressure derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial \rho}{\partial P}\right)_{H}$$

#### Returns

**drho\_dP\_H** [float] The pressure derivative of density of the phase at constant enthalpy, [mol/m^3/Pa]

**drho\_dP\_S**(*property='rho'*, *differentiate\_by='P'*, *at\_constant='S'*) Method to calculate and return the pressure derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial P}\right)_S$$

**drho\_dP\_S** [float] The pressure derivative of density of the phase at constant entropy, [mol/m^3/Pa]

**drho\_dP\_U**(*property='rho'*, *differentiate\_by='P'*, *at\_constant='U'*) Method to calculate and return the pressure derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial P}\right)_{U}$$

#### Returns

**drho\_dP\_U** [float] The pressure derivative of density of the phase at constant internal energy, [mol/m^3/Pa]

# drho\_dT()

Method to calculate and return the temperature derivative of molar density of the phase.

$$\frac{\partial \rho}{\partial T} = -\frac{1}{V^2} \left( \frac{\partial V}{\partial T} \right)_P$$

Returns

drho\_dT [float] Temperature derivative of molar density, [mol/(K\*m^3)]

**drho\_dT\_A**(*property='rho'*, *differentiate\_by='T'*, *at\_constant='A'*)

Method to calculate and return the temperature derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial T}\right)_A$$

## Returns

**drho\_dT\_A** [float] The temperature derivative of density of the phase at constant Helmholtz energy, [mol/m^3/K]

 $drho_dT_G(property='rho', differentiate_by='T', at_constant='G')$ Method to calculate and return the temperature derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial T}\right)_G$$

Returns

**drho\_dT\_G** [float] The temperature derivative of density of the phase at constant Gibbs energy, [mol/m^3/K]

**drho\_dT\_H**(property='rho', differentiate\_by='T', at\_constant='H')

Method to calculate and return the temperature derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial\rho}{\partial T}\right)_H$$

#### Returns

**drho\_dT\_H** [float] The temperature derivative of density of the phase at constant enthalpy, [mol/m^3/K]

**drho\_dT\_S**(*property='rho'*, *differentiate\_by='T'*, *at\_constant='S'*) Method to calculate and return the temperature derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial T}\right)_S$$

#### Returns

**drho\_dT\_S** [float] The temperature derivative of density of the phase at constant entropy, [mol/m^3/K]

**drho\_dT\_U**(*property='rho'*, *differentiate\_by='T'*, *at\_constant='U'*) Method to calculate and return the temperature derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial T}\right)_U$$

#### Returns

**drho\_dT\_U** [float] The temperature derivative of density of the phase at constant internal energy, [mol/m^3/K]

# drho\_dT\_V()

Method to calculate and return the temperature derivative of molar density of the phase at constant volume.

$$\left(\frac{\partial\rho}{\partial T}\right)_V = 0$$

#### Returns

**drho\_dT\_V** [float] Temperature derivative of molar density of the phase at constant volume, [mol/(m^3\*K)]

**drho\_dV\_A**(*property='rho'*, *differentiate\_by='V'*, *at\_constant='A'*) Method to calculate and return the volume derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial V}\right)_A$$

#### Returns

**drho\_dV\_A** [float] The volume derivative of density of the phase at constant Helmholtz energy, [mol/m^3/m^3/mol]

**drho\_dV\_G**(*property='rho'*, *differentiate\_by='V'*, *at\_constant='G'*) Method to calculate and return the volume derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial V}\right)_G$$

## Returns

**drho\_dV\_G** [float] The volume derivative of density of the phase at constant Gibbs energy, [mol/m^3/m^3/mol]

 $drho_dV_H(property='rho', differentiate_by='V', at_constant='H')$ Method to calculate and return the volume derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial\rho}{\partial V}\right)_{H}$$

# Returns

**drho\_dV\_H** [float] The volume derivative of density of the phase at constant enthalpy, [mol/m^3/m^3/mol]

**drho\_dV\_S**(*property='rho'*, *differentiate\_by='V'*, *at\_constant='S'*) Method to calculate and return the volume derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial V}\right)_S$$

# Returns

**drho\_dV\_S** [float] The volume derivative of density of the phase at constant entropy, [mol/m^3/m^3/mol]

# drho\_dV\_T()

Method to calculate and return the volume derivative of molar density of the phase.

$$\frac{\partial \rho}{\partial V} = -\frac{1}{V^2}$$

#### Returns

**drho\_dV\_T** [float] Molar density derivative of volume, [mol<sup>2</sup>/m<sup>6</sup>]

**drho\_dV\_U**(*property='rho'*, *differentiate\_by='V'*, *at\_constant='U'*) Method to calculate and return the volume derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial V}\right)_U$$

Returns

**drho\_dV\_U** [float] The volume derivative of density of the phase at constant internal energy, [mol/m^3/m^3/mol]

**drho\_drho\_A**(*property='rho'*, *differentiate\_by='rho'*, *at\_constant='A'*) Method to calculate and return the density derivative of density of the phase at constant Helmholtz energy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_A$$

#### Returns

**drho\_drho\_A** [float] The density derivative of density of the phase at constant Helmholtz energy, [mol/m^3/mol/m^3]

**drho\_drho\_G**(*property='rho'*, *differentiate\_by='rho'*, *at\_constant='G'*) Method to calculate and return the density derivative of density of the phase at constant Gibbs energy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_{G}$$

#### Returns

**drho\_drho\_G** [float] The density derivative of density of the phase at constant Gibbs energy, [mol/m^3/mol/m^3]

**drho\_drho\_H**(*property='rho'*, *differentiate\_by='rho'*, *at\_constant='H'*) Method to calculate and return the density derivative of density of the phase at constant enthalpy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_{H}$$

#### Returns

**drho\_drho\_H** [float] The density derivative of density of the phase at constant enthalpy, [mol/m^3/mol/m^3]

**drho\_drho\_S**(*property='rho'*, *differentiate\_by='rho'*, *at\_constant='S'*) Method to calculate and return the density derivative of density of the phase at constant entropy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_{S}$$

## Returns

**drho\_drho\_S** [float] The density derivative of density of the phase at constant entropy, [mol/m^3/mol/m^3]

**drho\_drho\_U**(*property='rho'*, *differentiate\_by='rho'*, *at\_constant='U'*) Method to calculate and return the density derivative of density of the phase at constant internal energy.

$$\left(\frac{\partial\rho}{\partial\rho}\right)_U$$

Returns

**drho\_drho\_U** [float] The density derivative of density of the phase at constant internal energy, [mol/m^3/mol/m^3]

## drho\_mass\_dP()

Method to calculate the mass density derivative with respect to pressure, at constant temperature.

$$\left(\frac{\partial\rho}{\partial P}\right)_T = \frac{-\mathrm{MW}\frac{\partial V_m}{\partial P}}{1000V_m^2}$$

Returns

**drho\_mass\_dP** [float] Pressure derivative of mass density at constant temperature, [kg/m^3/Pa]

# Notes

Requires dV\_dP, MW, and V.

This expression is readily obtainable with SymTy:

```
>>> from sympy import *
>>> P, T, MW = symbols('P, T, MW')
>>> Vm = symbols('Vm', cls=Function)
>>> rho_mass = (Vm(P))**-1*MW/1000
>>> diff(rho_mass, P)
-MW*Derivative(Vm(P), P)/(1000*Vm(P)**2)
```

# drho\_mass\_dT()

Method to calculate the mass density derivative with respect to temperature, at constant pressure.

$$\left(\frac{\partial \rho}{\partial T}\right)_P = \frac{-\mathbf{M}\mathbf{W}\frac{\partial V_m}{\partial T}}{1000V_m^2}$$

Returns

**drho\_mass\_dT** [float] Temperature derivative of mass density at constant pressure, [kg/m^3/K]

# Notes

Requires  $dV_dT$ , MW, and V.

This expression is readily obtainable with SymPy:

```
>>> from sympy import *
>>> T, P, MW = symbols('T, P, MW')
>>> Vm = symbols('Vm', cls=Function)
>>> rho_mass = (Vm(T))**-1*MW/1000
>>> diff(rho_mass, T)
-MW*Derivative(Vm(T), T)/(1000*Vm(T)**2)
```

# $dspeed_of_sound_dP_T()$

Method to calculate the pressure derivative of speed of sound at constant temperature in molar units.

$$\left(\frac{\partial c}{\partial P}\right)_{T} = -\frac{\sqrt{\frac{-\frac{Cp\left(P\right)V^{2}\left(P\right)dPdV_{T}\left(P\right)}{Cv\left(P\right)}\left(-\frac{Cp\left(P\right)V^{2}\left(P\right)\frac{d}{dP}dPdV_{T}\left(P\right)}{2Cv\left(P\right)} - \frac{Cp\left(P\right)V\left(P\right)dPdV_{T}\left(P\right)\frac{d}{dP}V\left(P\right)}{Cv\left(P\right)} + \frac{Cp\left(P\right)V^{2}\left(P\right)dPdV_{T}\left(P\right)}{2Cv^{2}\left(P\right)} + \frac{Cp\left(P\right)V^{2}\left(P\right)}{2Cv^{2}\left(P\right)} + \frac{Cp\left(P\right)V^{2}\left(P\right$$

**dspeed\_of\_sound\_dP\_T** [float] Pressure derivative of speed of sound at constant temperature, [m\*kg^0.5/s/mol^0.5/Pa]

# dspeed\_of\_sound\_dT\_P()

Method to calculate the temperature derivative of speed of sound at constant pressure in molar units.

$$\left(\frac{\partial c}{\partial T}\right)_{P} = -\frac{\sqrt{-\frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cv}\left(T\right)}}\left(-\frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{d}_{dT}\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cv}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} - \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{\operatorname{Cp}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}^{2}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right)}{2\,\operatorname{Cv}\left(T\right)} + \frac{\operatorname{Cp}\left(T\right)V^{2}\left(T\right)\,\mathrm{dPdV_{T}}\left(T\right$$

# Returns

**dspeed\_of\_sound\_dT\_P** [float] Temperature derivative of speed of sound at constant pressure, [m\*kg^0.5/s/mol^0.5/K]

# Notes

Requires the temperature derivative of Cp and Cv both at constant pressure, as well as the volume and temperature derivative of pressure, calculated at constant temperature and then pressure respectively. These can be tricky to obtain.

# property economic\_statuses

Status of each component in in relation to import and export from various regions, [-].

# Returns

**economic\_statuses** [list[dict]] Status of each component in in relation to import and export from various regions, [-].

# force\_phase = None

Attribute which can be set to a global Phase object to force the phases identification routines to label it a certain phase. Accepts values of ('g', 'l', 's').

# property formulas

Formulas of each component, [-].

# Returns

formulas [list[str]] Formulas of each component, [-].

# classmethod from\_json(json\_repr)

Method to create a phase from a JSON serialization of another phase.

# Parameters

json\_repr [dict] JSON-friendly representation, [-]

# Returns

phase [Phase] Newly created phase object from the json serialization, [-]

## **Notes**

It is important that the input string be in the same format as that created by Phase.as\_json.

# fugacities()

Method to calculate and return the fugacities of the phase.

$$f_i = P z_i \exp(\ln \phi_i)$$

Returns

fugacities [list[float]] Fugacities, [Pa]

# fugacities\_at\_zs(zs)

Method to directly calculate the figacities at a different composition than the current phase. This is implemented to allow for the possibility of more direct calls to obtain fugacities than is possible with the phase interface. This base method simply creates a new phase, gets its log fugacity coefficients, exponentiates them, and multiplies them by P and compositions.

Returns

fugacities [list[float]] Fugacities, [Pa]

# fugacities\_lowest\_Gibbs()

Method to calculate and return the fugacities of the phase.

$$f_i = P z_i \exp(\ln \phi_i)$$

Returns

fugacities [list[float]] Fugacities, [Pa]

# fugacity()

Method to calculate and return the fugacity of the phase; provided the phase is 1 component.

#### Returns

fugacity [list[float]] Fugacity, [Pa]

# gammas()

Method to calculate and return the activity coefficients of the phase, [-].

Activity coefficients are defined as the ratio of the actual fugacity coefficients times the pressure to the reference pure fugacity coefficients times the reference pressure. The reference pressure can be set to the actual pressure (the Lewis Randall standard state) which makes the pressures cancel.

$$\gamma_i(T, P, x; f_i^0(T, P_i^0)) = \frac{\phi_i(T, P, x)P}{\phi_i^0(T, P_i^0)P_i^0}$$

Returns

gammas [list[float]] Activity coefficients, [-]

# ideal\_gas\_basis = False

# is\_solid = False

## isentropic\_exponent()

Method to calculate and return the real gas isentropic exponent of the phase, which satisfies the relationship  $PV^k = \text{const.}$ 

$$k = -\frac{V}{P} \frac{C_p}{C_v} \left(\frac{\partial P}{\partial V}\right)_T$$

**k\_PV** [float] Isentropic exponent of a real fluid, [-]

# isentropic\_exponent\_PT()

Method to calculate and return the real gas is entropic exponent of the phase, which satisfies the relationship  $P^{(1-k)}T^k = \text{const.}$ 

$$k = \frac{1}{1 - \frac{P}{C_p} \left(\frac{\partial V}{\partial T}\right)_P}$$

Returns

k\_PT [float] Isentropic exponent of a real fluid, [-]

## isentropic\_exponent\_PV()

Method to calculate and return the real gas isentropic exponent of the phase, which satisfies the relationship  $PV^k = \text{const.}$ 

$$k = -\frac{V}{P} \frac{C_p}{C_v} \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

k\_PV [float] Isentropic exponent of a real fluid, [-]

# isentropic\_exponent\_TV()

Method to calculate and return the real gas isentropic exponent of the phase, which satisfies the relationship  $TV^{k-1} = \text{const.}$ 

$$k = 1 + \frac{V}{C_v} \left(\frac{\partial P}{\partial T}\right)_V$$

Returns

**k\_TV** [float] Isentropic exponent of a real fluid, [-]

# isobaric\_expansion()

Method to calculate and return the isobatic expansion coefficient of the phase.

$$\beta = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

Returns

beta [float] Isobaric coefficient of a thermal expansion, [1/K]

# isothermal\_bulk\_modulus()

Method to calculate and return the isothermal bulk modulus of the phase.

$$K_T = -V \left(\frac{\partial P}{\partial V}\right)_T$$

Returns

## isothermal\_compressibility()

Method to calculate and return the isothermal compressibility of the phase.

$$\kappa = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

Returns

kappa [float] Isothermal coefficient of compressibility, [1/Pa]

## kappa()

Method to calculate and return the isothermal compressibility of the phase.

$$\kappa = -\frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

Returns

kappa [float] Isothermal coefficient of compressibility, [1/Pa]

# property legal\_statuses

Status of each component in in relation to import and export rules from various regions, [-].

#### Returns

**legal\_statuses** [list[dict]] Status of each component in in relation to import and export rules from various regions, [-].

#### lnfugacities()

Method to calculate and return the log of fugacities of the phase.

$$\ln f_i = \ln \left( P z_i \exp(\ln \phi_i) \right) = \ln(P) + \ln(z_i) + \ln \phi_i$$

Returns

**Infugacities** [list[float]] Log fugacities, [log(Pa)]

# lnphi()

Method to calculate and return the log of fugacity coefficient of the phase; provided the phase is 1 component.

# Returns

**Inphi** [list[float]] Log fugacity coefficient, [-]

# lnphis()

Method to calculate and return the log of fugacity coefficients of each component in the phase.

# Returns

Inphis [list[float]] Log fugacity coefficients, [-]

# lnphis\_G\_min()

Method to calculate and return the log fugacity coefficients of the phase. If the phase can have multiple solutions at its T and P, this method should return those with the lowest Gibbs energy. This needs to be implemented on phases with that criteria like cubic EOSs.

#### Returns

**Inphis** [list[float]] Log fugacity coefficients, [-]

# lnphis\_at\_zs(zs)

Method to directly calculate the log fugacity coefficients at a different composition than the current phase. This is implemented to allow for the possibility of more direct calls to obtain fugacities than is possible with the phase interface. This base method simply creates a new phase, gets its log fugacity coefficients, and returns them.

#### Returns

Inphis [list[float]] Log fugacity coefficients, [-]

# property logPs

Octanol-water partition coefficients for each component, [-].

logPs [list[float]] Octanol-water partition coefficients for each component, [-].

# log\_zs()

Method to calculate and return the log of mole fractions specified. These are used in calculating entropy and in many other formulas.

 $\ln z_i$ 

# Returns

log\_zs [list[float]] Log of mole fractions, [-]

## model\_hash(ignore\_phase=False)

Method to compute a hash of a phase.

# Parameters

ignore\_phase [bool] Whether or not to include the specifc class of the model in the hash

#### Returns

**hash** [int] Hash representing the settings of the phase; phases with all identical model parameters should have the same hash.

# molar\_water\_content()

Method to calculate and return the molar water content; this is the g/mol of the fluid which is coming from water, [g/mol].

water content =  $MW_{H2O}w_{H2O}$ 

#### Returns

molar\_water\_content [float] Molar water content, [g/mol]

# property molecular\_diameters

Lennard-Jones molecular diameters for each component, [angstrom].

# Returns

**molecular\_diameters** [list[float]] Lennard-Jones molecular diameters for each component, [angstrom].

# mu()

## property names

Names for each component, [-].

# Returns

names [list[str]] Names for each component, [-].

# obj\_references = ()

Tuple of object instances which should be stored as json using their own as\_json method.

# property omegas

Acentric factors for each component, [-].

#### Returns

omegas [list[float]] Acentric factors for each component, [-].

# property phase\_STPs

Standard states ('g', 'l', or 's') for each component, [-].

```
phase_STPs [list[str]] Standard states ('g', 'l', or 's') for each component, [-].
```

# phi()

Method to calculate and return the fugacity coefficient of the phase; provided the phase is 1 component.

#### Returns

phi [list[float]] Fugacity coefficient, [-]

# phis()

Method to calculate and return the fugacity coefficients of the phase.

$$\phi_i = \exp(\ln \phi_i)$$

Returns

phis [list[float]] Fugacity coefficients, [-]

# pointer\_reference\_dicts = ()

Tuple of dictionaries for string -> object

# pointer\_references = ()

Tuple of attributes which should be stored by converting them to a string, and then they will be looked up in their corresponding *pointer\_reference\_dicts* entry.

## pseudo\_Pc()

Method to calculate and return the pseudocritical pressure calculated using Kay's rule (linear mole fractions):

$$P_{c,pseudo} = \sum_{i} z_i P_{c,i}$$

Returns

**pseudo\_Pc** [float] Pseudocritical pressure of the phase, [Pa]

# pseudo\_Tc()

Method to calculate and return the pseudocritical temperature calculated using Kay's rule (linear mole fractions):

$$T_{c,pseudo} = \sum_{i} z_i T_{c,i}$$

Returns

**pseudo\_Tc** [float] Pseudocritical temperature of the phase, [K]

## pseudo\_Vc()

Method to calculate and return the pseudocritical volume calculated using Kay's rule (linear mole fractions):

$$V_{c,pseudo} = \sum_{i} z_i V_{c,i}$$

Returns

pseudo\_Vc [float] Pseudocritical volume of the phase, [m^3/mol]

pseudo\_Zc()

Method to calculate and return the pseudocritical compressibility calculated using Kay's rule (linear mole fractions):

$$Z_{c,pseudo} = \sum_{i} z_i Z_{c,i}$$

pseudo\_Zc [float] Pseudocritical compressibility of the phase, [-]

# pure\_reference\_types = ()

Tuple of types of thermo.utils.TDependentProperty or thermo.utils.TPDependentProperty corresponding to *pure\_references*.

# pure\_references = ()

Tuple of attribute names which hold lists of thermo.utils.TDependentProperty or thermo.utils. TPDependentProperty instances.

# reference\_pointer\_dicts = ()

Tuple of dictionaries for object -> string

# rho()

Method to calculate and return the molar density of the phase.

 $\rho = frac1V$ 

Returns

rho [float] Molar density, [mol/m^3]

# rho\_mass()

Method to calculate and return mass density of the phase.

$$\rho = \frac{MW}{1000 \cdot VM}$$

#### Returns

**rho\_mass** [float] Mass density, [kg/m<sup>3</sup>]

# rho\_mass\_liquid\_ref()

Method to calculate and return the liquid reference mass density according to the temperature variable *T\_liquid\_volume\_ref* of *thermo.bulk.BulkSettings* and the composition of the phase.

## Returns

rho\_mass\_liquid\_ref [float] Liquid mass density at the reference condition, [kg/m^3]

# property rhocs

Molar densities at the critical point for each component, [mol/m^3].

#### Returns

rhocs [list[float]] Molar densities at the critical point for each component, [mol/m^3].

# property rhocs\_mass

Densities at the critical point for each component, [kg/m^3].

## Returns

rhocs\_mass [list[float]] Densities at the critical point for each component, [kg/m^3].

#### property rhog\_STPs

Molar gas densities at STP for each component; metastable if normally another state, [mol/m^3].

# Returns

**rhog\_STPs** [list[float]] Molar gas densities at STP for each component; metastable if normally another state, [mol/m<sup>3</sup>].

# property rhog\_STPs\_mass

Gas densities at STP for each component; metastable if normally another state, [kg/m^3].

**rhog\_STPs\_mass** [list[float]] Gas densities at STP for each component; metastable if normally another state, [kg/m^3].

## property rhol\_60Fs

Liquid molar densities for each component at 60 °F, [mol/m^3].

#### Returns

rhol\_60Fs [list[float]] Liquid molar densities for each component at 60 °F, [mol/m^3].

# property rhol\_60Fs\_mass

Liquid mass densities for each component at 60 °F, [kg/m^3].

Returns

rhol\_60Fs\_mass [list[float]] Liquid mass densities for each component at 60 °F, [kg/m^3].

# property rhol\_STPs

Molar liquid densities at STP for each component, [mol/m^3].

#### Returns

rhol\_STPs [list[float]] Molar liquid densities at STP for each component, [mol/m^3].

# property rhol\_STPs\_mass

Liquid densities at STP for each component, [kg/m^3].

Returns

rhol\_STPs\_mass [list[float]] Liquid densities at STP for each component, [kg/m^3].

# property rhos\_Tms

Solid molar densities for each component at their respective melting points, [mol/m^3].

#### Returns

**rhos\_Tms** [list[float]] Solid molar densities for each component at their respective melting points, [mol/m^3].

# property rhos\_Tms\_mass

Solid mass densities for each component at their melting point, [kg/m^3].

# Returns

**rhos\_Tms\_mass** [list[float]] Solid mass densities for each component at their melting point, [kg/m^3].

# scalar = True

# sigma()

Calculate and return the surface tension of the phase. For details of the implementation, see *SurfaceTensionMixture*.

This property is strictly the ideal-gas to liquid surface tension, not a true inter-phase property.

#### Returns

sigma [float] Surface tension, [N/m]

# property sigma\_STPs

Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].

Returns

**sigma\_STPs** [list[float]] Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].

# property sigma\_Tbs

Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].

#### Returns

**sigma\_Tbs** [list[float]] Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].

# property sigma\_Tms

Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].

#### Returns

**sigma\_Tms** [list[float]] Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].

# property similarity\_variables

Similarity variables for each component, [mol/g].

# Returns

similarity\_variables [list[float]] Similarity variables for each component, [mol/g].

# property smiless

SMILES identifiers for each component, [-].

## Returns

smiless [list[str]] SMILES identifiers for each component, [-].

# property solubility\_parameters

Solubility parameters for each component at 298.15 K, [Pa<sup>^0.5</sup>].

## Returns

**solubility\_parameters** [list[float]] Solubility parameters for each component at 298.15 K, [Pa^0.5].

# speed\_of\_sound()

Method to calculate and return the molar speed of sound of the phase.

$$w = \left[-V^2 \left(\frac{\partial P}{\partial V}\right)_T \frac{C_p}{C_v}\right]^{1/2}$$

A similar expression based on molar density is:

$$w = \left[ \left( \frac{\partial P}{\partial \rho} \right)_T \frac{C_p}{C_v} \right]^{1/2}$$

#### Returns

w [float] Speed of sound for a real gas, [m\*kg^0.5/(s\*mol^0.5)]

# speed\_of\_sound\_mass()

Method to calculate and return the speed of sound of the phase.

$$w = \left[-V^2 \frac{1000}{MW} \left(\frac{\partial P}{\partial V}\right)_T \frac{C_p}{C_v}\right]^{1/2}$$

Returns

w [float] Speed of sound for a real gas, [m/s]

## state\_hash()

Basic method to calculate a hash of the state of the phase and its model parameters.

Note that the hashes should only be compared on the same system running in the same process!

#### Returns

state\_hash [int] Hash of the object's model parameters and state, [-]

# to(zs, T=None, P=None, V=None)

Method to create a new Phase object with the same constants as the existing Phase but at different conditions. Mole fractions zs are always required and any two of T, P, and V are required.

## Parameters

zs [list[float]] Molar composition of the new phase, [-]

T [float, optional] Temperature of the new phase, [K]

**P** [float, optional] Pressure of the new phase, [Pa]

V [float, optional] Molar volume of the new phase, [m^3/mol]

# Returns

new\_phase [Phase] New phase at the specified conditions, [-]

## **Examples**

These sample cases illustrate the three combinations of inputs. Note that some thermodynamic models may have multiple solutions for some inputs!

```
>>> from thermo import IdealGas
>>> phase = IdealGas(T=300, P=1e5, zs=[.79, .21], HeatCapacityGases=[])
>>> phase.to(T=1e5, P=1e3, zs=[.5, .5])
IdealGas(HeatCapacityGases=[], T=100000.0, P=1000.0, zs=[0.5, 0.5])
>>> phase.to(V=1e-4, P=1e3, zs=[.1, .9])
IdealGas(HeatCapacityGases=[], T=0.012027235504, P=1000.0, zs=[0.1, 0.9])
>>> phase.to(T=1e5, V=1e12, zs=[.2, .8])
IdealGas(HeatCapacityGases=[], T=100000.0, P=8.31446261e-07, zs=[0.2, 0.8])
```

# $to_TP_zs(T, P, zs)$

Method to create a new Phase object with the same constants as the existing Phase but at a different T and P.

#### **Parameters**

zs [list[float]] Molar composition of the new phase, [-]

T [float] Temperature of the new phase, [K]

**P** [float] Pressure of the new phase, [Pa]

#### Returns

new\_phase [Phase] New phase at the specified conditions, [-]

## Notes

This method is marginally faster than Phase. to as it does not need to check what the inputs are.

# **Examples**

```
>>> from thermo import IdealGas
>>> phase = IdealGas(T=300, P=1e5, zs=[.79, .21], HeatCapacityGases=[])
>>> phase.to_TP_zs(T=1e5, P=1e3, zs=[.5, .5])
IdealGas(HeatCapacityGases=[], T=100000.0, P=1000.0, zs=[0.5, 0.5])
```

# value(name)

Method to retrieve a property from a string. This more or less wraps getattr.

name could be a python property like 'Tms' or a callable method like 'H'.

#### **Parameters**

name [str] String representing the property, [-]

#### Returns

value [various] Value specified, [various]

#### ws()

Method to calculate and return the mass fractions of the phase, [-]

#### Returns

ws [list[float]] Mass fractions, [-]

# ws\_no\_water()

Method to calculate and return the mass fractions of all species in the phase, normalized to a water-free basis (the mass fraction of water returned is zero).

## Returns

ws\_no\_water [list[float]] Mass fractions on a water free basis, [-]

# zs\_no\_water()

Method to calculate and return the mole fractions of all species in the phase, normalized to a water-free basis (the mole fraction of water returned is zero).

## Returns

zs\_no\_water [list[float]] Mole fractions on a water free basis, [-]

# 7.22.2 Ideal Gas Equation of State

class thermo.phases.IdealGas(HeatCapacityGases=None, Hfs=None, Gfs=None, T=None, P=None,

zs=None)

Bases: thermo.phases.phase.Phase

Class for representing an ideal gas as a phase object. All departure properties are zero.

$$P = \frac{RT}{V}$$

Parameters

- **HeatCapacityGases** [list[HeatCapacityGas]] Objects proiding pure-component heat capacity correlations, [-]
- Hfs [list[float]] Molar ideal-gas standard heats of formation at 298.15 K and 1 atm, [J/mol]
- **Gfs** [list[float]] Molar ideal-gas standard Gibbs energies of formation at 298.15 K and 1 atm, [J/mol]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- zs [list[float], optional] Mole fractions of each component, [-]

# **Examples**

T-P initialization for oxygen and nitrogen, using Poling's polynomial heat capacities:

```
>>> HeatCapacityGases = [HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*-9.9e-13, R*1.

→57e-09, R*7e-08, R*-0.000261, R*3.539])),

... HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*1.79e-12, R*-6e-

→09, R*6.58e-06, R*-0.001794, R*3.63]))]

>>> phase = IdealGas(T=300, P=1e5, zs=[.79, .21],

→HeatCapacityGases=HeatCapacityGases)

>>> phase.Cp()

29.1733530
```

Cp()	Method to calculate and return the molar heat capac-
	ity of the phase.
H()	Method to calculate and return the enthalpy of the
	phase.
<i>S</i> ()	Method to calculate and return the entropy of the
	phase.
d2H_dP2()	Method to calculate and return the second pressure
	derivative of molar enthalpy of the phase.
d2H_dT2()	Method to calculate and return the first temperature
	derivative of molar heat capacity of the phase.
d2P_dT2()	Method to calculate and return the second tempera-
	ture derivative of pressure of the phase.
d2P_dTdV()	Method to calculate and return the second derivative
	of pressure with respect to temperature and volume
	of the phase.
d2P_dV2()	Method to calculate and return the second volume
	derivative of pressure of the phase.
d2S_dP2()	Method to calculate and return the second pressure
	derivative of molar entropy of the phase.
dH_dP()	Method to calculate and return the first pressure
	derivative of molar enthalpy of the phase.
dH_dP_V()	Method to calculate and return the pressure derivative
	of molar enthalpy at constant volume of the phase.
	continues on next page

# Methods

	e 81 – continued from previous page
dH_dT_V()	Method to calculate and return the molar heat capac-
	ity of the phase.
dH_dV_P()	Method to calculate and return the volume derivative
	of molar enthalpy at constant pressure of the phase.
dH_dV_T()	Method to calculate and return the volume deriva-
	tive of molar enthalpy at constant temperature of the
	phase.
dP_dT()	Method to calculate and return the first temperature
	derivative of pressure of the phase.
dP_dV()	Method to calculate and return the first volume
	derivative of pressure of the phase.
dS_dP()	Method to calculate and return the first pressure
	derivative of molar entropy of the phase.
dS_dP_V()	Method to calculate and return the first pressure
	derivative of molar entropy at constant volume of the
	phase.
$dS_dT()$	Method to calculate and return the first temperature
	derivative of molar entropy of the phase.
$dS_dT_V()$	Method to calculate and return the first temperature
	derivative of molar entropy at constant volume of the
	phase.
dlnphis_dP()	Method to calculate and return the pressure derivative
	of the log of fugacity coefficients of each component
	in the phase.
dlnphis_dT()	Method to calculate and return the temperature
	derivative of the log of fugacity coefficients of each
	component in the phase.
dphis_dP()	Method to calculate and return the pressure deriva-
	tive of fugacity coefficients of each component in the
	phase.
dphis_dT()	Method to calculate and return the temperature
	derivative of fugacity coefficients of each component
	in the phase.
fugacities()	Method to calculate and return the fugacities of each
	component in the phase.
lnphis()	Method to calculate and return the log of fugacity co-
	efficients of each component in the phase.
phis()	Method to calculate and return the fugacity coeffi-
	cients of each component in the phase.

Table 81 – continued from previous page

# **Cp**()

Method to calculate and return the molar heat capacity of the phase.

$$C_p = \sum_i z_i C_{p,i}^{ig}$$

# Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

H()

Method to calculate and return the enthalpy of the phase.

$$H = \sum_{i} z_i H_i^{ig}$$

**H** [float] Molar enthalpy, [J/(mol)]

**S**()

Method to calculate and return the entropy of the phase.

$$S = \sum_{i} z_i S_i^{ig} - R \ln\left(\frac{P}{P_{ref}}\right) - R \sum_{i} z_i \ln(z_i)$$

Returns

**S** [float] Molar entropy, [J/(mol\*K)]

\_\_repr\_\_()

Method to create a string representation of the phase object, with the goal of making it easy to obtain standalone code which reproduces the current state of the phase. This is extremely helpful in creating new test cases.

#### Returns

**recreation** [str] String which is valid Python and recreates the current state of the object if ran, [-]

# **Examples**

```
>>> from thermo import HeatCapacityGas, IdealGas
>>> HeatCapacityGases = [HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*-9.9e-13,]
\rightarrow R^{*1.57e-09}, R^{*7e-08}, R^{*-0.000261}, R^{*3.539})),
                          HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*1.79e-12,]
. . .
→R*-6e-09, R*6.58e-06, R*-0.001794, R*3.63]))]
>>> phase = IdealGas(T=300, P=1e5, zs=[.79, .21],_
Generation HeatCapacityGases=HeatCapacityGases)
>>> phase
IdealGas(HeatCapacityGases=[HeatCapacityGas(extrapolation="linear", method=
↔ "POLY_FIT", poly_fit=(50.0, 1000.0, [-8.231317991971707e-12, 1.
→3053706310500586e-08, 5.820123832707268e-07, -0.0021700747433379955, 29.
→424883205644317])), HeatCapacityGas(extrapolation="linear", method="POLY_FIT",
→ poly_fit=(50.0, 1000.0, [1.48828880864943e-11, -4.9886775708919434e-08, 5.
→4709164027448316e-05, -0.014916145936966912, 30.18149930389626]))], T=300,
\rightarrow P=100000.0. zs=[0.79. 0.21])
```

## $d2H_dP2()$

Method to calculate and return the second pressure derivative of molar enthalpy of the phase.

$$\frac{\partial^2 H}{\partial P^2} = 0$$

Returns

**d2H\_dP2** [float] Second pressure derivative of molar enthalpy, [J/(mol\*Pa^2)]

d2H\_dT2()

Method to calculate and return the first temperature derivative of molar heat capacity of the phase.

$$\frac{\partial C_p}{\partial T} = \sum_i z_i \frac{\partial C_{p,i}^{ig}}{\partial T}$$

**d2H\_dT2** [float] Second temperature derivative of enthalpy, [J/(mol\*K^2)]

# d2P\_dT2()

Method to calculate and return the second temperature derivative of pressure of the phase.

$$\frac{\partial^2 P}{\partial T^2} = 0$$

## Returns

d2P\_dT2 [float] Second temperature derivative of pressure, [Pa/K^2]

# d2P\_dTdV()

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the phase.

$$\frac{\partial^2 P}{\partial V \partial T} = \frac{-P^2}{RT^2}$$

## Returns

d2P\_dTdV [float] Second volume derivative of pressure, [mol\*Pa^2/(J\*K)]

## $d2P_dV2()$

Method to calculate and return the second volume derivative of pressure of the phase.

$$\frac{\partial^2 P}{\partial V^2} = \frac{2P^3}{R^2T^2}$$

## Returns

d2P\_dV2 [float] Second volume derivative of pressure, [Pa\*mol^2/m^6]

## d2S\_dP2()

Method to calculate and return the second pressure derivative of molar entropy of the phase.

$$\frac{\partial^2 S}{\partial P^2} = \frac{R}{P^2}$$

#### Returns

d2S\_dP2 [float] Second pressure derivative of molar entropy, [J/(mol\*K\*Pa^2)]

## $dH_dP()$

Method to calculate and return the first pressure derivative of molar enthalpy of the phase.

$$\frac{\partial H}{\partial P} = 0$$

#### Returns

dH\_dP [float] First pressure derivative of molar enthalpy, [J/(mol\*Pa)]

 $dH_dP_V()$ 

Method to calculate and return the pressure derivative of molar enthalpy at constant volume of the phase.

$$\left(\frac{\partial H}{\partial P}\right)_V = C_p \left(\frac{\partial T}{\partial P}\right)_V$$

Returns

dH\_dP\_V [float] First pressure derivative of molar enthalpy at constant volume, [J/(mol\*Pa)]

# dH\_dT\_V()

Method to calculate and return the molar heat capacity of the phase.

$$C_p = \sum_i z_i C_{p,i}^{ig}$$

## Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

# $dH_dV_P()$

Method to calculate and return the volume derivative of molar enthalpy at constant pressure of the phase.

$$\left(\frac{\partial H}{\partial V}\right)_P = C_p \left(\frac{\partial T}{\partial V}\right)_P$$

# Returns

dH\_dV\_T [float] First pressure derivative of molar enthalpy at constant volume, [J/(m^3)]

# $dH_dV_T()$

Method to calculate and return the volume derivative of molar enthalpy at constant temperature of the phase.

$$\left(\frac{\partial H}{\partial V}\right)_T=0$$

Returns

 $dH_dV_T$  [float] First pressure derivative of molar enthalpy at constant volume, [J/(m^3)]

 $dP_dT()$ 

Method to calculate and return the first temperature derivative of pressure of the phase.

$$\frac{\partial P}{\partial T} = \frac{P}{T}$$

# Returns

dP\_dT [float] First temperature derivative of pressure, [Pa/K]

# $dP_dV()$

Method to calculate and return the first volume derivative of pressure of the phase.

$$\frac{\partial P}{\partial V} = \frac{-P^2}{RT}$$

#### Returns

dP\_dV [float] First volume derivative of pressure, [Pa\*mol/m^3]

 $dS_dP()$ 

Method to calculate and return the first pressure derivative of molar entropy of the phase.

$$\frac{\partial S}{\partial P} = -\frac{R}{P}$$

# Returns

dS\_dP [float] First pressure derivative of molar entropy, [J/(mol\*K\*Pa)]

 $dS_dP_V()$ 

Method to calculate and return the first pressure derivative of molar entropy at constant volume of the phase.

$$\left(\frac{\partial S}{\partial P}\right)_V = \frac{-R}{P} + \frac{C_p}{T}\frac{\partial T}{\partial P}$$

**dS\_dP\_V** [float] First pressure derivative of molar entropy at constant volume, [J/(mol\*K\*Pa)]

dS\_dT()

Method to calculate and return the first temperature derivative of molar entropy of the phase.

$$\frac{\partial S}{\partial T} = \frac{C_p}{T}$$

#### Returns

dS\_dT [float] First temperature derivative of molar entropy, [J/(mol\*K^2)]

#### $dS_dT_V()$

Method to calculate and return the first temperature derivative of molar entropy at constant volume of the phase.

$$\left(\frac{\partial S}{\partial T}\right)_V = \frac{C_p}{T} - \frac{R}{P}\frac{\partial P}{\partial T}$$

Returns

 $dS_dT_V$  [float] First temperature derivative of molar entropy at constant volume,  $[J/(mol^*K^2)]$ 

# dlnphis\_dP()

Method to calculate and return the pressure derivative of the log of fugacity coefficients of each component in the phase.

$$\frac{\partial \ln \phi_i}{\partial P} = 0$$

Returns

**dlnphis\_dP** [list[float]] Log fugacity coefficients, [1/Pa]

# dlnphis\_dT()

Method to calculate and return the temperature derivative of the log of fugacity coefficients of each component in the phase.

$$\frac{\partial \ln \phi_i}{\partial T} = 0$$

Returns

**dlnphis\_dT** [list[float]] Log fugacity coefficients, [1/K]

#### dphis\_dP()

Method to calculate and return the pressure derivative of fugacity coefficients of each component in the phase.

$$\frac{\partial \phi_i}{\partial P} = 0$$

#### Returns

dphis\_dP [list[float]] Pressure derivative of fugacity fugacity coefficients, [1/Pa]

#### dphis\_dT()

Method to calculate and return the temperature derivative of fugacity coefficients of each component in the phase.

$$\frac{\partial \phi_i}{\partial T} = 0$$

Returns

dphis\_dT [list[float]] Temperature derivative of fugacity fugacity coefficients, [1/K]

fugacities()

Method to calculate and return the fugacities of each component in the phase.

$$fugacitiy_i = z_i P$$

Returns

fugacities [list[float]] Fugacities, [Pa]

**Examples** 

#### lnphis()

Method to calculate and return the log of fugacity coefficients of each component in the phase.

 $\ln \phi_i = 0.0$ 

Returns

Inphis [list[float]] Log fugacity coefficients, [-]

phis()

Method to calculate and return the fugacity coefficients of each component in the phase.

 $\phi_i = 1$ 

Returns

phis [list[float]] Fugacity fugacity coefficients, [-]

## 7.22.3 Cubic Equations of State

#### **Gas Phases**

**class** thermo.phases.**CEOSGas**(*eos\_class*, *eos\_kwargs*, *HeatCapacityGases=None*, *Hfs=None*, *Gfs=None*, *Sfs=None*, *T=None*, *P=None*, *zs=None*)

Bases: thermo.phases.phase.Phase

Class for representing a cubic equation of state gas phase as a phase object. All departure properties are actually calculated by the code in *thermo.eos* and *thermo.eos\_mix*.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V^2 + \delta V + \epsilon}$$

**Parameters** 

eos\_class [thermo.eos\_mix.GCEOSMIX] EOS class, [-]

- eos\_kwargs [dict] Parameters to be passed to the created EOS, [-]
- **HeatCapacityGases** [list[HeatCapacityGas]] Objects proiding pure-component heat capacity correlations, [-]
- Hfs [list[float]] Molar ideal-gas standard heats of formation at 298.15 K and 1 atm, [J/mol]
- **Gfs** [list[float]] Molar ideal-gas standard Gibbs energies of formation at 298.15 K and 1 atm, [J/mol]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- zs [list[float], optional] Mole fractions of each component, [-]

## **Examples**

T-P initialization for oxygen and nitrogen with the PR EOS, using Poling's polynomial heat capacities:

>>> from thermo import HeatCapacityGas, PRMIX, CEOSGas >>> eos\_kwargs = dict(Tcs=[154.58, 126.2], Pcs=[5042945.25, 3394387.5], omegas=[0. ..021, 0.04], kijs=[[0.0, -0.0159], [-0.0159, 0.0]]) >>> HeatCapacityGases = [HeatCapacityGas(poly\_fit=(50.0, 1000.0, [R\*-9.9e-13, R\*1. ...57e-09, R\*7e-08, R\*-0.000261, R\*3.539])), ... HeatCapacityGas(poly\_fit=(50.0, 1000.0, [R\*1.79e-12, R\*-6e-.09, R\*6.58e-06, R\*-0.001794, R\*3.63]))] >>> phase = CEOSGas(eos\_class=PRMIX, eos\_kwargs=eos\_kwargs, T=300, P=1e5, zs=[.79, . ...21], HeatCapacityGases=HeatCapacityGases) >>> phase.Cp() 29.2285050

## Methods

<i>Cp(</i> )	Method to calculate and return the constant-pressure
	heat capacity of the phase.
Cv()	Method to calculate and return the constant-volume
	heat capacity $Cv$ of the phase.
H()	Method to calculate and return the enthalpy of the
	phase.
<i>S</i> ()	Method to calculate and return the entropy of the
	phase.
V_iter([force])	Method to calculate and return the volume of the
	phase in a way suitable for a TV resolution to con-
	verge on the same pressure.
d2P_dT2()	Method to calculate and return the second tempera-
	ture derivative of pressure of the phase.
d2P_dTdV()	Method to calculate and return the second derivative
	of pressure with respect to temperature and volume
	of the phase.
d2P_dV2()	Method to calculate and return the second volume
	derivative of pressure of the phase.
	continues on next page

continues on next page

Table 82 – continued from previous page	
$dP_dT()$	Method to calculate and return the first temperature
	derivative of pressure of the phase.
$dP_dV()$	Method to calculate and return the first volume
	derivative of pressure of the phase.
$dS_dT_V()$	Method to calculate and return the first temperature
	derivative of molar entropy at constant volume of the
	phase.
dlnphis_dP()	Method to calculate and return the first pressure
	derivative of the log of fugacity coefficients of each
	component in the phase.
dlnphis_dT()	Method to calculate and return the first temperature
	derivative of the log of fugacity coefficients of each
	component in the phase.
lnphis()	Method to calculate and return the log of fugacity co-
	efficients of each component in the phase.
to_TP_zs(T, P, zs[, other_eos])	Method to create a new Phase object with the same
	constants as the existing Phase but at a different $T$ and
	Р.

## Cp()

Method to calculate and return the constant-pressure heat capacity of the phase.

#### Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

**Cv**()

Method to calculate and return the constant-volume heat capacity Cv of the phase.

$$C_v = T \left(\frac{\partial P}{\partial T}\right)_V^2 / \left(\frac{\partial P}{\partial V}\right)_T + Cp$$

#### Returns

**Cv** [float] Constant volume molar heat capacity, [J/(mol\*K)]

H()

Method to calculate and return the enthalpy of the phase. The reference state for most subclasses is an ideal-gas enthalpy of zero at 298.15 K and 101325 Pa.

#### Returns

**H** [float] Molar enthalpy, [J/(mol)]

## **S**()

Method to calculate and return the entropy of the phase. The reference state for most subclasses is an ideal-gas entropy of zero at 298.15 K and 101325 Pa.

#### Returns

**S** [float] Molar entropy, [J/(mol\*K)]

## V\_iter(force=False)

Method to calculate and return the volume of the phase in a way suitable for a TV resolution to converge on the same pressure. This often means the return value of this method is an mpmath *mpf*. This dummy method simply returns the implemented V method.

#### Returns

V [float or mpf] Molar volume, [m^3/mol]

#### \_\_repr\_\_()

Method to create a string representation of the phase object, with the goal of making it easy to obtain standalone code which reproduces the current state of the phase. This is extremely helpful in creating new test cases.

#### Returns

**recreation** [str] String which is valid Python and recreates the current state of the object if ran, [-]

#### **Examples**

```
>>> from thermo import HeatCapacityGas, PRMIX, CEOSGas
>>> eos_kwargs = dict(Tcs=[154.58, 126.2], Pcs=[5042945.25, 3394387.5],.
→omegas=[0.021, 0.04], kijs=[[0.0, -0.0159], [-0.0159, 0.0]])
>>> HeatCapacityGases = [HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*-9.9e-13,]
\rightarrow R^{*1.57e-09}, R^{*7e-08}, R^{*-0.000261}, R^{*3.539})),
                         HeatCapacityGas(poly_fit=(50.0, 1000.0, [R*1.79e-12,
. . .
⇔R*-6e-09, R*6.58e-06, R*-0.001794, R*3.63]))]
>>> phase = CEOSGas(eos_class=PRMIX, eos_kwargs=eos_kwargs, T=300, P=1e5, zs=[.
→79, .21], HeatCapacityGases=HeatCapacityGases)
>>> phase
CEOSGas(eos_class=PRMIX, eos_kwargs={"Tcs": [154.58, 126.2], "Pcs": [5042945.25,
→ 3394387.5], "omegas": [0.021, 0.04], "kijs": [[0.0, -0.0159], [-0.0159, 0.
→0]]}, HeatCapacityGases=[HeatCapacityGas(extrapolation="linear", method="POLY_
→FIT", poly_fit=(50.0, 1000.0, [-8.231317991971707e-12, 1.3053706310500586e-08,
\rightarrow 5.820123832707268e-07, -0.0021700747433379955, 29.424883205644317])),
→HeatCapacityGas(extrapolation="linear", method="POLY_FIT", poly_fit=(50.0,_
→1000.0, [1.48828880864943e-11, -4.9886775708919434e-08, 5.4709164027448316e-
→05, -0.014916145936966912, 30.18149930389626]))], T=300, P=100000.0, zs=[0.79,
→ 0.21])
```

#### d2P\_dT2()

Method to calculate and return the second temperature derivative of pressure of the phase.

$$\left(\frac{\partial^2 P}{\partial T^2}\right)_V = -\frac{a\frac{d^2\alpha(T)}{dT^2}}{V^2 + V\delta + \epsilon}$$

Returns

**d2P\_dT2** [float] Second temperature derivative of pressure, [Pa/K^2]

#### d2P\_dTdV()

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the phase.

$$\left(\frac{\partial^2 P}{\partial T \partial V}\right) = -\frac{R}{\left(V-b\right)^2} + \frac{a\left(2V+\delta\right)\frac{d\alpha(T)}{dT}}{\left(V^2+V\delta+\epsilon\right)^2}$$

Returns

**d2P\_dTdV** [float] Second volume derivative of pressure, [mol\*Pa^2/(J\*K)]

d2P\_dV2()

Method to calculate and return the second volume derivative of pressure of the phase.

$$\left(\frac{\partial^2 P}{\partial V^2}\right)_T = 2\left(\frac{RT}{\left(V-b\right)^3} - \frac{a\left(2V+\delta\right)^2\alpha(T)}{\left(V^2+V\delta+\epsilon\right)^3} + \frac{a\alpha(T)}{\left(V^2+V\delta+\epsilon\right)^2}\right)_T$$

Returns

d2P\_dV2 [float] Second volume derivative of pressure, [Pa\*mol^2/m^6]

 $dP_dT()$ 

Method to calculate and return the first temperature derivative of pressure of the phase.

$$\left(\frac{\partial P}{\partial T}\right)_V = \frac{R}{V-b} - \frac{a\frac{d\alpha(T)}{dT}}{V^2 + V\delta + \epsilon}$$

Returns

**dP\_dT** [float] First temperature derivative of pressure, [Pa/K]

 $dP_dV()$ 

Method to calculate and return the first volume derivative of pressure of the phase.

$$\left(\frac{\partial P}{\partial V}\right)_{T} = -\frac{RT}{\left(V-b\right)^{2}} - \frac{a\left(-2V-\delta\right)\alpha(T)}{\left(V^{2}+V\delta+\epsilon\right)^{2}}$$

Returns

dP\_dV [float] First volume derivative of pressure, [Pa\*mol/m^3]

## dS\_dT\_V()

Method to calculate and return the first temperature derivative of molar entropy at constant volume of the phase.

$$\left(\frac{\partial S}{\partial T}\right)_{V} = \frac{C_{p}^{ig}}{T} - \frac{R}{P}\frac{\partial P}{\partial T} + \left(\frac{\partial S_{dep}}{\partial T}\right)_{V}$$

#### Returns

 $dS_dT_V$  [float] First temperature derivative of molar entropy at constant volume, [J/(mol\*K^2)]

#### dlnphis\_dP()

Method to calculate and return the first pressure derivative of the log of fugacity coefficients of each component in the phase. The calculation is performed by *thermo.eos\_mix.GCEOSMIX.dlnphis\_dP* or a simpler formula in the case of most specific models.

#### Returns

dlnphis\_dP [list[float]] First pressure derivative of log fugacity coefficients, [1/Pa]

#### dlnphis\_dT()

Method to calculate and return the first temperature derivative of the log of fugacity coefficients of each component in the phase. The calculation is performed by *thermo.eos\_mix.GCEOSMIX.dlnphis\_dT* or a simpler formula in the case of most specific models.

#### Returns

dlnphis\_dT [list[float]] First temperature derivative of log fugacity coefficients, [1/K]

## lnphis()

Method to calculate and return the log of fugacity coefficients of each component in the phase. The calculation is performed by *thermo.eos\_mix.GCEOSMIX.fugacity\_coefficients* or a simpler formula in the case of most specific models.

#### Returns

Inphis [list[float]] Log fugacity coefficients, [-]

#### to\_TP\_zs(T, P, zs, other\_eos=None)

Method to create a new Phase object with the same constants as the existing Phase but at a different T and P. This method has a special parameter *other\_eos*.

This is added to allow a gas-type phase to be created from a liquid-type phase at the same conditions (and vice-versa), as *GCEOSMIX* objects were designed to have vapor and liquid properties in the same phase. This argument is mostly for internal use.

### **Parameters**

- zs [list[float]] Molar composition of the new phase, [-]
- T [float] Temperature of the new phase, [K]
- **P** [float] Pressure of the new phase, [Pa]
- **other\_eos** [obj:*GCEOSMIX < thermo.eos\_mix.GCEOSMIX >* object] Other equation of state object at the same conditions, [-]

#### Returns

new\_phase [Phase] New phase at the specified conditions, [-]

#### Notes

This method is marginally faster than Phase. to as it does not need to check what the inputs are.

## **Examples**

```
>>> from thermo.eos_mix import PRMIX
>>> eos_kwargs = dict(Tcs=[305.32, 369.83], Pcs=[4872000.0, 4248000.0],_
...omegas=[0.098, 0.152])
>>> gas = CEOSGas(PRMIX, T=300.0, P=1e6, zs=[.2, .8], eos_kwargs=eos_kwargs)
>>> liquid = CEOSLiquid(PRMIX, T=500.0, P=1e7, zs=[.3, .7], eos_kwargs=eos_
...kwargs)
>>> new_liq = liquid.to_TP_zs(T=gas.T, P=gas.P, zs=gas.zs, other_eos=gas.eos_
...mix)
>>> new_liq
CEOSLiquid(eos_class=PRMIX, eos_kwargs={"Tcs": [305.32, 369.83], "Pcs":_
...[4872000.0, 4248000.0], "omegas": [0.098, 0.152]}, HeatCapacityGases=[],_
...[4T=300.0, P=1000000.0, zs=[0.2, 0.8])
>>> new_liq.eos_mix is gas.eos_mix
True
```

## **Liquid Phases**

```
class thermo.phases.CEOSLiquid(eos_class, eos_kwargs, HeatCapacityGases=None, Hfs=None, Gfs=None, Sfs=None, T=None, P=None, zs=None)
```

Bases: thermo.phases.phase.Phase

Class for representing a cubic equation of state gas phase as a phase object. All departure properties are actually calculated by the code in *thermo.eos* and *thermo.eos\_mix*.

$$P = \frac{RT}{V-b} - \frac{a\alpha(T)}{V^2 + \delta V + \epsilon}$$

#### Parameters

eos\_class [thermo.eos\_mix.GCEOSMIX] EOS class, [-]

- eos\_kwargs [dict] Parameters to be passed to the created EOS, [-]
- **HeatCapacityGases** [list[HeatCapacityGas]] Objects proiding pure-component heat capacity correlations, [-]
- Hfs [list[float]] Molar ideal-gas standard heats of formation at 298.15 K and 1 atm, [J/mol]
- **Gfs** [list[float]] Molar ideal-gas standard Gibbs energies of formation at 298.15 K and 1 atm, [J/mol]
- T [float, optional] Temperature, [K]
- P [float, optional] Pressure, [Pa]
- zs [list[float], optional] Mole fractions of each component, [-]

## **Examples**

T-P initialization for oxygen and nitrogen with the PR EOS, using Poling's polynomial heat capacities:

## 7.22.4 Activity Based Liquids

class thermo.phases.GibbsExcessLiquid(VaporPressures, VolumeLiquids=None, HeatCapacityGases=None, GibbsExcessModel=None, eos\_pure\_instances=None, EnthalpyVaporizations=None, HeatCapacityLiquids=None, VolumeSupercriticalLiquids=None, use\_Hvap\_caloric=False, use\_Poynting=False, use\_phis\_sat=False, use\_Tait=False, use\_eos\_volume=False, Hfs=None, Gfs=None, Sfs=None, henry\_components=None, henry\_data=None, T=None, P=None, zs=None, Psat\_extrpolation='AB', equilibrium\_basis=None, caloric\_basis=None)

Bases: thermo.phases.phase.Phase

Phase based on combining Raoult's law with a *GibbsExcess* model, optionally including saturation fugacity coefficient corrections (if the vapor phase is a cubic equation of state) and Poynting correction factors (if more accuracy is desired).

The equilibrium equation options (controlled by *equilibrium\_basis*) are as follows:

- 'Psat':  $\phi_i = \frac{\gamma_i P_i^{sat}}{P}$
- 'Poynting&PhiSat':  $\phi_i = \frac{\gamma_i P_i^{sat} \phi_i^{sat} Poynting_i}{P}$

- 'Poynting':  $\phi_i = \frac{\gamma_i P_i^{sat} \text{Poynting}_i}{P}$
- 'PhiSat':  $\phi_i = \frac{\gamma_i P_i^{sat} \phi_i^{sat}}{P}$

In all cases, the activity coefficient is derived from the *GibbsExcess* model specified as input; use the *IdealSolution* class as an input to set the activity coefficients to one.

The enthalpy *H* and entropy *S* (and other caloric properties *U*, *G*, *A*) equation options are similar to the equilibrium ones. If the same option is selected for *equilibrium\_basis* and *caloric\_basis*, the phase will be *thermodynamically consistent*. This is recommended for many reasons. The full 'Poynting&PhiSat' equations for *H* and *S* are as follows; see *GibbsExcessLiquid*.*H* and *GibbsExcessLiquid*.*S* for all of the other equations:

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -RT^{2} \left( \frac{\frac{\partial \phi_{\text{sat},i}}{\partial T}}{\phi_{\text{sat},i}} + \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + \frac{\frac{P_{\text{oynting}}}{\partial T}}{P_{\text{oynting}}} \right) + \int_{T,ref}^{T} C_{p,ig} dT \right]$$

$$S = S_{\text{excess}} - R \sum_{i} z_{i} \ln z_{i} - R \ln \left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( T \frac{\frac{\partial \phi_{\text{sat},i}}{\partial T}}{\phi_{\text{sat},i}} + T \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + T \frac{\frac{P_{\text{oynting}}}{\partial T}}{P_{\text{oynting}}} + \ln(P_{\text{sat},i}) + \ln \left(\frac{P_{\text{oynting}} \cdot \phi_{\text{sat},i}}{P_{\text{sat},i}} + \frac{P_{\text{sat},i}}{P_{\text{sat},i}} + \frac{P_{\text{sat},i}}{P_{\text{sa$$

An additional caloric mode is *Hvap*, which uses enthalpy of vaporization; this mode can never be thermodynamically consistent, but is still widely used.

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -H_{vap,i} + \int_{T,ref}^{T} C_{p,ig} dT \right]$$
$$S = S_{\text{excess}} - R \sum_{i} z_{i} \ln z_{i} - R \ln \left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( \ln P_{\text{sat},i} + \ln \left(\frac{1}{P}\right) \right) + \frac{H_{vap,i}}{T} - \int_{T,ref}^{T} \frac{C_{p,ig,i}}{T} dT \right]$$

**Warning:** Note that above the critical point, there is no definition for what vapor pressure is. The vapor pressure also tends to reach zero at temperatures in the 4-20 K range. These aspects mean extrapolation in the supercritical and very low temperature region is critical to ensure the equations will still converge. Extrapolation can be performed using either the equation  $P^{\text{sat}} = \exp\left(A - \frac{B}{T}\right)$  or  $P^{\text{sat}} = \exp\left(A + \frac{B}{T} + C \cdot \ln T\right)$  by setting *Psat\_extrpolation* to either 'AB' or 'ABC' respectively. The extremely low temperature region's issue is solved by calculating the logarithm of vapor pressures instead of the actual value. While floating point values in Python (doubles) can reach a minimum value of around 1e-308, if only the logarithm of that number is computed no issues arise. Both of these features only work when the vapor pressure correlations are polynomials.

**Warning:** When using 'PhiSat' as an option, note that the factor cannot be calculated when a compound is supercritical, as there is no longer any vapor-liquid pure-component equilibrium (by definition).

## Parameters

- **VaporPressures** [list[thermo.vapor\_pressure.VaporPressure]] Objects holding vapor pressure data and methods, [-]
- **VolumeLiquids** [list[*thermo.volume.VolumeLiquid*], optional] Objects holding liquid volume data and methods; required for Poynting factors and volumetric properties, [-]
- **HeatCapacityGases** [list[*thermo.heat\_capacity.HeatCapacityGas*], optional] Objects proiding pure-component heat capacity correlations; required for caloric properties, [-]
- **GibbsExcessModel** [*GibbsExcess*, optional] Configured instance for calculating activity coefficients and excess properties; set to *IdealSolution* if not provided, [-]

- eos\_pure\_instances [list[thermo.eos.GCEOS], optional] Cubic equation of state object instances for each pure component, [-]
- **EnthalpyVaporizations** [list[thermo.phase\_change.EnthalpyVaporization], optional] Objects holding enthalpy of vaporization data and methods; used only with the 'Hvap' optional, [-]
- **HeatCapacityLiquids** [list[thermo.heat\_capacity.HeatCapacityLiquid], optional]Objects holding liquid heat capacity data and methods; not used at present, [-]
- **VolumeSupercriticalLiquids** [list[*thermo.volume.VolumeLiquid*], optional] Objects holding liquid volume data and methods but that are used for supercritical temperatures on a per-component basis only; required for Poynting factors and volumetric properties at supercritical conditions; *VolumeLiquids* is used if not provided, [-]
- **Hfs** [list[float], optional] Molar ideal-gas standard heats of formation at 298.15 K and 1 atm, [J/mol]
- **Gfs** [list[float], optional] Molar ideal-gas standard Gibbs energies of formation at 298.15 K and 1 atm, [J/mol]
- T [float, optional] Temperature, [K]
- **P** [float, optional] Pressure, [Pa]
- zs [list[float], optional] Mole fractions of each component, [-]
- equilibrium\_basis [str, optional] Which set of equilibrium equations to use when calculating fugacities and related properties; valid options are 'Psat', 'Poynting&PhiSat', 'Poynting', 'PhiSat', [-]
- **caloric\_basis** [str, optional] Which set of caloric equations to use when calculating fugacities and related properties; valid options are 'Psat', 'Poynting&PhiSat', 'Poynting', 'PhiSat', 'Hvap' [-]
- **Psat\_extrpolation** [str, optional] One of 'AB' or 'ABC'; configures extrapolation for vapor pressure, [-]
- **use\_Hvap\_caloric** [bool, optional] If True, enthalpy and entropy will be calculated using idealgas heat capacity and the heat of vaporization of the fluid only. This forces enthalpy to be pressure-independent. This supersedes other options which would otherwise impact these properties. The molar volume of the fluid has no impact on enthalpy or entropy if this option is True. This option is not thermodynamically consistent, but is still often an assumption that is made.

#### Methods

<i>Cp(</i> )	Method to calculate and return the constant-pressure
	heat capacity of the phase.
H()	Method to calculate the enthalpy of the
	GibbsExcessLiquid phase.
Poyntings()	Method to calculate and return the Poynting pressure
	correction factors of the phase, [-].
S()	Method to calculate the entropy of the
	GibbsExcessLiquid phase.
gammas()	Method to calculate and return the activity coeffi-
	cients of the phase, [-].

continues on next page

Table 83 – continued from previous page	
phis_sat()	Method to calculate and return the saturation fugacity
	coefficient correction factors of the phase, [-].

## **Cp**()

Method to calculate and return the constant-pressure heat capacity of the phase.

## Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

## **H**()

Method to calculate the enthalpy of the *GibbsExcessLiquid* phase. Depending on the settings of the phase, this can include the effects of activity coefficients *gammas*, pressure correction terms *Poyntings*, and pure component saturation fugacities *phis\_sat* as well as the pure component vapor pressures.

When caloric\_basis is 'Poynting&PhiSat':

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -RT^{2} \left( \frac{\frac{\partial \phi_{\text{sat},i}}{\partial T}}{\phi_{\text{sat},i}} + \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + \frac{\frac{P_{\text{oynting}}}{\partial T}}{P_{\text{oynting}}} \right) + \int_{T,ref}^{T} C_{p,ig} dT \right]$$

When *caloric\_basis* is 'PhiSat':

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -RT^{2} \left( \frac{\frac{\partial \phi_{\text{sat},i}}{\partial T}}{\phi_{\text{sat},i}} + \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} \right) + \int_{T,ref}^{T} C_{p,ig} dT \right]$$

When *caloric\_basis* is 'Poynting':

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -RT^{2} \left( + \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + \frac{\frac{\text{Poynting}}{\partial T}}{\text{Poynting}} \right) + \int_{T,ref}^{T} C_{p,ig} dT \right]$$

When *caloric\_basis* is 'Psat':

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -RT^{2} \left( + \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} \right) + \int_{T,ref}^{T} C_{p,ig} dT \right]$$

When *caloric\_basis* is 'Hvap':

$$H = H_{\text{excess}} + \sum_{i} z_{i} \left[ -H_{vap,i} + \int_{T,ref}^{T} C_{p,ig} dT \right]$$

Returns

H [float] Enthalpy of the phase, [J/(mol)]

#### Poyntings()

Method to calculate and return the Poynting pressure correction factors of the phase, [-].

$$\operatorname{Poynting}_{i} = \exp\left(\frac{V_{m,i}(P - P_{sat})}{RT}\right)$$

Returns

**Poyntings** [list[float]] Poynting pressure correction factors, [-]

#### Notes

The above formula is correct for pressure-independent molar volumes. When the volume does depend on pressure, the full expression is:

Poynting = exp 
$$\left[ \frac{\int_{P_i^{sat}}^{P} V_i^l dP}{RT} \right]$$

When a specified model e.g. the Tait equation is used, an analytical integral of this term is normally available.

**S**()

Method to calculate the entropy of the *GibbsExcessLiquid* phase. Depending on the settings of the phase, this can include the effects of activity coefficients *gammas*, pressure correction terms *Poyntings*, and pure component saturation fugacities *phis\_sat* as well as the pure component vapor pressures.

When caloric\_basis is 'Poynting&PhiSat':

$$S = S_{\text{excess}} - R \sum_{i} z_{i} \ln z_{i} - R \ln \left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( T \frac{\frac{\partial \phi_{\text{sat},i}}{\partial T}}{\phi_{\text{sat},i}} + T \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + T \frac{\frac{P \text{oynting}}{\partial T}}{P \text{oynting}} + \ln(P_{\text{sat},i}) + \ln \left(\frac{P \text{oynting}}{P} + \ln(P_{\text{sat},i}) + \ln$$

When *caloric\_basis* is 'PhiSat':

$$S = S_{\text{excess}} - R \sum_{i} z_{i} \ln z_{i} - R \ln \left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( T \frac{\frac{\partial \phi_{\text{sat},i}}{\partial T}}{\phi_{\text{sat},i}} + T \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + \ln(P_{\text{sat},i}) + \ln \left(\frac{\phi_{\text{sat},i}}{P}\right) \right) - \int_{T,ref}^{T} \frac{C_{p,ig}}{T} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \left[ \frac{P_{\text{sat},i}}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \right] \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}} + \frac{1}{P_{\text{sat},i}} \frac{1}{P_{\text{sat},i}}$$

When *caloric\_basis* is 'Poynting':

$$S = S_{\text{excess}} - R \sum_{i} z_{i} \ln z_{i} - R \ln \left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( T \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + T \frac{\frac{P_{\text{oynting}}}{\partial T}}{P_{\text{oynting}}} + \ln(P_{\text{sat},i}) + \ln \left(\frac{P_{\text{oynting}}}{P}\right) \right) - \int_{T,ref}^{T} \frac{P_{\text{sat},i}}{P_{\text{sat},i}} + \frac{P_{\text{sat$$

When *caloric\_basis* is 'Psat':

$$S = S_{\text{excess}} - R\sum_{i} z_{i} \ln z_{i} - R \ln\left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( T \frac{\frac{\partial P_{\text{sat},i}}{\partial T}}{P_{\text{sat},i}} + \ln(P_{\text{sat},i}) + \ln\left(\frac{1}{P}\right) \right) - \int_{T,ref}^{T} \frac{C_{p,ig,i}}{T} dT \right]$$

When *caloric\_basis* is 'Hvap':

$$S = S_{\text{excess}} - R \sum_{i} z_{i} \ln z_{i} - R \ln \left(\frac{P}{P_{ref}}\right) - \sum_{i} z_{i} \left[ R \left( \ln P_{\text{sat},i} + \ln \left(\frac{1}{P}\right) \right) + \frac{H_{vap,i}}{T} - \int_{T,ref}^{T} \frac{C_{p,ig,i}}{T} dT \right]$$

Returns

**S** [float] Entropy of the phase, [J/(mol\*K)]

gammas()

Method to calculate and return the activity coefficients of the phase, [-]. This is a direct call to *GibbsExcess.gammas*.

#### Returns

gammas [list[float]] Activity coefficients, [-]

#### phis\_sat()

Method to calculate and return the saturation fugacity coefficient correction factors of the phase, [-].

These are calculated from the provided pure-component equations of state. This term should only be used with a consistent vapor-phase cubic equation of state.

#### Returns

phis\_sat [list[float]] Saturation fugacity coefficient correction factors, [-]

## Notes

**Warning:** This factor cannot be calculated when a compound is supercritical, as there is no longer any vapor-liquid pure-component equilibrium (by definition).

## 7.22.5 Fundamental Equations of State

HelmholtzEOS is the base class for all Helmholtz energy fundamental equations of state.

## class thermo.phases.HelmholtzEOS

Bases: thermo.phases.phase.Phase

## **Methods**

<i>Cp</i> ()	Method to calculate and return the constant-pressure
	heat capacity of the phase.
Cv()	Method to calculate and return the constant-volume
	heat capacity Cv of the phase.
H()	Method to calculate and return the enthalpy of the
	phase.
S()	Method to calculate and return the entropy of the
	phase.
V_iter([force])	Method to calculate and return the volume of the
	phase in a way suitable for a TV resolution to con-
	verge on the same pressure.
d2P_dT2()	Method to calculate and return the second tempera-
	ture derivative of pressure of the phase.
d2P_dTdV()	Method to calculate and return the second derivative
	of pressure with respect to temperature and volume
	of the phase.
d2P_dV2()	Method to calculate and return the second volume
	derivative of pressure of the phase.
dH_dP()	Method to calculate and return the pressure derivative
	of enthalpy of the phase at constant pressure.
$dP_dT()$	Method to calculate and return the first temperature
	derivative of pressure of the phase.
dP_dV()	Method to calculate and return the first volume
	derivative of pressure of the phase.
dS_dP()	Method to calculate and return the pressure derivative
	of entropy of the phase at constant pressure.
lnphis()	Method to calculate and return the log of fugacity co-
	efficients of each component in the phase.
to_ <i>TP_zs</i> (T, P, zs)	Method to create a new Phase object with the same
	constants as the existing Phase but at a different $T$ and
	Р.

## **Cp**()

Method to calculate and return the constant-pressure heat capacity of the phase.

Returns

**Cp** [float] Molar heat capacity, [J/(mol\*K)]

**Cv**()

Method to calculate and return the constant-volume heat capacity Cv of the phase.

$$C_v = T \left(\frac{\partial P}{\partial T}\right)_V^2 / \left(\frac{\partial P}{\partial V}\right)_T + Cp$$

#### Returns

**Cv** [float] Constant volume molar heat capacity, [J/(mol\*K)]

H()

Method to calculate and return the enthalpy of the phase. The reference state for most subclasses is an ideal-gas enthalpy of zero at 298.15 K and 101325 Pa.

#### Returns

**H** [float] Molar enthalpy, [J/(mol)]

## **S**()

Method to calculate and return the entropy of the phase. The reference state for most subclasses is an ideal-gas entropy of zero at 298.15 K and 101325 Pa.

#### Returns

**S** [float] Molar entropy, [J/(mol\*K)]

#### V\_iter(force=False)

Method to calculate and return the volume of the phase in a way suitable for a TV resolution to converge on the same pressure. This often means the return value of this method is an mpmath *mpf*. This dummy method simply returns the implemented V method.

## Returns

V [float or mpf] Molar volume, [m^3/mol]

## \_\_repr\_\_()

Method to create a string representation of the phase object, with the goal of making it easy to obtain standalone code which reproduces the current state of the phase. This is extremely helpful in creating new test cases.

#### Returns

**recreation** [str] String which is valid Python and recreates the current state of the object if ran, [-]

## **Examples**

```
>>> from thermo import IAPWS95Gas
>>> phase = IAPWS95Gas(T=300, P=1e5, zs=[1])
>>> phase
IAPWS95Gas(T=300, P=100000.0, zs=[1.0])
```

## d2P\_dT2()

Method to calculate and return the second temperature derivative of pressure of the phase.

#### Returns

d2P\_dT2 [float] Second temperature derivative of pressure, [Pa/K^2]

#### d2P\_dTdV()

Method to calculate and return the second derivative of pressure with respect to temperature and volume of the phase.

## Returns

d2P\_dTdV [float] Second volume derivative of pressure, [mol\*Pa^2/(J\*K)]

## $d2P_dV2()$

Method to calculate and return the second volume derivative of pressure of the phase.

Returns

d2P\_dV2 [float] Second volume derivative of pressure, [Pa\*mol^2/m^6]

#### $dH_dP()$

Method to calculate and return the pressure derivative of enthalpy of the phase at constant pressure.

#### Returns

**dH\_dP\_T** [float] Pressure derivative of enthalpy, [J/(mol\*Pa)]

## $dP_dT()$

Method to calculate and return the first temperature derivative of pressure of the phase.

Returns

dP\_dT [float] First temperature derivative of pressure, [Pa/K]

#### $dP_dV()$

Method to calculate and return the first volume derivative of pressure of the phase.

#### Returns

**dP\_dV** [float] First volume derivative of pressure, [Pa\*mol/m^3]

### $dS_dP()$

Method to calculate and return the pressure derivative of entropy of the phase at constant pressure.

#### Returns

dS\_dP\_T [float] Pressure derivative of entropy, [J/(mol\*K\*Pa)]

#### lnphis()

Method to calculate and return the log of fugacity coefficients of each component in the phase.

#### Returns

Inphis [list[float]] Log fugacity coefficients, [-]

## $to_TP_zs(T, P, zs)$

Method to create a new Phase object with the same constants as the existing Phase but at a different T and P.

## Parameters

zs [list[float]] Molar composition of the new phase, [-]

T [float] Temperature of the new phase, [K]

**P** [float] Pressure of the new phase, [Pa]

#### Returns

new\_phase [Phase] New phase at the specified conditions, [-]

## Notes

This method is marginally faster than Phase. to as it does not need to check what the inputs are.

## **Examples**

```
>>> from thermo import IdealGas
>>> phase = IdealGas(T=300, P=1e5, zs=[.79, .21], HeatCapacityGases=[])
>>> phase.to_TP_zs(T=1e5, P=1e3, zs=[.5, .5])
IdealGas(HeatCapacityGases=[], T=100000.0, P=1000.0, zs=[0.5, 0.5])
```

*IAPWS95* is the base class for the IAPWS-95 formulation for water; *IAPWS95Gas* and *IAPWS95Liquid* are the gas and liquid sub-phases respectively.

class thermo.phases.IAPWS95(T=None, P=None, zs=None)
Bases: thermo.phases.helmholtz\_eos.HelmholtzEOS

## Methods

k()	Calculate and return the thermal conductivity of wa-
	ter according to the IAPWS.
mu()	Calculate and return the viscosity of water according
	to the IAPWS.

**k**()

Calculate and return the thermal conductivity of water according to the IAPWS. For details, see chemicals.thermal\_conductivity.k\_IAPWS.

#### Returns

**k** [float] Thermal conductivity of water, [W/m/K]

#### mu()

Calculate and return the viscosity of water according to the IAPWS. For details, see chemicals. viscosity.mu\_IAPWS.

## Returns

**mu** [float] Viscosity of water, [Pa\*s]

- class thermo.phases.IAPWS95Gas(T=None, P=None, zs=None)
  Bases: thermo.phases.iapws\_phase.IAPWS95
- class thermo.phases.IAPWS95Liquid(T=None, P=None, zs=None)
  Bases: thermo.phases.iapws\_phase.IAPWS95

DryAirLemmon is an implementation of thermophysical properties of air by Lemmon (2000).

class thermo.phases.DryAirLemmon(T=None, P=None, zs=None)
Bases: thermo.phases.helmholtz\_eos.HelmholtzEOS

## Methods

<b>k</b> ()	Calculate and return the thermal conductivity of
	air according to Lemmon and Jacobsen (2004) For
	details, see chemicals.thermal_conductivity.
	k_air_lemmon.
mu()	Calculate and return the viscosity of air according to
	the Lemmon and Jacobsen (2003).

## **k**()

Calculate and return the thermal conductivity of air according to Lemmon and Jacobsen (2004) For details, see chemicals.thermal\_conductivity.k\_air\_lemmon.

## Returns

**k** [float] Thermal conductivity of air, [W/m/K]

## mu()

Calculate and return the viscosity of air according to the Lemmon and Jacobsen (2003). For details, see chemicals.viscosity.mu\_air\_lemmon.

## Returns

mu [float] Viscosity of air, [Pa\*s]

## 7.22.6 CoolProp Wrapper

**class** thermo.phases.**CoolPropGas**(*backend*, *fluid*, *T=None*, *P=None*, *zs=None*, *Hfs=None*, *Gfs=None*, *Sfs=None*)

Bases: thermo.phases.coolprop\_phase.CoolPropPhase

**class** thermo.phases.**CoolPropLiquid**(*backend*, *fluid*, *T=None*, *P=None*, *zs=None*, *Hfs=None*, *Gfs=None*, *Sfs=None*)

Bases: thermo.phases.coolprop\_phase.CoolPropPhase

# 7.23 Phase Change Properties (thermo.phase\_change)

This module contains implementations of *thermo.utils.TDependentProperty* representing enthalpy of vaporization and enthalpy of sublimation. A variety of estimation and data methods are available as included in the *chemicals* library.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Enthalpy of Vaporization
- Enthalpy of Sublimation

# 7.23.1 Enthalpy of Vaporization

**class** thermo.phase\_change.**EnthalpyVaporization**(*CASRN=", Tb=None, Tc=None, Pc=None,* 

omega=None, similarity\_variable=None, Psat=None, Zl=None, Zg=None, extrapolation='Watson',

\*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with heat of vaporization as a function of temperature. Consists of three constant value data sources, one source of tabular information, three coefficient-based methods, nine corresponding-states estimators, and the external library CoolProp.

#### **Parameters**

**Tb** [float, optional] Boiling point, [K]

- Tc [float, optional] Critical temperature, [K]
- Pc [float, optional] Critical pressure, [Pa]

omega [float, optional] Acentric factor, [-]

similarity\_variable [float, optional] similarity variable, n\_atoms/MW, [mol/g]

Psat [float or callable, optional] Vapor pressure at T or callable for the same, [Pa]

ZI [float or callable, optional] Compressibility of liquid at T or callable for the same, [-]

Zg [float or callable, optional] Compressibility of gas at T or callable for the same, [-]

CASRN [str, optional] The CAS number of the chemical

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

#### See also:

chemicals.phase\_change.MK

chemicals.phase\_change.SMK

chemicals.phase\_change.Velasco

chemicals.phase\_change.Clapeyron

chemicals.phase\_change.Riedel

chemicals.phase\_change.Chen

chemicals.phase\_change.Vetere

chemicals.phase\_change.Liu

chemicals.phase\_change.Watson

## Notes

To iterate over all methods, use the list stored in enthalpy\_vaporization\_methods.

- **CLAPEYRON:** The Clapeyron fundamental model desecribed in Clapeyron. This is the model which uses *Zl*, *Zg*, and *Psat*, all of which must be set at each temperature change to allow recalculation of the heat of vaporization.
- MORGAN\_KOBAYASHI: The MK CSP model equation documented in MK.
- SIVARAMAN\_MAGEE\_KOBAYASHI: The SMK CSP model equation documented in SMK.
- VELASCO: The Velasco CSP model equation documented in Velasco.
- **PITZER:** The Pitzer CSP model equation documented in Pitzer.
- **RIEDEL:** The Riedel CSP model equation, valid at the boiling point only, documented in Riedel. This is adjusted with the Watson equation unless *Tc* is not available.
- **CHEN:** The Chen CSP model equation, valid at the boiling point only, documented in Chen. This is adjusted with the Watson equation unless *Tc* is not available.
- **VETERE:** The Vetere CSP model equation, valid at the boiling point only, documented in Vetere. This is adjusted with the Watson equation unless *Tc* is not available.
- **LIU:** The Liu CSP model equation, valid at the boiling point only, documented in Liu. This is adjusted with the Watson equation unless *Tc* is not available.
- **CRC\_HVAP\_TB:** The constant value available in [4] at the normal boiling point. This is adusted with the Watson equation unless *Tc* is not available. Data is available for 707 chemicals.
- **CRC\_HVAP\_298:** The constant value available in [4] at 298.15 K. This is adusted with the Watson equation unless *Tc* is not available. Data is available for 633 chemicals.
- **GHARAGHEIZI\_HVAP\_298:** The constant value available in [5] at 298.15 K. This is adusted with the Watson equation unless *Tc* is not available. Data is available for 2730 chemicals.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [3]. Very slow but accurate.
- **VDI\_TABULAR:** Tabular data in [4] along the saturation curve; interpolation is as set by the user or the default.
- **VDI\_PPDS:** Coefficients for a equation form developed by the PPDS, published openly in [3]. Extrapolates poorly at low temperatures.
- **DIPPR\_PERRY\_8E:** A collection of 344 coefficient sets from the DIPPR database published openly in [6]. Provides temperature limits for all its fluids. chemicals.dippr.EQ106 is used for its fluids.
- ALIBAKHSHI: One-constant limited temperature range regression method presented in [7], with constants for ~2000 chemicals from the DIPPR database. Valid up to 100 K below the critical point, and 50 K under the boiling point.

#### References

## [1], [2], [3], [4], [5], [6], [7]

#### Attributes

interpolation\_T interpolation\_property interpolation\_property\_inv

#### **Methods**

calculate(T, method)	Method to calculate heat of vaporization of a liquid
	at temperature $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

#### Watson\_exponent = 0.38

Exponent used in the Watson equation

### calculate(T, method)

Method to calculate heat of vaporization of a liquid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### Parameters

T [float] Temperature at which to calculate heat of vaporization, [K]

method [str] Name of the method to use

#### Returns

Hvap [float] Heat of vaporization of the liquid at T, [J/mol]

#### interpolation\_T = None

No interpolation transformation by default.

#### interpolation\_property = None

No interpolation transformation by default.

#### interpolation\_property\_inv = None

No interpolation transformation by default.

#### name = 'Enthalpy of vaporization'

## $property_max = 1000000.0$

Maximum valid of heat of vaporization. Set to twice the value in the available data.

#### property\_min = 0

Mimimum valid value of heat of vaporization. This occurs at the critical point exactly.

```
ranked_methods = ['COOLPROP', 'DIPPR_PERRY_8E', 'VDI_PPDS', 'MORGAN_KOBAYASHI',
'SIVARAMAN_MAGEE_KOBAYASHI', 'VELASCO', 'PITZER', 'VDI_TABULAR', 'ALIBAKHSHI',
'CRC_HVAP_TB', 'CRC_HVAP_298', 'GHARAGHEIZI_HVAP_298', 'CLAPEYRON', 'RIEDEL',
'CHEN', 'VETERE', 'LIU']
```

Default rankings of the available methods.

#### test\_method\_validity(T, method)

Method to check the validity of a method. For CSP methods, the models are considered valid from 0 K to the critical point. For tabular data, extrapolation outside of the range is used if

tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

The constant methods **CRC\_HVAP\_TB**, **CRC\_HVAP\_298**, and **GHARAGHEIZI\_HVAP** are adjusted for temperature dependence according to the Watson equation, with a temperature exponent as set in *Watson\_exponent*, usually regarded as 0.38. However, if Tc is not set, then the adjustment cannot be made. In that case the methods are considered valid for within 5 K of their boiling point or 298.15 K as appropriate.

#### **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

```
units = 'J/mol'
```

```
thermo.phase_change.enthalpy_vaporization_methods = ['DIPPR_PERRY_8E', 'VDI_PPDS',
'COOLPROP', 'VDI_TABULAR', 'MORGAN_KOBAYASHI', 'SIVARAMAN_MAGEE_KOBAYASHI', 'VELASCO',
'PITZER', 'ALIBAKHSHI', 'CRC_HVAP_TB', 'CRC_HVAP_298', 'GHARAGHEIZI_HVAP_298',
'CLAPEYRON', 'RIEDEL', 'CHEN', 'VETERE', 'LIU']
```

Holds all methods available for the EnthalpyVaporization class, for use in iterating over them.

## 7.23.2 Enthalpy of Sublimation

class thermo.phase\_change.EnthalpySublimation(CASRN=", Tm=None, Tt=None, Cpg=None, Cps=None, Hvap=None, extrapolation='linear', \*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with heat of sublimation as a function of temperature. Consists of one temperature-dependent method based on the heat of sublimation at 298.15 K.

#### **Parameters**

CASRN [str, optional] The CAS number of the chemical

**Tm** [float, optional] Normal melting temperature, [K]

- Tt [float, optional] Triple point temperature, [K]
- **Cpg** [float or callable, optional] Gaseous heat capacity at a given temperature or callable for the same, [J/mol/K]
- **Cps** [float or callable, optional] Solid heat capacity at a given temperature or callable for the same, [J/mol/K]
- **Hvap** [float of callable, optional] Enthalpy of Vaporization at a given temperature or callable for the same, [J/mol]
- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]

**method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

## **Notes**

To iterate over all methods, use the list stored in enthalpy\_sublimation\_methods.

WEBBOOK\_HSUB: Enthalpy of sublimation at a constant temperature of 298.15 K as given in [3].

- GHARAGHEIZI\_HSUB\_298: Enthalpy of sublimation at a constant temperature of 298 K as given in [1].
- **GHARAGHEIZI\_HSUB:** Enthalpy of sublimation at a constant temperature of 298 K as given in [1] are adjusted using the solid and gas heat capacity functions to correct for any temperature.
- **CRC\_HFUS\_HVAP\_TM:** Enthalpies of fusion in [1] are corrected to be enthalpies of sublimation by adding the enthalpy of vaporization at the fusion temperature, and then adjusted using the solid and gas heat capacity functions to correct for any temperature.

## References

#### [1], [2], [3]

## Attributes

interpolation\_T interpolation\_property interpolation\_property\_inv

#### **Methods**

calculate(T, method)	Method to calculate heat of sublimation of a solid at
	temperature $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

#### calculate(T, method)

Method to calculate heat of sublimation of a solid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature at which to calculate heat of sublimation, [K]

method [str] Name of the method to use

#### Returns

Hsub [float] Heat of sublimation of the solid at T, [J/mol]

#### interpolation\_T = None

No interpolation transformation by default.

### interpolation\_property = None

No interpolation transformation by default.

#### interpolation\_property\_inv = None

No interpolation transformation by default.

name = 'Enthalpy of sublimation'

#### $property_max = 1000000.0$

Maximum valid of heat of sublimation. A theoretical concept only.

```
property_min = 0
```

Mimimum valid value of heat of vaporization. A theoretical concept only.

```
ranked_methods = ['WEBBOOK_HSUB', 'GHARAGHEIZI_HSUB', 'CRC_HFUS_HVAP_TM',
'GHARAGHEIZI_HSUB_298']
```

#### test\_method\_validity(T, method)

Method to check the validity of a method. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

units = 'J/mol'

thermo.phase\_change.enthalpy\_sublimation\_methods = ['WEBBOOK\_HSUB', 'GHARAGHEIZI\_HSUB',
'CRC\_HFUS\_HVAP\_TM', 'GHARAGHEIZI\_HSUB\_298']

Holds all methods available for the EnthalpySublimation class, for use in iterating over them.

# 7.24 Legacy Property Packages (thermo.property\_package)

**Warning:** These classes were a first attempt at rigorous multiphase equilibrium. They may be useful in some special cases but they are not complete and further development will not happen. They were never documented as well.

It is recommended to switch over to the *thermo.flash* interface which seeks to be more modular, easier to maintain and extend, higher-performance, and easier to modify.

# 7.25 Phase Identification (thermo.phase\_identification)

This module contains functions for identifying phases as liquid, solid, and gas.

Solid identification is easy using the phase identification parameter. There is never more than one gas by definition. For pure species, the phase identification parameter is a clear vapor-liquid differentiator in the subcritical region and it provides line starting at the critical point for the supercritical region.

However for mixtures, there is no clear calcuation that can be performed to identify the phase of a mixture. Many different criteria that have been proposed are included here. The phase identification parameter or PIP. is recommended in general and is the default.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Phase Identification
  - Main Interface
  - Secondary Interfaces
  - Scoring Functions
- Sorting Phases

# 7.25.1 Phase Identification

## **Main Interface**

Identify and sort all phases given the provided parameters.

## Parameters

phases [list[Phase]] Phases to be identified and sorted, [-]

betas [list[float]] Phase molar fractions, [-]

constants [ChemicalConstantsPackage] Constants used in the identification, [-]

correlations [PropertyCorrelationsPackage] Correlations used in the identification, [-]

settings [BulkSettings] Settings object controlling the phase ID, [-]

skip\_solids [bool] Set this to True if no phases are provided which can represent a solid phase,
[-]

## Returns

gas [Phase] Gas phase, if one was identified, [-]

liquids [list[Phase]] Liquids that were identified and sorted, [-]

solids [list[Phase]] Solids that were identified and sorted, [-]

betas [list[float]] Sorted phase molar fractions, in order (gas, liquids..., solids...) [-]

## Notes

This step is very important as although phase objects are designed to represent a single phase, cubic equations of state can be switched back and forth by the flash algorithms. Thermodynamics doesn't care about gases, liquids, or solids; it just cares about minimizing Gibbs energy!

## **Examples**

A butanol-water-ethanol flash yields three phases. For brevity we skip the flash and initialize our *gas*, *liq0*, and *liq1* object with the correct phase composition. Then we identify the phases into liquid, gas, and solid.

```
>>> from thermo import ChemicalConstantsPackage, PropertyCorrelationsPackage,
→HeatCapacityGas, SRKMIX, CEOSGas, CEOSLiquid
>>> constants = ChemicalConstantsPackage(Tcs=[563.0, 647.14, 514.0], Vcs=[0.000274,
→5.6e-05, 0.000168], Pcs=[4414000.0, 22048320.0, 6137000.0], omegas=[0.59, 0.344,
→0.635], MWs=[74.1216, 18.01528, 46.06844], CASs=['71-36-3', '7732-18-5', '64-17-5
→'])
>>> properties = PropertyCorrelationsPackage(constants=constants, skip_missing=True,
                                        HeatCapacityGases=[HeatCapacityGas(load_
→data=False, poly_fit=(50.0, 1000.0, [-3.787200194613107e-20, 1.7692887427654656e-
→16, -3.445247207129205e-13, 3.612771874320634e-10, -2.1953250181084466e-07, 7.
→707135849197655e-05, -0.014658388538054169, 1.5642629364740657, -7.
\leftrightarrow 614560475001724)),
                                         HeatCapacityGas(load_data=False, poly_
. . .
→fit=(50.0, 1000.0, [5.543665000518528e-22, -2.403756749600872e-18, 4.
→2166477594350336e-15, -3.7965208514613565e-12, 1.823547122838406e-09, -4.
→3747690853614695e-07, 5.437938301211039e-05, -0.003220061088723078, 33.
\rightarrow 32731489750759])),
                                         HeatCapacityGas(load_data=False, poly_
. . .
→ fit=(50.0, 1000.0, [-1.162767978165682e-20, 5.4975285700787494e-17, -1.
→0861242757337942e-13, 1.1582703354362728e-10, -7.160627710867427e-08, 2.
→5392014654765875e-05, -0.004732593693568646, 0.5072291035198603, 20.
\rightarrow 037826650765965])),], )
>>> eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
>>> gas = CEOSGas(SRKMIX, eos_kwargs, HeatCapacityGases=properties.
→HeatCapacityGases)
>>> liq = CEOSLiquid(SRKMIX, eos_kwargs, HeatCapacityGases=properties.
→HeatCapacityGases)
>>> T, P = 361, 1e5
>>> gas = gas.to(T=T, P=P, zs=[0.2384009970908655, 0.5786839935180925, 0.
\rightarrow 1829150093910419
>>> liq0 = liq.to(T=T, P=P, zs=[7.619975052238032e-05, 0.9989622883894993, 0.
→0009615118599781474])
>>> liq1 = liq.to(T=T, P=P, zs=[0.6793120076703771, 0.19699746328631124, 0.
\rightarrow 12369052904331178
>>> res = identity_phase_states(phases=[liq0, liq1, gas], constants=constants,_

→correlations=properties, VL_method='PIP')

>>> res[0] is gas, res[1][0] is liq0, res[1][1] is liq1, res[2]
(True, True, True, [])
```

## **Secondary Interfaces**

```
thermo.phase_identification.identity_phase_states(phases, constants, correlations, VL_method='PIP',
S_method='d2P_dVdT', VL_ID_settings=None,
S_ID_settings=None, skip_solids=False)
```

Identify and the actial phase of all the given phases given the provided settings.

### Parameters

phases [list[Phase]] Phases to be identified and sorted, [-]

constants [ChemicalConstantsPackage] Constants used in the identification, [-]

correlations [PropertyCorrelationsPackage] Correlations used in the identification, [-]

VL\_method [str, optional] One of VL\_ID\_METHODS, [-]

**S\_method** [str, optional] One of *S\_ID\_METHODS*, [-]

- VL\_ID\_settings [dict[str][float] or None, optional] Additional configuration options for vaporliquid phase ID, [-]
- **S\_ID\_settings** [dict[str][float] or None, optional] Additional configuration options for solidliquid phase ID, [-]
- skip\_solids [bool] Set this to True if no phases are provided which can represent a solid phase,
  [-]

#### Returns

gas [Phase] Gas phase, if one was identified, [-]

liquids [list[Phase]] Liquids that were identified and sorted, [-]

solids [list[Phase]] Solids that were identified and sorted, [-]

```
thermo.phase_identification.VL_ID_METHODS = ['Tpc', 'Vpc', 'Tpc Vpc weighted', 'Tpc Vpc',
'Wilson', 'Poling', 'PIP', 'Bennett-Schmidt', 'Traces']
List of all the methods available to perform the Vapor-Liquid phase ID.
```

thermo.phase\_identification.S\_ID\_METHODS = ['d2P\_dVdT'] List of all the methods available to perform the solid-liquid phase ID.

## **Scoring Functions**

```
thermo.phase_identification.score_phases_VL(phases, constants, correlations, method)
Score all phases given the provided parameters and a selected method.
```

A score above zero indicates a potential gas. More than one phase may have a score above zero, in which case the highest scoring phase is the gas, and the other is a liquid.

## Parameters

phases [list[thermo.phases.Phase]] Phases to be identified and sorted, [-]

constants [ChemicalConstantsPackage] Constants used in the identification, [-]

correlations [PropertyCorrelationsPackage] Correlations used in the identification, [-]

**method** [str] Setting configuring how the scoring is performed; one of 'Tpc', 'Vpc', 'Tpc Vpc weighted', 'Tpc Vpc', 'Wilson', 'Poling', 'PIP', 'Bennett-Schmidt', 'Traces', [-]

#### Returns

scores [list[float]] Scores for the phases in the order provided, [-]

## **Examples**

```
>>> from thermo import ChemicalConstantsPackage, PropertyCorrelationsPackage,
→CEOSGas, CEOSLiquid, PRMIX, HeatCapacityGas
>>> constants = ChemicalConstantsPackage(CASs=['124-38-9', '110-54-3'], Vcs=[9.4e-
→05, 0.000368], MWs=[44.0095, 86.17536], names=['carbon dioxide', 'hexane'],
→omegas=[0.2252, 0.2975], Pcs=[7376460.0, 3025000.0], Tbs=[194.67, 341.87],
→Tcs=[304.2, 507.6], Tms=[216.65, 178.075])
>>> correlations = PropertyCorrelationsPackage(constants=constants, skip_
→missing=True, HeatCapacityGases=[HeatCapacityGas(poly_fit=(50.0, 1000.0, [-3.
→1115474168865828e-21, 1.39156078498805e-17, -2.5430881416264243e-14, 2.
→4175307893014295e-11, -1.2437314771044867e-08, 3.1251954264658904e-06, -0.
→00021220221928610925, 0.000884685506352987, 29.266811602924644])),
→HeatCapacityGas(poly_fit=(200.0, 1000.0, [1.3740654453881647e-21, -8.
→ 344496203280677e-18, 2.2354782954548568e-14, -3.4659555330048226e-11, 3.
\rightarrow 410703030634579e-08, -2.1693611029230923e-05, 0.008373280796376588, -1.
→356180511425385, 175.67091124888998]))])
>>> T, P, zs = 300.0, 1e6, [.5, .5]
>>> eos_kwargs = {'Pcs': constants.Pcs, 'Tcs': constants.Tcs, 'omegas': constants.
\rightarrowomegas}
>>> gas = CEOSGas(PRMIX, eos_kwargs, HeatCapacityGases=correlations.
→HeatCapacityGases, T=T, P=P, zs=zs)
>>> liq = CEOSLiquid(PRMIX, eos_kwargs, HeatCapacityGases=correlations.
\rightarrow HeatCapacityGases, T=T, P=P, zs=zs)
```

A sampling of different phase identification methods is below:

```
>>> score_phases_VL([gas, liq], constants, correlations, method='PIP')
[1.6409446310, -7.5692120928]
>>> score_phases_VL([gas, liq], constants, correlations, method='Vpc')
[0.00144944049, -0.0001393075288]
>>> score_phases_VL([gas, liq], constants, correlations, method='Tpc Vpc')
[113.181283525, -29.806038704]
>>> score_phases_VL([gas, liq], constants, correlations, method='Bennett-Schmidt')
[0.0003538299416, -2.72255439503e-05]
>>> score_phases_VL([gas, liq], constants, correlations, method='Poling')
[0.1767828268, -0.004516837897]
```

thermo.phase\_identification.score\_phases\_S(phases, constants, correlations, method='d2P\_dVdT', S\_ID\_settings=None)

Score all phases according to how wolid they appear given the provided parameters and a selected method.

A score above zero indicates a solid. More than one phase may have a score above zero. A score under zero means the phase is a liquid or gas.

#### Parameters

phases [list[thermo.phases.Phase]] Phases to be identified and sorted, [-]

constants [ChemicalConstantsPackage] Constants used in the identification, [-]

correlations [PropertyCorrelationsPackage] Correlations used in the identification, [-]

method [str] Setting configuring how the scoring is performed; one of ('d2P\_dVdT',), [-]

**S\_ID\_settings** [dict[str][float] or None, optional] Additional configuration options for solidliquid phase ID, [-]

#### Returns

scores [list[float]] Scores for the phases in the order provided, [-]

thermo.phase\_identification.vapor\_score\_traces(zs, CASs, Tcs, trace\_CASs=['74-82-8', '7727-37-9'],

min\_trace=0.0)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the concept of which phase has the most of the lightest compound. This nicely sidesteps issues in many other methods, at the expense that it cannot be applied when there is only one phase and it is not smart enough to handle liquid-liquid cases.

If no trace components are present, the component with the lowest critical temperature's concentration is returned. Because of the way this is implemented, the score is always larger than 1.0.

## Parameters

zs [list[float]] Mole fractions of the phase being identified, [-]

CASs [list[str]] CAS numbers of all components, [-]

Tcs [list[float]] Critical temperatures of all species, [K]

- **trace\_CASs** [list[str]] Trace components to use for identification; if more than one component is given, the first component present in both *CASs* and *trace\_CASs* is the one used, [-]
- **min\_trace** [float] Minimum concentration to make a phase appear vapor-like; subtracted from the concentration which would otherwise be returned, [-]

#### Returns

score [float] Vapor like score, [-]

## **Examples**

A flash of equimolar CO2/n-hexane at 300 K and 1 MPa is computed, and there is a two phase solution. The phase must be identified for each result:

Liquid-like phase:

```
>>> vapor_score_traces(zs=[.218, .782], Tcs=[304.2, 507.6], CASs=['124-38-9', '110-

→54-3'])

0.218
```

Vapor-like phase:

```
>>> vapor_score_traces(zs=[.975, .025], Tcs=[304.2, 507.6], CASs=['124-38-9', '110-

→54-3'])

0.975
```

thermo.phase\_identification.vapor\_score\_Tpc(T, Tcs, zs)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the following criteria

$$T - \sum_{i} z_i T_{c,i}$$

Parameters

T [float] Temperature, [K]

**Tcs** [list[float]] Critical temperatures of all species, [K]

**zs** [list[float]] Mole fractions of the phase being identified, [-]

#### Returns

score [float] Vapor like score, [-]

## **Examples**

A flash of equimolar CO2/n-hexane at 300 K and 1 MPa is computed, and there is a two phase solution. The phase must be identified for each result:

Liquid-like phase:

```
>>> vapor_score_Tpc(T=300.0, Tcs=[304.2, 507.6], zs=[0.21834418746784942, 0.

→7816558125321506])

-163.18879226903942
```

Vapor-like phase:

```
>>> vapor_score_Tpc(T=300.0, Tcs=[304.2, 507.6], zs=[0.9752234962374878, 0.

→024776503762512052])

-9.239540865294941
```

In this result, the vapor phase is not identified as a gas at all! It has a mass density of ~  $20 \text{ kg/m}^3$ , which would usually be called a gas by most people.

#### thermo.phase\_identification.vapor\_score\_Vpc(V, Vcs, zs)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the following criteria

$$V - \sum_{i} z_i V_{c,i}$$

## Parameters

V [float] Molar volume, [m^3/mol]

Vcs [list[float]] Critical molar volumes of all species, [m^3/mol]

zs [list[float]] Mole fractions of the phase being identified, [-]

#### Returns

score [float] Vapor like score, [-]

#### **Examples**

A flash of equimolar CO2/n-hexane at 300 K and 1 MPa is computed, and there is a two phase solution. The phase must be identified for each result:

Liquid-like phase:

```
>>> vapor_score_Vpc(V=0.00011316308855449715, Vcs=[9.4e-05, 0.000368], zs=[0.

→21834418746784942, 0.7816558125321506])

-0.000195010604079
```

Vapor-like phase:

```
>>> vapor_score_Vpc(V=0.0023406573328250335, Vcs=[9.4e-05, 0.000368], zs=[0.

→9752234962374878, 0.024776503762512052])

0.002239868570
```

## thermo.phase\_identification.vapor\_score\_Tpc\_weighted(T, Tcs, Vcs, zs, rl=1.0)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the following criteria, said to be implemented in ECLIPSE [1]:

$$T-T_{pc}$$
 
$$T_{p,c}=r_1\frac{\sum_j x_j V_{c,j}T_{c,j}}{\sum_j x_j V_{c,j}}$$

## Parameters

T [float] Temperature, [K]

Tcs [list[float]] Critical temperatures of all species, [K]

Vcs [list[float]] Critical molar volumes of all species, [m^3/mol]

zs [list[float]] Mole fractions of the phase being identified, [-]

r1 [float] Tuning factor, [-]

## Returns

score [float] Vapor like score, [-]

## References

[1]

## **Examples**

A flash of equimolar CO2/n-hexane at 300 K and 1 MPa is computed, and there is a two phase solution. The phase must be identified for each result:

Liquid-like phase:

```
>>> vapor_score_Tpc_weighted(T=300.0, Tcs=[304.2, 507.6], Vcs=[9.4e-05, 0.000368],

→zs=[0.21834418746784942, 0.7816558125321506])

-194.0535694431
```

Vapor-like phase:

```
>>> vapor_score_Tpc_weighted(T=300.0, Tcs=[304.2, 507.6], Vcs=[9.4e-05, 0.000368],

→zs=[0.9752234962374878, 0.024776503762512052])

-22.60037521107
```

As can be seen, the CO2-phase is incorrectly identified as a liquid.

thermo.phase\_identification.vapor\_score\_Tpc\_Vpc(T, V, Tcs, Vcs, zs)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the following criteria, said to be implemented in Multiflash [1]:

$$VT^2 - V_{pc}T_{pc}^2$$

## Parameters

**T** [float] Temperature, [K]

V [float] Molar volume, [m^3/mol]

Tcs [list[float]] Critical temperatures of all species, [K]

Vcs [list[float]] Critical molar volumes of all species, [m^3/mol]

zs [list[float]] Mole fractions of the phase being identified, [-]

#### Returns

score [float] Vapor like score, [-]

#### References

[1]

## **Examples**

A flash of equimolar CO2/n-hexane at 300 K and 1 MPa is computed, and there is a two phase solution. The phase must be identified for each result:

Liquid-like phase:

Vapor-like phase:

```
>>> vapor_score_Tpc_Vpc(T=300.0, V=0.0023406573328250335, Tcs=[304.2, 507.6],

→Vcs=[9.4e-05, 0.000368], zs=[0.9752234962374878, 0.024776503762512052])

201.020821992
```

#### thermo.phase\_identification.vapor\_score\_Wilson(T, P, zs, Tcs, Pcs, omegas)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the Rachford-Rice Wilson method of Perschke [1].

After calculating Wilson's K values, the following expression is evaluated at  $\frac{V}{F} = 0.5$ ; the result is the score.

$$\sum_{i} \frac{z_i(K_i - 1)}{1 + \frac{V}{F}(K_i - 1)}$$

#### Parameters

T [float] Temperature, [K]

P [float] Pressure, [Pa]

zs [list[float]] Mole fractions of the phase being identified, [-]

Tcs [list[float]] Critical temperatures of all species, [K]

Pcs [list[float]] Critical pressures of all species, [Pa]

omegas [list[float]] Acentric factors of all species, [-]

#### Returns

score [float] Vapor like score, [-]

#### References

[1]

#### **Examples**

A flash of equimolar CO2/n-hexane at 300 K and 1 MPa is computed, and there is a two phase solution. The phase must be identified for each result:

Liquid-like phase:

```
>>> vapor_score_Wilson(T=300.0, P=1e6, zs=[.218, .782], Tcs=[304.2, 507.6],

→Pcs=[7376460.0, 3025000.0], omegas=[0.2252, 0.2975])

-1.16644793
```

Vapor-like phase:

```
>>> vapor_score_Wilson(T=300.0, P=1e6, zs=[.975, .025], Tcs=[304.2, 507.6],

→Pcs=[7376460.0, 3025000.0], omegas=[0.2252, 0.2975])

1.397678492
```

This method works well in many conditions, like the Wilson equation itself, but fundamentally it cannot do a great job because it is not tied to the phase model itself.

A dew point flash at P = 100 Pa for the same mixture shows both phases being identified as vapor-like:

thermo.phase\_identification.vapor\_score\_Poling(kappa)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the isothermal compressibility *kappa* concept by Poling [1].

score = 
$$(\kappa - 0.005 \text{atm}^{-1})$$

Parameters

kappa [float] Isothermal coefficient of compressibility, [1/Pa]

Returns

score [float] Vapor like score, [-]

## Notes

A second criteria which is not implemented as it does not fit with the scoring concept is for liquids:

$$\frac{0.9}{P} < \beta < \frac{3}{P}$$

## References

[1]

#### **Examples**

CO2 vapor properties computed with Peng-Robinson at 300 K and 1 bar:

```
>>> vapor_score_Poling(1.0054239121594122e-05)
1.013745778995
```

n-hexane liquid properties computed with Peng-Robinson at 300 K and 10 bar:

```
>>> vapor_score_Poling(2.121777078782957e-09)
-0.00478501093
```

thermo.phase\_identification.vapor\_score\_PIP(V, dP\_dT, dP\_dV, d2P\_dV2, d2P\_dVdT)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the PIP concept.

score = 
$$-(\Pi - 1)$$

$$\Pi = V \left[ \frac{\frac{\partial^2 P}{\partial V \partial T}}{\frac{\partial P}{\partial T}} - \frac{\frac{\partial^2 P}{\partial V^2}}{\frac{\partial P}{\partial V}} \right]$$

#### **Parameters**

V [float] Molar volume at T and P, [m^3/mol]

 $dP_dT$  [float] Derivative of P with respect to T, [Pa/K]

**dP\_dV** [float] Derivative of *P* with respect to *V*, [Pa\*mol/m^3]

d2P\_dV2 [float] Second derivative of P with respect to V, [Pa\*mol^2/m^6]

d2P\_dVdT [float] Second derivative of P with respect to both V and T, [Pa\*mol/m^3/K]

## Returns

score [float] Vapor like score, [-]

## References

[1]

## **Examples**

CO2 vapor properties computed with Peng-Robinson at 300 K and 1 bar:

```
>>> vapor_score_PIP(0.024809176851423774, 337.0119286073647, -4009021.959558917, _

→321440573.3615088, -13659.63987996052)

0.016373735005
```

n-hexane liquid properties computed with Peng-Robinson at 300 K and 10 bar:

```
>>> vapor_score_PIP(0.00013038156684574785, 578477.8796379718, -3614798144591.8984,
...4.394997991022487e+17, -20247865009.795322)
-10.288635225
```

#### thermo.phase\_identification.vapor\_score\_Bennett\_Schmidt(*dbeta\_dT*)

Compute a vapor score representing how vapor-like a phase is (higher, above zero = more vapor like) using the Bennet-Schmidt temperature derivative of isobaric expansion suggestion.

score 
$$= -\left(\frac{\partial\beta}{\partial T}\right)$$

**Parameters** 

dbeta\_dT [float] Temperature derivative of isobaric coefficient of a thermal expansion, [1/K^2]

Returns

score [float] Vapor like score, [-]

## References

[1]

#### **Examples**

CO2 vapor properties computed with Peng-Robinson at 300 K and 1 bar:

```
>>> vapor_score_Bennett_Schmidt(-1.1776172267959163e-05)
1.1776172267959163e-05
```

n-hexane liquid properties computed with Peng-Robinson at 300 K and 10 bar:

```
>>> vapor_score_Bennett_Schmidt(7.558572848883679e-06)
-7.558572848883679e-06
```

## 7.25.2 Sorting Phases

thermo.phase\_identification.sort\_phases(liquids, solids, constants, settings)

Identify and sort all phases given the provided parameters. This is not a thermodynamic concept; it is just a convinience method to make the results of the flash more consistent, because the flash algorithms don't care about density or ordering the phases.

## Parameters

liquids [list[*Phase*]] Liquids that were identified, [-]

solids [list[Phase]] Solids that were identified, [-]

constants [ChemicalConstantsPackage] Constants used in the identification, [-]

correlations [PropertyCorrelationsPackage] Correlations used in the identification, [-]

settings [BulkSettings] Settings object controlling the phase sorting, [-]

#### Returns

liquids [list[Phase]] Liquids that were identified and sorted, [-]
solids [list[Phase]] Solids that were identified and sorted, [-]

#### **Notes**

The settings object uses the preferences *liquid\_sort\_method*, *liquid\_sort\_prop*, *liquid\_sort\_cmps*, *liquid\_sort\_cmps\_neg*, and *phase\_sort\_higher\_first*.

# 7.26 Regular Solution Gibbs Excess Model (thermo.regular\_solution)

This module contains a class *RegularSolution* for performing activity coefficient calculations with the regular solution model.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Regular Solution Class
- Regular Solution Regression Calculations

## 7.26.1 Regular Solution Class

class thermo.regular\_solution.RegularSolution(T, xs, Vs, SPs, lambda\_coeffs=None)
Bases: thermo.activity.GibbsExcess

Class for representing an a liquid with excess gibbs energy represented by the Regular Solution model. This model is not temperature dependent and has limited predictive ability, but can be used without interaction parameters. This model is described in [1].

$$G^{E} = \frac{\sum_{m} \sum_{n} (x_{m} x_{n} V_{m} V_{n} A_{mn})}{\sum_{m} x_{m} V_{m}}$$
$$A_{mn} = 0.5(\delta_{m} - \delta_{n})^{2} - \delta_{m} \delta_{n} k_{mn}$$

In the above equation,  $\delta$  represents the solubility parameters, and  $k_{mn}$  is the interaction coefficient between *m* and *n*. The model makes no assumption about the symmetry of this parameter.

#### Parameters

- T [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]
- Vs [list[float]] Molar volumes of each compond at a reference temperature (often 298.15 K), [m^3/mol]

**SPs** [list[float]] Solubility parameters of each compound; normally at a reference temperature of 298.15 K, [Pa^0.5]

lambda\_coeffs [list[list[float]], optional] Optional interaction parameters, [-]

#### Notes

In addition to the methods presented here, the methods of its base class thermo.activity.GibbsExcess are available as well.

Additional equations of note are as follows.

$$G^{E} = H^{E}$$
$$S^{E} = 0$$
$$\delta = \sqrt{\frac{\Delta H_{vap} - RT}{V_{m}}}$$

#### References

[1], [2], [3], [4]

## **Examples**

#### **Example 1**

From [2], calculate the activity coefficients at infinite dilution for the system benzene-cyclohexane at 253.15 K using the regular solution model (example 5.20, with unit conversion in-line):

This matches the solution given of [1.135, 1.168].

#### Example 2

Benzene and cyclohexane calculation from [3], without interaction parameters.

```
>>> GE = RegularSolution(T=353, xs=[0.01, 0.99], Vs=[8.90e-05, 1.09e-04], SPs=[9.

→2*(calorie/1e-6)**0.5, 8.2*(calorie/1e-6)**0.5])
>>> GE.gammas()
[1.1329295, 1.00001039]
```

#### Example 3

Another common model is the Flory-Huggins model. This isn't implemented as a separate model, but it is possible to modify the activity coefficient results of *RegularSolution* to obtain the activity coefficients from the Flory-Huggins model anyway. ChemSep [4] implements the Flory-Huggins model and calls it the regular solution model, so results can't be compared with ChemSep except when making the following manual solution. The example below uses parameters from ChemSep for ethanol and water.

```
>>> GE = RegularSolution(T=298.15, xs=[0.5, 0.5], Vs=[0.05868e-3, 0.01807e-3],_

...,SPs=[26140.0, 47860.0])

>>> GE.gammas() # Regular solution activity coefficients

[1.8570955489, 7.464567232]

>>> lngammass = [log(g) for g in GE.gammas()]

>>> thetas = [GE.Vs[i]/sum(GE.xs[i]*GE.Vs[i] for i in range(GE.N)) for i in_

...,range(GE.N)]

>>> gammas_flory_huggins = [exp(lngammass[i] + log(thetas[i]) + 1 - thetas[i]) for_

...,i in range(GE.N)]

>>> gammas_flory_huggins

[1.672945693, 5.9663471]
```

This matches the values calculated from ChemSep exactly.

## Attributes

- T [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]
- Vs [list[float]] Molar volumes of each compond at a reference temperature (often 298.15 K), [K]
- **SPs** [list[float]] Solubility parameters of each compound; normally at a reference temperature of 298.15 K, [Pa^0.5]

lambda\_coeffs [list[list[float]]] Interaction parameters, [-]

## Methods

<i>GE</i> ()	Calculate and return the excess Gibbs energy of a liq-
	uid phase using the regular solution model.
d2GE_dT2()	Calculate and return the second temperature deriva-
	tive of excess Gibbs energy of a liquid phas.
d2GE_dTdxs()	Calculate and return the temperature derivative of
	mole fraction derivatives of excess Gibbs energy.
d2GE_dxixjs()	Calculate and return the second mole fraction deriva-
	tives of excess Gibbs energy of a liquid phase using
	the regular solution model.
d3GE_dT3()	Calculate and return the third temperature derivative
	of excess Gibbs energy of a liquid phase.
d3GE_dxixjxks()	Calculate and return the third mole fraction deriva-
	tives of excess Gibbs energy.
dGE_dT()	Calculate and return the temperature derivative of ex-
	cess Gibbs energy of a liquid phase.
dGE_dxs()	Calculate and return the mole fraction derivatives of
	excess Gibbs energy of a liquid phase using the reg-
	ular solution model.
to_T_xs(T, xs)	Method to construct a new RegularSolution in-
	stance at temperature $T$ , and mole fractions $xs$ with
	the same parameters as the existing object.

GE()

Calculate and return the excess Gibbs energy of a liquid phase using the regular solution model.

$$G^{E} = \frac{\sum_{m} \sum_{n} (x_{m} x_{n} V_{m} V_{n} A_{mn})}{\sum_{m} x_{m} V_{m}}$$
$$A_{mn} = 0.5 (\delta_{m} - \delta_{n})^{2} - \delta_{m} \delta_{n} k_{mn}$$

Returns

GE [float] Excess Gibbs energy, [J/mol]

#### d2GE\_dT2()

Calculate and return the second temperature derivative of excess Gibbs energy of a liquid phas.

$$\frac{\partial^2 g^E}{\partial T^2} = 0$$

## Returns

 $d2GE_dT2$  [float] Second temperature derivative of excess Gibbs energy, [J/(mol\*K^2)]

## d2GE\_dTdxs()

Calculate and return the temperature derivative of mole fraction derivatives of excess Gibbs energy.

$$\frac{\partial^2 g^E}{\partial x_i \partial T} = 0$$

#### Returns

**d2GE\_dTdxs** [list[float]] Temperature derivative of mole fraction derivatives of excess Gibbs energy, [J/(mol\*K)]

# d2GE\_dxixjs()

Calculate and return the second mole fraction derivatives of excess Gibbs energy of a liquid phase using the regular solution model.

$$\frac{\partial^2 G^E}{\partial x_i \partial x_j} = \frac{V_j (V_i G^E - H_{ij})}{(\sum_m V_m x_m)^2} - \frac{V_i \frac{\partial G^E}{\partial x_j}}{\sum_m V_m x_m} + \frac{V_i V_j [\delta_i \delta_j (k_{ji} + k_{ij}) + (\delta_i - \delta_j)^2]}{\sum_m V_m x_m}$$

## Returns

**d2GE\_dxixjs** [list[list[float]]] Second mole fraction derivatives of excess Gibbs energy, [J/mol]

# d3GE\_dT3()

Calculate and return the third temperature derivative of excess Gibbs energy of a liquid phase.

$$\frac{\partial^3 g^E}{\partial T^3}=0$$

Returns

d3GE\_dT3 [float] Third temperature derivative of excess Gibbs energy, [J/(mol\*K^3)]

#### d3GE\_dxixjxks()

Calculate and return the third mole fraction derivatives of excess Gibbs energy.

$$\frac{\partial^3 G^E}{\partial x_i \partial x_j \partial x_k} = \frac{-2V_i V_j V_k G^E + 2V_j V_k H_{ij}}{(\sum_m V_m x_m)^3} + \frac{V_i \left(V_j \frac{\partial G^E}{\partial x_k} + V_k \frac{\partial G^E}{\partial x_j}\right)}{(\sum_m V_m x_m)^2} - \frac{V_i \frac{\partial^2 G^E}{\partial x_j \partial x_k}}{\sum_m V_m x_m} - \frac{V_i V_j V_k [\delta_i (\delta_j (k_{ij} + k_{ji}) + \delta_k (k_{ij} + k_$$

Returns

**d3GE\_dxixjxks** [list[list[float]]]] Third mole fraction derivatives of excess Gibbs energy, [J/mol]

 $dGE_dT()$ 

Calculate and return the temperature derivative of excess Gibbs energy of a liquid phase.

$$\frac{\partial g^E}{\partial T}=0$$

Returns

**dGE\_dT** [float] First temperature derivative of excess Gibbs energy, [J/(mol\*K)]

#### dGE\_dxs()

Calculate and return the mole fraction derivatives of excess Gibbs energy of a liquid phase using the regular solution model.

$$\frac{\partial G^E}{\partial x_i} = \frac{-V_i G^E + \sum_m V_i V_m x_m [\delta_i \delta_m (k_{mi} + k_{im}) + (\delta_i - \delta_m)^2]}{\sum_m V_m x_m}$$

Returns

dGE\_dxs [list[float]] Mole fraction derivatives of excess Gibbs energy, [J/mol]

# $to_T_xs(T, xs)$

Method to construct a new *RegularSolution* instance at temperature *T*, and mole fractions *xs* with the same parameters as the existing object.

## Parameters

T [float] Temperature, [K]

xs [list[float]] Mole fractions of each component, [-]

## Returns

obj [RegularSolution] New RegularSolution object at the specified conditions [-]

# 7.26.2 Regular Solution Regression Calculations

thermo.regular\_solution.regular\_solution\_gammas\_binaries(xs, Vs, SPs, Ts, lambda12, lambda21,

gammas=None)

Calculates activity coefficients with the regular solution model at fixed *lambda* values for a binary system at a series of mole fractions at specified temperatures. This is used for regression of *lambda* parameters. This function is highly optimized, and operates on multiple points at a time.

$$\ln \gamma_{1} = \frac{V_{1}\phi_{2}^{2}}{RT} \left[ (\mathbf{SP}_{1} - \mathbf{SP}_{2})^{2} + \lambda_{12}\mathbf{SP}_{1}\mathbf{SP}_{2} + \lambda_{21}\mathbf{SP}_{1}\mathbf{SP}_{2} \right]$$
$$\ln \gamma_{2} = \frac{V_{2}\phi_{1}^{2}}{RT} \left[ (\mathbf{SP}_{1} - \mathbf{SP}_{2})^{2} + \lambda_{12}\mathbf{SP}_{1}\mathbf{SP}_{2} + \lambda_{21}\mathbf{SP}_{1}\mathbf{SP}_{2} \right]$$
$$\phi_{1} = \frac{x_{1}V_{1}}{x_{1}V_{1} + x_{2}V_{2}}$$
$$\phi_{2} = \frac{x_{2}V_{2}}{x_{1}V_{1} + x_{2}V_{2}}$$

#### **Parameters**

**xs** [list[float]] Liquid mole fractions of each species in the format x0\_0, x1\_0, (component 1 point1, component 2 point 1), x0\_1, x1\_1, (component 1 point2, component 2 point 2), ... size pts\*2 [-]

- Vs [list[float]] Molar volumes of each of the two components, [m^3/mol]
- SPs [list[float]] Solubility parameters of each of the two components, [Pa^0.5]
- Ts [flist[float]] Temperatures of each composition point; half the length of xs, [K]
- lambda12 [float] lambda parameter for 12, [-]
- lambda21 [float] *lambda* parameter for 21, [-]
- gammas [list[float], optional] Array to store the activity coefficient for each species in the liquid mixture, indexed the same as xs; can be omitted or provided for slightly better performance [-]

#### Returns

gammas [list[float]] Activity coefficient for each species in the liquid mixture, indexed the same as xs, [-]

# **Examples**

```
>>> regular_solution_gammas_binaries([.1, .9, 0.3, 0.7, .85, .15], Vs=[7.421e-05, 8.
→068e-05], SPs=[19570.2, 18864.7], Ts=[300.0, 400.0, 500.0], lambda12=0.1759,
\rightarrowlambda21=0.7991)
[6818.90697, 1.105437, 62.6628, 2.01184, 1.181434, 137.6232]
```

copy

# 7.27 Streams (thermo.stream)

**class** thermo.stream.**EnergyStream**(Q, medium=None)

```
Bases: object
```

Attributes

Hm

Q

energy

energy\_calc

medium

# **Methods**

Hm = None	
Q = None	
copy()	
property energy	
<pre>property energy_calc</pre>	

medium = None

Bases: thermo.equilibrium.EquilibriumState

#### Attributes

CASs CAS registration numbers for each component, [-].

Carcinogens Status of each component in cancer causing registries, [-].

- **Ceilings** Ceiling exposure limits to chemicals (and their units; ppm or mg/m^3), [various].
- **EnthalpySublimations** Wrapper to obtain the list of EnthalpySublimations objects of the associated *PropertyCorrelationsPackage*.
- **EnthalpyVaporizations** Wrapper to obtain the list of EnthalpyVaporizations objects of the associated *PropertyCorrelationsPackage*.
- **GWPs** Global Warming Potentials for each component (impact/mass chemical)/(impact/mass CO2), [-].

**Gfgs** Ideal gas standard molar Gibbs free energy of formation for each component, [J/mol].

Gfgs\_mass Ideal gas standard Gibbs free energy of formation for each component, [J/kg].

**Hcs** Higher standard molar heats of combustion for each component, [J/mol].

Hcs\_lower Lower standard molar heats of combustion for each component, [J/mol].

- Hcs\_lower\_mass Lower standard heats of combustion for each component, [J/kg].
- **Hcs\_mass** Higher standard heats of combustion for each component, [J/kg].
- **HeatCapacityGasMixture** Wrapper to obtain the list of HeatCapacityGasMixture objects of the associated *PropertyCorrelationsPackage*.
- **HeatCapacityGases** Wrapper to obtain the list of HeatCapacityGases objects of the associated *PropertyCorrelationsPackage*.
- HeatCapacityLiquidMixture Wrapper to obtain the list of HeatCapacityLiquidMixture objects of the associated PropertyCorrelationsPackage.
- **HeatCapacityLiquids** Wrapper to obtain the list of HeatCapacityLiquids objects of the associated *PropertyCorrelationsPackage*.
- **HeatCapacitySolidMixture** Wrapper to obtain the list of HeatCapacitySolidMixture objects of the associated *PropertyCorrelationsPackage*.
- **HeatCapacitySolids** Wrapper to obtain the list of HeatCapacitySolids objects of the associated *PropertyCorrelationsPackage*.
- **Hf\_STPs** Standard state molar enthalpies of formation for each component, [J/mol].

Hf\_STPs\_mass Standard state mass enthalpies of formation for each component, [J/kg].

Hfgs Ideal gas standard molar enthalpies of formation for each component, [J/mol].

Hfgs\_mass Ideal gas standard enthalpies of formation for each component, [J/kg].

Hfus\_Tms Molar heats of fusion for each component at their respective melting points, [J/mol].

Hfus\_Tms\_mass Heats of fusion for each component at their respective melting points, [J/kg].

- Hsub\_Tts Heats of sublimation for each component at their respective triple points, [J/mol].
- Hsub\_Tts\_mass Heats of sublimation for each component at their respective triple points, [J/kg].
- Hvap\_298s Molar heats of vaporization for each component at 298.15 K, [J/mol].
- Hvap\_298s\_mass Heats of vaporization for each component at 298.15 K, [J/kg].
- Hvap\_Tbs Molar heats of vaporization for each component at their respective normal boiling points, [J/mol].
- Hvap\_Tbs\_mass Heats of vaporization for each component at their respective normal boiling points, [J/kg].

IDs Alias of CASs.

InChI\_Keys InChI Keys for each component, [-].

InChIs InChI strings for each component, [-].

**LF** Method to return the liquid fraction of the equilibrium state.

LFLs Lower flammability limits for each component, [-].

MWs Similatiry variables for each component, [g/mol].

**ODPs** Ozone Depletion Potentials for each component (impact/mass chemical)/(impact/mass CFC-11), [-].

**PSRK\_groups** PSRK subgroup: count groups for each component, [-].

P\_calc

Parachors Parachors for each component, [N^0.25\*m^2.75/mol].

**Pcs** Critical pressures for each component, [Pa].

**PermittivityLiquids** Wrapper to obtain the list of PermittivityLiquids objects of the associated *PropertyCorrelationsPackage*.

Psat\_298s Vapor pressures for each component at 298.15 K, [Pa].

Pts Triple point pressures for each component, [Pa].

PubChems Pubchem IDs for each component, [-].

Q

Q\_calc

Qgs

Qgs\_calc

Qls

Qls\_calc

**RI\_Ts** Temperatures at which the refractive indexes were reported for each component, [K].

**RIs** Refractive indexes for each component, [-].

**S0gs** Ideal gas absolute molar entropies at 298.15 K at 1 atm for each component, [J/(mol\*K)].

S0gs\_mass Ideal gas absolute entropies at 298.15 K at 1 atm for each component, [J/(kg\*K)].

STELS Short term exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

**Sfgs** Ideal gas standard molar entropies of formation for each component, [J/(mol\*K)].

**Sfgs\_mass** Ideal gas standard entropies of formation for each component, [J/(kg\*K)].

Skins Whether each compound can be absorbed through the skin or not, [-].

- StielPolars Stiel polar factors for each component, [-].
- **Stockmayers** Lennard-Jones Stockmayer parameters (depth of potential-energy minimum over k) for each component, [K].
- **SublimationPressures** Wrapper to obtain the list of SublimationPressures objects of the associated *PropertyCorrelationsPackage*.
- **SurfaceTensionMixture** Wrapper to obtain the list of SurfaceTensionMixture objects of the associated *PropertyCorrelationsPackage*.
- **SurfaceTensions** Wrapper to obtain the list of SurfaceTensions objects of the associated *PropertyCorrelationsPackage*.
- **TWAS** Time-weighted average exposure limits to chemicals (and their units; ppm or mg/m^3), [various].

T\_calc

**Tautoignitions** Autoignition temperatures for each component, [K].

- Tbs Boiling temperatures for each component, [K].
- Tcs Critical temperatures for each component, [K].

Tflashs Flash point temperatures for each component, [K].

- **ThermalConductivityGasMixture** Wrapper to obtain the list of ThermalConductivityGas-Mixture objects of the associated *PropertyCorrelationsPackage*.
- **ThermalConductivityGases** Wrapper to obtain the list of ThermalConductivityGases objects of the associated *PropertyCorrelationsPackage*.
- **ThermalConductivityLiquidMixture** Wrapper to obtain the list of ThermalConductivityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- **ThermalConductivityLiquids** Wrapper to obtain the list of ThermalConductivityLiquids objects of the associated *PropertyCorrelationsPackage*.
- Tms Melting temperatures for each component, [K].
- **Tts** Triple point temperatures for each component, [K].
- **UFLs** Upper flammability limits for each component, [-].
- **UNIFAC\_Dortmund\_groups** UNIFAC\_Dortmund\_group: count groups for each component, [-].
- **UNIFAC\_Qs** UNIFAC *Q* parameters for each component, [-].
- **UNIFAC\_Rs** UNIFAC *R* parameters for each component, [-].

UNIFAC\_groups UNIFAC\_group: count groups for each component, [-].

**VF** Method to return the vapor fraction of the equilibrium state.

VF\_calc

Van\_der\_Waals\_areas Unnormalized Van der Waals areas for each component, [m^2/mol].

Van\_der\_Waals\_volumes Unnormalized Van der Waals volumes for each component, [m^3/mol].

- **VaporPressures** Wrapper to obtain the list of VaporPressures objects of the associated *PropertyCorrelationsPackage*.
- Vcs Critical molar volumes for each component, [m<sup>3</sup>/mol].
- **ViscosityGasMixture** Wrapper to obtain the list of ViscosityGasMixture objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityGases** Wrapper to obtain the list of ViscosityGases objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityLiquidMixture** Wrapper to obtain the list of ViscosityLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- **ViscosityLiquids** Wrapper to obtain the list of ViscosityLiquids objects of the associated *PropertyCorrelationsPackage*.
- Vmg\_STPs Gas molar volumes for each component at STP; metastable if normally another state, [m^3/mol].
- Vml\_60Fs Liquid molar volumes for each component at 60 °F, [m^3/mol].
- Vml\_STPs Liquid molar volumes for each component at STP, [m^3/mol].
- Vml\_Tms Liquid molar volumes for each component at their respective melting points, [m^3/mol].
- Vms\_Tms Solid molar volumes for each component at their respective melting points, [m^3/mol].
- **VolumeGasMixture** Wrapper to obtain the list of VolumeGasMixture objects of the associated *PropertyCorrelationsPackage*.
- **VolumeGases** Wrapper to obtain the list of VolumeGases objects of the associated *PropertyCorrelationsPackage*.
- **VolumeLiquidMixture** Wrapper to obtain the list of VolumeLiquidMixture objects of the associated *PropertyCorrelationsPackage*.
- **VolumeLiquids** Wrapper to obtain the list of VolumeLiquids objects of the associated *PropertyCorrelationsPackage*.
- **VolumeSolidMixture** Wrapper to obtain the list of VolumeSolidMixture objects of the associated *PropertyCorrelationsPackage*.
- **VolumeSolids** Wrapper to obtain the list of VolumeSolids objects of the associated *PropertyCorrelationsPackage*.
- **Zcs** Critical compressibilities for each component, [-].
- atomss Breakdown of each component into its elements and their counts, as a dict, [-].
- **betas\_liquids** Method to calculate and return the fraction of the liquid phase that each liquid phase is, by molar phase fraction.
- **betas\_mass** Method to calculate and return the mass fraction of all of the phases in the system.
- **betas\_mass\_liquids** Method to calculate and return the fraction of the liquid phase that each liquid phase is, by mass phase fraction.
- **betas\_mass\_states** Method to return the mass phase fractions of each of the three fundamental *types* of phases.
- **betas\_states** Method to return the molar phase fractions of each of the three fundamental *types* of phases.

- **betas\_volume** Method to calculate and return the volume fraction of all of the phases in the system.
- **betas\_volume\_liquids** Method to calculate and return the fraction of the liquid phase that each liquid phase is, by volume phase fraction.
- **betas\_volume\_states** Method to return the volume phase fractions of each of the three fundamental *types* of phases.

charges Charge number (valence) for each component, [-].

composition\_specified Always needs a composition

- conductivities Electrical conductivities for each component, [S/m].
- **conductivity\_Ts** Temperatures at which the electrical conductivities for each component were measured, [K].
- dipoles Dipole moments for each component, [debye].
- **economic\_statuses** Status of each component in in relation to import and export from various regions, [-].

energy

energy\_calc

energy\_reactive

energy\_reactive\_calc

**flow\_specified** Always needs a flow specified

formulas Formulas of each component, [-].

heaviest\_liquid The liquid-like phase with the highest mass density, [-]

legal\_statuses Status of each component in in relation to import and export rules from various regions, [-].

**lightest\_liquid** The liquid-like phase with the lowest mass density, [-]

liquid\_bulk

logPs Octanol-water partition coefficients for each component, [-].

**molecular\_diameters** Lennard-Jones molecular diameters for each component, [angstrom].

ms\_calc

n\_calc

names Names for each component, [-].

**non\_pressure\_spec\_specified** Cannot have a stream without an energy-type spec.

ns\_calc

omegas Acentric factors for each component, [-].

**phase** Method to calculate and return a string representing the phase of the mixture.

phase\_STPs Standard states ('g', 'l', or 's') for each component, [-].

property\_package

**quality** Method to return the mass vapor fraction of the equilibrium state.

**rhocs** Molar densities at the critical point for each component, [mol/m<sup>3</sup>].

**rhocs\_mass** Densities at the critical point for each component, [kg/m<sup>3</sup>].

- **rhog\_STPs** Molar gas densities at STP for each component; metastable if normally another state, [mol/m^3].
- **rhog\_STPs\_mass** Gas densities at STP for each component; metastable if normally another state, [kg/m<sup>3</sup>].
- rhol\_60Fs Liquid molar densities for each component at 60 °F, [mol/m^3].
- rhol\_60Fs\_mass Liquid mass densities for each component at 60 °F, [kg/m^3].
- rhol\_STPs Molar liquid densities at STP for each component, [mol/m^3].
- rhol\_STPs\_mass Liquid densities at STP for each component, [kg/m^3].
- **rhos\_Tms** Solid molar densities for each component at their respective melting points, [mol/m^3].
- **rhos\_Tms\_mass** Solid mass densities for each component at their melting point, [kg/m^3].
- **sigma\_STPs** Liquid-air surface tensions at 298.15 K and the higher of 101325 Pa or the saturation pressure, [N/m].
- **sigma\_Tbs** Liquid-air surface tensions at the normal boiling point and 101325 Pa, [N/m].
- sigma\_Tms Liquid-air surface tensions at the melting point and 101325 Pa, [N/m].

**similarity\_variables** Similarity variables for each component, [mol/g].

smiless SMILES identifiers for each component, [-].

solid\_bulk

solubility\_parameters Solubility parameters for each component at 298.15 K, [Pa^0.5].

specified\_composition\_vars number of composition variables

specified\_flow\_vars Always needs only one flow specified

- specified\_state\_vars Always needs two states
- state\_specified Always needs a state
- *state\_specs* Returns a list of tuples of (state\_variable, state\_value) representing the thermodynamic state of the system.

water\_index The index of the component water in the components.

water\_phase The liquid-like phase with the highest water mole fraction, [-]

water\_phase\_index The liquid-like phase with the highest mole fraction of water, [-]
zs calc

# **Methods**

A()	Method to calculate and return the Helmholtz energy
	of the phase.
API([phase])	Method to calculate and return the API of the phase.
A_dep()	Method to calculate and return the departure
	Helmholtz energy of the phase.

Table 90 – contin	nued from previous page
A_formation_ideal_gas([phase])	Method to calculate and return the ideal-gas
	Helmholtz energy of formation of the phase (as if
	the phase was an ideal gas).
A_ideal_gas([phase])	Method to calculate and return the ideal-gas
	Helmholtz energy of the phase.
A_mass([phase])	Method to calculate and return mass Helmholtz en-
	ergy of the phase.
A_reactive()	Method to calculate and return the Helmholtz free en-
	ergy of the phase on a reactive basis.
Bvirial([phase])	Method to calculate and return the <i>B</i> virial coefficient
bvii iui([phuse])	of the phase at its current conditions.
Cp()	Method to calculate and return the constant-
Ср()	temperature and constant phase-fraction heat
	capacity of the bulk phase.
Cp_Cv_ratio()	Method to calculate and return the Cp/Cv ratio of the
	phase.
<pre>Cp_Cv_ratio_ideal_gas([phase])</pre>	Method to calculate and return the ratio of the ideal-
	gas heat capacity to its constant-volume heat capac-
	ity.
Cp_dep([phase])	Method to calculate and return the difference between
	the actual $Cp$ and the ideal-gas heat capacity $C_p^{ig}$ of
	the phase.
<pre>Cp_ideal_gas([phase])</pre>	Method to calculate and return the ideal-gas heat ca-
	pacity of the phase.
Cp_mass([phase])	Method to calculate and return mass constant pres-
	sure heat capacity of the phase.
Cv()	Method to calculate and return the constant-volume
	heat capacity Cv of the phase.
Cv_dep([phase])	Method to calculate and return the difference between
	the actual Cv and the ideal-gas constant volume heat
	capacity $C_v^{ig}$ of the phase.
Cv_ideal_gas([phase])	Method to calculate and return the ideal-gas constant
-	volume heat capacity of the phase.
Cv_mass([phase])	Method to calculate and return mass constant volume
	heat capacity of the phase.
G()	Method to calculate and return the Gibbs free energy
	of the phase.
G_dep()	Method to calculate and return the departure Gibbs
	free energy of the phase.
G_formation_ideal_gas([phase])	Method to calculate and return the ideal-gas Gibbs
	free energy of formation of the phase (as if the phase
	was an ideal gas).
G_ideal_gas([phase])	Method to calculate and return the ideal-gas Gibbs
d_iucui_gub([phuse])	free energy of the phase.
G_mass([phase])	Method to calculate and return mass Gibbs energy of
-mess([pnuse])	the phase.
G_reactive()	-
G_TEACLIVE()	Method to calculate and return the Gibbs free energy
що	of the phase on a reactive basis.
H()	Method to calculate and return the constant-
	temperature and constant phase-fraction enthalpy of
	the bulk phase.
	continues on next page

Table	90 – continued	from	previous	page

Method to calculate and return the atomic ratio of hy- drogen atoms to carbon atoms, based on the current composition of the phase. Method to calculate and return the mass ratio of hy- drogen atoms to carbon atoms, based on the current composition of the phase. Method to calculate and return the difference between the actual <i>H</i> and the ideal-gas enthalpy of the phase. Method to calculate and return the ideal-gas enthalpy of formation of the phase (as if the phase was an ideal gas). Method to calculate and return the ideal-gas enthalpy of the phase. Method to calculate and return mass enthalpy of the phase. Method to calculate and return mass enthalpy of the phase.
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Method to calculate and return the mass ratio of hy- drogen atoms to carbon atoms, based on the current composition of the phase. Method to calculate and return the difference between the actual <i>H</i> and the ideal-gas enthalpy of the phase. Method to calculate and return the ideal-gas enthalpy of formation of the phase (as if the phase was an ideal gas). Method to calculate and return the ideal-gas enthalpy of the phase. Method to calculate and return the ideal-gas enthalpy of the phase.
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of the phase. Method to calculate and return mass enthalpy of the phase.
Method to calculate and return mass enthalpy of the phase.
phase.
-
include to curculate and retain the constant
temperature and constant phase-fraction reactive
enthalpy of the bulk phase.
Method to calculate and return the molar ideal-gas
higher heat of combustion of the object, [J/mol]
Method to calculate and return the molar ideal-gas
lower heat of combustion of the object, [J/mol]
Method to calculate and return the mass ideal-gas
lower heat of combustion of the object, [J/mol]
Method to calculate and return the volumetric ideal-
gas lower heat of combustion of the object using the
normal gas volume, [J/m^3]
Method to calculate and return the volumetric ideal-
gas lower heat of combustion of the object using the standard gas volume $[I(m \triangle 3)]$
standard gas volume, [J/m <sup>3</sup> ] Method to calculate and return the mass ideal-gas
•
higher heat of combustion of the object, [J/mol] Method to calculate and return the volumetric ideal-
gas higher heat of combustion of the object using the
normal gas volume, [J/m^3]
Method to calculate and return the volumetric ideal-
gas higher heat of combustion of the object using the
standard gas volume, [J/m^3]
Method to calculate and return the Joule-Thomson
coefficient of the bulk according to the selected cal-
culation methodology.
Method to calculate and return the K-values of each
phase.
Method to calculate and return the molecular weight
of the phase.
Method to calculate and return the phase identifica-
tion parameter of the phase.
Method to calculate and return the mechanical criti-
cal pressure of the phase.

Table 90 – continu	led from previous page
- S()	Method to calculate and return the constant-
	temperature and constant phase-fraction entropy of
	the bulk phase.
SG([phase])	Method to calculate and return the standard liquid
	specific gravity of the phase, using constant liquid
	pure component densities not calculated by the phase
	object, at 60 °F.
SG_gas([phase])	Method to calculate and return the specific gravity of
	the phase with respect to a gas reference density.
S_dep([phase])	Method to calculate and return the difference between
-	the actual S and the ideal-gas entropy of the phase.
S_formation_ideal_gas([phase])	Method to calculate and return the ideal-gas entropy
	of formation of the phase (as if the phase was an ideal
	gas).
S_ideal_gas([phase])	Method to calculate and return the ideal-gas entropy
	of the phase.
S_mass([phase])	Method to calculate and return mass entropy of the
- · (rt · · · · · )	phase.
S_reactive()	Method to calculate and return the constant-
	temperature and constant phase-fraction reactive
	entropy of the bulk phase.
StreamArgs()	Goal to create a StreamArgs instance, with the user
Streaming go()	specified variables always being here.
Tmc([phase])	Method to calculate and return the mechanical criti-
	cal temperature of the phase.
U()	Method to calculate and return the internal energy of
	the phase.
U_dep()	Method to calculate and return the departure internal
	energy of the phase.
U_formation_ideal_gas([phase])	Method to calculate and return the ideal-gas internal
o_ioimacion_iacai_gao([phase])	energy of formation of the phase (as if the phase was
	an ideal gas).
U_ideal_gas([phase])	Method to calculate and return the ideal-gas internal
o_iucui_guo([pinuse])	energy of the phase.
U_mass([phase])	Method to calculate and return mass internal energy
	of the phase.
U_reactive()	Method to calculate and return the internal energy of
0_leactive()	the phase on a reactive basis.
<u>V()</u>	Method to calculate and return the molar volume of
۲U	the bulk phase.
V_dep()	Method to calculate and return the departure (from
1_ucp()	ideal gas behavior) molar volume of the phase.
V_gas([phase])	Method to calculate and return the ideal-gas molar
-Sac([humo])	volume of the phase at the chosen reference tempera-
	ture and pressure, according to the temperature vari-
	able $T_{gas\_ref}$ and pressure variable $P_{gas\_ref}$ of
	the thermo.bulk.BulkSettings.
	continues on next page

Table 90 – continu	ed from previous page
V_gas_normal([phase])	Method to calculate and return the ideal-gas mo-
	lar volume of the phase at the normal temperature
	and pressure, according to the temperature variable
	$T_normal$ and pressure variable $P_normal$ of the
	thermo.bulk.BulkSettings.
V_gas_standard([phase])	Method to calculate and return the ideal-gas mo-
	lar volume of the phase at the standard temperature
	and pressure, according to the temperature variable
	$T_{standard}$ and pressure variable $P_{standard}$ of the
	thermo.bulk.BulkSettings.
V_ideal_gas([phase])	Method to calculate and return the ideal-gas molar
	volume of the phase.
V_iter([phase, force])	Method to calculate and return the volume of the
v_itei([phase, loice])	phase in a way suitable for a TV resolution to con-
	verge on the same pressure.
V_liquid_ref([phase])	Method to calculate and return the liquid refer-
v_11qu1d_rer([pnase])	-
	ence molar volume according to the temperature
	variable <i>T_liquid_volume_ref</i> of thermo.bulk.
	BulkSettings and the composition of the phase.
<pre>V_liquids_ref()</pre>	Method to calculate and return the liquid refer-
	ence molar volumes according to the temperature
	variable <i>T_liquid_volume_ref</i> of thermo.bulk.
	BulkSettings.
V_mass([phase])	Method to calculate and return the specific volume of
	the phase.
Vfgs([phase])	Method to calculate and return the ideal-gas volume
	fractions of the components of the phase.
Vfls([phase])	Method to calculate and return the ideal-liquid vol-
	ume fractions of the components of the phase,
	using the standard liquid densities at the tem-
	perature variable <i>T_liquid_volume_ref</i> of thermo.
	bulk.BulkSettings and the composition of the
	phase.
Vmc([phase])	Method to calculate and return the mechanical criti-
	cal volume of the phase.
Wobbe_index([phase])	Method to calculate and return the molar Wobbe in-
	dex of the object, [J/mol].
<pre>Wobbe_index_lower([phase])</pre>	Method to calculate and return the molar lower
	Wobbe index of the
Wobbe_index_lower_mass([phase])	Method to calculate and return the lower mass Wobbe
	index of the object, [J/kg].
<pre>Wobbe_index_lower_normal([phase])</pre>	Method to calculate and return the volumetric normal
(If	lower Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_lower_standard([phase])</pre>	Method to calculate and return the volumetric stan-
	dard lower Wobbe index of the object, [J/m^3].
<pre>Wobbe_index_mass([phase])</pre>	Method to calculate and return the mass Wobbe index
"oose_rimes_mass([pimee])	of the object, [J/kg].
<pre>Wobbe_index_normal([phase])</pre>	Method to calculate and return the volumetric normal
$modde_timer_iotimat([himse])$	
Wohho indox standand([nhasa])	Wobbe index of the object, [J/m^3].           Method to calculate and return the volumetric stan-
<pre>Wobbe_index_standard([phase])</pre>	
	dard Wobbe index of the object, [J/m^3].
	continues on next page

	nued from previous page
Z()	Method to calculate and return the compressibility
	factor of the phase.
Zmc([phase])	Method to calculate and return the mechanical criti-
	cal compressibility of the phase.
alpha([phase])	Method to calculate and return the thermal diffusivity
	of the equilibrium state.
atom_fractions([phase])	Method to calculate and return the atomic composi-
	tion of the phase; returns a dictionary of atom frac-
	tion (by count), containing only those elements who
	are present.
<pre>atom_mass_fractions([phase])</pre>	Method to calculate and return the atomic mass frac-
	tions of the phase; returns a dictionary of atom frac-
	tion (by mass), containing only those elements who
	are present.
d2P_dT2()	Method to calculate and return the second tempera-
	ture derivative of pressure of the bulk according to
	the selected calculation methodology.
d2P_dT2_frozen()	Method to calculate and return the second constant-
v	volume derivative of pressure with respect to temper-
	ature of the bulk phase, at constant phase fractions
	and phase compositions.
d2P_dTdV()	Method to calculate and return the second deriva-
V	tive of pressure with respect to temperature and vol-
	ume of the bulk according to the selected calculation
	methodology.
d2P_dTdV_frozen()	Method to calculate and return the second derivative
	of pressure with respect to volume and temperature of
	the bulk phase, at constant phase fractions and phase
	compositions.
d2P_dV2()	Method to calculate and return the second volume
	derivative of pressure of the bulk according to the se-
	lected calculation methodology.
d2P_dV2_frozen()	Method to calculate and return the constant-
v	temperature second derivative of pressure with
	respect to volume of the bulk phase, at constant
	phase fractions and phase compositions.
dA_dP()	Method to calculate and return the constant-
~	temperature pressure derivative of Helmholtz
	energy.
dA_dP_T()	Method to calculate and return the constant-
0	temperature pressure derivative of Helmholtz
	energy.
dA_dP_V()	Method to calculate and return the constant-volume
v	pressure derivative of Helmholtz energy.
dA_dT()	Method to calculate and return the constant-pressure
	temperature derivative of Helmholtz energy.
dA_dT_P()	Method to calculate and return the constant-pressure
	temperature derivative of Helmholtz energy.
dA_dT_V()	Method to calculate and return the constant-volume
un_u1_v()	memore to calculate and return the constant-volume
	temperature derivative of Helmholtz energy.

Table 90 – c	continued from previous page
dA_dV_P()	Method to calculate and return the constant-pressure
	volume derivative of Helmholtz energy.
dA_dV_T()	Method to calculate and return the constant-
V	temperature volume derivative of Helmholtz energy.
dA_mass_dP()	Method to calculate and return the pressure derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
dA_mass_dP_T()	Method to calculate and return the pressure derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
dA_mass_dP_V()	Method to calculate and return the pressure derivative
	of mass Helmholtz energy of the phase at constant
	volume.
dA_mass_dT()	Method to calculate and return the temperature
uA_mass_u1()	derivative of mass Helmholtz energy of the phase at
dA mass dT D()	constant pressure.
dA_mass_dT_P()	Method to calculate and return the temperature derivative of mass Helmholtz energy of the phase at
	constant pressure.
dA_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass Helmholtz energy of the phase at
	constant volume.
dA_mass_dV_P()	Method to calculate and return the volume derivative
	of mass Helmholtz energy of the phase at constant
	pressure.
dA_mass_dV_T()	Method to calculate and return the volume derivative
	of mass Helmholtz energy of the phase at constant
	temperature.
dCv_dP_T()	Method to calculate the pressure derivative of Cv,
	constant volume heat capacity, at constant tempera-
	ture.
dCv_dT_P()	Method to calculate the temperature derivative of Cv,
	constant volume heat capacity, at constant pressure.
dCv_mass_dP_T()	Method to calculate and return the pressure derivative
	of mass Constant-volume heat capacity of the phase
	at constant temperature.
dCv_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass Constant-volume heat capacity of
	the phase at constant pressure.
dG_dP()	Method to calculate and return the constant-
	temperature pressure derivative of Gibbs free
	energy.
dG_dP_T()	Method to calculate and return the constant-
	temperature pressure derivative of Gibbs free
	energy.
dG_dP_V()	Method to calculate and return the constant-volume
	pressure derivative of Gibbs free energy.
dG_dT()	Method to calculate and return the constant-pressure
-	temperature derivative of Gibbs free energy.
dG_dT_P()	Method to calculate and return the constant-pressure
	temperature derivative of Gibbs free energy.
	continues on next page

Table 90	) – continued from previous page
$dG_dT_V()$	Method to calculate and return the constant-volume
	temperature derivative of Gibbs free energy.
dG_dV_P()	Method to calculate and return the constant-pressure
	volume derivative of Gibbs free energy.
dG_dV_T()	Method to calculate and return the constant-
	temperature volume derivative of Gibbs free energy.
dG_mass_dP()	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dG_mass_dP_T()	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dG_mass_dP_V()	Method to calculate and return the pressure derivative
	of mass Gibbs free energy of the phase at constant
	volume.
dG_mass_dT()	Method to calculate and return the temperature
uu_mass_ui()	
	derivative of mass Gibbs free energy of the phase at
	constant pressure.
dG_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant pressure.
dG_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass Gibbs free energy of the phase at
	constant volume.
dG_mass_dV_P()	Method to calculate and return the volume derivative
	of mass Gibbs free energy of the phase at constant
	pressure.
dG_mass_dV_T()	Method to calculate and return the volume derivative
	of mass Gibbs free energy of the phase at constant
	temperature.
dH_dP()	Method to calculate and return the pressure derivative
	of enthalpy of the phase at constant pressure.
dH_dP_T()	Method to calculate and return the pressure derivative
	of enthalpy of the phase at constant pressure.
dH_dT()	Method to calculate and return the constant-
	temperature and constant phase-fraction heat
	capacity of the bulk phase.
dH_dT_P()	Method to calculate and return the temperature
	derivative of enthalpy of the phase at constant pres-
	sure.
dH_mass_dP()	Method to calculate and return the pressure deriva-
un_mass_ur()	tive of mass enthalpy of the phase at constant tem-
	perature.
dH_mass_dP_T()	Method to calculate and return the pressure deriva-
	tive of mass enthalpy of the phase at constant tem-
	perature.
dH_mass_dP_V()	Method to calculate and return the pressure derivative
	of mass enthalpy of the phase at constant volume.
	Method to calculate and return the temperature
dH_mass_dT()	Method to calculate and return the temperature
dH_mass_dT()	derivative of mass enthalpy of the phase at constant

Table 90 – continued from previous page

Table 90	) – continued from previous page
dH_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass enthalpy of the phase at constant
	pressure.
dH_mass_dT_V()	Method to calculate and return the temperature
~	derivative of mass enthalpy of the phase at constant
	volume.
dH_mass_dV_P()	Method to calculate and return the volume derivative
	of mass enthalpy of the phase at constant pressure.
dH_mass_dV_T()	Method to calculate and return the volume derivative
	of mass enthalpy of the phase at constant tempera-
	ture.
$dP_dP_A()$	Method to calculate and return the pressure derivative
	of pressure of the phase at constant Helmholtz energy.
$dP_dP_G()$	Method to calculate and return the pressure derivative
	of pressure of the phase at constant Gibbs energy.
dP_dP_H()	Method to calculate and return the pressure derivative
	of pressure of the phase at constant enthalpy.
$dP_dP_S()$	Method to calculate and return the pressure derivative
	of pressure of the phase at constant entropy.
dP_dP_U()	Method to calculate and return the pressure derivative
	of pressure of the phase at constant internal energy.
dP_dT()	Method to calculate and return the first temperature
	derivative of pressure of the bulk according to the se-
	lected calculation methodology.
$dP_dT_A()$	Method to calculate and return the temperature
`	derivative of pressure of the phase at constant
	Helmholtz energy.
dP_dT_G()	Method to calculate and return the temperature
	derivative of pressure of the phase at constant Gibbs
	energy.
dP_dT_H()	Method to calculate and return the temperature
	derivative of pressure of the phase at constant en-
	thalpy.
dP_dT_S()	Method to calculate and return the temperature
ur_u1_3()	-
	derivative of pressure of the phase at constant en-
ער דו א	tropy.
dP_dT_U()	Method to calculate and return the temperature
	derivative of pressure of the phase at constant internal
	energy.
dP_dT_frozen()	Method to calculate and return the constant-volume
	derivative of pressure with respect to temperature of
	the bulk phase, at constant phase fractions and phase
	compositions.
dP_dV()	Method to calculate and return the first volume
	derivative of pressure of the bulk according to the se-
	lected calculation methodology.
$dP_dV_A()$	Method to calculate and return the volume derivative
	of pressure of the phase at constant Helmholtz energy.
$dP_dV_G()$	Method to calculate and return the volume derivative
-	of pressure of the phase at constant Gibbs energy.
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Table 90 – cont	inued from previous page
dP_dV_H()	Method to calculate and return the volume derivative
	of pressure of the phase at constant enthalpy.
dP_dV_S()	Method to calculate and return the volume derivative
	of pressure of the phase at constant entropy.
dP_dV_U()	Method to calculate and return the volume derivative
V	of pressure of the phase at constant internal energy.
dP_dV_frozen()	Method to calculate and return the constant-
	temperature derivative of pressure with respect to
	volume of the bulk phase, at constant phase fractions
	and phase compositions.
dP_drho_A()	Method to calculate and return the density derivative
	of pressure of the phase at constant Helmholtz energy.
dP_drho_G()	Method to calculate and return the density derivative
	of pressure of the phase at constant Gibbs energy.
dP_drho_H()	Method to calculate and return the density derivative
	of pressure of the phase at constant enthalpy.
dP_drho_S()	Method to calculate and return the density derivative
ur_ur110_3()	of pressure of the phase at constant entropy.
dP_drho_U()	
	Method to calculate and return the density derivative
	of pressure of the phase at constant internal energy.
dS_dP()	Method to calculate and return the pressure derivative
	of entropy of the phase at constant pressure.
dS_dP_T()	Method to calculate and return the pressure derivative
	of entropy of the phase at constant pressure.
dS_dV_P()	Method to calculate and return the volume derivative
	of entropy of the phase at constant pressure.
dS_dV_T()	Method to calculate and return the volume derivative
	of entropy of the phase at constant temperature.
dS_mass_dP()	Method to calculate and return the pressure derivative
	of mass entropy of the phase at constant temperature.
dS_mass_dP_T()	Method to calculate and return the pressure derivative
	of mass entropy of the phase at constant temperature.
dS_mass_dP_V()	Method to calculate and return the pressure derivative
	of mass entropy of the phase at constant volume.
dS_mass_dT()	Method to calculate and return the temperature
	derivative of mass entropy of the phase at constant
	pressure.
dS_mass_dT_P()	Method to calculate and return the temperature
	derivative of mass entropy of the phase at constant
	pressure.
dS_mass_dT_V()	Method to calculate and return the temperature
	derivative of mass entropy of the phase at constant
	volume.
dS_mass_dV_P()	Method to calculate and return the volume derivative
	of mass entropy of the phase at constant pressure.
dS_mass_dV_T()	Method to calculate and return the volume derivative
	of mass entropy of the phase at constant temperature.
dT_dP_A()	Method to calculate and return the pressure derivative
~	of temperature of the phase at constant Helmholtz en-
	ergy.
	continues on next page

Table 90 – continued from previous page

dT_dP_G()       Method to calculate and return the pressure derivative of temperature of the phase at constant Gibbs energy.         dT_dP_B()       Method to calculate and return the pressure derivative of temperature of the phase at constant entalpy.         dT_dP_U()       Method to calculate and return the pressure derivative of temperature of the phase at constant internal energy.         dT_dP_U()       Method to calculate and return the pressure derivative of temperature of the phase at constant internal energy.         dT_dT_A()       Method to calculate and return the temperature derivative of temperature of the phase at constant internal energy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant fleinholtz energy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant enthalpy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant enthalpy.         dT_dT_U()       Method to calculate and return the temperature derivative of temperature of the phase at constant enthalpy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant entimpy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant entimpy.         dT_dT_G()       Method to calculate and return the temperature derivative of temperature of the phase at constant internal energy.	Table 90 -	<ul> <li>continued from previous page</li> </ul>
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	dU_dP()	Method to calculate and return the constant-
continues on next page		temperature pressure derivative of internal energy.
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Table	90 – continued from previous page
dU_dP_T()	Method to calculate and return the constant-
	temperature pressure derivative of internal energy.
dU_dP_V()	Method to calculate and return the constant-volume
0	pressure derivative of internal energy.
dU_dT()	Method to calculate and return the constant-pressure
	temperature derivative of internal energy.
dU_dT_P()	Method to calculate and return the constant-pressure
u0_u1_P()	-
	temperature derivative of internal energy.
dU_dT_V()	Method to calculate and return the constant-volume
	temperature derivative of internal energy.
$dU_dV_P()$	Method to calculate and return the constant-pressure
	volume derivative of internal energy.
dU_dV_T()	Method to calculate and return the constant-
	temperature volume derivative of internal energy.
dU_mass_dP()	Method to calculate and return the pressure deriva-
~	tive of mass internal energy of the phase at constant
	temperature.
dU_mass_dP_T()	Method to calculate and return the pressure deriva-
uo_muoo_ur_1()	tive of mass internal energy of the phase at constant
	temperature.
dU_mass_dP_V()	Method to calculate and return the pressure deriva-
	tive of mass internal energy of the phase at constant
	volume.
dU_mass_dT()	Method to calculate and return the temperature
	derivative of mass internal energy of the phase at con-
	stant pressure.
dU_mass_dT_P()	Method to calculate and return the temperature
~	derivative of mass internal energy of the phase at con-
	stant pressure.
dU_mass_dT_V()	Method to calculate and return the temperature
uo_muoo_ur_v()	derivative of mass internal energy of the phase at con-
	stant volume.
dU_mass_dV_P()	Method to calculate and return the volume derivative
uo_mass_uv_r()	
	of mass internal energy of the phase at constant pres-
··· · · · ·	sure.
dU_mass_dV_T()	Method to calculate and return the volume derivative
	of mass internal energy of the phase at constant tem-
	perature.
$dV_dP_A()$	Method to calculate and return the pressure derivative
	of volume of the phase at constant Helmholtz energy.
dV_dP_G()	Method to calculate and return the pressure derivative
	of volume of the phase at constant Gibbs energy.
dV_dP_H()	Method to calculate and return the pressure derivative
	of volume of the phase at constant enthalpy.
dV_dP_S()	Method to calculate and return the pressure derivative
u, _ui _5()	of volume of the phase at constant entropy.
dV_dP_U()	Method to calculate and return the pressure derivative
	of volume of the phase at constant internal energy.
dV_dT_A()	Method to calculate and return the temperature
	derivative of volume of the phase at constant
	Helmholtz energy.
	continues on next page

Table	90 - continued from	m previous	nad
Table	30 - continued not	ii pievious	pay

Table	90 – continued from previous page
dV_dT_G()	Method to calculate and return the temperature
	derivative of volume of the phase at constant Gibbs
	energy.
dV_dT_H()	Method to calculate and return the temperature
···	derivative of volume of the phase at constant en-
	thalpy.
dV_dT_S()	Method to calculate and return the temperature
uv_u1_5()	derivative of volume of the phase at constant entropy.
dV_dT_U()	Method to calculate and return the temperature
uv_u1_0()	derivative of volume of the phase at constant inter-
	nal energy.
dV_dV_A()	Method to calculate and return the volume derivative
	of volume of the phase at constant Helmholtz energy. Method to calculate and return the volume derivative
$dV_dV_G()$	
	of volume of the phase at constant Gibbs energy.
dV_dV_H()	Method to calculate and return the volume derivative
	of volume of the phase at constant enthalpy. Method to calculate and return the volume derivative
dV_dV_S()	
1	of volume of the phase at constant entropy.
dV_dV_U()	Method to calculate and return the volume derivative
	of volume of the phase at constant internal energy.
dV_drho_A()	Method to calculate and return the density derivative
	of volume of the phase at constant Helmholtz energy.
dV_drho_G()	Method to calculate and return the density derivative
	of volume of the phase at constant Gibbs energy.
dV_drho_H()	Method to calculate and return the density derivative
	of volume of the phase at constant enthalpy.
dV_drho_S()	Method to calculate and return the density derivative
	of volume of the phase at constant entropy.
dV_drho_U()	Method to calculate and return the density derivative
	of volume of the phase at constant internal energy.
drho_dP_A()	Method to calculate and return the pressure derivative
	of density of the phase at constant Helmholtz energy.
drho_dP_G()	Method to calculate and return the pressure derivative
	of density of the phase at constant Gibbs energy.
drho_dP_H()	Method to calculate and return the pressure derivative
	of density of the phase at constant enthalpy.
drho_dP_S()	Method to calculate and return the pressure derivative
	of density of the phase at constant entropy.
drho_dP_U()	Method to calculate and return the pressure derivative
	of density of the phase at constant internal energy.
drho_dT_A()	Method to calculate and return the temperature
	derivative of density of the phase at constant
	Helmholtz energy.
drho_dT_G()	Method to calculate and return the temperature
	derivative of density of the phase at constant Gibbs
	energy.
drho_dT_H()	Method to calculate and return the temperature
	derivative of density of the phase at constant en-
	thalpy.
	continues on next page

Table 90 – continu	ed from previous page
drho_dT_S()	Method to calculate and return the temperature
	derivative of density of the phase at constant entropy.
drho_dT_U()	Method to calculate and return the temperature
	derivative of density of the phase at constant internal
	energy.
drho_dV_A()	Method to calculate and return the volume derivative
	of density of the phase at constant Helmholtz energy.
drho_dV_G()	Method to calculate and return the volume derivative
	of density of the phase at constant Gibbs energy.
drho_dV_H()	Method to calculate and return the volume derivative
	of density of the phase at constant enthalpy.
drho_dV_S()	Method to calculate and return the volume derivative
d1110_dV_3()	
	of density of the phase at constant entropy. Method to calculate and return the volume derivative
drho_dV_U()	
	of density of the phase at constant internal energy.
drho_drho_A()	Method to calculate and return the density derivative
	of density of the phase at constant Helmholtz energy.
drho_drho_G()	Method to calculate and return the density derivative
	of density of the phase at constant Gibbs energy.
drho_drho_H()	Method to calculate and return the density derivative
	of density of the phase at constant enthalpy.
drho_drho_S()	Method to calculate and return the density derivative
	of density of the phase at constant entropy.
drho_drho_U()	Method to calculate and return the density derivative
	of density of the phase at constant internal energy.
<pre>isentropic_exponent()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship $PV^k = \text{const.}$
isentropic_exponent_PT()	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$P^{(1-k)}T^k = \text{const.}$
<pre>isentropic_exponent_PV()</pre>	Method to calculate and return the real gas isentropic
	exponent of the phase, which satisfies the relationship
	$PV^k = \text{const.}$
<pre>isentropic_exponent_TV()</pre>	Method to calculate and return the real gas isentropic
ischeropic_exponent_iv()	exponent of the phase, which satisfies the relationship
	$TV^{k-1} = \text{const.}$
<pre>isobaric_expansion()</pre>	Method to calculate and return the isobatic expansion
	coefficient of the bulk according to the selected cal-
	culation methodology.
i aathaamal hull madulua()	
<pre>isothermal_bulk_modulus()</pre>	Method to calculate and return the isothermal bulk
1-()	modulus of the phase.
<b>k</b> ()	Calculate and return the thermal conductivity
	of the bulk according to the selected thermal
	conductivity settings in BulkSettings, the set-
	tings in ThermalConductivityGasMixture
	and ThermalConductivityLiquidMixture,
	and the configured pure-component set-
	tings in ThermalConductivityGas and
	ThermalConductivityLiquid.
	continues on next page

Table 90 – continued from previous page

Table 90 - c	continued from previous page
kappa()	Method to calculate and return the isothermal com- pressibility of the bulk according to the selected cal- culation methodology.
log_zs()	Method to calculate and return the log of mole frac- tions specified.
<pre>molar_water_content([phase])</pre>	Method to calculate and return the molar water con- tent; this is the g/mol of the fluid which is coming from water, [g/mol].
mu()	Calculate and return the viscosity of the bulk according to the selected viscos- ity settings in BulkSettings, the set- tings in ViscosityGasMixture and ViscosityLiquidMixture, and the config- ured pure-component settings in ViscosityGas and ViscosityLiquid.
nu([phase])	Method to calculate and return the kinematic viscos- ity of the equilibrium state.
<pre>pseudo_Pc([phase])</pre>	Method to calculate and return the pseudocritical pressure calculated using Kay's rule (linear mole fractions):
<pre>pseudo_Tc([phase])</pre>	Method to calculate and return the pseudocritical temperature calculated using Kay's rule (linear mole fractions):
<pre>pseudo_Vc([phase])</pre>	Method to calculate and return the pseudocritical vol- ume calculated using Kay's rule (linear mole frac- tions):
<pre>pseudo_Zc([phase])</pre>	Method to calculate and return the pseudocritical compressibility calculated using Kay's rule (linear mole fractions):
rho()	Method to calculate and return the molar density of the phase.
rho_mass([phase])	Method to calculate and return mass density of the phase.
<pre>rho_mass_liquid_ref([phase])</pre>	Method to calculate and return the liquid refer- ence mass density according to the temperature variable <i>T_liquid_volume_ref</i> of <i>thermo.bulk</i> . <i>BulkSettings</i> and the composition of the phase.
<pre>sigma()</pre>	Calculate and return the surface tension of the bulk according to the selected surface ten- sion settings in BulkSettings, the settings in <i>SurfaceTensionMixture</i> and the configured pure-component settings in <i>SurfaceTension</i> .
<pre>speed_of_sound()</pre>	Method to calculate and return the molar speed of sound of the bulk according to the selected calculation methodology.
<pre>speed_of_sound_mass()</pre>	Method to calculate and return the speed of sound of the phase.
<pre>value(name[, phase])</pre>	Method to retrieve a property from a string.
ws([phase])	Method to calculate and return the mass fractions of the phase, [-]
	continues on next page

Table 90 – continued from previous page	
<pre>ws_no_water([phase])</pre>	Method to calculate and return the mass fractions of
	all species in the phase, normalized to a water-free
	basis (the mass fraction of water returned is zero).
<pre>zs_no_water([phase])</pre>	Method to calculate and return the mole fractions of
	all species in the phase, normalized to a water-free
	basis (the mole fraction of water returned is zero).

Table 90 – continued from previous page

dH_dP_V	
dH_dT_V	
dH_dV_P	
dH_dV_T	
dS_dP_V	
dS_dT	
dS_dT_P	
dS_dT_V	

## property P\_calc

property Q

property Q\_calc

property Qgs

property Qgs\_calc

property Qls

property Qls\_calc

## StreamArgs()

Goal to create a StreamArgs instance, with the user specified variables always being here.

The state variables are currently correctly tracked. The flow rate and composition variable needs to be tracked as a function of what was specified as the input variables.

The flow rate needs to be changed wen the stream flow rate is changed. Note this stores unnormalized specs, but that this is OK.

# property T\_calc

# property VF\_calc

property composition\_specified

Always needs a composition

property energy

property energy\_calc

property energy\_reactive

property energy\_reactive\_calc

flashed = True

property flow\_specified Always needs a flow specified

property ms\_calc

## property n\_calc

#### property non\_pressure\_spec\_specified

Cannot have a stream without an energy-type spec.

property ns\_calc

#### property property\_package

property specified\_composition\_vars number of composition variables

property specified\_flow\_vars Always needs only one flow specified

# property specified\_state\_vars

Always needs two states

property state\_specified Always needs a state

## property state\_specs

Returns a list of tuples of (state\_variable, state\_value) representing the thermodynamic state of the system.

# property zs\_calc

class thermo.stream.Stream(IDs=None, zs=None, ws=None, Vfls=None, Vfls=None, ns=None, ms=None, Qls=None, Qgs=None, n=None, m=None, Q=None, T=None, P=None, VF=None, H=None, Hm=None, S=None, Sm=None, energy=None, pkg=None, Vf\_TP=(None, None), Q\_TP=(None, None, "))

Bases: thermo.mixture.Mixture

Creates a Stream object which is useful for modeling mass and energy balances.

Streams have five variables. The flow rate, composition, and components are mandatory; and two of the variables temperature, pressure, vapor fraction, enthalpy, or entropy are required. Entropy and enthalpy may also be provided in a molar basis; energy can also be provided, which when combined with either a flow rate or enthalpy will calculate the other variable.

The composition and flow rate may be specified together or separately. The options for specifying them are:

- Mole fractions zs
- Mass fractions ws
- Liquid standard volume fractions Vfls
- Gas standard volume fractions Vfgs
- Mole flow rates ns
- Mass flow rates ms
- Liquid flow rates Qls (based on pure component volumes at the T and P specified by  $Q_TP$ )
- Gas flow rates Qgs (based on pure component volumes at the T and P specified by  $Q_TP$ )

If only the composition is specified by providing any of *zs*, *ws*, *Vfls* or *Vfgs*, the flow rate must be specified by providing one of these:

- Mole flow rate *n*
- Mass flow rate *m*
- Volumetric flow rate Q at the provided T and P or if specified, Q\_TP
- Energy energy

The state variables must be two of the following. Not all combinations result in a supported flash.

- Tempetarure T
- Pressure P
- Vapor fraction VF
- Enthalpy H
- Molar enthalpy Hm
- Entropy S
- Molar entropy Sm
- Energy energy

## Parameters

- **IDs** [list, optional] List of chemical identifiers names, CAS numbers, SMILES or InChi strings can all be recognized and may be mixed [-]
- zs [list or dict, optional] Mole fractions of all components in the stream [-]
- ws [list or dict, optional] Mass fractions of all components in the stream [-]
- Vfls [list or dict, optional] Volume fractions of all components as a hypothetical liquid phase based on pure component densities [-]
- **Vfgs** [list or dict, optional] Volume fractions of all components as a hypothetical gas phase based on pure component densities [-]
- ns [list or dict, optional] Mole flow rates of each component [mol/s]
- ms [list or dict, optional] Mass flow rates of each component [kg/s]
- **Qls** [list or dict, optional] Liquid flow rates of all components as a hypothetical liquid phase based on pure component densities [m^3/s]
- **Qgs** [list or dict, optional] Gas flow rates of all components as a hypothetical gas phase based on pure component densities [m^3/s]
- **n** [float, optional] Total mole flow rate of all components in the stream [mol/s]
- **m** [float, optional] Total mass flow rate of all components in the stream [kg/s]
- **Q** [float, optional] Total volumetric flow rate of all components in the stream based on the temperature and pressure specified by *T* and *P*  $[m^3/s]$
- T [float, optional] Temperature of the stream (default 298.15 K), [K]
- P [float, optional] Pressure of the stream (default 101325 Pa) [Pa]
- VF [float, optional] Vapor fraction (mole basis) of the stream, [-]
- H [float, optional] Mass enthalpy of the stream, [J]

Hm [float, optional] Molar enthalpy of the stream, [J/mol]

**S** [float, optional] Mass entropy of the stream, [J/kg/K]

Sm [float, optional] Molar entropy of the stream, [J/mol/K]

energy [float, optional] Flowing energy of the stream (H`\*`m), [W]

pkg [object] The thermodynamic property package to use for flash calculations; one of the caloric packages in thermo.property\_package; defaults to the ideal model [-]

- Vf\_TP [tuple(2, float), optional] The (T, P) at which the volume fractions are specified to be at, [K] and [Pa]
- **Q\_TP** [tuple(3, float, float, str), optional] The (T, P, phase) at which the volumetric flow rate is specified to be at, [K] and [Pa]

## Notes

**Warning:** The Stream class is not designed for high-performance or the ability to use different thermodynamic models. It is especially limited in its multiphase support and the ability to solve with specifications other than temperature and pressure. It is impossible to change constant properties such as a compound's critical temperature in this interface.

It is recommended to switch over to the *thermo.flash* and *EquilibriumStream* interfaces which solves those problems and are better positioned to grow. That interface also requires users to be responsible for their chemical constants and pure component correlations; while default values can easily be loaded for most compounds, the user is ultimately responsible for them.

#### **Examples**

Creating Stream objects:

A stream of vodka with volume fractions 60% water, 40% ethanol, 1 kg/s:

```
>>> from thermo import Stream
```

A stream of air at 400 K and 1 bar, flow rate of 1 mol/s:

A flow of 1 L/s of 10 wt% phosphoric acid at 320 K:

Instead of specifying the composition and flow rate separately, they can be specified as a list of flow rates in the appropriate units.

80 kg/s of furfuryl alcohol/water solution:

A stream of 100 mol/s of 400 K, 1 MPa argon:

A large stream of vinegar, 8 volume %:

A very large stream of 100 m<sup>3</sup>/s of steam at 500 K and 2 MPa:

A real example of a stream from a pulp mill:

For streams with large numbers of components, it may be confusing to enter the composition separate from the names of the chemicals. For that case, the syntax using dictionaries as follows is supported with any composition specification:

```
>>> comp = OrderedDict([('methane', 0.96522),
                           ('nitrogen', 0.00259),
. . .
                           ('carbon dioxide', 0.00596),
. . .
                           ('ethane', 0.01819),
. . .
                           ('propane', 0.0046),
. . .
                           ('isobutane', 0.00098),
. . .
                           ('butane', 0.00101),
. . .
                           ('2-methylbutane', 0.00047),
. . .
                           ('pentane', 0.00032),
. . .
                           ('hexane', 0.00066)])
. . .
>>> m = Stream(ws=comp, m=33)
```

Attributes

A Helmholtz energy of the mixture at its current state, in units of [J/kg].

**API** API gravity of the hypothetical liquid phase of the mixture, [degrees].

- Am Helmholtz energy of the mixture at its current state, in units of [J/mol].
- **Bvirial** Second virial coefficient of the gas phase of the mixture at its current temperature, pressure, and composition in units of [mol/m^3].
- **Cp** Mass heat capacity of the mixture at its current phase and temperature, in units of [J/kg/K].
- **Cpg** Gas-phase heat capacity of the mixture at its current temperature , and composition in units of [J/kg/K].

- **Cpgm** Gas-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- **Cpgms** Gas-phase ideal gas heat capacity of the chemicals at its current temperature, in units of [J/mol/K].
- **Cpgs** Gas-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].
- **Cpl** Liquid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/kg/K].
- **Cplm** Liquid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- **Cplms** Liquid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/mol/K].
- **Cpls** Liquid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].
- Cpm Molar heat capacity of the mixture at its current phase and temperature, in units of [J/mol/K].
- **Cps** Solid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/kg/K].
- **Cpsm** Solid-phase heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- **Cpsms** Solid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/mol/K].
- **Cpss** Solid-phase pure component heat capacity of the chemicals in the mixture at its current temperature, in units of [J/kg/K].
- **Cvg** Gas-phase ideal-gas contant-volume heat capacity of the mixture at its current temperature, in units of [J/kg/K].
- **Cvgm** Gas-phase ideal-gas contant-volume heat capacity of the mixture at its current temperature and composition, in units of [J/mol/K].
- **Cvgms** Gas-phase pure component ideal-gas contant-volume heat capacities of the chemicals in the mixture at its current temperature, in units of [J/mol/K].
- **Cvgs** Gas-phase pure component ideal-gas contant-volume heat capacities of the chemicals in the mixture at its current temperature, in units of [J/kg/K].

#### Н

**Hc** Standard higher heat of combustion of the mixture, in units of [J/kg].

**Hc\_lower** Standard lower heat of combustion of the mixture, in units of [J/kg].

Hcm Standard higher molar heat of combustion of the mixture, in units of [J/mol].

Hcm\_lower Standard lower molar heat of combustion of the mixture, in units of [J/mol].

Hm

- **Hvapms** Pure component enthalpies of vaporization of the chemicals in the mixture at its current temperature, in units of [J/mol].
- **Hvaps** Enthalpy of vaporization of the chemicals in the mixture at its current temperature, in units of [J/kg].

**IUPAC\_names** IUPAC names for all chemicals in the mixture.

InChI\_Keys InChI keys for all chemicals in the mixture.

- **InChIs** InChI strings for all chemicals in the mixture.
- **JT** Joule Thomson coefficient of the mixture at its current phase, temperature, and pressure in units of [K/Pa].
- **JTg** Joule Thomson coefficient of the gas phase of the mixture if one exists at its current temperature and pressure, in units of [K/Pa].
- **JTgs** Pure component Joule Thomson coefficients of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [K/Pa].
- **JT1** Joule Thomson coefficient of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [K/Pa].
- **JT1s** Pure component Joule Thomson coefficients of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [K/Pa].
- **PSRK\_groups** List of dictionaries of PSRK subgroup: count groups for each chemical in the mixture.
- **Parachor** Parachor of the mixture at its current temperature and pressure, in units of [N^0.25\*m^2.75/mol].
- **Parachors** Pure component Parachor parameters of the chemicals in the mixture at its current temperature and pressure, in units of [N^0.25\*m^2.75/mol].
- **Pbubble** Bubble point pressure of the mixture at its current temperature and composition, in units of [Pa].
- **Pdew** Dew point pressure of the mixture at its current temperature and composition, in units of [Pa].
- **Pr** Prandtl number of the mixture at its current temperature, pressure, and phase; [dimension-less].
- **Prg** Prandtl number of the gas phase of the mixture if one exists at its current temperature and pressure, [dimensionless].
- **Prgs** Pure component Prandtl numbers of the gas phase of the chemicals in the mixture at its current temperature and pressure, [dimensionless].
- **Pr1** Prandtl number of the liquid phase of the mixture if one exists at its current temperature and pressure, [dimensionless].
- **Prls** Pure component Prandtl numbers of the liquid phase of the chemicals in the mixture at its current temperature and pressure, [dimensionless].
- **Psats** Pure component vapor pressures of the chemicals in the mixture at its current temperature, in units of [Pa].
- PubChems PubChem Component ID numbers for all chemicals in the mixture.
- **R\_specific** Specific gas constant of the mixture, in units of [J/kg/K].
- SG Specific gravity of the mixture, [dimensionless].
- SGg Specific gravity of a hypothetical gas phase of the mixture, .
- **SG1** Specific gravity of a hypothetical liquid phase of the mixture at the specified temperature and pressure, [dimensionless].
- **SGs** Specific gravity of a hypothetical solid phase of the mixture at the specified temperature and pressure, [dimensionless].

- **Tbubble** Bubble point temperature of the mixture at its current pressure and composition, in units of [K].
- **Tdew** Dew point temperature of the mixture at its current pressure and composition, in units of [K].
- **U** Internal energy of the mixture at its current state, in units of [J/kg].
- **UNIFAC\_Dortmund\_groups** List of dictionaries of Dortmund UNIFAC subgroup: count groups for each chemcial in the mixture.
- **UNIFAC\_Qs** UNIFAC Q (normalized Van der Waals area) values, dimensionless.
- **UNIFAC\_Rs** UNIFAC *R* (normalized Van der Waals volume) values, dimensionless.
- **UNIFAC\_groups** List of dictionaries of UNIFAC subgroup: count groups for each chemical in the mixture.
- Um Internal energy of the mixture at its current state, in units of [J/mol].

V\_over\_F

- Van\_der\_Waals\_areas List of unnormalized Van der Waals areas of all the chemicals in the mixture, in units of [m<sup>2</sup>/mol].
- **Van\_der\_Waals\_volumes** List of unnormalized Van der Waals volumes of all the chemicals in the mixture, in units of [m^3/mol].
- **Vm** Molar volume of the mixture at its current phase and temperature and pressure, in units of [m^3/mol].
- **Vmg** Gas-phase molar volume of the mixture at its current temperature, pressure, and composition in units of [m^3/mol].
- **Vmg\_STP** Gas-phase molar volume of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [m^3/mol].
- **Vmgs** Pure component gas-phase molar volumes of the chemicals in the mixture at its current temperature and pressure, in units of [m^3/mol].
- **Vml** Liquid-phase molar volume of the mixture at its current temperature, pressure, and composition in units of [m^3/mol].
- Vml\_STP Liquid-phase molar volume of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [m<sup>3</sup>/mol].
- **Vmls** Pure component liquid-phase molar volumes of the chemicals in the mixture at its current temperature and pressure, in units of [m^3/mol].

Vms

- **Vmss** Pure component solid-phase molar volumes of the chemicals in the mixture at its current temperature, in units of [m^3/mol].
- **Z** Compressibility factor of the mixture at its current phase and temperature and pressure, [dimensionless].
- **Zg** Compressibility factor of the mixture in the gas phase at the current temperature, pressure, and composition, [dimensionless].
- **Zg\_STP** Gas-phase compressibility factor of the mixture at 298.15 K and 101.325 kPa, and the current composition, [dimensionless].
- **Zgs** Pure component compressibility factors of the chemicals in the mixture in the gas phase at the current temperature and pressure, [dimensionless].

- **Z1** Compressibility factor of the mixture in the liquid phase at the current temperature, pressure, and composition, [dimensionless].
- **Z1\_STP** Liquid-phase compressibility factor of the mixture at 298.15 K and 101.325 kPa, and the current composition, [dimensionless].
- **Zls** Pure component compressibility factors of the chemicals in the liquid phase at the current temperature and pressure, [dimensionless].
- **Zss** Pure component compressibility factors of the chemicals in the mixture in the solid phase at the current temperature and pressure, [dimensionless].
- **alpha** Thermal diffusivity of the mixture at its current temperature, pressure, and phase in units of  $[m^2/s]$ .
- **alphag** Thermal diffusivity of the gas phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .
- **alphags** Pure component thermal diffusivities of the chemicals in the mixture in the gas phase at the current temperature and pressure, in units of [m<sup>2</sup>/s].
- **alphal** Thermal diffusivity of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- **alphals** Pure component thermal diffusivities of the chemicals in the mixture in the liquid phase at the current temperature and pressure, in units of  $[m^2/s]$ .

**atom\_fractions** Dictionary of atomic fractions for each atom in the mixture.

**atom\_fractionss** List of dictionaries of atomic fractions for all chemicals in the mixture.

atoms Mole-averaged dictionary of atom counts for all atoms of the chemicals in the mixture.

atomss List of dictionaries of atom counts for all chemicals in the mixture.

charge\_balance Charge imbalance of the mixture, in units of [faraday].

**charges** Charges for all chemicals in the mixture, [faraday].

*composition\_specified* Always needs a composition

conductivity

**constants** Returns a :obj:`thermo.chemical\_package.ChemicalConstantsPackage instance with constants from the mixture, [-].

economic\_statuses List of dictionaries of the economic status for all chemicals in the mixture.

eos Equation of state object held by the mixture.

flow\_specified Always needs a flow specified

formulas Chemical formulas for all chemicals in the mixture.

- **isentropic\_exponent** Gas-phase ideal-gas isentropic exponent of the mixture at its current temperature, [dimensionless].
- **isentropic\_exponents** Gas-phase pure component ideal-gas isentropic exponent of the chemicals in the mixture at its current temperature, [dimensionless].
- **isobaric\_expansion** Isobaric (constant-pressure) expansion of the mixture at its current phase, temperature, and pressure in units of [1/K].
- **isobaric\_expansion\_g** Isobaric (constant-pressure) expansion of the gas phase of the mixture at its current temperature and pressure, in units of [1/K].

- **isobaric\_expansion\_gs** Pure component isobaric (constant-pressure) expansions of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [1/K].
- **isobaric\_expansion\_1** Isobaric (constant-pressure) expansion of the liquid phase of the mixture at its current temperature and pressure, in units of [1/K].
- **isobaric\_expansion\_1s** Pure component isobaric (constant-pressure) expansions of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [1/K].
- **k** Thermal conductivity of the mixture at its current phase, temperature, and pressure in units of [W/m/K].
- **kg** Thermal conductivity of the mixture in the gas phase at its current temperature, pressure, and composition in units of [Pa\*s].
- **kgs** Pure component thermal conductivies of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [W/m/K].
- **k1** Thermal conductivity of the mixture in the liquid phase at its current temperature, pressure, and composition in units of [Pa\*s].
- **kls** Pure component thermal conductivities of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [W/m/K].

ks

**legal\_statuses** List of dictionaries of the legal status for all chemicals in the mixture.

**mass\_fractions** Dictionary of mass fractions for each atom in the mixture.

- mass\_fractionss List of dictionaries of mass fractions for all chemicals in the mixture.
- **mu** Viscosity of the mixture at its current phase, temperature, and pressure in units of [Pa\*s].
- **mug** Viscosity of the mixture in the gas phase at its current temperature, pressure, and composition in units of [Pa\*s].
- **mugs** Pure component viscosities of the chemicals in the mixture in the gas phase at its current temperature and pressure, in units of [Pa\*s].
- **mul** Viscosity of the mixture in the liquid phase at its current temperature, pressure, and composition in units of [Pa\*s].
- **muls** Pure component viscosities of the chemicals in the mixture in the liquid phase at its current temperature and pressure, in units of [Pa\*s].

**non\_pressure\_spec\_specified** Cannot have a stream without an energy-type spec.

- **nu** Kinematic viscosity of the mixture at its current temperature, pressure, and phase in units of  $[m^2/s]$ .
- **nug** Kinematic viscosity of the gas phase of the mixture if one exists at its current temperature and pressure, in units of  $[m^2/s]$ .
- **nugs** Pure component kinematic viscosities of the gas phase of the chemicals in the mixture at its current temperature and pressure, in units of  $[m^2/s]$ .
- **nul** Kinematic viscosity of the liquid phase of the mixture if one exists at its current temperature and pressure, in units of [m<sup>2</sup>/s].
- **nuls** Pure component kinematic viscosities of the liquid phase of the chemicals in the mixture at its current temperature and pressure, in units of [m<sup>2</sup>/s].

**permittivites** Pure component relative permittivities of the chemicals in the mixture at its current temperature, [dimensionless].

## phase

#### property\_package\_constants

- **rho** Mass density of the mixture at its current phase and temperature and pressure, in units of [kg/m^3].
- **rhog** Gas-phase mass density of the mixture at its current temperature, pressure, and composition in units of [kg/m^3].
- **rhog\_STP** Gas-phase mass density of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [kg/m<sup>3</sup>].
- **rhogm** Molar density of the mixture in the gas phase at the current temperature, pressure, and composition in units of [mol/m<sup>3</sup>].
- **rhogm\_STP** Molar density of the mixture in the gas phase at 298.15 K and 101.325 kPa, and the current composition, in units of [mol/m<sup>3</sup>].
- **rhogms** Pure component molar densities of the chemicals in the gas phase at the current temperature and pressure, in units of [mol/m^3].
- **rhogs** Pure-component gas-phase mass densities of the chemicals in the mixture at its current temperature and pressure, in units of [kg/m^3].
- **rhol** Liquid-phase mass density of the mixture at its current temperature, pressure, and composition in units of [kg/m^3].
- **rhol\_STP** Liquid-phase mass density of the mixture at 298.15 K and 101.325 kPa, and the current composition in units of [kg/m<sup>3</sup>].
- **rholm** Molar density of the mixture in the liquid phase at the current temperature, pressure, and composition in units of [mol/m<sup>3</sup>].
- **rholm\_STP** Molar density of the mixture in the liquid phase at 298.15 K and 101.325 kPa, and the current composition, in units of [mol/m<sup>3</sup>].
- **rholms** Pure component molar densities of the chemicals in the mixture in the liquid phase at the current temperature and pressure, in units of [mol/m^3].
- **rhols** Pure-component liquid-phase mass density of the chemicals in the mixture at its current temperature and pressure, in units of [kg/m^3].
- **rhom** Molar density of the mixture at its current phase and temperature and pressure, in units of [mol/m^3].

#### rhos

- **rhosms** Pure component molar densities of the chemicals in the solid phase at the current temperature and pressure, in units of [mol/m^3].
- **rhoss** Pure component solid-phase mass density of the chemicals in the mixture at its current temperature, in units of [kg/m^3].
- **ringss** List of ring counts for all chemicals in the mixture.
- sigma Surface tension of the mixture at its current temperature and composition, in units of [N/m].
- **sigmas** Pure component surface tensions of the chemicals in the mixture at its current temperature, in units of [N/m].

similarity\_variables Similarity variables for all chemicals in the mixture, see

smiless SMILES strings for all chemicals in the mixture.

**solubility\_parameters** Pure component solubility parameters of the chemicals in the mixture at its current temperature and pressure, in units of [Pa^0.5].

specified\_composition\_vars number of composition variables

specified\_flow\_vars Always needs only one flow specified

specified\_state\_vars Always needs two states

speed\_of\_sound Bulk speed of sound of the mixture at its current temperature, [m/s].

**speed\_of\_sound\_g** Gas-phase speed of sound of the mixture at its current temperature, [m/s].

speed\_of\_sound\_l Liquid-phase speed of sound of the mixture at its current temperature, [m/s].

state\_specified Always needs a state

*state\_specs* Returns a list of tuples of (state\_variable, state\_value) representing the thermodynamic state of the system.

synonymss Lists of synonyms for all chemicals in the mixture.

XS

## ys

# **Methods**

<pre>Hc_volumetric_g([T, P])</pre>	Standard higher molar heat of combustion of the mix-
	ture, in units of $[J/m^3]$ at the specified T and P in the
	gas phase.
<pre>Hc_volumetric_g_lower([T, P])</pre>	Standard lower molar heat of combustion of the mix-
	ture, in units of $[J/m^3]$ at the specified T and P in
	the gas phase.
StreamArgs()	Goal to create a StreamArgs instance, with the user
	specified variables always being here.
Vfgs([T, P])	Volume fractions of all species in a hypothetical pure-
	gas phase at the current or specified temperature and
	pressure.
Vfls([T, P])	Volume fractions of all species in a hypothetical pure-
	liquid phase at the current or specified temperature
	and pressure.
draw_2d([Hs])	Interface for drawing a 2D image of all the molecules
	in the mixture.
<pre>set_chemical_TP([T, P])</pre>	Basic method to change all chemical instances to be
	at the T and P specified.
<pre>set_chemical_constants()</pre>	Basic method which retrieves and sets constants of
	chemicals to be accessible as lists from a Mixture ob-
	ject.

Bond	
Capillary	
Grashof	
Jakob	
Peclet_heat	
Reynolds	
Weber	
calculate	
compound_index	
eos_pures	
flash	
flash_caloric	
properties	
set_Chemical_property_objects	
set_TP_sources	
set_constant_sources	
set_constants	
set_eos	
set_extensive_flow	
set_extensive_properties	
set_property_package	

# StreamArgs()

Goal to create a StreamArgs instance, with the user specified variables always being here.

The state variables are currently correctly tracked. The flow rate and composition variable needs to be tracked as a function of what was specified as the input variables.

The flow rate needs to be changed wen the stream flow rate is changed. Note this stores unnormalized specs, but that this is OK.

calculate(T=None, P=None)

## property composition\_specified

Always needs a composition

flash(T=None, P=None, VF=None, H=None, Hm=None, S=None, Sm=None, energy=None)

# flashed = True

property flow\_specified Always needs a flow specified

property non\_pressure\_spec\_specified

Cannot have a stream without an energy-type spec.

set\_extensive\_flow(n=None)

set\_extensive\_properties()

property specified\_composition\_vars

number of composition variables

### property specified\_flow\_vars

Always needs only one flow specified

## property specified\_state\_vars

Always needs two states

## property state\_specified

Always needs a state

## property state\_specs

Returns a list of tuples of (state\_variable, state\_value) representing the thermodynamic state of the system.

class	thermo.stream.StreamArgs(IDs=None, zs=None, ws=None, Vfls=None, Vfgs=None, T=None, P=None,
	VF=None, H=None, Hm=None, S=None, Sm=None, ns=None, ms=None,
	Qls=None, Qgs=None, m=None, n=None, Q=None, energy=None,
	Vf_TP=(None, None), Q_TP=(None, None, "), pkg=None,
	single_composition_basis=True)

Bases: object

Attributes Η Hm Hm\_calc IDs MW Р P\_calc Q Qgs Qls S Sm Т T\_calc VF VF\_calc Vfgs Vfls *clean* If no variables (other than IDs) have been specified, return True, otherwise return False. composition\_spec composition\_specified energy

energy\_calc

flow\_spec

flow_specified
m
m_calc
mixture
ms
n
n_calc
non_pressure_spec_specified
ns
ns_calc
specified_composition_vars
specified_flow_vars
specified_state_vars
state_specified
state_specs
stream
WS
ZS
zs_calc

## Methods

сору	
flash	
flash_state	
reconcile_flows	
update	

property	н
property	Hm
property	Hm_calc
property	IDs
property	MW
property	Р
property	P_calc
property	Q
property	Qgs
property	Qls

- property S
- property Sm
- property T
- property T\_calc
- property VF
- property VF\_calc
- property Vfgs
- property Vfls

#### property clean

If no variables (other than IDs) have been specified, return True, otherwise return False.

property composition\_spec

property composition\_specified

copy()

#### property energy

property energy\_calc

flash(hot\_start=None, existing\_flash=None)

flash\_state(hot\_start=None)

flashed = False property flow\_spec property flow\_specified property m property m\_calc property mixture property ms property n property n\_calc property non\_pressure\_spec\_specified property ns property ns\_calc **reconcile\_flows**(*n\_tol=2e-15*, *m\_tol=2e-15*) property specified\_composition\_vars property specified\_flow\_vars property specified\_state\_vars property state\_specified

property state\_specs
property stream
update(\*\*kwargs)

property ws
property zs
property zs\_calc
thermo.stream.energy\_balance(inlets, outlets)

thermo.stream.mole\_balance(inlets, outlets, compounds)

## 7.28 Thermal Conductivity (thermo.thermal\_conductivity)

This module contains implementations of *TPDependentProperty* representing liquid and vapor thermal conductivity. A variety of estimation and data methods are available as included in the *chemicals* library. Additionally liquid and vapor mixture thermal conductivity predictor objects are implemented subclassing *MixtureProperty*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Pure Liquid Thermal Conductivity
- Pure Gas Thermal Conductivity
- Mixture Liquid Thermal Conductivity
- Mixture Gas Thermal Conductivity

## 7.28.1 Pure Liquid Thermal Conductivity

class thermo.thermal\_conductivity.ThermalConductivityLiquid(CASRN=", MW=None, Tm=None,

Tb=None, Tc=None, Pc=None, omega=None, Hfus=None, extrapolation='linear', extrapolation\_min=0.0001, \*\*kwargs)

Bases: thermo.utils.tp\_dependent\_property.TPDependentProperty

Class for dealing with liquid thermal conductivity as a function of temperature and pressure.

For low-pressure (at 1 atm while under the vapor pressure; along the saturation line otherwise) liquids, there is one source of tabular information, one polynomial-based method, 7 corresponding-states estimators, and the external library CoolProp.

For high-pressure liquids (also, <1 atm liquids), there are two corresponding-states estimator, and the external library CoolProp.

## **Parameters**

CAS [str, optional] The CAS number of the compound, [-]

MW [float, optional] Molecular weight, [g/mol]

**Tm** [float, optional] Melting point, [K]

**Tb** [float, optional] Boiling point, [K]

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

omega [float, optional] Acentric factor, [-]

Hfus [float, optional] Heat of fusion, [J/mol]

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

#### See also:

chemicals.thermal\_conductivity.Sheffy\_Johnson chemicals.thermal\_conductivity.Sato\_Riedel chemicals.thermal\_conductivity.Lakshmi\_Prasad chemicals.thermal\_conductivity.Gharagheizi\_liquid chemicals.thermal\_conductivity.Nicola\_original chemicals.thermal\_conductivity.Nicola chemicals.thermal\_conductivity.Bahadori\_liquid chemicals.thermal\_conductivity.DIPPR9G chemicals.thermal\_conductivity.Missenard

## Notes

To iterate over all methods, use the lists stored in thermal\_conductivity\_liquid\_methods and thermal\_conductivity\_liquid\_methods\_P for low and high pressure methods respectively.

Low pressure methods:

GHARAGHEIZI\_L: CSP method, described in Gharagheizi\_liquid.

SATO\_RIEDEL: CSP method, described in Sato\_Riedel.

NICOLA: CSP method, described in Nicola.

NICOLA\_ORIGINAL: CSP method, described in Nicola\_original.

SHEFFY\_JOHNSON: CSP method, described in Sheffy\_Johnson.

BAHADORI\_L: CSP method, described in Bahadori\_liquid.

LAKSHMI\_PRASAD: CSP method, described in Lakshmi\_Prasad.

**DIPPR\_PERRY\_8E:** A collection of 340 coefficient sets from the DIPPR database published openly in [3]. Provides temperature limits for all its fluids. EQ100 is used for its fluids.

- **VDI\_PPDS:** Coefficients for a equation form developed by the PPDS, published openly in [2]. Covers a large temperature range, but does not extrapolate well at very high or very low temperatures. 271 compounds.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [1]. Very slow.
- VDI\_TABULAR: Tabular data in [2] along the saturation curve; interpolation is as set by the user or the default.

High pressure methods:

- **DIPPR\_9G:** CSP method, described in DIPPR9G. Calculates a low-pressure thermal conductivity first from the low-pressure method.
- **MISSENARD:** CSP method, described in Missenard. Calculates a low-pressure thermal conductivity first from the low-pressure method.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [1]. Very slow, but unparalled in accuracy for pressure dependence.

## References

## [1], [2], [3]

#### Attributes

Tmax Maximum temperature (K) at which the current method can calculate the property.

Tmin Minimum temperature (K) at which the current method can calculate the property.

#### **Methods**

calculate(T, method)	Method to calculate low-pressure liquid thermal con-
	ductivity at tempearture T with a given method.
<pre>calculate_P(T, P, method)</pre>	Method to calculate pressure-dependent liquid ther-
	mal conductivity at temperature $T$ and pressure $P$
	with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a temperature-
	dependent low-pressure method.
<pre>test_method_validity_P(T, P, method)</pre>	Method to check the validity of a high-pressure
	method.

#### property Tmax

Maximum temperature (K) at which the current method can calculate the property.

## property Tmin

Minimum temperature (K) at which the current method can calculate the property.

#### calculate(T, method)

Method to calculate low-pressure liquid thermal conductivity at tempearture T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature of the liquid, [K]

method [str] Name of the method to use

#### Returns

**kl** [float] Thermal conductivity of the liquid at T and a low pressure, [W/m/K]

#### calculate\_P(T, P, method)

Method to calculate pressure-dependent liquid thermal conductivity at temperature T and pressure P with a given method.

This method has no exception handling; see *TP\_dependent\_property* for that.

#### Parameters

T [float] Temperature at which to calculate liquid thermal conductivity, [K]

P [float] Pressure at which to calculate liquid thermal conductivity, [K]

method [str] Name of the method to use

#### Returns

kl [float] Thermal conductivity of the liquid at T and P, [W/m/K]

name = 'liquid thermal conductivity'

#### property\_max = 10.0

Maximum valid value of liquid thermal conductivity. Generous limit.

## property\_min = 0.0

Mimimum valid value of liquid thermal conductivity.

```
ranked_methods = ['COOLPROP', 'DIPPR_PERRY_8E', 'VDI_PPDS', 'VDI_TABULAR',
'GHARAGHEIZI_L', 'SHEFFY_JOHNSON', 'SATO_RIEDEL', 'LAKSHMI_PRASAD', 'BAHADORI_L',
'NICOLA', 'NICOLA_ORIGINAL']
```

Default rankings of the low-pressure methods.

ranked\_methods\_P = ['COOLPROP', 'DIPPR\_9G', 'MISSENARD']

Default rankings of the high-pressure methods.

#### test\_method\_validity(T, method)

Method to check the validity of a temperature-dependent low-pressure method. For CSP methods, the models **BAHADORI\_L**, **LAKSHMI\_PRASAD**, and **SHEFFY\_JOHNSON** are considered valid for all temperatures. For methods **GHARAGHEIZI\_L**, **NICOLA**, and **NICOLA\_ORIGINAL**, the methods are considered valid up to 1.5Tc and down to 0 K. Method **SATO\_RIEDEL** does not work above the critical point, so it is valid from 0 K to the critical point.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

#### test\_method\_validity\_P(T, P, method)

Method to check the validity of a high-pressure method. For **COOLPROP**, the fluid must be both a liquid and under the maximum pressure of the fluid's EOS. **MISSENARD** has defined limits; between 0.5Tc and 0.8Tc, and below 200Pc. The CSP method **DIPPR\_9G** is considered valid for all temperatures and pressures.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures and pressures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

## Parameters

T [float] Temperature at which to test the method, [K]

**P** [float] Pressure at which to test the method, [Pa]

method [str] Name of the method to test

#### Returns

validity [bool] Whether or not a method is valid

## units = 'W/m/K'

The following variables are available to specify which method to use.

thermo.thermal\_conductivity.COOLPROP

thermo.thermal\_conductivity.DIPPR\_PERRY\_8E

thermo.thermal\_conductivity.VDI\_PPDS

thermo.thermal\_conductivity.VDI\_TABULAR

thermo.thermal\_conductivity.GHARAGHEIZI\_L

thermo.thermal\_conductivity.SHEFFY\_JOHNSON

thermo.thermal\_conductivity.SATO\_RIEDEL

thermo.thermal\_conductivity.LAKSHMI\_PRASAD

thermo.thermal\_conductivity.BAHADORI\_L

thermo.thermal\_conductivity.NICOLA

thermo.thermal\_conductivity.NICOLA\_ORIGINAL

The following variables contain lists of available methods.

thermo.thermal\_conductivity.thermal\_conductivity\_liquid\_methods = ['COOLPROP',

'DIPPR\_PERRY\_8E', 'VDI\_PPDS', 'VDI\_TABULAR', 'GHARAGHEIZI\_L', 'SHEFFY\_JOHNSON',

'SATO\_RIEDEL', 'LAKSHMI\_PRASAD', 'BAHADORI\_L', 'NICOLA', 'NICOLA\_ORIGINAL'] Holds all low-pressure methods available for the *ThermalConductivityLiquid* class, for use in iterating over them.

# thermo.thermal\_conductivity.thermal\_conductivity\_liquid\_methods\_P = ['COOLPROP', 'DIPPR\_9G', 'MISSENARD']

Holds all high-pressure methods available for the *ThermalConductivityLiquid* class, for use in iterating over them.

## 7.28.2 Pure Gas Thermal Conductivity

**class** thermo.thermal\_conductivity.**ThermalConductivityGas**(*CASRN='', MW=None, Tb=None,* 

Tc=None, Pc=None, Vc=None, Zc=None,<br/>omega=None, dipole=None, Vmg=None,<br/>Cpgm=None, mug=None,<br/>extrapolation='linear',<br/>extrapolation\_min=0.0001, \*\*kwargs)

Bases: thermo.utils.tp\_dependent\_property.TPDependentProperty

Class for dealing with gas thermal conductivity as a function of temperature and pressure.

For gases at atmospheric pressure, there are 7 corresponding-states estimators, one source of tabular information, and the external library CoolProp.

For gases under the fluid's boiling point (at sub-atmospheric pressures), and high-pressure gases above the boiling point, there are three corresponding-states estimators, and the external library CoolProp.

## **Parameters**

CAS [str, optional] The CAS number of the compound, [-]

**MW** [float, optional] Molecular weight, [g/mol]

Tb [float, optional] Boiling point, [K]

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

Vc [float, optional] Critical volume, [m^3/mol]

Zc [float, optional] Critical compressibility, [-]

omega [float, optional] Acentric factor, [-]

- dipole [float, optional] Dipole moment of the fluid, [debye]
- **Vmg** [float or callable, optional] Molar volume of the fluid at a pressure and temperature or callable for the same, [m^3/mol]
- **Cpgm** [float or callable, optional] Molar constant-pressure heat capacity of the fluid at a pressure and temperature or callable for the same, [J/mol/K]
- **mug** [float or callable, optional] Gas viscosity of the fluid at a pressure and temperature or callable for the same, [Pa\*s]
- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

## See also:

chemicals.thermal\_conductivity.Bahadori\_gas

chemicals.thermal\_conductivity.Gharagheizi\_gas

chemicals.thermal\_conductivity.Eli\_Hanley

chemicals.thermal\_conductivity.Chung

chemicals.thermal\_conductivity.DIPPR9B chemicals.thermal\_conductivity.Eucken\_modified chemicals.thermal\_conductivity.Eucken chemicals.thermal\_conductivity.Stiel\_Thodos\_dense chemicals.thermal\_conductivity.Eli\_Hanley\_dense chemicals.thermal\_conductivity.Chung\_dense

## Notes

To iterate over all methods, use the lists stored in *thermal\_conductivity\_gas\_methods* and *thermal\_conductivity\_gas\_methods\_P* for low and high pressure methods respectively.

Low pressure methods:

GHARAGHEIZI\_G: CSP method, described in Gharagheizi\_gas.

**DIPPR\_9B:** CSP method, described in DIPPR9B.

CHUNG: CSP method, described in Chung.

**ELI\_HANLEY:** CSP method, described in Eli\_Hanley.

**EUCKEN\_MOD:** CSP method, described in Eucken\_modified.

EUCKEN: CSP method, described in Eucken.

**BAHADORI\_G:** CSP method, described in Bahadori\_gas.

- **DIPPR\_PERRY\_8E:** A collection of 345 coefficient sets from the DIPPR database published openly in [3]. Provides temperature limits for all its fluids. chemicals.dippr.EQ102 is used for its fluids.
- **VDI\_PPDS:** Coefficients for a equation form developed by the PPDS, published openly in [2]. Covers a large temperature range, but does not extrapolate well at very high or very low temperatures. 275 compounds.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [1]. Very slow.
- **VDI\_TABULAR:** Tabular data in [2] along the saturation curve; interpolation is as set by the user or the default.

High pressure methods:

- **STIEL\_THODOS\_DENSE:** CSP method, described in Stiel\_Thodos\_dense. Calculates a low-pressure thermal conductivity first.
- **ELI\_HANLEY\_DENSE:** CSP method, described in Eli\_Hanley\_dense. Calculates a low-pressure thermal conductivity first.
- **CHUNG\_DENSE:** CSP method, described in Chung\_dense. Calculates a low-pressure thermal conductivity first.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [1]. Very slow, but unparalled in accuracy for pressure dependence.

## References

[1], [2], [3]

## Methods

calculate(T, method)	Method to calculate low-pressure gas thermal con- ductivity at tempearture $T$ with a given method.
calculate_P(T, P, method)	Method to calculate pressure-dependent gas thermal conductivity at temperature $T$ and pressure $P$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a temperature- dependent low-pressure method.
<pre>test_method_validity_P(T, P, method)</pre>	Method to check the validity of a high-pressure method.

## calculate(T, method)

Method to calculate low-pressure gas thermal conductivity at tempearture T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

## Parameters

T [float] Temperature of the gas, [K]

method [str] Name of the method to use

## Returns

kg [float] Thermal conductivity of the gas at T and a low pressure, [W/m/K]

## calculate\_P(T, P, method)

Method to calculate pressure-dependent gas thermal conductivity at temperature T and pressure P with a given method.

This method has no exception handling; see *TP\_dependent\_property* for that.

## **Parameters**

T [float] Temperature at which to calculate gas thermal conductivity, [K]

P [float] Pressure at which to calculate gas thermal conductivity, [K]

method [str] Name of the method to use

## Returns

kg [float] Thermal conductivity of the gas at T and P, [W/m/K]

## name = 'gas thermal conductivity'

## property\_max = 10

Maximum valid value of gas thermal conductivity. Generous limit.

## property\_min = 0

Mimimum valid value of gas thermal conductivity.

```
ranked_methods = ['COOLPROP', 'VDI_PPDS', 'DIPPR_PERRY_8E', 'VDI_TABULAR',
'GHARAGHEIZI_G', 'DIPPR_9B', 'CHUNG', 'ELI_HANLEY', 'EUCKEN_MOD', 'EUCKEN',
'BAHADORI_G']
```

Default rankings of the low-pressure methods.

## ranked\_methods\_P = ['COOLPROP', 'ELI\_HANLEY\_DENSE', 'CHUNG\_DENSE',

#### 'STIEL\_THODOS\_DENSE']

Default rankings of the high-pressure methods.

## test\_method\_validity(T, method)

Method to check the validity of a temperature-dependent low-pressure method. For CSP methods, the all methods are considered valid from 0 K and up.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid. **GHARAGHEIZI\_G** and **BAHADORI\_G** are known to sometimes produce negative results.

## **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

## test\_method\_validity\_P(T, P, method)

Method to check the validity of a high-pressure method. For **COOLPROP**, the fluid must be both a gas and under the maximum pressure of the fluid's EOS. The CSP method **ELI\_HANLEY\_DENSE**, **CHUNG\_DENSE**, and **STIEL\_THODOS\_DENSE** are considered valid for all temperatures and pressures.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures and pressures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

## Parameters

**T** [float] Temperature at which to test the method, [K]

**P** [float] Pressure at which to test the method, [Pa]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

```
units = 'W/m/K'
```

```
thermo.thermal_conductivity.thermal_conductivity_gas_methods = ['COOLPROP',
'DIPPR_PERRY_8E', 'VDI_PPDS', 'VDI_TABULAR', 'GHARAGHEIZI_G', 'DIPPR_9B', 'CHUNG',
'ELI_HANLEY', 'EUCKEN_MOD', 'EUCKEN', 'BAHADORI_G']
```

Holds all low-pressure methods available for the *ThermalConductivityGas* class, for use in iterating over them.

thermo.thermal\_conductivity.thermal\_conductivity\_gas\_methods\_P = ['COOLPROP',

'ELI\_HANLEY\_DENSE', 'CHUNG\_DENSE', 'STIEL\_THODOS\_DENSE']

Holds all high-pressure methods available for the *ThermalConductivityGas* class, for use in iterating over them.

## 7.28.3 Mixture Liquid Thermal Conductivity

## 

## Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with thermal conductivity of a liquid mixture as a function of temperature, pressure, and composition. Consists of two mixing rule specific to liquid thremal conductivity, one coefficient-based method for aqueous electrolytes, and mole weighted averaging. Most but not all methods are shown in [1].

Prefered method is DIPPR\_9H which requires mass fractions, and pure component liquid thermal conductivities. This is substantially better than the ideal mixing rule based on mole fractions, **LINEAR**. Filippov is of similar accuracy but applicable to binary systems only.

## **Parameters**

CASs [str, optional] The CAS numbers of all species in the mixture, [-]

- **ThermalConductivityLiquids** [list[ThermalConductivityLiquid], optional] ThermalConductivityLiquid objects created for all species in the mixture, [-]
- MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]
- **correct\_pressure\_pure** [bool, optional] Whether to try to use the better pressure-corrected pure component models or to use only the T-only dependent pure species models, [-]

## See also:

chemicals.thermal\_conductivity.DIPPR9H

chemicals.thermal\_conductivity.Filippov

chemicals.thermal\_conductivity.thermal\_conductivity\_Magomedov

## Notes

To iterate over all methods, use the list stored in thermal\_conductivity\_liquid\_mixture\_methods.

**DIPPR\_9H:** Mixing rule described in DIPPR9H.

FILIPPOV: Mixing rule described in Filippov; for two binary systems only.

**MAGOMEDOV:** Coefficient-based method for aqueous electrolytes only, described in *thermo*. *electrochem.thermal\_conductivity\_Magomedov*.

LINEAR: Mixing rule described in mixing\_simple.

## References

[1]

## Methods

calculate(T, P, zs, ws, method)	Method to calculate thermal conductivity of a liquid mixture at temperature <i>T</i> , pressure <i>P</i> , mole fractions <i>zs</i> and weight fractions <i>ws</i> with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for the given conditions.

## calculate(T, P, zs, ws, method)

Method to calculate thermal conductivity of a liquid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

## Parameters

- T [float] Temperature at which to calculate the property, [K]
- **P** [float] Pressure at which to calculate the property, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]
- method [str] Name of the method to use

## Returns

**k** [float] Thermal conductivity of the liquid mixture, [W/m/K]

## name = 'liquid thermal conductivity'

## property\_max = 10

Maximum valid value of liquid thermal conductivity. Generous limit.

## property\_min = 0

Mimimum valid value of liquid thermal conductivity.

```
ranked_methods = ['MAGOMEDOV', 'DIPPR_9H', 'LINEAR', 'FILIPPOV']
```

## test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. If **MAGOMEDOV** is applicable (electrolyte system), no other methods are considered viable. Otherwise, there are no easy checks that can be performed here.

## **Parameters**

- T [float] Temperature at which to check method validity, [K]
- **P** [float] Pressure at which to check method validity, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]
- method [str] Method name to use

## Returns

validity [bool] Whether or not a specifid method is valid

units = 'W/m/K'

```
thermo.thermal_conductivity_liquid_mixture_methods = ['MAGOMEDOV',
'DIPPR_9H', 'FILIPPOV', 'LINEAR']
```

Holds all mixing rules available for the *ThermalConductivityLiquidMixture* class, for use in iterating over them.

## 7.28.4 Mixture Gas Thermal Conductivity

**class** thermo.thermal\_conductivity.**ThermalConductivityGasMixture**(*MWs=[]*, *Tbs=[]*, *CASs=[]*,

*ThermalConductivityGases=[], ViscosityGases=[],* \*\*kwargs)

Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with thermal conductivity of a gas mixture as a function of temperature, pressure, and composition. Consists of one mixing rule specific to gas thremal conductivity, and mole weighted averaging.

Prefered method is Lindsay\_Bromley which requires mole fractions, pure component viscosities and thermal conductivities, and the boiling point and molecular weight of each pure component. This is substantially better than the ideal mixing rule based on mole fractions, **LINEAR** which is also available. More information on this topic can be found in [1].

## Parameters

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

Tbs [list[float], optional] Boiling points of all species in the mixture, [K]

CASs [str, optional] The CAS numbers of all species in the mixture

- **ThermalConductivityGases** [list[ThermalConductivityGas], optional] ThermalConductivity-Gas objects created for all species in the mixture, [-]
- **ViscosityGases** [list[ViscosityGas], optional] ViscosityGas objects created for all species in the mixture, [-]
- **correct\_pressure\_pure** [bool, optional] Whether to try to use the better pressure-corrected pure component models or to use only the T-only dependent pure species models, [-]

## See also:

chemicals.thermal\_conductivity.Lindsay\_Bromley

## Notes

To iterate over all methods, use the list stored in thermal\_conductivity\_gas\_methods.

LINDSAY\_BROMLEY: Mixing rule described in Lindsay\_Bromley.

LINEAR: Mixing rule described in mixing\_simple.

## References

[1]

## **Methods**

calculate(T, P, zs, ws, method)	Method to calculate thermal conductivity of a gas mixture at temperature <i>T</i> , pressure <i>P</i> , mole fractions <i>zs</i> and weight fractions <i>ws</i> with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for the given conditions.

#### Tmax

Maximum temperature at which no method can calculate the property above.

## Tmin

Minimum temperature at which no method can calculate the property under.

## calculate(T, P, zs, ws, method)

Method to calculate thermal conductivity of a gas mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

## **Parameters**

T [float] Temperature at which to calculate the property, [K]

**P** [float] Pressure at which to calculate the property, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

## Returns

kg [float] Thermal conductivity of gas mixture, [W/m/K]

## name = 'gas thermal conductivity'

## property\_max = 10.0

Maximum valid value of gas thermal conductivity. Generous limit.

## property\_min = 0.0

Mimimum valid value of gas thermal conductivity.

ranked\_methods = ['LINDSAY\_BROMLEY', 'LINEAR']

## test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

## Parameters

T [float] Temperature at which to check method validity, [K]

- P [float] Pressure at which to check method validity, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

Returns

validity [bool] Whether or not a specifid method is valid

units = 'W/m/K'

thermo.thermal\_conductivity.thermal\_conductivity\_gas\_mixture\_methods =

## ['LINDSAY\_BROMLEY', 'LINEAR']

Holds all mixing rules available for the *ThermalConductivityGasMixture* class, for use in iterating over them.

## 7.29 UNIFAC Gibbs Excess Model (thermo.unifac)

This module contains functions and classes related to the UNIFAC and its many variants. The bulk of the code relates to calculating derivativies, or is tables of data.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker or contact the author at Caleb.Andrew.Bell@gmail.com.

- Main Model (Object-Oriented)
- Main Model (Functional)
- Misc Functions
- Data for Original UNIFAC
- Data for Dortmund UNIFAC
- Data for NIST UNIFAC (2015)
- Data for NIST KT UNIFAC (2011)
- Data for UNIFAC LLE
- Data for Lyngby UNIFAC
- Data for PSRK UNIFAC
- Data for VTPR UNIFAC

## 7.29.1 Main Model (Object-Oriented)

**class** thermo.unifac.**UNIFAC**(*T*, *xs*, *rs*, *qs*, *Qs*, *vs*, *psi\_coeffs=None*, *psi\_abc=None*, *version=0*)

Class for representing an a liquid with excess gibbs energy represented by the UNIFAC equation. This model is capable of representing VL and LL behavior, provided the correct interaction parameters are used. [1] and [2] are good references on this model.

## Parameters

- **T** [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]
- **rs** [list[float]] *r* parameters  $r_i = \sum_{k=1}^n \nu_k R_k$ , [-]

- **qs** [list[float]] q parameters  $q_i = \sum_{k=1}^n \nu_k Q_k$ , [-]
- **Qs** [list[float]] *Q* parameter for each subgroup; subgroups are not required to but are suggested to be sorted from lowest number to highest number, [-]
- vs [list[list[float]]] Indexed by [subgroup][count], this variable is the count of each subgroups in each compound, [-]
- **psi\_abc** [tuple(list[float]], 3), optional] *psi* interaction parameters between each subgroup; indexed [subgroup][subgroup], not symmetrical; first arg is the matrix for *a*, then *b*, and then *c*. Only one of *psi\_abc* or *psi\_coeffs* is required, [-]
- **psi\_coeffs** [list[list[tuple(float, 3)]], optional] *psi* interaction parameters between each subgroup; indexed [subgroup][subgroup][letter], not symmetrical. Only one of *psi\_abc* or *psi\_coeffs* is required, [-]

version [int, optional] Which version of the model to use [-]

- 0 original UNIFAC, OR UNIFAC LLE
- 1 Dortmund UNIFAC (adds T dept, 3/4 power)
- 2 PSRK (original with T dept function)
- 3 VTPR (drops combinatorial term, Dortmund UNIFAC otherwise)
- 4 Lyngby/Larsen has different combinatorial, 2/3 power
- 5 UNIFAC KT (2 params for psi, Lyngby/Larsen formulation; otherwise same as original)

#### **Notes**

In addition to the methods presented here, the methods of its base class thermo.activity.GibbsExcess are available as well.

#### References

[1], [2]

#### **Examples**

The DDBST has published numerous sample problems using UNIFAC; a simple binary system from example P05.22a in [2] with n-hexane and butanone-2 is shown below:

```
>>> from thermo.unifac import UFIP, UFSG
>>> GE = UNIFAC.from_subgroups(chemgroups=[{1:2, 2:4}, {1:1, 2:1, 18:1}], T=60+273.
...15, xs=[0.5, 0.5], version=0, interaction_data=UFIP, subgroups=UFSG)
>>> GE.gammas()
[1.4276025835, 1.3646545010]
>>> GE.GE(), GE.dGE_dT(), GE.d2GE_dT2()
(923.641197, 0.206721488, -0.00380070204)
>>> GE.HE(), GE.SE(), GE.dHE_dT(), GE.dSE_dT()
(854.77193363, -0.2067214889, 1.266203886, 0.0038007020460)
```

The solution given by the DDBST has the same values [1.428, 1.365], and can be found here: http:// chemthermo.ddbst.com/Problems\_Solutions/Mathcad\_Files/05.22a%20VLE%20of%20Hexane-Butanone-2% 20Via%20UNIFAC%20-%20Step%20by%20Step.xps

## Attributes

- T [float] Temperature, [K]
- **xs** [list[float]] Mole fractions, [-]

## Methods

CpE()	Calculate and return the first temperature derivative of excess enthalpy of a liquid phase using an activity
	coefficient model.
Fis()	Calculate the $F_i$ terms used in calculating the combi-
	natorial part.
<i>GE</i> ()	Calculate the excess Gibbs energy with the UNIFAC
	model.
HE()	Calculate and return the excess entropy of a liquid
	phase using an activity coefficient model.
SE()	Calculates the excess entropy of a liquid phase using
	an activity coefficient model.
Thetas()	Calculate the $\Theta_m$ parameters used in calculating the
	residual part.
Thetas_pure()	Calculate the $\Theta_m$ parameters for each chemical in
	the mixture as a pure species, used in calculating the
	residual part.
Vis()	Calculate the $V_i$ terms used in calculating the combi-
	natorial part.
Vis_modified()	Calculate the $V'_i$ terms used in calculating the com-
	binatorial part.
Xs()	Calculate the $X_m$ parameters used in calculating the
	residual part.
Xs_pure()	Calculate the $X_m$ parameters for each chemical in
• •	the mixture as a pure species, used in calculating the
	residual part.
as_json()	Method to create a JSON-friendly representation of
	the Gibbs Excess model which can be stored, and
	reloaded later.
d2Fis_dxixjs()	Calculate the second mole fraction derivative of the
	$F_i$ terms used in calculating the combinatorial part.
d2GE_dT2()	Calculate the second temperature derivative of excess
	Gibbs energy with the UNIFAC model.
d2GE_dTdns()	Calculate and return the mole number derivative of
	the first temperature derivative of excess Gibbs en-
	ergy of a liquid phase using an activity coefficien
	model.
d2GE_dTdxs()	Calculate the first composition derivative and tem-
	perature derivative of excess Gibbs energy with the
	UNIFAC model.
d2GE_dxixjs()	Calculate the second composition derivative of ex-
	cess Gibbs energy with the UNIFAC model.
d2Thetas_dxixjs()	Calculate the mole fraction derivatives of the $\Theta_m$ pa-
	rameters.
	continues on next page

d2Vis_dxixjs()	ntinued from previous page Calculate the second mole fraction derivative of the
alvio_axixjo()	$V_i$ terms used in calculating the combinatorial part.
d2Vis_modified_dxixjs()	Calculate the second mole fraction derivative of the
uzvis_moutifeu_uxixj5()	$V'_i$ terms used in calculating the combinatorial part.
d2lnGammas_subgroups_dT2()	$v_i$ terms used in calculating the combinatorial part. Calculate the second temperature derivative of the
uzinganunas_subgroups_uiz()	$\ln \Gamma_k$ parameters for the phase; depends on the
	phases's composition and temperature.
d2lnGammas_subgroups_dTdxs()	Calculate the temperature and mole fraction deriva
uzinganimas_subgroups_uruxs()	tives of the $\ln \Gamma_k$ parameters for the phase; dependence
	on the phases's composition and temperature.
d2lnGammas_subgroups_dxixjs()	Calculate the second mole fraction derivatives of
uzinganunas_subgroups_uxixjs()	the $\ln \Gamma_k$ parameters for the phase; depends on the
dolar Common on the success of the data	phases's composition and temperature.
d21nGammas_subgroups_pure_dT2()	Calculate the second temperature derivative of $\ln \Gamma_{\mu}$
	pure component parameters for the phase; depends
101	on the phases's temperature only.
d2lngammas_c_dT2()	Second temperature derivatives of the combinatoria
	part of the UNIFAC model.
d2lngammas_c_dTdx()	Second temperature derivative and first mole fraction
	derivative of the combinatorial part of the UNIFAC
	model.
d2lngammas_c_dxixjs()	Second composition derivative of the combinatoria
	part of the UNIFAC model.
d2lngammas_dT2()	Calculates the second temperature derivative of the
	residual part of the UNIFAC model.
d2lngammas_r_dT2()	Calculates the second temperature derivative of the
	residual part of the UNIFAC model.
d2lngammas_r_dTdxs()	Calculates the first mole fraction derivative of the
	temperature derivative of the residual part of the
	UNIFAC model.
d2lngammas_r_dxixjs()	Calculates the second mole fraction derivative of the
	residual part of the UNIFAC model.
d2nGE_dTdns()	Calculate and return the partial mole number deriva
	tive of the first temperature derivative of excess Gibbs
	energy of a liquid phase using an activity coefficien
	model.
d2nGE_dninjs()	Calculate and return the second partial mole number
	derivative of excess Gibbs energy of a liquid phase
	using an activity coefficient model.
d2psis_dT2()	Calculate the $\Psi$ term second temperature derivative
	matrix for all groups interacting with all other groups
d3Fis_dxixjxks()	Calculate the third mole fraction derivative of the F
	terms used in calculating the combinatorial part.
d3GE_dT3()	Calculate the third temperature derivative of excess
-	Gibbs energy with the UNIFAC model.
d3Vis_dxixjxks()	Calculate the third mole fraction derivative of the V
	terms used in calculating the combinatorial part.
d3Vis_modified_dxixjxks()	Calculate the third mole fraction derivative of the $V_i$
usvis_moulileu_uxixixks()	

Table 96 – continued from previous page	Table	96 –	continued	from	previous	page
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Calculate the third temperature derivative of the $\ln \Gamma_k$ barameters for the phase; depends on the phases's composition and temperature. Calculate the third temperature derivative of $\ln \Gamma_k$ bure component parameters for the phase; depends on the phases's temperature only. Third temperature derivatives of the combinatorial bart of the UNIFAC model. Third composition derivative of the combinatorial bart of the UNIFAC model. Calculates the third temperature derivative of the
composition and temperature. Calculate the third temperature derivative of $\ln \Gamma_k$ bure component parameters for the phase; depends on the phases's temperature only. Third temperature derivatives of the combinatorial bart of the UNIFAC model. Third composition derivative of the combinatorial bart of the UNIFAC model.
Calculate the third temperature derivative of $\ln \Gamma_k$ pure component parameters for the phase; depends on the phases's temperature only. Third temperature derivatives of the combinatorial part of the UNIFAC model. Third composition derivative of the combinatorial part of the UNIFAC model.
oure component parameters for the phase; depends on the phases's temperature only. Third temperature derivatives of the combinatorial part of the UNIFAC model. Third composition derivative of the combinatorial part of the UNIFAC model.
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esidual part of the UNIFAC model.
Calculates the third temperature derivative of the
esidual part of the UNIFAC model.
Calculate the $\Psi$ term third temperature derivative
matrix for all groups interacting with all other groups.
Calculate the mole fraction derivative of the $F_i$ terms
used in calculating the combinatorial part.
Calculate the first temperature derivative of excess
Gibbs energy with the UNIFAC model.
Calculate and return the mole number derivative of
excess Gibbs energy of a liquid phase using an activ-
ty coefficient model.
Calculate the first composition derivative of excess
Gibbs energy with the UNIFAC model.
Calculate and return the first temperature derivative
of excess enthalpy of a liquid phase using an activity
coefficient model.
Calculate and return the mole number derivative of
excess enthalpy of a liquid phase using an activity co-
efficient model.
Calculate and return the mole fraction derivative of
excess enthalpy of a liquid phase using an activity co-
efficient model.
Calculate and return the first temperature derivative
of excess entropy of a liquid phase using an activity
coefficient model.
Calculate and return the mole number derivative of
excess entropy of a liquid phase using an activity co-
efficient model.
Calculate and return the mole fraction derivative of
excess entropy of a liquid phase using an activity co-
efficient model.
Calculate the mole fraction derivatives of the $\Theta_m$ pa-
ameters. Colour the mole function derivative of the $V$ terms
Calculate the mole fraction derivative of the $V_i$ terms
used in calculating the combinatorial part.
Calculate the mole fraction derivative of the $V'_i$ terms
used in calculating the combinatorial part.
Calculates the first temperature derivative of activity
coefficients with the UNIFAC model.

Table 96 - continued from previous page

Table 96 – conti	nued from previous page
dgammas_dns()	Calculate and return the mole number derivative of
	activity coefficients of a liquid phase using an activity
	coefficient model.
dgammas_dxs()	Calculates the first mole fraction derivative of activ-
	ity coefficients with the UNIFAC model.
dlnGammas_subgroups_dT()	Calculate the first temperature derivative of the $\ln \Gamma_k$
	parameters for the phase; depends on the phases's
	composition and temperature.
dlnGammas_subgroups_dxs()	Calculate the mole fraction derivatives of the $\ln \Gamma_k$
	parameters for the phase; depends on the phases's
	composition and temperature.
dlnGammas_subgroups_pure_dT()	Calculate the first temperature derivative of $\ln \Gamma_k$
	pure component parameters for the phase; depends
	on the phases's temperature only.
dlngammas_c_dT()	Temperature derivatives of the combinatorial part of
5 = = 0	the UNIFAC model.
dlngammas_c_dxs()	First composition derivative of the combinatorial part
<b>· ·</b>	of the UNIFAC model.
dlngammas_dT()	Calculates the first temperature derivative of the
	residual part of the UNIFAC model.
dlngammas_r_dT()	Calculates the first temperature derivative of the
5	residual part of the UNIFAC model.
dlngammas_r_dxs()	Calculates the first mole fraction derivative of the
5	residual part of the UNIFAC model.
dnGE_dns()	Calculate and return the partial mole number deriva-
	tive of excess Gibbs energy of a liquid phase using an
	activity coefficient model.
dnHE_dns()	Calculate and return the partial mole number deriva-
	tive of excess enthalpy of a liquid phase using an ac-
	tivity coefficient model.
dnSE_dns()	Calculate and return the partial mole number deriva-
v	tive of excess entropy of a liquid phase using an ac-
	tivity coefficient model.
dpsis_dT()	Calculate the $\Psi$ term first temperature derivative ma-
	trix for all groups interacting with all other groups.
<pre>from_json(json_repr)</pre>	Method to create a Gibbs Excess model from a JSON-
5 5 - 1 /	friendly serialization of another Gibbs Excess model.
<pre>from_subgroups(T, xs, chemgroups[,])</pre>	Method to construct a UNIFAC object from a dictio-
	nary of interaction parameters parameters and a list
	of dictionaries of UNIFAC keys.
gammas()	Calculates the activity coefficients with the UNIFAC
	model.
<pre>gammas_infinite_dilution()</pre>	Calculate and return the infinite dilution activity co-
	efficients of each component.
<pre>lnGammas_subgroups()</pre>	Calculate the $\ln \Gamma_k$ parameters for the phase; depends
	on the phases's composition and temperature.
<pre>lnGammas_subgroups_pure()</pre>	Calculate the $\ln \Gamma_k$ pure component parameters for
	the phase; depends on the phases's temperature only.
lngammas_c()	Calculates the combinatorial part of the UNIFAC
Inguinto_C()	model.
lngammas_r()	Calculates the residual part of the UNIFAC model.
IIIgaillia3_I()	Calculates the residual part of the Ottil AC model.

Table	96 – 0	continued	from	previous	page
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Table 96 – continued from previous page		
<pre>model_hash()</pre>	Basic method to calculate a hash of the non-state	
	parts of the model This is useful for comparing to	
	models to determine if they are the same, i.e. in a	
	VLL flash it is important to know if both liquids have	
	the same model.	
psis()	Calculate the $\Psi$ term matrix for all groups interacting	
	with all other groups.	
<pre>state_hash()</pre>	Basic method to calculate a hash of the state of the	
	model and its model parameters.	
$to_T_xs(T, xs)$	Method to construct a new UNIFAC instance at tem-	
	perature $T$ , and mole fractions $xs$ with the same pa-	
	rameters as the existing object.	

Inphis\_args

## Fis()

Calculate the  $F_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters q only.

$$F_i = \frac{q_i}{\sum_j q_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

#### Returns

Fis [list[float]] F terms size number of components, [-]

#### GE()

Calculate the excess Gibbs energy with the UNIFAC model.

$$G^E = RT \sum_i x_i \left( \ln \gamma_i^c + \ln \gamma_i^r \right)$$

For the VTPR model, the combinatorial component is set to zero.

## Returns

GE [float] Excess Gibbs energy, [J/mol]

## Thetas()

Calculate the  $\Theta_m$  parameters used in calculating the residual part. A function of mole fractions and group counts only.

$$\Theta_m = \frac{Q_m X_m}{\sum_n Q_n X_n}$$

## Returns

**Thetas** [list[float]]  $\Theta_m$  terms, size number of subgroups, [-]

## Thetas\_pure()

Calculate the  $\Theta_m$  parameters for each chemical in the mixture as a pure species, used in calculating the residual part. A function of group counts only.

$$\Theta_m = \frac{Q_m X_m}{\sum_n Q_n X_n}$$

Returns

**Thetas\_pure** [list[list[float]]]  $\Theta_m$  terms, size number of components by number of subgroups and indexed in that order, [-]

#### Vis()

Calculate the  $V_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$V_i = \frac{r_i}{\sum_j r_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

#### Returns

**Vis** [list[float]] *V* terms size number of components, [-]

## Vis\_modified()

Calculate the  $V'_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$V_i' = \frac{r_i^n}{\sum_j r_j^n x_j}$$

This is used in the UNIFAC Dortmund and UNIFAC-NIST model with n=0.75, and the Lyngby model with n=2/3.

## Returns

**Vis\_modified** [list[float]] Modified V terms size number of components, [-]

**Xs**()

Calculate the  $X_m$  parameters used in calculating the residual part. A function of mole fractions and group counts only.

$$X_m = \frac{\sum_j \nu_m^j x_j}{\sum_j \sum_n \nu_n^j x_j}$$

#### Returns

**Xs** [list[float]]  $X_m$  terms, size number of subgroups, [-]

#### Xs\_pure()

Calculate the  $X_m$  parameters for each chemical in the mixture as a pure species, used in calculating the residual part. A function of group counts only, not even mole fractions or temperature.

$$X_m = \frac{\nu_m}{\sum_n^{gr} \nu_n}$$

#### Returns

**Xs\_pure** [list[list[float]]]  $X_m$  terms, size number of subgroups by number of components and indexed in that order, [-]

#### d2Fis\_dxixjs()

Calculate the second mole fraction derivative of the  $F_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters q only.

$$\frac{\partial F_i}{\partial x_j \partial x_k} = 2q_i q_j q_k G_{sum}^3$$
$$G_{sum} = \frac{1}{\sum_j q_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

## Returns

**d2Fis\_dxixjs** [list[list[float]]]] *F* terms size number of components by number of components, [-]

#### $d2GE_dT2()$

Calculate the second temperature derivative of excess Gibbs energy with the UNIFAC model.

$$\frac{\partial^2 G^E}{\partial T^2} = RT \sum_i x_i \frac{\partial^2 \ln \gamma_i^r}{\partial T^2} + 2R \sum_i x_i \frac{\partial \ln \gamma_i^r}{\partial T}$$

Returns

#### d2GE\_dTdxs()

Calculate the first composition derivative and temperature derivative of excess Gibbs energy with the UNI-FAC model.

$$\frac{\partial^2 G^E}{\partial T \partial x_i} = RT \left( \frac{\partial \ln \gamma_i^r}{\partial T} + \sum_j x_j \frac{\partial \ln \gamma_j^r}{\partial x_i} \right) + R \left[ \frac{\partial \ln \gamma_i^c}{\partial x_i} + \frac{\partial \ln \gamma_i^r}{\partial x_i} + \sum_j x_j \left( \frac{\partial \ln \gamma_j^c}{\partial x_i} + \frac{\partial \ln \gamma_j^r}{\partial x_i} \right) \right]$$

Returns

**dGE\_dxs** [list[float]] First composition derivative and first temperature derivative of excess Gibbs energy, [J/mol/K]

## d2GE\_dxixjs()

Calculate the second composition derivative of excess Gibbs energy with the UNIFAC model.

$$\frac{\partial^2 G^E}{\partial x_j \partial x_k} = RT \left[ \sum_i \left( \frac{\partial \ln \gamma_i^c}{\partial x_j \partial x_k} + \frac{\partial \ln \gamma_i^r}{\partial x_j \partial x_k} \right) + \frac{\partial \ln \gamma_j^c}{\partial x_k} + \frac{\partial \ln \gamma_j^r}{\partial x_k} + \frac{\partial \ln \gamma_k^c}{\partial x_j} + \frac{\partial \ln \gamma_k^c}{\partial x_j} \right] \right]$$

#### Returns

**d2GE\_dxixjs** [list[list[float]]] Second composition derivative of excess Gibbs energy, [J/mol]

## d2Thetas\_dxixjs()

Calculate the mole fraction derivatives of the  $\Theta_m$  parameters. A function of mole fractions and group counts only.

$$\begin{split} \frac{\partial^2 \Theta_i}{\partial x_j \partial x_k} &= \frac{Q_i}{\sum_n Q_n (\nu x)_{sum,n}} \left[ -F(\nu)_{sum,j} \nu_{i,k} - F(\nu)_{sum,k} \nu_{i,j} + 2F^2(\nu)_{sum,j} (\nu)_{sum,k} (\nu x)_{sum,i} + \frac{F(\nu x)_{sum,i} \left[\sum_n V_n (\nu x)_{sum,i}\right]}{G = \frac{1}{\sum_j Q_j X_j}} \right] \\ &= \frac{1}{\sum_j \sum_n \nu_n^j x_j} \\ &= \frac{1}{\sum_j \sum_n \nu_n^j x_j} \\ &= \frac{1}{\sum_j \nu_{i,j} x_j} \end{split}$$

Returns

**d2Thetas\_dxixjs** [list[list[float]]]]  $\Theta_m$  terms, size number of subgroups by mole fractions and indexed in that order, [-]

#### d2Vis\_dxixjs()

Calculate the second mole fraction derivative of the  $V_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$\frac{\partial V_i}{\partial x_j \partial x_k} = 2r_i r_j r_k V_{sun}^3$$
$$V_{sum} = \frac{1}{\sum_j r_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

#### Returns

**d2Vis\_dxixjs** [list[list[float]]]] *V* terms size number of components by number of components, [-]

## d2Vis\_modified\_dxixjs()

Calculate the second mole fraction derivative of the  $V'_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$\frac{\partial V'_i}{\partial x_j \partial x_k} = 2r_i^n r_j^n r_k^n V_{sum}^3$$
$$V_{sum} = \frac{1}{\sum_i r_i^n x_j}$$

This is used in the UNIFAC Dortmund and UNIFAC-NIST model with n=0.75, and the Lyngby model with n=2/3.

#### Returns

**d2Vis\_modified\_dxixjs** [list[list[list[float]]]] *V*' terms size number of components by number of components, [-]

### d2lnGammas\_subgroups\_dT2()

Calculate the second temperature derivative of the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\begin{split} \frac{\partial^2 \ln \Gamma_i}{\partial T^2} &= -Q_i \left[ Z(i)G(i) - F(i)^2 Z(i)^2 + \sum_j \left( \theta_j Z(j) \frac{\partial^2 \psi_{i,j}}{\partial T} - Z(j)^2 \left( G(j) \theta_j \psi_{i,j} + 2F_j \theta_j \frac{\partial \psi_{i,j}}{\partial T} \right) + 2Z(j)^3 F(j)^2 \right. \\ \left. F(k) &= \sum_m^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T} \right. \\ \left. G(k) &= \sum_m^{gr} \theta_m \frac{\partial^2 \psi_{m,k}}{\partial T^2} \right. \\ \left. Z(k) &= \frac{1}{\sum_m \Theta_m \Psi_{m,k}} \end{split}$$

Returns

**d2lnGammas\_subgroups\_dT2** [list[float]] Second temperature derivative of ln Gamma parameters for each subgroup, size number of subgroups, [1/K^2]

#### d2lnGammas\_subgroups\_dTdxs()

Calculate the temperature and mole fraction derivatives of the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\frac{\partial^2 \ln \Gamma_k}{\partial x_i \partial T} = -Q_k \left( D(k,i)Z(k) - B(k)W(k,i)Z(k)^2 + \sum_m^{gr} (Z(m)\frac{\partial \theta_m}{\partial x_i}\frac{\partial \psi_{k,m}}{\partial T}) - \sum_m^{gr} (B(m)Z(m)^2\psi_{k,m}\frac{\partial \theta_m}{\partial x_i}) - \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k)^2) + \sum_m^{gr} (Z(m)\frac{\partial \theta_m}{\partial x_i}\frac{\partial \psi_{k,m}}{\partial T}) - \sum_m^{gr} (B(m)Z(m)^2\psi_{k,m}\frac{\partial \theta_m}{\partial x_i}) - \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k)^2) + \sum_m^{gr} (Z(m)\frac{\partial \theta_m}{\partial x_i}\frac{\partial \psi_{k,m}}{\partial T}) - \sum_m^{gr} (B(m)Z(m)^2\psi_{k,m}\frac{\partial \theta_m}{\partial x_i}) - \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k)^2) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k)) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k)) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k) + \sum_m^{gr} (D(k,i)Z(k) - B(k)W(k,i)Z(k) + \sum_m^{gr} (D(k,i)Z(k) + \sum$$

The following groups are used as follows to simplfy the number of evaluations:

$$W(k,i) = \sum_{m}^{gr} \psi_{m,k} \frac{\partial \theta_m}{\partial x_i}$$
$$Z(k) = \frac{1}{\sum_{m} \Theta_m \Psi_{mk}}$$
$$F(k) = \sum_{m}^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T}$$

In the below expression, k` refers to a group, and *i* refers to a component.

$$D(k,i) = \sum_{m}^{gr} \frac{\partial \theta_m}{\partial x_i} \frac{\partial \psi_{m,k}}{\partial T}$$

#### Returns

**d2lnGammas\_subgroups\_dTdxs** [list[list[float]]] Temperature and mole fraction derivatives of Gamma parameters for each subgroup, size number of subgroups by number of components and indexed in that order, [1/K]

#### d2lnGammas\_subgroups\_dxixjs()

Calculate the second mole fraction derivatives of the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\frac{\partial^2 \ln \Gamma_k}{\partial x_i \partial x_j} = -Q_k \left( -Z(k)K(k,i,j) - \sum_m^{gr} Z(m)^2 K(m,i,j) \theta_m \psi_{k,m} - W(k,i)W(k,j)Z(k)^2 + \sum_m^{gr} Z_m \psi_{k,m} \frac{\partial^2 \theta_m}{\partial x_i \partial x_j} - \frac{\partial^2 (1 - C_k)}{\partial x_i \partial x_j} \right) = -Q_k \left( -Z(k)K(k,i,j) - \sum_m^{gr} Z(m)^2 K(m,i,j) \theta_m \psi_{k,m} - W(k,i)W(k,j)Z(k)^2 + \sum_m^{gr} Z_m \psi_{k,m} \frac{\partial^2 \theta_m}{\partial x_i \partial x_j} - \frac{\partial^2 (1 - C_k)}{\partial x_i \partial x_j} \right) \right)$$

The following groups are used as follows to simplfy the number of evaluations:

$$W(k,i) = \sum_{m}^{gr} \psi_{m,k} \frac{\partial \theta_m}{\partial x_i}$$
$$Z(k) = \frac{1}{\sum_{m} \Theta_m \Psi_{mk}}$$
$$K(k,i,j) = \sum_{m}^{gr} \psi_{m,k} \frac{\partial^2 \theta_m}{\partial x_i \partial x_j}$$

Returns

**d2lnGammas\_subgroups\_dxixjs** [list[list[float]]]] Second mole fraction derivatives of Gamma parameters for each subgroup, size number of components by number of subgroups and indexed in that order, [-]

## d2lnGammas\_subgroups\_pure\_dT2()

Calculate the second temperature derivative of  $\ln \Gamma_k$  pure component parameters for the phase; depends on the phases's temperature only.

$$\frac{\partial^2 \ln \Gamma_i}{\partial T^2} = -Q_i \left[ Z(i)G(i) - F(i)^2 Z(i)^2 + \sum_j \left( \theta_j Z(j) \frac{\partial^2 \psi_{i,j}}{\partial T} - Z(j)^2 \left( G(j) \theta_j \psi_{i,j} + 2F_j \theta_j \frac{\partial \psi_{i,j}}{\partial T} \right) + 2Z(j)^3 F(j)^2 \theta_j \frac{\partial \psi_{i,j}}{\partial T} \right] \right]$$

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$$F(k) = \sum_{m}^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T}$$
$$G(k) = \sum_{m}^{gr} \theta_m \frac{\partial^2 \psi_{m,k}}{\partial T^2}$$
$$Z(k) = \frac{1}{\sum_{m} \Theta_m \Psi_{m,k}}$$

In this model, the  $\Theta$  values come from the UNIFAC. Thetas\_pure method, where each compound is assumed to be pure.

#### Returns

**d2lnGammas\_subgroups\_pure\_dT2** [list[list[float]]] Second temperature derivative of ln Gamma parameters for each subgroup, size number of subgroups by number of components and indexed in that order, [1/K^2]

#### d2lngammas\_c\_dT2()

Second temperature derivatives of the combinatorial part of the UNIFAC model. Zero in all variations.

$$\frac{\partial^2 \ln \gamma_i^c}{\partial T^2} = 0$$

#### Returns

d2lngammas\_c\_dT2 [list[float]] Combinatorial lngammas term second temperature derivatives, size number of components, [-]

#### d2lngammas\_c\_dTdx()

Second temperature derivative and first mole fraction derivative of the combinatorial part of the UNIFAC model. Zero in all variations.

$$\frac{\partial^3 \ln \gamma_i^c}{\partial T^2 \partial x_i} = 0$$

#### Returns

**d2lngammas\_c\_dTdx** [list[list[float]]] Combinatorial lngammas term second temperature derivatives, size number of components by number of components, [-]

## d2lngammas\_c\_dxixjs()

Second composition derivative of the combinatorial part of the UNIFAC model. For the modified UNIFAC model, the equation is as follows; for the original UNIFAC and UNIFAC LLE, replace  $V'_i$  with  $V_i$ .

$$\frac{\partial \ln \gamma_i^c}{\partial x_j \partial x_k} = 5q_i \left( \frac{-\frac{d^2}{dx_k dx_j} V_i + \frac{V_i \frac{d^2}{dx_k dx_j} F_i}{F_i} + \frac{\frac{d}{dx_j} F_i \frac{d}{dx_k} V_i}{F_i} + \frac{\frac{d}{dx_k} F_i \frac{d}{dx_j} V_i}{F_i} - \frac{2V_i \frac{d}{dx_j} F_i \frac{d}{dx_k} F_i}{F_i^2}}{V_i^2} + \frac{\left(\frac{d}{dx_j} V_i - \frac{V_i \frac{d}{dx_j} F_i}{F_i}\right) \frac{d}{dx_k} V_i}{V_i^2} \right)$$

For the Lyngby model, the following equations are used:

$$\frac{\partial^2 \ln \gamma_i^c}{\partial x_j \partial x_k} = -\frac{\partial^2 V_i'}{\partial x_j \partial x_k} + \frac{1}{V_i'} \frac{\partial^2 V_i'}{\partial x_j \partial x_k} - \frac{1}{(V_i')^2} \frac{\partial V_i'}{\partial x_j} \frac{\partial V_i'}{\partial x_k}$$

#### Returns

**d2lngammas\_c\_dxixjs** [list[list[list[float]]]] Combinatorial lngammas term second composition derivative, size number of components by number of components by number of components, [-]

#### d2lngammas\_dT2()

Calculates the second temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial^2 \ln \gamma_i^r}{\partial T^2} = \sum_k^{gr} \nu_k^{(i)} \left[ \frac{\partial^2 \ln \Gamma_k}{\partial T^2} - \frac{\partial^2 \ln \Gamma_k^{(i)}}{\partial T^2} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

Returns

d2lngammas\_r\_dT2 [list[float]] Residual lngammas terms second temperature derivative, size number of components [1/K^2]

#### d2lngammas\_r\_dT2()

Calculates the second temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial^2 \ln \gamma_i^r}{\partial T^2} = \sum_k^{gr} \nu_k^{(i)} \left[ \frac{\partial^2 \ln \Gamma_k}{\partial T^2} - \frac{\partial^2 \ln \Gamma_k^{(i)}}{\partial T^2} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

#### Returns

**d2lngammas\_r\_dT2** [list[float]] Residual lngammas terms second temperature derivative, size number of components [1/K^2]

## d2lngammas\_r\_dTdxs()

Calculates the first mole fraction derivative of the temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial^2 \ln \gamma_i^r}{\partial x_j \partial T} = \sum_m^{gr} \nu_m^{(i)} \frac{\partial^2 \ln \Gamma_m}{\partial x_j \partial T}$$

#### Returns

**d2lngammas\_r\_dTdxs** [list[list[float]]] First mole fraction derivative and temperature derivative of residual lngammas terms, size number of components by number of components [-]

## d2lngammas\_r\_dxixjs()

Calculates the second mole fraction derivative of the residual part of the UNIFAC model.

$$\frac{\partial^2 \ln \gamma_i^r}{\partial x_j^2} = \sum_m^{gr} \nu_m^{(i)} \frac{\partial^2 \ln \Gamma_m}{\partial x_j^2}$$

#### Returns

**d2lngammas\_r\_dxixjs** [list[list[list[float]]]] Second mole fraction derivative of the residual lngammas terms, size number of components by number of components by number of components [-]

#### d2psis\_dT2()

Calculate the  $\Psi$  term second temperature derivative matrix for all groups interacting with all other groups.

The main model calculates the derivative as a function of three coefficients;

$$\frac{\partial^2 \Psi_{mn}}{\partial T^2} = \frac{\left(-2c_{mn} + \frac{2(2Tc_{mn} + b_{mn})}{T} + \frac{\left(2Tc_{mn} + b_{mn} - \frac{T^2c_{mn} + Tb_{mn} + a_{mn}}{T}\right)^2}{T} - \frac{2\left(T^2c_{mn} + Tb_{mn} + a_{mn}\right)}{T^2}\right)e^{-\frac{T^2c_{mn} + Tb_{mn} + a_{mn}}{T}}$$

Only the first, *a* coefficient, is used in the original UNIFAC model as well as the UNIFAC-LLE model, so the expression simplifies to:

$$\frac{\partial^2 \Psi_{mn}}{\partial T^2} = \frac{a_{mn} \left(-2 + \frac{a_{mn}}{T}\right) e^{-\frac{a_{mn}}{T}}}{T^3}$$

For the Lyngby model, the second temperature derivative is:

$$\frac{\partial^2 \Psi_{mk}}{\partial T^2} = \frac{\left(2a_2 + 2a_3 \ln\left(\frac{T_0}{T}\right) + a_3 + \left(a_2 + a_3 \ln\left(\frac{T_0}{T}\right) - \frac{a_1 + a_2(T - T_0) + a_3\left(T \ln\left(\frac{T_0}{T}\right) + T - T_0\right)}{T}\right)^2 - \frac{2\left(a_1 + a_2(T - T_0) + a_3\left(T \ln\left(\frac{T_0}{T}\right) + T - T_0\right)}{T}\right)^2}{T^2}$$

with  $T_0 = 298.15$  K and the *a* coefficients are specific to each pair of main groups, and they are asymmetric, so  $a_{0,mk} \neq a_{0,km}$ .

#### Returns

**d2psis\_dT2** [list[list[float]]] Second temperature derivative of psi` terms, size subgroups x subgroups [-]

## d3Fis\_dxixjxks()

Calculate the third mole fraction derivative of the  $F_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters q only.

$$\frac{\partial F_i}{\partial x_j \partial x_k \partial x_m} = -6q_i q_j q_k q_m G_{sum}^4$$
$$G_{sum} = \frac{1}{\sum_j q_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

## Returns

**d3Fis\_dxixjxks** [list[list[list[float]]]]] *F* terms size number of components by number of components by number of components, [-]

#### d3GE\_dT3()

Calculate the third temperature derivative of excess Gibbs energy with the UNIFAC model.

$$\frac{\partial^3 G^E}{\partial T^3} = RT \sum_i x_i \frac{\partial^3 \ln \gamma_i^r}{\partial T^3} + 3R \sum_i x_i \frac{\partial^2 \ln \gamma_i^r}{\partial T^2}$$

#### Returns

d3GE\_dT3 [float] Third temperature derivative of excess Gibbs energy, [J/mol/K^3]

## d3Vis\_dxixjxks()

Calculate the third mole fraction derivative of the  $V_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$\frac{\partial V_i}{\partial x_j \partial x_k \partial x_m} = -6r_i r_j r_k r_m V_{sum}^4$$
$$V_{sum} = \frac{1}{\sum_j r_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

#### Returns

**d3Vis\_dxixjxks** [list[list[list[float]]]]] *V* terms size number of components by number of components by number of components, [-]

## d3Vis\_modified\_dxixjxks()

Calculate the third mole fraction derivative of the  $V'_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$\frac{\partial V'_i}{\partial x_j \partial x_k \partial x_m} = -6r_i^n r_j^n r_k^n r_m^n V_{sum}^4$$
$$V_{sum} = \frac{1}{\sum_j r_j x_j}$$

This is used in the UNIFAC Dortmund and UNIFAC-NIST model with n=0.75, and the Lyngby model with n=2/3.

#### Returns

**d3Vis\_modified\_dxixjxks** [list[list[list[list[float]]]]] *V*' terms size number of components by number of components by number of components, [-]

## d3lnGammas\_subgroups\_dT3()

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Calculate the third temperature derivative of the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\begin{split} \frac{\partial^3 \ln \Gamma_i}{\partial T^3} &= Q_i \left[ -H(i)Z(i) - 2F(i)^3 Z(i)^3 + 3F(i)G(i)Z(i)^2 + \left( -\theta_j Z(j) \frac{\partial^3 \psi}{\partial T^3} + H(j)Z(j)^2 \theta(j)\psi_{i,j} - 6F(j)^2 Z(j)^3 \theta \right) \right] \\ &\quad F(k) = \sum_m^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T} \\ &\quad G(k) = \sum_m^{gr} \theta_m \frac{\partial^2 \psi_{m,k}}{\partial T^2} \\ &\quad H(k) = \sum_m^{gr} \theta_m \frac{\partial^3 \psi_{m,k}}{\partial T^3} \\ &\quad Z(k) = \frac{1}{\sum_m \Theta_m \Psi_{m,k}} \end{split}$$
Returns

**d3lnGammas\_subgroups\_dT3** [list[float]] Third temperature derivative of ln Gamma parameters for each subgroup, size number of subgroups, [1/K^3]

#### d3lnGammas\_subgroups\_pure\_dT3()

Calculate the third temperature derivative of  $\ln \Gamma_k$  pure component parameters for the phase; depends on the phases's temperature only.

$$\begin{split} \frac{\partial^3 \ln \Gamma_i}{\partial T^3} &= Q_i \left[ -H(i)Z(i) - 2F(i)^3 Z(i)^3 + 3F(i)G(i)Z(i)^2 + \left( -\theta_j Z(j) \frac{\partial^3 \psi}{\partial T^3} + H(j)Z(j)^2 \theta(j)\psi_{i,j} - 6F(j)^2 Z(j)^3 \right) \right] \\ &\quad F(k) = \sum_m^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T} \\ &\quad G(k) = \sum_m^{gr} \theta_m \frac{\partial^2 \psi_{m,k}}{\partial T^2} \\ &\quad H(k) = \sum_m^{gr} \theta_m \frac{\partial^3 \psi_{m,k}}{\partial T^3} \\ &\quad Z(k) = \frac{1}{\sum_m \Theta_m \Psi_{m,k}} \end{split}$$

In this model, the  $\Theta$  values come from the UNIFAC. Thetas\_pure method, where each compound is assumed to be pure.

#### Returns

**d3lnGammas\_subgroups\_pure\_dT3** [list[list[float]]] Third temperature derivative of ln Gamma parameters for each subgroup, size number of subgroups by number of components and indexed in that order, [1/K^3]

## d3lngammas\_c\_dT3()

Third temperature derivatives of the combinatorial part of the UNIFAC model. Zero in all variations.

$$\frac{\partial^3 \ln \gamma_i^c}{\partial T^3} = 0$$

#### Returns

d3lngammas\_c\_dT3 [list[float]] Combinatorial lngammas term second temperature derivatives, size number of components, [-]

## d3lngammas\_c\_dxixjxks()

Third composition derivative of the combinatorial part of the UNIFAC model. For the modified UNIFAC model, the equation is as follows; for the original UNIFAC and UNIFAC LLE, replace  $V'_i$  with  $V_i$ .

$$\frac{\partial \ln \gamma_i^c}{\partial x_j \partial x_k \partial x_m} = -\frac{d^3}{dx_m dx_k dx_j} Vi' + \frac{\frac{d^3}{dx_m dx_k dx_j} Vi'}{Vi'} - \frac{\frac{d}{dx_j} Vi' \frac{d^2}{dx_m dx_k} Vi'}{Vi'^2} - \frac{\frac{d}{dx_k} Vi' \frac{d^2}{dx_m dx_j} Vi'}{Vi'^2} - \frac{\frac{d}{dx_m} Vi' \frac{d^2}{dx_k dx_j} Vi'}{Vi'^2} + \frac{\frac{d}{dx_m} Vi' \frac{dx_m}{Vi'^2} Vi'}{Vi'^2} + \frac{\frac{d}{dx_m} Vi' \frac{dx_m}{Vi'^2} Vi'$$

For the Lyngby model, the following equations are used:

$$\frac{\partial^3 \ln \gamma_i^c}{\partial x_j \partial x_k \partial x_m} = \frac{\partial^3 V_i'}{\partial x_j \partial x_k \partial x_m} \left( \frac{1}{V_i'} - 1 \right) - \frac{1}{(V_i')^2} \left( \frac{\partial V_i'}{\partial x_j} \frac{\partial V_i'}{\partial x_k \partial x_m} + \frac{\partial V_i'}{\partial x_k} \frac{\partial V_i'}{\partial x_j \partial x_m} + \frac{\partial V_i'}{\partial x_m} \frac{\partial V_i'}{\partial x_j \partial x_k} \right) + \frac{2}{(V_i')^3} \frac{\partial V_i'}{\partial x_j} \frac{\partial V_i'}{\partial x_k} \frac{\partial V_i'}{\partial x_k} + \frac{2}{(V_i')^3} \frac{\partial V_i'}{\partial x_j} \frac{\partial V_i'}{\partial x_k} \frac{\partial V_i'}{\partial x_k} + \frac{2}{(V_i')^3} \frac{\partial V_i'}{\partial x_j} \frac{\partial V_i'}{\partial x_k} \frac{\partial V_i'}{\partial x_k} + \frac{2}{(V_i')^3} \frac{\partial V_i'}{\partial x_j} \frac{\partial V_i'}{\partial x_k} + \frac{2}{(V_i')^3} \frac{\partial V_i'}{\partial x_k} \frac{\partial V_i$$

Returns

**d3lngammas\_c\_dxixjxks** [list[list[list[list[float]]]]] Combinatorial lngammas term third composition derivative, size number of components by number of components by number of components by number of components, [-]

## d3lngammas\_dT3()

Calculates the third temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial^3 \ln \gamma_i^r}{\partial T^3} = \sum_k^{gr} \nu_k^{(i)} \left[ \frac{\partial^2 3 \ln \Gamma_k}{\partial T^3} - \frac{\partial^3 \ln \Gamma_k^{(i)}}{\partial T^3} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

## Returns

**d3lngammas\_r\_dT3** [list[float]] Residual lngammas terms third temperature derivative, size number of components [1/K^3]

#### d3lngammas\_r\_dT3()

Calculates the third temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial^3 \ln \gamma_i^r}{\partial T^3} = \sum_k^{gr} \nu_k^{(i)} \left[ \frac{\partial^2 3 \ln \Gamma_k}{\partial T^3} - \frac{\partial^3 \ln \Gamma_k^{(i)}}{\partial T^3} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

#### Returns

d3lngammas\_r\_dT3 [list[float]] Residual lngammas terms third temperature derivative, size number of components [1/K^3]

#### d3psis\_dT3()

Calculate the  $\Psi$  term third temperature derivative matrix for all groups interacting with all other groups.

The main model calculates the derivative as a function of three coefficients;

$$\frac{\partial^3 \Psi_{mn}}{\partial T^3} = \frac{\left(6c_{mn} + 6\left(c_{mn} - \frac{2Tc_{mn} + b_{mn}}{T} + \frac{T^2 c_{mn} + T b_{mn} + a_{mn}}{T^2}\right)\left(2Tc_{mn} + b_{mn} - \frac{T^2 c_{mn} + T b_{mn} + a_{mn}}{T}\right) - \frac{6(2Tc_{mn} + b_{mn} - T b_{mn} + a_{mn})}{T^2}\right)}{T^2}$$

Only the first, *a* coefficient, is used in the original UNIFAC model as well as the UNIFAC-LLE model, so the expression simplifies to:

$$\frac{\partial^3 \Psi_{mn}}{\partial T^3} = \frac{a_{mn} \left(6 - \frac{6a_{mn}}{T} + \frac{a_{mn}^2}{T^2}\right) e^{-\frac{a_{mn}}{T}}}{T^4}$$

For the Lyngby model, the third temperature derivative is:

$$\frac{\partial^{3}\Psi_{mk}}{\partial T^{3}} = -\frac{\left(6a_{2} + 6a_{3}\ln\left(\frac{T_{0}}{T}\right) + 4a_{3} + \left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + T - T_{0}\right)}{T}\right)^{3} + 3\left(a_{2} + a_{3}\ln\left(\frac{T_{0}}{T}\right) - \frac{a_{1} + a_{2}(T - T_{0}) + a_{3}\left(T\ln\left(\frac{T_{0}}{T}\right) + a_{3}\left(T$$

with  $T_0 = 298.15$  K and the *a* coefficients are specific to each pair of main groups, and they are asymmetric, so  $a_{0,mk} \neq a_{0,km}$ .

#### Returns

**d3psis\_dT3** [list[list[float]]] Third temperature derivative of psi` terms, size subgroups x subgroups [-]

#### dFis\_dxs()

Calculate the mole fraction derivative of the  $F_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters q only.

$$\frac{\partial F_i}{\partial x_j} = -q_i q_j G_{sum}^2$$
$$G_{sum} = \frac{1}{\sum_j q_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

#### Returns

dFis\_dxs [list[list[float]]] F terms size number of components by number of components, [-]

 $dGE_dT()$ 

Calculate the first temperature derivative of excess Gibbs energy with the UNIFAC model.

$$\frac{\partial G^E}{\partial T} = RT \sum_i x_i \frac{\partial \ln \gamma_i^r}{\partial T} + \frac{G^E}{T}$$

Returns

**dGE\_dT** [float] First temperature derivative of excess Gibbs energy, [J/mol/K]

dGE\_dxs()

Calculate the first composition derivative of excess Gibbs energy with the UNIFAC model.

$$\frac{\partial G^E}{\partial x_i} = RT \left( \ln \gamma_i^c + \ln \gamma_i^r \right) + RT \sum_j x_j \left( \frac{\partial \ln \gamma_j^c}{\partial x_i} + \frac{\partial \ln \gamma_j^r}{\partial x_i} \right)$$

#### Returns

dGE\_dxs [list[float]] First composition derivative of excess Gibbs energy, [J/mol]

#### dThetas\_dxs()

Calculate the mole fraction derivatives of the  $\Theta_m$  parameters. A function of mole fractions and group counts only.

$$\begin{split} \frac{\partial \Theta_i}{\partial x_j} &= FGQ_i \left[ FG(\nu x)_{sum,i} \left( \sum_k^{gr} FQ_k(\nu)_{sum,j}(\nu x)_{sum,k} - \sum_k^{gr} Q_k \nu_{k,j} \right) - F(\nu)_{sum,j}(\nu x)_{sum,i} + \nu_{ij} \right] \\ G &= \frac{1}{\sum_j Q_j X_j} \\ F &= \frac{1}{\sum_j \sum_n \nu_n^j x_j} \\ (\nu)_{sum,i} &= \sum_j \nu_{j,i} \\ (\nu x)_{sum,i} &= \sum_j \nu_{i,j} x_j \end{split}$$

#### Returns

**dThetas\_dxs** [list[list[float]]] Mole fraction derivatives of  $\Theta_m$  terms, size number of subgroups by mole fractions and indexed in that order, [-]

## dVis\_dxs()

Calculate the mole fraction derivative of the  $V_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$\frac{\partial V_i}{\partial x_j} = -r_i r_j V_{sum}^2$$
$$V_{sum} = \frac{1}{\sum_j r_j x_j}$$

This is used in the UNIFAC, UNIFAC-LLE, UNIFAC Dortmund, UNIFAC-NIST, and PSRK models.

#### Returns

**dVis\_dxs** [list[list[float]]] *V* terms size number of components by number of components, [-]

### dVis\_modified\_dxs()

Calculate the mole fraction derivative of the  $V'_i$  terms used in calculating the combinatorial part. A function of mole fractions and the parameters r only.

$$\frac{\partial V_i'}{\partial x_j} = -r_i^n r_j^n V_{sum}^2$$
$$V_{sum} = \frac{1}{\sum_j r_j^n x_j}$$

This is used in the UNIFAC Dortmund and UNIFAC-NIST model with n=0.75, and the Lyngby model with n=2/3.

#### Returns

**dVis\_modified\_dxs** [list[list[float]]] V' terms size number of components by number of components, [-]

#### dgammas\_dT()

Calculates the first temperature derivative of activity coefficients with the UNIFAC model.

$$\frac{\partial \gamma_i}{\partial T} = \gamma_i \frac{\partial \ln \gamma_i^r}{\partial T}$$

Returns

**dgammas\_dT** [list[float]] First temperature derivative of activity coefficients, size number of components [1/K]

## dgammas\_dns()

Calculate and return the mole number derivative of activity coefficients of a liquid phase using an activity coefficient model.

$$\frac{\partial \gamma_i}{\partial n_i} = \gamma_i \left( \frac{\frac{\partial^2 G^E}{\partial x_i \partial x_j}}{RT} \right)$$

Returns

dgammas\_dns [list[list[float]]] Mole number derivatives of activity coefficients, [1/mol]

#### dgammas\_dxs()

Calculates the first mole fraction derivative of activity coefficients with the UNIFAC model.

$$\frac{\partial \gamma_i}{\partial x_j} = \gamma_i \left( \frac{\partial \ln \gamma_i^r}{\partial x_j} + \frac{\partial \ln \gamma_i^c}{\partial x_j} \right)$$

For the VTPR variant, the combinatorial part is skipped:

$$\frac{\partial \gamma_i}{\partial x_j} = \gamma_i \left( \frac{\partial \ln \gamma_i^r}{\partial x_j} \right)$$

Returns

**dgammas\_dxs** [list[list[float]]] First mole fraction derivative of activity coefficients, size number of components by number of components [-]

#### dlnGammas\_subgroups\_dT()

Calculate the first temperature derivative of the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\begin{aligned} \frac{\partial \ln \Gamma_i}{\partial T} &= Q_i \left( \sum_{j}^{gr} Z(j) \left[ \theta_j \frac{\partial \psi_{i,j}}{\partial T} + \theta_j \psi_{i,j} F(j) Z(j) \right] - F(i) Z(i) \right) \\ F(k) &= \sum_{m}^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T} \\ Z(k) &= \frac{1}{\sum_m \Theta_m \Psi_{m,k}} \end{aligned}$$

Returns

**dlnGammas\_subgroups\_dT** [list[float]] First temperature derivative of ln Gamma parameters for each subgroup, size number of subgroups, [1/K]

#### dlnGammas\_subgroups\_dxs()

Calculate the mole fraction derivatives of the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\frac{\partial \ln \Gamma_k}{\partial x_i} = Q_k \left( -\frac{\sum_m^{gr} \psi_{m,k} \frac{\partial \theta_m}{\partial x_i}}{\sum_m^{gr} \theta_m \psi_{m,k}} - \sum_m^{gr} \frac{\psi_{k,m} \frac{\partial \theta_m}{\partial x_i}}{\sum_n^{gr} \theta_n \psi_{n,m}} + \sum_m^{gr} \frac{(\sum_n^{gr} \psi_{n,m} \frac{\partial \theta_n}{\partial x_i})\theta_m \psi_{k,m}}{(\sum_n^{gr} \theta_n \psi_{n,m})^2} \right)$$

The group W is used internally as follows to simplfy the number of evaluations.

$$W(k,i) = \sum_{m}^{gr} \psi_{m,k} \frac{\partial \theta_m}{\partial x_i}$$

#### Returns

**dlnGammas\_subgroups\_dxs** [list[list[float]]] Mole fraction derivatives of Gamma parameters for each subgroup, size number of subgroups by number of components and indexed in that order, [-]

## dlnGammas\_subgroups\_pure\_dT()

Calculate the first temperature derivative of  $\ln \Gamma_k$  pure component parameters for the phase; depends on the phases's temperature only.

$$\begin{aligned} \frac{\partial \ln \Gamma_i}{\partial T} &= Q_i \left( \sum_{j}^{gr} Z(j) \left[ \theta_j \frac{\partial \psi_{i,j}}{\partial T} + \theta_j \psi_{i,j} F(j) Z(j) \right] - F(i) Z(i) \right) \\ F(k) &= \sum_{m}^{gr} \theta_m \frac{\partial \psi_{m,k}}{\partial T} \\ Z(k) &= \frac{1}{\sum_m \Theta_m \Psi_{m,k}} \end{aligned}$$

In this model, the  $\Theta$  values come from the UNIFAC. Thetas\_pure method, where each compound is assumed to be pure.

#### Returns

**dlnGammas\_subgroups\_pure\_dT** [list[list[float]]] First temperature derivative of ln Gamma parameters for each subgroup, size number of subgroups by number of components and indexed in that order, [1/K]

## dlngammas\_c\_dT()

Temperature derivatives of the combinatorial part of the UNIFAC model. Zero in all variations.

$$\frac{\partial \ln \gamma_i^c}{\partial T} = 0$$

#### Returns

**dlngammas\_c\_dT** [list[float]] Combinatorial lngammas term temperature derivatives, size number of components, [-]

#### dlngammas\_c\_dxs()

First composition derivative of the combinatorial part of the UNIFAC model. For the modified UNIFAC model, the equation is as follows; for the original UNIFAC and UNIFAC LLE, replace  $V'_i$  with  $V_i$ .

$$\frac{\partial \ln \gamma_i^c}{\partial x_j} = -5q_i \left[ \left( \frac{\frac{\partial V_i}{\partial x_j}}{F_i} - \frac{V_i \frac{\partial F_i}{\partial x_j}}{F_i^2} \right) \frac{F_i}{V_i} - \frac{\frac{\partial V_i}{\partial x_j}}{F_i} + \frac{V_i \frac{\partial F_i}{\partial x_j}}{F_i^2} \right] - \frac{\partial V_i'}{\partial x_j} + \frac{\frac{\partial V_i'}{\partial x_j}}{V_i'}$$

For the Lyngby model, the following equations are used:

$$\frac{\partial \ln \gamma_i^c}{\partial x_j} = \frac{-\partial V_i'}{\partial x_j} + \frac{1}{V_i'} \frac{\partial V_i'}{\partial x_j}$$

#### Returns

**dlngammas\_c\_dxs** [list[list[float]]] Combinatorial lngammas term first composition derivative, size number of components by number of components, [-]

#### dlngammas\_dT()

Calculates the first temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial \ln \gamma_i^r}{\partial T} = \sum_k^{gr} \nu_k^{(i)} \left[ \frac{\partial \ln \Gamma_k}{\partial T} - \frac{\partial \ln \Gamma_k^{(i)}}{\partial T} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

Returns

**dlngammas\_r\_dT** [list[float]] Residual lngammas terms first temperature derivative, size number of components [1/K]

#### dlngammas\_r\_dT()

Calculates the first temperature derivative of the residual part of the UNIFAC model.

$$\frac{\partial \ln \gamma_i^r}{\partial T} = \sum_k^{gr} \nu_k^{(i)} \left[ \frac{\partial \ln \Gamma_k}{\partial T} - \frac{\partial \ln \Gamma_k^{(i)}}{\partial T} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

#### Returns

**dlngammas\_r\_dT** [list[float]] Residual lngammas terms first temperature derivative, size number of components [1/K]

#### dlngammas\_r\_dxs()

Calculates the first mole fraction derivative of the residual part of the UNIFAC model.

$$\frac{\partial \ln \gamma_i^r}{\partial x_j} = \sum_m^{gr} \nu_m^{(i)} \frac{\partial \ln \Gamma_m}{\partial x_j}$$

Returns

**dlngammas\_r\_dxs** [list[list[float]]] First mole fraction derivative of residual lngammas terms, size number of components by number of components [-]

#### dpsis\_dT()

Calculate the  $\Psi$  term first temperature derivative matrix for all groups interacting with all other groups.

The main model calculates the derivative as a function of three coefficients;

$$\frac{\partial \Psi_{mn}}{\partial T} = \left(\frac{-2Tc_{mn} - b_{mn}}{T} - \frac{-T^2c_{mn} - Tb_{mn} - a_{mn}}{T^2}\right)e^{\frac{-T^2c_{mn} - Tb_{mn} - a_{mn}}{T}}$$

Only the first, *a* coefficient, is used in the original UNIFAC model as well as the UNIFAC-LLE model, so the expression simplifies to:

$$\frac{\partial \Psi_{mn}}{\partial T} = \frac{a_{mn}e^{-\frac{a_{mn}}{T}}}{T^2}$$

For the Lyngby model, the first temperature derivative is:

$$\frac{\partial \Psi_{mk}}{\partial T} = \left(\frac{-a_2 - a_3 \ln\left(\frac{T_0}{T}\right)}{T} - \frac{-a_1 - a_2 \left(T - T_0\right) - a_3 \left(T \ln\left(\frac{T_0}{T}\right) + T - T_0\right)}{T^2}\right) e^{\frac{-a_1 - a_2 \left(T - T_0\right) - a_3 \left(T \ln\left(\frac{T_0}{T}\right) + T - T_0\right)}{T}}\right) e^{\frac{-a_1 - a_2 \left(T - T_0\right) - a_3 \left(T \ln\left(\frac{T_0}{T}\right) + T - T_0\right)}{T}}$$

with  $T_0 = 298.15$  K and the *a* coefficients are specific to each pair of main groups, and they are asymmetric, so  $a_{0,mk} \neq a_{0,km}$ .

Returns

**dpsis\_dT** [list[list[float]]] First temperature derivative of psi` terms, size subgroups x subgroups [-]

**static from\_subgroups**(*T*, *xs*, *chemgroups*, *subgroups=None*, *interaction\_data=None*, *version=0*)

Method to construct a UNIFAC object from a dictionary of interaction parameters parameters and a list of dictionaries of UNIFAC keys. As the actual implementation is matrix based not dictionary based, this method can be quite convenient.

### Parameters

- T [float] Temperature, [K]
- **xs** [list[float]] Mole fractions, [-]
- **chemgroups** [list[dict]] List of dictionaries of subgroup IDs and their counts for all species in the mixture, [-]
- **subgroups** [dict[int: UNIFAC\_subgroup], optional] UNIFAC subgroup data; available dictionaries in this module include UFSG (original), DOUFSG (Dortmund), or NISTUFSG. The default depends on the given *version*, [-]
- interaction\_data [dict[int: dict[int: tuple(a\_mn, b\_mn, c\_mn)]], optional] UNIFAC interaction parameter data; available dictionaries in this module include UFIP (original), DOUFIP2006 (Dortmund parameters published in 2006), DOUFIP2016 (Dortmund parameters published in 2016), and NISTUFIP. The default depends on the given *version*, [-]

version [int, optional] Which version of the model to use. Defaults to 0, [-]

- 0 original UNIFAC, OR UNIFAC LLE
- 1 Dortmund UNIFAC (adds T dept, 3/4 power)
- 2 PSRK (original with T dept function)
- 3 VTPR (drops combinatorial term, Dortmund UNIFAC otherwise)
- 4 Lyngby/Larsen has different combinatorial, 2/3 power
- 5 UNIFAC KT (2 params for psi, Lyngby/Larsen formulation; otherwise same as original)

### Returns

**UNIFAC** [UNIFAC] Object for performing calculations with the UNIFAC activity coefficient model, [-]

### Notes

**Warning:** For version 0, the interaction data and subgroups default to the original UNIFAC model (not LLE).

For version 1, the interaction data defaults to the Dortmund parameters published in 2016 (not 2006).

# **Examples**

Mixture of ['benzene', 'cyclohexane', 'acetone', 'ethanol'] according to the Dortmund UNIFAC model:

```
>>> from thermo, unifac import DOUFIP2006. DOUFSG
>>> T = 373.15
>>> xs = [0.2, 0.3, 0.1, 0.4]
>>> chemgroups = [{9: 6}, {78: 6}, {1: 1, 18: 1}, {1: 1, 2: 1, 14: 1}]
>>> GE = UNIFAC.from_subgroups(T=T, xs=xs, chemgroups=chemgroups, version=1,...
→interaction_data=DOUFIP2006, subgroups=DOUFSG)
>>> GE
UNIFAC(T=373.15, xs=[0.2, 0.3, 0.1, 0.4], rs=[2.2578, 4.2816, 2.3373, 2.
→4951999999999996], qs=[2.5926, 5.181, 2.7308, 2.6616], Qs=[1.0608, 0.7081, 0.
→4321, 0.8927, 1.67, 0.8635], vs=[[0, 0, 1, 1], [0, 0, 0, 1], [6, 0, 0, 0], [0,
→ 0, 0, 1], [0, 0, 1, 0], [0, 6, 0, 0]], psi_abc=([[0.0, 0.0, 114.2, 2777.0,
→433.6, -117.1], [0.0, 0.0, 114.2, 2777.0, 433.6, -117.1], [16.07, 16.07, 0.0, _
→ 3972.0, 146.2, 134.6], [1606.0, 1606.0, 3049.0, 0.0, -250.0, 3121.0], [199.0, -
→199.0, -57.53, 653.3, 0.0, 168.2], [170.9, 170.9, -2.619, 2601.0, 464.5, 0.
→0]], [[0.0, 0.0, 0.0933, -4.674, 0.1473, 0.5481], [0.0, 0.0, 0.0933, -4.674, _
→0.1473, 0.5481], [-0.2998, -0.2998, 0.0, -13.16, -1.237, -1.231], [-4.746, -4.
→746, -12.77, 0.0, 2.857, -13.69], [-0.8709, -0.8709, 1.212, -1.412, 0.0, -0.
\rightarrow 8197], [-0.8062, -0.8062, 1.094, -1.25, 0.1542, 0.0]], [[0.0, 0.0, 0.0, 0.
→001551, 0.0, -0.00098], [0.0, 0.0, 0.0, 0.001551, 0.0, -0.00098], [0.0, 0.0, _
→0.0, 0.01208, 0.004237, 0.001488], [0.0009181, 0.0009181, 0.01435, 0.0, -0.
→006022, 0.01446], [0.0, 0.0, -0.003715, 0.000954, 0.0, 0.0], [0.001291, 0.
→001291, -0.001557, -0.006309, 0.0, 0.0]]), version=1)
```

### gammas()

Calculates the activity coefficients with the UNIFAC model.

 $\gamma_i = \exp\left(\ln\gamma_i^c + \ln\gamma_i^r\right)$ 

For the VTPR variant, the combinatorial part is skipped:

$$\gamma_i = \exp(\ln \gamma_i^r)$$

Returns

gammas [list[float]] Activity coefficients, size number of components [-]

#### lnGammas\_subgroups()

Calculate the  $\ln \Gamma_k$  parameters for the phase; depends on the phases's composition and temperature.

$$\ln \Gamma_k = Q_k \left[ 1 - \ln \sum_m \Theta_m \Psi_{mk} - \sum_m \frac{\Theta_m \Psi_{km}}{\sum_n \Theta_n \Psi_{nm}} \right]$$

Returns

**InGammas\_subgroups** [list[float]] Gamma parameters for each subgroup, size number of subgroups, [-]

# lnGammas\_subgroups\_pure()

Calculate the  $\ln \Gamma_k$  pure component parameters for the phase; depends on the phases's temperature only.

$$\ln \Gamma_k = Q_k \left[ 1 - \ln \sum_m \Theta_m \Psi_{mk} - \sum_m \frac{\Theta_m \Psi_{km}}{\sum_n \Theta_n \Psi_{nm}} \right]$$

In this model, the  $\Theta$  values come from the UNIFAC. Thetas\_pure method, where each compound is assumed to be pure.

Returns

**InGammas\_subgroups\_pure** [list[list[float]]] Gamma parameters for each subgroup, size number of subgroups by number of components and indexed in that order, [-]

#### lngammas\_c()

Calculates the combinatorial part of the UNIFAC model. For the modified UNIFAC model, the equation is as follows; for the original UNIFAC and UNIFAC LLE, replace  $V'_i$  with  $V_i$ .

$$\ln \gamma_i^c = 1 - V'_i + \ln(V'_i) - 5q_i \left(1 - \frac{V_i}{F_i} + \ln\left(\frac{V_i}{F_i}\right)\right)$$

For the Lyngby model:

$$\ln \gamma_i^c = \ln \left( V_i' \right) + 1 - V_i'$$

Returns

**lngammas\_c** [list[float]] Combinatorial lngammas terms, size number of components [-]

#### lngammas\_r()

Calculates the residual part of the UNIFAC model.

$$\ln \gamma_i^r = \sum_k^{gr} \nu_k^{(i)} \left[ \ln \Gamma_k - \ln \Gamma_k^{(i)} \right]$$

where the second Gamma is the pure-component Gamma of group k in component i.

#### Returns

lngammas\_r [list[float]] Residual lngammas terms, size number of components [-]

#### property model\_id

A unique numerical identifier refering to the thermodynamic model being implemented. For internal use.

psis()

Calculate the  $\Psi$  term matrix for all groups interacting with all other groups.

The main model calculates it as a function of three coefficients;

$$\Psi_{mn} = \exp\left(\frac{-a_{mn} - b_{mn}T - c_{mn}T^2}{T}\right)$$

Only the first, *a* coefficient, is used in the original UNIFAC model as well as the UNIFAC-LLE model, so the expression simplifies to:

$$\Psi_{mn} = \exp\left(\frac{-a_{mn}}{T}\right)$$

For the Lyngby model, the temperature dependence is modified slightly, as follows:

$$\Psi_{mk} = e^{\frac{-a_1 - a_2(T - T_0) - a_3\left(T \ln\left(\frac{T_0}{T}\right) + T - T_0\right)}{T}}$$

with  $T_0 = 298.15$  K and the *a* coefficients are specific to each pair of main groups, and they are asymmetric, so  $a_{0,mk} \neq a_{0,km}$ .

#### Returns

**psis** [list[list[float]]] *psi* terms, size subgroups x subgroups [-]

 $to_T_xs(T, xs)$ 

Method to construct a new UNIFAC instance at temperature T, and mole fractions xs with the same parameters as the existing object.

### **Parameters**

**T** [float] Temperature, [K]

xs [list[float]] Mole fractions of each component, [-]

### Returns

obj [UNIFAC] New UNIFAC object at the specified conditions [-]

# Notes

If the new temperature is the same temperature as the existing temperature, if the *psi* terms or their derivatives have been calculated, they will be set to the new object as well. If the mole fractions are the same, various subgroup terms are also kept.

# 7.29.2 Main Model (Functional)

# 

Calculates activity coefficients using the UNIFAC model (optionally modified), given a mixture's temperature, liquid mole fractions, and optionally the subgroup data and interaction parameter data of your choice. The default is to use the original UNIFAC model, with the latest parameters published by DDBST. The model supports modified forms (Dortmund, NIST) when the *modified* parameter is True.

# Parameters

T [float] Temperature of the system, [K]

- xs [list[float]] Mole fractions of all species in the system in the liquid phase, [-]
- **chemgroups** [list[dict]] List of dictionaries of subgroup IDs and their counts for all species in the mixture, [-]
- **subgroup\_data** [dict[UNIFAC\_subgroup]] UNIFAC subgroup data; available dictionaries in this module are UFSG (original), DOUFSG (Dortmund), or NISTUFSG ([4]).
- interaction\_data [dict[dict[tuple(a\_mn, b\_mn, c\_mn)]]] UNIFAC interaction parameter data; available dictionaries in this module are UFIP (original), DOUFIP2006 (Dortmund parameters as published by 2006), DOUFIP2016 (Dortmund parameters as published by 2016), and NISTUFIP ([4]).

modified [bool] True if using the modified form and temperature dependence, otherwise False.

### Returns

gammas [list[float]] Activity coefficients of all species in the mixture, [-]

# Notes

The actual implementation of UNIFAC is formulated slightly different than the formulas above for computational efficiency. DDBST switched to using the more efficient forms in their publication, but the numerical results are identical.

The model is as follows:

$$\ln \gamma_i = \ln \gamma_i^c + \ln \gamma_i^r$$

**Combinatorial component** 

$$\ln \gamma_i^c = \ln \frac{\phi_i}{x_i} + \frac{z}{2} q_i \ln \frac{\theta_i}{\phi_i} + L_i - \frac{\phi_i}{x_i} \sum_{j=1}^n x_j L_j$$
$$\theta_i = \frac{x_i q_i}{\sum_{j=1}^n x_j q_j}$$
$$\phi_i = \frac{x_i r_i}{\sum_{j=1}^n x_j r_j}$$
$$L_i = 5(r_i - q_i) - (r_i - 1)$$

**Residual component** 

$$\ln \gamma_i^r = \sum_k^n \nu_k^{(i)} \left[ \ln \Gamma_k - \ln \Gamma_k^{(i)} \right]$$
$$\ln \Gamma_k = Q_k \left[ 1 - \ln \sum_m \Theta_m \Psi_{mk} - \sum_m \frac{\Theta_m \Psi_{km}}{\sum_n \Theta_n \Psi_{nm}} \right]$$
$$\Theta_m = \frac{Q_m X_m}{\sum_n Q_n X_n}$$
$$X_m = \frac{\sum_j \nu_m^j x_j}{\sum_j \sum_n \nu_n^j x_j}$$

R and Q

$$r_i = \sum_{k=1}^n \nu_k R_k$$
$$q_i = \sum_{k=1}^n \nu_k Q_k$$

The newer forms of UNIFAC (Dortmund, NIST) calculate the combinatorial part slightly differently:

$$\ln \gamma_i^c = 1 - V'_i + \ln(V'_i) - 5q_i \left(1 - \frac{V_i}{F_i} + \ln\left(\frac{V_i}{F_i}\right)\right)$$
$$V'_i = \frac{r_i^{3/4}}{\sum_j r_j^{3/4} x_j}$$
$$V_i = \frac{r_i}{\sum_j r_j x_j}$$
$$F_i = \frac{q_i}{\sum_j q_j x_j}$$

Although this form looks substantially different than the original, it infact reverts to the original form if only  $V'_i$  is replaced by  $V_i$ . This is more clear when looking at the full rearranged form as in [3].

In some publications such as [5], the nomenclature is such that  $\theta_i$  and  $\phi$  do not contain the top  $x_i$ , making  $\theta_i = F_i$  and  $\phi_i = V_i$ . [5] is also notable for having supporting information containing very nice sets of analytical derivatives.

UNIFAC LLE uses the original formulation of UNIFAC, and otherwise only different interaction parameters.

# References

[1], [2], [3], [4], [5]

# **Examples**

```
>>> from thermo.unifac import DOUFIP2006
>>> UNIFAC_gammas(373.15, [0.2, 0.3, 0.2, 0.2],
... [{9:6}, {78:6}, {1:1, 18:1}, {1:1, 2:1, 14:1}],
... subgroup_data=DOUFSG, interaction_data=DOUFIP2006, modified=True)
[1.1864311137, 1.44028013391, 1.20447983349, 1.972070609029]
```

thermo.unifac.UNIFAC\_psi(T, subgroup1, subgroup2, subgroup\_data, interaction\_data, modified=False)

Calculates the interaction parameter psi(m, n) for two UNIFAC subgroups, given the system temperature, the UNIFAC subgroups considered for the variant of UNIFAC used, the interaction parameters for the variant of UNIFAC used, and whether or not the temperature dependence is modified from the original form, as shown below.

Original temperature dependence:

$$\Psi_{mn} = \exp\left(\frac{-a_{mn}}{T}\right)$$

Modified temperature dependence:

$$\Psi_{mn} = \exp\left(\frac{-a_{mn} - b_{mn}T - c_{mn}T^2}{T}\right)$$

## Parameters

T [float] Temperature of the system, [K]

subgroup1 [int] First UNIFAC subgroup for identifier, [-]

subgroup2 [int] Second UNIFAC subgroup for identifier, [-]

- subgroup\_data [dict[UNIFAC\_subgroup]] Normally provided as inputs to UNIFAC.
- **interaction\_data** [dict[dict[tuple(a\_mn, b\_mn, c\_mn)]]] Normally provided as inputs to UNI-FAC.
- **modified** [bool] True if the modified temperature dependence is used by the interaction parameters, otherwise False

### Returns

psi [float] UNIFAC interaction parameter term, [-]

# Notes

UNIFAC interaction parameters are asymmetric. No warning is raised if an interaction parameter is missing.

# References

[1], [2]

# **Examples**

>>> from thermo.unifac import UFSG, UFIP, DOUFSG, DOUFIP2006

```
>>> UNIFAC_psi(307, 18, 1, UFSG, UFIP)
0.9165248264184787
```

>>> UNIFAC\_psi(373.15, 9, 78, DOUFSG, DOUFIP2006, modified=True) 1.3703140538273264

# 7.29.3 Misc Functions

thermo.unifac.UNIFAC\_RQ(groups, subgroup\_data=None)

Calculates UNIFAC parameters R and Q for a chemical, given a dictionary of its groups, as shown in [1]. Most UNIFAC methods use the same subgroup values; however, a dictionary of *UNIFAC\_subgroup* instances may be specified as an optional second parameter.

$$r_i = \sum_{k=1}^n \nu_k R_k$$
$$q_i = \sum_{k=1}^n \nu_k Q_k$$

# Parameters

groups [dict[count]] Dictionary of numeric subgroup IDs : their counts

**subgroup\_data** [None or dict[UNIFAC\_subgroup]] Optional replacement for standard subgroups; leave as None to use the original UNIFAC subgroup r and q values.

# Returns

- **R** [float] R UNIFAC parameter (normalized Van der Waals Volume) [-]
- **Q** [float] Q UNIFAC parameter (normalized Van der Waals Area) [-]

# Notes

These parameters have some predictive value for other chemical properties.

### References

[1]

# **Examples**

Hexane

```
>>> UNIFAC_RQ({1:2, 2:4})
(4.4998000000000005, 3.856)
```

### thermo.unifac.Van\_der\_Waals\_volume(R)

Calculates a species Van der Waals molar volume with the UNIFAC method, given a species's R parameter.

 $V_{wk} = 15.17R_k$ 

#### Parameters

**R** [float] R UNIFAC parameter (normalized Van der Waals Volume) [-]

# Returns

V\_vdw [float] Unnormalized Van der Waals volume, [m^3/mol]

#### **Notes**

The volume was originally given in cm<sup>3</sup>/mol, but is converted to SI here.

# References

[1]

#### **Examples**

```
>>> Van_der_Waals_volume(4.4998)
6.826196599999999e-05
```

# thermo.unifac.Van\_der\_Waals\_area(Q)

Calculates a species Van der Waals molar surface area with the UNIFAC method, given a species's Q parameter.

$$A_{wk} = 2.5 \times 10^9 Q_k$$

#### Parameters

Q [float] Q UNIFAC parameter (normalized Van der Waals Area) [-]

#### Returns

A\_vdw [float] Unnormalized Van der Waals surface area, [m^2/mol]

# Notes

The volume was originally given in cm<sup>2</sup>/mol, but is converted to SI here.

# References

[1]

# Examples

```
>>> Van_der_Waals_area(3.856)
964000.0
```

### thermo.unifac.chemgroups\_to\_matrix(chemgroups)

Index by [group index][compound index]

```
>>> chemgroups_to_matrix([{9: 6}, {2: 6}, {1: 1, 18: 1}, {1: 1, 2: 1, 14: 1}])
[[0, 0, 1, 1], [0, 6, 0, 1], [6, 0, 0, 0], [0, 0, 0, 1], [0, 0, 1, 0]]
```

# thermo.unifac.load\_group\_assignments\_DDBST()

Data is stored in the format InChI key bool bool bool subgroup count ... subgroup count subgroup count... where the bools refer to whether or not the original UNIFAC, modified UNIFAC, and PSRK group assignments were completed correctly. The subgroups and their count have an indefinite length.

# 7.29.4 Data for Original UNIFAC

thermo.unifac.UFSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH2=C>, 8: <CH=C>, 9: <ACH>, 10: <AC>, 11: <ACCH3>, 12: <ACCH2>, 13: <ACCH>, 14: <OH>, 15: <CH3OH>, 16: <H2O>, 17: <ACOH>, 18: <CH3CO>, 19: <CH2CO>, 20: <CHO>, 21: <CH3COO>, 22: <CH2COO>, 23: <HCOO>, 24: <CH3O>, 25: <CH2O>, 26: <CH0>, 27: <THF>, 28: <CH3NH2>, 29: <CH2NH2>, 30: <CH1NH2>, 31: <CH3NH>, 32: <CH2NH>, 33: <CH1NH>, 34: <CH3N>, 35: <CH2N>, 36: <ACNH2>, 37: <C5H5N>, 38: <C5H4N>, 39: <C5H3N>, 40: <CH3CN>, 41: <CH2CN>, 42: <C00H>, 43: <HC00H>, 44: <CH2CL>, 45: <CHCL>, 46: <CCL>, 47: <CH2CL2>, 48: <CHCL2>, 49: <CCL2>, 50: <CHCL3>, 51: <CCL3>, 52: <CCL4>, 53: <ACCL>, 54: <CH3N02>, 55: <CH2N02>, 56: <CHN02>, 57: <ACN02>, 58: <CS2>, 59: <CH3SH>, 60: <CH2SH>, 61: <FURFURAL>, 62: <D0H>, 63: <I>, 64: <BR>, 65: <CH=-C>, 66: <C=-C>, 67: <DMSO>, 68: <ACRY>, 69: <CL-(C=C)>, 70: <C=C>, 71: <ACF>, 72: <DMF>, 73: <HCON(CH2)2>, 74: <CF3>, 75: <CF2>, 76: <CF>, 77: <C00>, 78: <SIH3>, 79: <SIH2>, 80: <SIH>, 81: <SI>, 82: <SIH20>, 83: <SIH0>, 84: <SI0>, 85: <NMP>, 86: <CCL3F>, 87: <CCL2F>, 88: <HCCL2F>, 89: <HCCLF>, 90: <CCLF2>, 91: <HCCLF2>, 92: <CCLF3>, 93: <CCL2F2>, 94: <AMH2>, 95: <AMHCH3>, 96: <AMHCH2>, 97: <AM(CH3)2>, 98: <AMCH3CH2>, 99: <AM(CH2)2>, 100: <C2H502>, 101: <C2H402>, 102: <CH3S>, 103: <CH2S>, 104: <CHS>, 105: <MORPH>, 106: <C4H4S>, 107: <C4H3S>, 108: <C4H2S>, 109: <NCO>, 118: <(CH2)2SU>, 119: <CH2CHSU>, 178: <IMIDAZOL>, 179: <BTI>}

thermo.unifac.UFMG = {1: ('CH2', [1, 2, 3, 4]), 2: ('C=C', [5, 6, 7, 8, 70]), 3: ('ACH', [9, 10]), 4: ('ACCH2', [11, 12, 13]), 5: ('OH', [14]), 6: ('CH3OH', [15]), 7: ('H2O', [16]), 8: ('ACOH', [17]), 9: ('CH2CO', [18, 19]), 10: ('CHO', [20]), 11: ('CCOO', [21, 22]), 12: ('HCOO', [23]), 13: ('CH2O', [24, 25, 26, 27]), 14: ('CNH2', [28, 29, 30]), 15: ('CNH', [31, 32, 33]), 16: ('(C)3N', [34, 35]), 17: ('ACNH2', [36]), 18: ('PYRIDINE', [37, 38, 39]), 19: ('CCN', [40, 41]), 20: ('COOH', [42, 43]), 21: ('CCL', [44, 45, 46]), 22: ('CCL2', [47, 48, 49]), 23: ('CCL3', [50, 51]), 24: ('CCL4', [52]), 25: ('ACCL', [53]), 26: ('CNO2', [54, 55, 56]), 27: ('ACNO2', [57]), 28: ('CS2', [58]), 29: ('CH3SH', [59, 60]), 30: ('FURFURAL', [61]), 31: ('DOH', [62]), 32: ('I', [63]), 33: ('BR', [64]), 34: ('C=-C', [65, 66]), 35: ('DMSO', [67]), 36: ('ACRY', [68]), 37: ('CLCC', [69]), 38: ('ACF', [71]), 39: ('DMF', [72, 73]), 40: ('CF2', [74, 75, 76]), 41: ('COO', [77]), 42: ('SIH2', [78, 79, 80, 81]), 43: ('SIO', [82, 83, 84]), 44: ('NMP', [85]), 45: ('CCLF', [86, 87, 88, 89, 90, 91, 92, 93]), 46: ('CON(AM)', [94, 95, 96, 97, 98, 99]), 47: ('OCCOH', [100, 101]), 48: ('CH2S', [102, 103, 104]), 49: ('MORPH', [105]), 50: ('THIOPHEN', [106, 107, 108]), 51: ('NCO', [109]), 55: ('SULFONES', [118, 119]), 84: ('IMIDAZOL', [178]), 85: ('BTI', [179])}

### thermo.unifac.UFIP

Interaction parameters for the original unifac model.

Type dict[int: dict[int: float]]

# 7.29.5 Data for Dortmund UNIFAC

thermo.unifac.DOUFSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH2=C>, 8: <CH=C>, 9: <ACH>, 10: <AC>, 11: <ACCH3>, 12: <ACCH2>, 13: <ACCH>, 14: <OH(P)>, 15: <CH3OH>, 16: <H2O>, 17: <ACOH>, 18: <CH3CO>, 19: <CH2CO>, 20: <CH0>, 21: <CH3C00>, 22: <CH2C00>, 23: <HC00>, 24: <CH30>, 25: <CH20>, 26: <CH0>, 27: <THF>, 28: <CH3NH2>, 29: <CH2NH2>, 30: <CHNH2>, 31: <CH3NH>, 32: <CH2NH>, 33: <CHNH>, 34: <CH3N>, 35: <CH2N>, 36: <ACNH2>, 37: <AC2H2N>, 38: <AC2HN>, 39: <AC2N>, 40: <CH3CN>, 41: <CH2CN>, 42: <COOH>, 43: <HCOOH>, 44: <CH2CL>, 45: <CHCL>, 46: <CCL>, 47: <CH2CL2>, 48: <CHCL2>, 49: <CCL2>, 50: <CHCL3>, 51: <CCL3>, 52: <CCL4>, 53: <ACCL>, 54: <CH3N02>, 55: <CH2N02>, 56: <CHN02>, 57: <ACN02>, 58: <CS2>, 59: <CH3SH>, 60: <CH2SH>, 61: <FURFURAL>, 62: <DOH>, 63: <I>, 64: <BR>, 65: <CH=-C>, 66: <C=-C>, 67: <DMSO>, 68: <ACRY>, 69: <CL-(C=C)>, 70: <C=C>, 71: <ACF>, 72: <DMF>, 73: <HCON(CH2)2>, 74: <CF3>, 75: <CF2>, 76: <CF>, 77: <C00>, 78: <CY-CH2>, 79: <CY-CH>, 80: <CY-C>, 81: <OH(S)>, 82: <OH(T)>, 83: <CY-CH2O>, 84: <TRIOXAN>, 85: <CNH2>, 86: <NMP>, 87: <NEP>, 88: <NIPP>, 89: <NTBP>, 91: <CONH2>, 92: <CONHCH3>, 100: <CONHCH2>, 101: <AM(CH3)2>, 102: <AMCH3CH2>, 103: <AM(CH2)2>, 104: <AC2H2S>, 105: <AC2HS>, 106: <AC2S>, 107: <H2C0CH>, 108: <COCH>, 109: <HCOCH>, 110: <(CH2)2SU>, 111: <CH2SUCH>, 112: <(CH3)2CB>, 113: <(CH2)2CB>, 114: <CH2CH3CB>, 119: <H2COCH2>, 122: <CH3S>, 123: <CH2S>, 124: <CHS>, 153: <H2COC>, 178: <C3H2N2+>, 179: <BTI->, 184: <C3H3N2+>, 189: <C4H8N+>, 195: <BF4->, 196: <C5H5N+>, 197: <OTF->, 201: <-S-S->}

thermo.unifac.DOUFMG = {1: ('CH2', [1, 2, 3, 4]), 2: ('C=C', [5, 6, 7, 8, 70]), 3: ('ACH', [9, 10]), 4: ('ACCH2', [11, 12, 13]), 5: ('OH', [14, 81, 82]), 6: ('CH3OH', [15]), 7: ('H2O', [16]), 8: ('ACOH', [17]), 9: ('CH2CO', [18, 19]), 10: ('CHO', [20]), 11: ('CC00', [21, 22]), 12: ('HC00', [23]), 13: ('CH20', [24, 25, 26]), 14: ('CH2NH2', [28, 29, 30, 85]), 15: ('CH2NH', [31, 32, 33]), 16: ('(C)3N', [34, 35]), 17: ('ACNH2', [36]), 18: ('PYRIDINE', [37, 38, 39]), 19: ('CH2CN', [40, 41]), 20: ('COOH', [42]), 21: ('CCL', [44, 45, 46]), 22: ('CCL2', [47, 48, 49]), 23: ('CCL3', [51]), 24: ('CCL4', [52]), 25: ('ACCL', [53]), 26: ('CNO2', [54, 55, 56]), 27: ('ACNO2', [57]), 28: ('CS2', [58]), 29: ('CH3SH', [59, 60]), 30: ('FURFURAL', [61]), 31: ('DOH', [62]), 32: ('I', [63]), 33: ('BR', [64]), 34: ('C=-C', [65, 66]), 35: ('DMSO', [67]), 36: ('ACRY', [68]), 37: ('CLCC', [69]), 38: ('ACF', [71]), 39: ('DMF', [72, 73]), 40: ('CF2', [74, 75, 76]), 41: ('C00', [77]), 42: ('CY-CH2', [78, 79, 80]), 43: ('CY-CH20', [27, 83, 84]), 44: ('HCOOH', [43]), 45: ('CHCL3', [50]), 46: ('CY-CONC', [86, 87, 88, 89]), 47: ('CONR', [91, 92, 100]), 48: ('CONR2', [101, 102, 103]), 49: ('HCONR', [93, 94]), 52: ('ACS', [104, 105, 106]), 53: ('EPOXIDES', [107, 108, 109, 119, 153]), 55: ('CARBONAT', [112, 113, 114]), 56: ('SULFONE', [110, 111]), 61: ('SULFIDES', [122, 123, 124]), 84: ('IMIDAZOL', [178, 184]), 85: ('BTI', [179]), 87: ('PYRROL', [189]), 89: ('BF4', [195]), 90: ('PYRIDIN', [196]), 91: ('OTF', [197]), 93: ('DISULFIDES', [201])}

### thermo.unifac.DOUFIP2016

Interaction parameters for the Dornmund unifac model.

# 7.29.6 Data for NIST UNIFAC (2015)

thermo.unifac.NISTUFSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH2=C>, 8: <CH=C>, 9: <ACH>, 10: <AC>, 11: <ACCH3>, 12: <ACCH2>, 13: <ACCH>, 14: <OH prim>, 15: <CH3OH>, 16: <H2O>, 17: <ACOH>, 18: <CH3CO>, 19: <CH2CO>, 20: <CHO>, 21: <CH3C00>, 22: <CH2C00>, 23: <HC00>, 24: <CH30>, 25: <CH20>, 26: <CH0>, 27: <CH2-0-CH2>, 28: <CH3NH2>, 29: <CH2NH2>, 30: <CHNH2>, 31: <CH3NH>, 32: <CH2NH>, 33: <CHNH>, 34: <CH3N>, 35: <CH2N>, 36: <ACNH2>, 37: <AC2H2N>, 38: <AC2HN>, 39: <AC2N>, 40: <CH3CN>, 41: <CH2CN>, 42: <C00H>, 43: <HC00H>, 44: <CH2Cl>, 45: <CHCl>, 46: <CCl>, 47: <CH2Cl2>, 48: <CHCl2>, 49: <CCl2>, 50: <CHCl3>, 51: <CCl3>, 52: <CCl4>, 53: <ACCl>, 54: <CH3N02>, 55: <CH2NO2>, 56: <CHNO2>, 57: <ACNO2>, 58: <CS2>, 59: <CH3SH>, 60: <CH2SH>, 61: <Furfural>, 62: <CH2(0H)-CH2(0H)>, 63: <I>, 64: <Br>, 65: <CH#C>, 66: <C#C>, 67: <DMSO>, 68: <Acrylonitrile>, 69: <Cl-(C=C)>, 70: <C=C>, 71: <ACF>, 72: <DMF>, 73: <HCON(CH2)2>, 74: <CF3>, 75: <CF2>, 76: <CF>, 77: <C00>, 78: <c-CH2>, 79: <c-CH>, 80: <c-C>, 81: <OH sec>, 82: <OH tert>, 83: <CH2-0-[CH2-0]1/2>, 84: <[0-CH2]1/2-0-[CH2-0]1/2>, 85: <CNH2>, 86: <c-CON-CH3>, 87: <c-CON-CH2>, 88: <c-CON-CH>, 89: <c-CON-C>, 92: <CONHCH3>, 93: <HCONHCH3>, 94: <HCONHCH2>, 100: <CONHCH2>, 101: <CON(CH3)2>, 102: <CON(CH3)CH2>, 103: <CON(CH2)2>. 104; <AC2H2S>. 105; <AC2HS>. 106; <AC2S>. 107; <H2C0CH>. 109; <HCOCH>. 110; <CH2SuCH2>, 111: <CH2SuCH >, 112: <(CH30)2CO>, 113: <(CH20)2CO>, 114: <(CH30)C00CH2>, 116: <ACCN>, 117: <CH3NCO>, 118: <CH2NCO>, 119: <CHNCO>, 120: <ACNCO>, 121: <COOCO>, 122: <ACS02>, 123: <ACCH0>, 124: <ACC00H>, 125: <c-C0-NH>, 126: <c-C0-0>, 127: <AC-0-C0-CH3 >, 128: <AC-0-C0-CH2>, 129: <AC-0-C0-CH>, 130: <AC-0-C0-C>, 131: <-0-CH2-CH2-OH>, 132: <-O-CH-CH2-OH>, 133: <-O-CH2-CH-OH>, 134: <CH3-S->, 135: <-CH2-S->, 136: <>CH-S->, 137: <->C-S->, 138: <CH30-(0)>, 139: <CH20-(0)>, 140: <CH0-(0)>, 141: <CO-(0)>, 142: <ACO-(0)>, 143: <CFH>, 144: <CFCl>, 145: <CFCl2>, 146: <CF2H>, 147: <CF2ClH>, 148: <CF2Cl2>, 149: <CF3H>, 150: <CF3Cl>, 151: <CF4>, 152: <C(0)2>, 153: <ACN(CH3)2>, 154: <ACN(CH3)CH2>, 155: <ACN(CH2)2>, 156: <ACNHCH3>, 157: <ACNHCH2>, 158: <ACNHCH>, 159: <AC2H20>, 160: <AC2H0>, 161: <AC20>, 162: <c-CH-NH>, 163: <c-C-NH>, 164: <c-CH-NCH3>, 165: <c-CH-NCH2>, 166: <c-CH-NCH>, 170: <SiH3->, 171: <-SiH2->, 172: <>SiH->, 173: Si<>, 174: <-SiH2-0->, 175: <>SiH-0->, 176: <->Si-0->, 177: <C=NOH>, 178: <ACCO>, 179: <C2C14>, 180: <c-CHH2>, 186: <CH(0)2>, 187: <ACS>, 188: <c-CH2-NH>, 189: <c-CH2-NCH3>, 190: <c-CH2-NCH2>, 191: <c-CH2-NCH>, 192: <CHSH>, 193: <CSH>, 194: <ACSH>, 195: <ACC>, 196: <AC2H2NH>, 197: <AC2HNH>, 198: <AC2NH>, 199: <(AC0)C00CH2>, 200: <(AC0)C0(0AC)>, 201: <c-CH=CH>, 202: <c-CH=C>, 203: <c-C=C>, 204: <Glycerol>, 205: <-CH(OH)-CH2(OH)>, 206: <-CH(OH)-CH(OH)->, 207: <>C(OH)-CH2(OH)>, 208: <>C(OH)-CH(OH)->, 209: <>C(OH)-C(OH)<>, 301: <CHCO>, 302: <CCO>, 303: <CHCN>, 304: <CCN>, 305: <CN02>, 306: <ACNH>, 307: <ACN>, 308: <HCHO>, 309: <CH=NOH>}

thermo.unifac.NISTUFMG = {1: ('CH2', [1, 2, 3, 4], 'Alkyl chains'), 2: ('C=C', [5, 6, 7, 8, 9], 'Double bonded alkyl chains'), 3: ('ACH', [15, 16, 17], 'Aromatic carbon'), 4: ('ACCH2', [18, 19, 20, 21], 'Aromatic carbon plus alkyl chain'), 5: ('OH', [34, 204, 205], 'Alcohols'), 6: ('CH3OH', [35], 'Methanol'), 7: ('H2O', [36], 'Water'), 8: ('ACOH', [37], 'Phenolic -OH groups '), 9: ('CH2CO', [42, 43, 44, 45], 'Ketones'), 10: ('CHO', [48], 'Aldehydes'), 11: ('CC00', [51, 52, 53, 54], 'Esters'), 12: ('HC00', [55], 'Formates'), 13: ('CH2O', [59, 60, 61, 62, 63], 'Ethers'), 14: ('CNH2', [66, 67, 68, 69], 'Amines with 1-alkyl group'), 15: ('(C)2NH', [71, 72, 73], 'Amines with 2-alkyl groups'), 16: ('(C)3N', [74, 75], 'Amines with 3-alkyl groups'), 17: ('ACNH2', [79, 80, 81], 'Anilines'), 18: ('PYRIDINE', [76, 77, 78], 'Pyridines'), 19: ('CCN', [85, 86, 87, 88], 'Nitriles'), 20: ('COOH', [94, 95], 'Acids'), 21: ('CCl', [99, 100, 101], 'Chlorocarbons'), 22: ('CCl2', [102, 103, 104], 'Dichlorocarbons'), 23: ('CCl3', [105, 106], 'Trichlorocarbons'), 24: ('CCl4', [107], 'Tetrachlorocarbons'), 25: ('ACCl', [109], 'Chloroaromatics'), 26: ('CN02', [132, 133, 134, 135], 'Nitro alkanes'), 27: ('ACN02', [136], 'Nitroaromatics'), 28: ('CS2', [146], 'Carbon disulfide'), 29: ('CH3SH', [138, 139, 140, 141], 'Mercaptans'), 30: ('FURFURAL', [50], 'Furfural'), 31: ('DOH', [38], 'Ethylene Glycol'), 32: ('I', [128], 'Iodides'), 33: ('BR', [130], 'Bromides'), 34: ('CC', [13, 14], 'Triplebonded alkyl chains'), 35: ('DMSO', [153], 'Dimethylsulfoxide'), 36: ('ACRY', [90], 'Acrylic'), 37: ('ClC=C', [108], 'Chlorine attached to double bonded alkyl chain'), 38: ('ACF', [118], 'Fluoroaromatics'), 39: ('DMF', [161, 162, 163, 164, 165], 'Amides'), 40: ('CF2', [111, 112, 113, 114, 115, 116, 117], 'Fluorines'), 41: ('COO', [58], 'Esters'), 42: ('SiH2', [197, 198, 199, 200], 'Silanes'), 43: ('SiO', [201, 202, 203], 'Siloxanes'), 44: ('NMP', [195], 'N-Methyl-2-pyrrolidone'), 45: ('CClF', [120, 121, 122, 123, 124, 125, 126, 127], 'Chloro-Fluorides'), 46: ('CONCH2', [166, 167, 168, 169], 'Amides'), 47: ('OCCOH', [39, 40, 41], 'Oxygenated Alcohols'), 48: ('CH2S', [142, 143, 144, 145], 'Sulfides'), 49: ('MORPHOLIN', [196], 'Morpholine'), 50: ('THIOPHENE', [147, 148, 149], 'Thiophene'), 51: ('CH2(cy)', [27, 28, 29], 'Cyclic hydrocarbon chains'), 52: ('C=C(cy)', [30, 31, 32], 'Cyclic unsaturated hydrocarbon chains')}

### thermo.unifac.NISTUFIP

Interaction parameters for the NIST (2015) unifac model.

# 7.29.7 Data for NIST KT UNIFAC (2011)

thermo.unifac.NISTKTUFSG = {1: <CH3->, 2: <-CH2->, 3: <-CH<>, 4: <>C<>, 5: <CH2=CH->, 6: <-CH=CH->, 7: <CH2=C<>, 8: <-CH=C<>, 9: <>C=C<>, 13: <CHC->, 14: <-CC->, 15: <-ACH->, 16: ◇AC- (link)>, 17: ◇AC- (cond)>, 18: ◇AC-CH3>, 19: ◇AC-CH2->, 20: ◇AC-CH<>, 21: AC-C<->, 27: <-CH2- (cy)>, 28: <>CH- (cy)>, 29: <>C< (cy)>, 30: <-CH=CH- (cy)>, 31: <CH2=C< (cy)>, 32: <-CH=C< (cy)>, 34: <-OH(primary)>, 35: <CH3OH>, 36: <H2O>, 37: AC-OH>, 38: <(CH2OH)2>, 39: <-0-CH2-CH2-OH>, 40: <-0-CH2-OH>, 41: <-0-CH2-CH-OH>, 42: <CH3-CO->, 43: <-CH2-CO->, 44: <>CH-CO->, 45: <->C-CO->, 48: <-CHO>, 50: <C5H402>, 51: <CH3-C00->, 52: <-CH2-C00->, 53: <>CH-C00->, 54: <->C-C00->, 55: <HC00->, 58: <-C00->, 59: <CH3-0->, 60: <-CH2-0->, 61: <>CH-0->, 62: <->C0->, 63: <-CH2-0- (cy)>, 66: <CH3-NH2>, 67: <-CH2-NH2>, 68: <>CH-NH2>, 69: <->C-NH2>, 71: <CH3-NH->, 72: <-CH2-NH->, 73: <>CH-NH->, 74: <CH3-N<>, 75: <-CH2-N<>, 76: <C5H5N>, 77: <C5H4N->, 78: <C5H3N<>, 79: AC-NH2>, 80: <>AC-NH->, 81: <>AC-N<>, 85: <CH3-CN>, 86: <-CH2-CN>, 87: <>CH-CN>, 88: <->C-CN>, 90: <CH2=CH-CN>, 94: <-COOH>, 95: <HCOOH>, 99: <-CH2-Cl>, 100: <>CH-Cl>, 101: <->CCl>, 102: <CH2Cl2>, 103: <-CHCl2>, 104: <>CCl2>, 105: <CHCl3>, 106: <-CCl3>, 107: <CC14>, 108: <Cl(C=C)>, 109: <>AC-Cl>, 111: <CHF3>, 112: <-CF3>, 113: <-CHF2>, 114: \$CF2>. 115: <-CH2F>. 116: <>CH-F>. 117: <->CF>. 118: <>AC-F>. 120: <CC13F>. 121: <-CCl2F>, 122: <HCCl2F>, 123: <-HCClF>, 124: <-CClF2>, 125: <HCClF2>, 126: <CClF3>, 127: <CC12F2>, 128: <-I>, 130: <-Br>, 132: <CH3-N02>, 133: <-CH2-N02>, 134: <>CH-N02>, 135: <->C-N02>, 136: <>AC-N02>, 138: <CH3-SH>, 139: <-CH2-SH>, 140: <>CH-SH>, 141: <->C-SH>, 142: <CH3-S->, 143: <-CH2-S->, 144: <>CH-S->, 145: <->C-S->, 146: <CS2>, 147: <THIOPHENE>, 148: <C4H3S->, 149: <C4H2S<>, 153: <DMSO>, 161: <DMF>, 162: <-CON(CH3)2>, 163: <-CON(CH2)(CH3)->, 164: <HCON(CH2)2<>, 165: <-CON(CH2)2<>, 166: <-CONH(CH3)>, 167: <HCONH(CH2)->, 168: <-CONH(CH2)->, 169: <-CONH2>, 195: <NMP>, 196: <MORPHOLIN>, 197: <\$iH3->, 198: <-\$iH2->, 199: <>\$iH->, 200: <>\$i<>, 201: <-\$iH2-0->, 202: <>\$iH-0->, 203: <->Si-O->, 204: <-OH(secondary)>, 205: <-OH(tertiary)>}

thermo.unifac.NISTKTUFMG = {1: ('C', [1, 2, 3, 4]), 2: ('C=C', [5, 6, 7, 8, 9]), 3: ('ACH', [15, 16, 17]), 4: ('ACCH2', [18, 19, 20, 21]), 5: ('OH', [34, 204, 205]), 6: ('CH2OH', [35]), 7: ('H2O', [36]), 8: ('ACOH', [37]), 9: ('CH2CO', [42, 43, 44, 45]), 10: ('CHO', [48]), 11: ('CCOO', [51, 52, 53, 54]), 12: ('HCOO', [55]), 13: ('CH2O', [59, 60, 61, 62]), 14: ('CNH2', [66, 67, 68, 69]), 15: ('(C)2NH', [71, 72, 73]), 16: ('(C)3N', [74, 75]), 17: ('ACNH2', [79, 80, 81]), 18: ('Pyridine', [76, 77, 78]), 19: ('CCN', [85, 86, 87, 88]), 20: ('COOH', [94, 95]), 21: ('CCl', [99, 100, 101]), 22: ('CCl2', [102, 103, 104]), 23: ('CCl3', [105, 106]), 24: ('CCl4', [107]), 25: ('ACCl', [109]), 26: ('CN02', [132, 133, 134, 135]), 27: ('ACN02', [136]), 28: ('CS2', [146]), 29: ('CH3SH', [138, 139, 140, 141]), 30: ('Furfural', [50]), 31: ('DOH', [38]), 32: ('I', [128]), 33: ('Br', [130]), 34: ('C=-C', [13, 14]), 35: ('DMSO', [153]), 36: ('ACRY', [90]), 37: ('Cl(C=C)', [108]), 38: ('ACF', [118]), 39: ('DMF', [161, 162, 163, 164, 165]), 40: ('CF2', [111, 112, 113, 114, 115, 116, 117]), 41: ('C00', [58]), 42: ('SiH2', [197, 198, 199, 200]), 43: ('SiO', [201, 202, 203]), 44: ('NMP', [195]), 45: ('CClF', [120, 121, 122, 123, 124, 125, 126, 127]), 46: ('CONCH2', [166, 167, 168, 169]), 47: ('OCCOH', [39, 40, 41]), 48: ('CH2S', [142, 143, 144, 145]), 49: ('Morpholin', [196]), 50: ('THIOPHENE', [147, 148, 149]), 51: ('CH2(cyc)', [27, 28, 29]), 52: ('C=C(cyc)', [30, 31, 32])} Compared to storing the values in dict[(int1, int2)] = (values), the dict-in-dict structure is found emperically to

take 111608 bytes vs. 79096 bytes, or 30% less memory.

# thermo.unifac.NISTKTUFIP

Interaction parameters for the NIST KT UNIFAC (2011) model.

# 7.29.8 Data for UNIFAC LLE

thermo.unifac.LLEUFSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH=C>, 8: <CH2=C>, 9: <ACH>, 10: <AC>, 11: <ACCH3>, 12: <ACCH2>, 13: <ACCH>, 14: <OH>, 15: <P1>, 16: <P2>, 17: <H2O>, 18: <ACOH>, 19: <CH3CO>, 20: <CH2CO>, 21: <CHO>, 22: <Furfural>, 23: <COOH>, 24: <HCOOH>, 25: <CH3COO>, 26: <CH2COO>, 27: <CH3O>, 28: <CH2O>, 29: <CHO>, 30: <FCH2O>, 31: <CH2CL>, 32: <CHCL>, 33: <CCL>, 34: <CH2CL2>, 35: <CH2CN>, 36: <CCL2>, 37: <CHCL3>, 38: <CCL3>, 39: <CCL4>, 40: <ACCL>, 41: <CH3CN>, 42: <CH2CN>, 43: <ACNH2>, 44: <CH3NO2>, 45: <CH2NO2>, 46: <CHNO2>, 47: <ACNO2>, 48: <DOH>, 49: <(HOCH2CH2)2O>, 50: <C5H5N>, 51: <C5H4N>, 52: <C5H3N>, 53: <CC12=CHC1>, 54: <HCONHCH3>, 55: <DMF>, 56: <(CH2)4SO2>, 57: <DMSO>}

thermo.unifac.LLEMG = {1: ('CH2', [1, 2, 3, 4]), 2: ('C=C', [5, 6, 7, 8]), 3: ('ACH', [9, 10]), 4: ('ACCH2', [11, 12, 13]), 5: ('OH', [14]), 6: ('P1', [15]), 7: ('P2', [16]), 8: ('H2O', [17]), 9: ('ACOH', [18]), 10: ('CH2CO', [19, 20]), 11: ('CHO', [21]), 12: ('Furfural', [22]), 13: ('COOH', [23, 24]), 14: ('CCOO', [25, 26]), 15: ('CH2O', [27, 28, 29, 30]), 16: ('CCL', [31, 32, 33]), 17: ('CCL2', [34, 35, 36]), 18: ('CCL3', [37, 38]), 19: ('CCL4', [39]), 20: ('ACCL', [40]), 21: ('CCN', [41, 42]), 22: ('ACNH2', [43]), 23: ('CNO2', [44, 45, 46]), 24: ('ACNO2', [47]), 25: ('DOH', [48]), 26: ('DEOH', [49]), 27: ('PYRIDINE', [50, 51, 52]), 28: ('TCE', [53]), 29: ('MFA', [54]), 30: ('DMFA', [55]), 31: ('TMS', [56]), 32: ('DMSO', [57])}

Larsen, Bent L., Peter Rasmussen, and Aage Fredenslund. "A Modified UNIFAC Group-Contribution Model for Prediction of Phase Equilibria and Heats of Mixing." Industrial & Engineering Chemistry Research 26, no. 11 (November 1, 1987): 2274-86. https://doi.org/10.1021/ie00071a018.

### thermo.unifac.LLEUFIP

Interaction parameters for the LLE unifac model.

Type dict[int: dict[int: float]]

# 7.29.9 Data for Lyngby UNIFAC

thermo.unifac.LUFSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH2=C>, 8: <CH=C>, 9: <C=C>, 10: <ACH>, 11: <AC>, 12: <OH>, 13: <CH3OH>, 14: <H2O>, 15: <CH3CO>, 16: <CH2CO>, 17: <CHO>, 18: <CH3COO>, 19: <CH2COO>, 20: <CH3O>, 21: <CH2O>, 22: <CHO>, 23: <THF>, 24: <NH2>, 25: <CH3NH>, 26: <CH2NH>, 27: <CHNH>, 28: <CH3N>, 29: <CH2N>, 30: <ANH2>, 31: <C5H5N>, 32: <C5H4N>, 33: <C5H3N>, 34: <CH3CN>, 35: <CH2CN>, 36: <COOH>, 37: <CH2CL>, 38: <CHCL>, 39: <CCL>, 40: <CH2CL2>, 41: <CHCL2>, 42: <CCL2>, 43: <CHCL3>, 44: <CCL3>, 45: <CCL4>}

thermo.unifac.LUFMG = {1: ('CH2', [1, 2, 3, 4]), 2: ('C=C', [5, 6, 7, 8, 9]), 3: ('ACH', [10, 11]), 4: ('OH', [12]), 5: ('CH30H', [13]), 6: ('H2O', [14]), 7: ('CH2CO', [15, 16]), 8: ('CHO', [17]), 9: ('CCOO', [18, 19]), 10: ('CH2O', [20, 21, 22, 23]), 11: ('NH2', [24]), 12: ('CNH2NG', [25, 26, 27]), 13: ('CH2N', [28, 29]), 14: ('ANH2', [30]), 15: ('PYRIDINE', [31, 32, 33]), 16: ('CCN', [34, 35]), 17: ('COOH', [36]), 18: ('CCL', [37, 38, 39]), 19: ('CCL2', [40, 41, 42]), 20: ('CCL3', [43, 44]), 21: ('CCL4', [45])}

thermo.unifac.LUFIP

Interaction parameters for the Lyngby UNIFAC model.

# 7.29.10 Data for PSRK UNIFAC

thermo.unifac.PSRKSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH2=C>, 8: <CH=C>, 9: <ACH>, 10: <AC>, 11: <ACCH3>, 12: <ACCH2>, 13: <ACCH>, 14: <OH>, 15: <CH3OH>, 16: <H2O>, 17: <ACOH>, 18: <CH3CO>, 19: <CH2CO>, 20: <CH0>, 21: <CH3CO>, 22: <CH2C00>, 23: <HC00>, 24: <CH30>, 25: <CH20>, 26: <CH0>, 27: <THF>, 28: <CH3NH2>, 29: <CH2NH2>, 30: <CH1NH2>, 31: <CH3NH>, 32: <CH2NH>, 33: <CH1NH>, 34: <CH3N>, 35: <CH2N>, 36: <ACNH2>, 37: <C5H5N>, 38: <C5H4N>, 39: <C5H3N>, 40: <CH3CN>, 41: <CH2CN>, 42: <C00H>, 43: <HC00H>, 44: <CH2CL>, 45: <CHCL>, 46: <CCL>, 47: <CH2CL2>, 48: <CHCL2>, 49: <CCL2>, 50: <CHCL3>, 51: <CCL3>, 52: <CCL4>, 53: <ACCL>, 54: <CH3N02>, 55: <CH2N02>, 56: <CHN02>, 57: <ACN02>, 58: <CS2>, 59: <CH3SH>, 60: <CH2SH>, 61: <FURFURAL>, 62: <D0H>, 63: <I>, 64: <BR>, 65: <CH=-C>, 66: <C=-C>, 67: <DMSO>, 68: <ACRY>, 69: <CL-(C=C)>, 70: <C=C>, 71: <ACF>, 72: <DMF>, 73: <HCON(CH2)2>, 74: <CF3>, 75: <CF2>, 76: <CF>, 77: <C00>, 78: <SIH3>, 79: <SIH2>, 80: <SIH>, 81: <SI>, 82: <SIH20>, 83: <SIH0>, 84: <SI0>, 85: <NMP>, 86: <CCL3F>, 87: <CCL2F>, 88: <HCCL2F>, 89: <HCCLF>, 90: <CCLF2>, 91: <HCCLF2>, 92: <CCLF3>, 93: <CCL2F2>, 94: <AMH2>, 95: <AMHCH3>, 96: <AMHCH2>, 97: <AM(CH3)2>, 98: <AMCH3CH2>, 99: <AM(CH2)2>, 100: <C2H502>, 101: <C2H402>, 102: <CH3S>, 103: <CH2S>, 104: <CHS>. 105: <MORPH>. 106: <C4H4S>. 107: <C4H3S>. 108: <C4H2S>. 109: <H2C=CH2>. 110: <CH=-CH>, 111: <NH3>, 112: <CO>, 113: <H2>, 114: <H2S>, 115: <N2>, 116: <AR>, 117: <CO2>, 118: <CH4>, 119: <02>, 120: <D2>, 121: <S02>, 122: <N0>, 123: <N20>, 124: <SF6>, 125: <HE>, 126: <NE>, 127: <KR>, 128: <XE>, 129: <HF>, 130: <HCL>, 131: <HBR>, 132: <HI>, 133: <COS>, 134: <CHSH>, 135: <CSH>, 136: <H2COCH>, 137: <HCOCH>, 138: <HCOC>, 139: <H2COCH2>, 140: <H2COC>, 141: <COC>, 142: <F2>, 143: <CL2>, 144: <BR2>, 145: <HCN>, 146: <NO2>, 147: <CF4>, 148: <03>, 149: <CLNO>, 152: <CNH2>}

thermo.unifac.PSRKMG = {1: ('CH2', [1, 2, 3, 4]), 2: ('C=C', [5, 6, 7, 8, 70, 109]), 3: ('ACH', [9, 10]), 4: ('ACCH2', [11, 12, 13]), 5: ('OH', [14]), 6: ('CH3OH', [15]), 7: ('H20', [16]), 8: ('ACOH', [17]), 9: ('CH2CO', [18, 19]), 10: ('CH0', [20]), 11: ('CCOO', [21, 22]), 12: ('HCOO', [23]), 13: ('CH2O', [24, 25, 26, 27]), 14: ('CNH2', [28, 29, 30, 152]), 15: ('CNH', [31, 32, 33]), 16: ('(C)3N', [34, 35]), 17: ('ACNH2', [36]), 18: ('PYRIDINE', [37, 38, 39]), 19: ('CCN', [40, 41]), 20: ('COOH', [42, 43]), 21: ('CCL', [44, 45, 46]), 22: ('CCL2', [47, 48, 49]), 23: ('CCL3', [50, 51]), 24: ('CCL4', [52]), 25: ('ACCL', [53]), 26: ('CNO2', [54, 55, 56]), 27: ('ACNO2', [57]), 28: ('CS2', [58]), 29: ('CH3SH', [59, 60, 134, 135]), 30: ('FURFURAL', [61]), 31: ('DOH', [62]), 32: ('I', [63]), 33: ('BR', [64]), 34: ('C=-C', [65, 66, 110]), 35: ('DMSO', [67]), 36: ('ACRY', [68]), 37: ('CLCC', [69]), 38: ('ACF', [71]), 39: ('DMF', [72, 73]), 40: ('CF2', [74, 75, 76]), 41: ('C00', [77]), 42: ('SIH2', [78, 79, 80, 81]), 43: ('SIO', [82, 83, 84]), 44: ('NMP', [85]), 45: ('CCLF', [86, 87, 88, 89, 90, 91, 92, 93]), 46: ('CON (AM)', [94, 95, 96, 97, 98, 99]), 47: ('OCCOH', [100, 101]), 48: ('CH2S', [102, 103, 104]), 49: ('MORPH', [105]), 50: ('THIOPHEN', [106, 107, 108]), 51: ('EPOXY', [136, 137, 138, 139, 140, 141]), 55: ('NH3', [111]), 56: ('CO2', [117]), 57: ('CH4', [118]), 58: ('O2', [119]), 59: ('AR', [116]), 60: ('N2', [115]), 61: ('H2S', [114]), 62: ('H2', [113, 120]), 63: ('CO', [112]), 65: ('SO2', [121]), 66: ('NO', [122]), 67: ('N2O', [123]), 68: ('SF6', [124]), 69: ('HE', [125]), 70: ('NE', [126]), 71: ('KR', [127]), 72: ('XE', [128]), 73: ('HF', [129]), 74: ('HCL', [130]), 75: ('HBR', [131]), 76: ('HI', [132]), 77: ('COS', [133]), 78: ('F2', [142]), 79: ('CL2', [143]), 80: ('BR2', [144]), 81: ('HCN', [145]), 82: ('NO2', [146]), 83: ('CF4', [147]), 84: ('03', [148]), 85: ('CLNO', [149])}

Magnussen, Thomas, Peter Rasmussen, and Aage Fredenslund. "UNIFAC Parameter Table for Prediction of Liquid-Liqu Industrial & Engineering Chemistry Process Design and Development 20, no. 2 (April 1, 1981): 331-39. https://doi.org/10.1021/i200013a024.

# thermo.unifac.PSRKIP

Interaction parameters for the PSRKIP UNIFAC model.

# 7.29.11 Data for VTPR UNIFAC

thermo.unifac.VTPRSG = {1: <CH3>, 2: <CH2>, 3: <CH>, 4: <C>, 5: <CH2=CH>, 6: <CH=CH>, 7: <CH2=C>, 8: <CH=C>, 9: <ACH>, 10: <AC>, 11: <ACCH3>, 12: <ACCH2>, 13: <ACCH>, 14: <OH(P)>, 15: <CH3OH>, 16: <H2O>, 17: <ACOH>, 18: <CH3CO>, 19: <CH2CO>, 20: <CH0>, 21: <CH3C00>, 22: <CH2C00>, 23: <HC00>, 24: <CH30>, 25: <CH20>, 26: <CH0>, 27: <THF>, 28: <CH3NH2>, 29: <CH2NH2>, 30: <CHNH2>, 31: <CH3NH>, 32: <CH2NH>, 33: <CHNH>, 34: <CH3N>, 35: <CH2N>, 36: <ACNH2>, 40: <CH3CN>, 41: <CH2CN>, 44: <CH2CL>, 45: <CHCL>, 46: <CCL>, 47: <CH2CL2>, 48: <CHCL2>, 49: <CCL2>, 50: <CHCL3>, 51: <CCL3>, 52: <CCL4>, 53: <ACCL>, 54: <CH3NO2>, 55: <CH2NO2>, 56: <CHNO2>, 58: <CS2>, 59: <CH3SH>, 60: <CH2SH>, 61: <FURFURAL>, 62: <DOH>, 63: <I>, 64: <BR>, 67: <DMSO>, 70: <C=C>, 72: <DMF>, 73: <HCON(...>, 78: <CY-CH2>, 79: <CY-CH>, 80: <CY-C>, 81: <OH(S)>, 82: <OH(T)>, 83: <CY-CH2O>, 84: <TRIOXAN>, 85: <CNH2>, 86: <NMP>, 87: <NEP>, 88: <NIPP>, 89: <NTBP>, 97: <Allene>, 98: <=CHCH=>, 99: <=CCH=>, 107: <H2COCH>, 108: <COCH>, 109: <HCOCH>, 116: <AC-CHO>, 119: <H2COCH2>, 129: <CHCOO>, 139: <CF2H>, 140: <CF2H2>, 142: <CF2Cl>, 143: <CF2C12>, 146: <CF4>, 148: <CF3Br>, 153: <H2COC>, 180: <CHCOO>, 250: <H2C=CH2>, 300: <NH3>, 301: <CO>, 302: <H2>, 303: <H2>, 304: <N2>, 305: <Ar>, 306: <CO2>, 307: <CH4>, 308: <02>. 309: <D2>. 310: <S02>. 312: <N20>. 314: <He>. 315: <Ne>. 319: <HC1>. 345: <Hg>}

thermo.unifac.VTPRMG = {1: ('CH2', [1, 2, 3, 4]), 2: ('H2C=CH2', [5, 6, 7, 8, 70, 97, 98, 99, 250]), 3: ('ACH', [9, 10]), 4: ('ACCH2', [11, 12, 13]), 5: ('OH', [14, 81, 82]), 6: ('CH30H', [15]), 7: ('H20', [16]), 8: ('ACOH', [17]), 9: ('CH2CO', [18, 19]), 10: ('CH0', [20]), 11: ('CC00', [21, 22, 129, 180]), 12: ('HC00', [23]), 13: ('CH20', [24, 25, 26]), 14: ('CH2NH2', [28, 29, 30, 85]), 15: ('CH2NH', [31, 32, 33]), 16: ('(C)3N', [34, 35]), 17: ('ACNH2', [36]), 19: ('CH2CN', [40, 41]), 21: ('CCL', [44, 45, 46]), 22: ('CCL2', [47, 48, 49]), 23: ('CCL3', [51]), 24: ('CCL4', [52]), 25: ('ACCL', [53]), 26: ('CN02', [54, 55, 56]), 28: ('CS2', [58]), 29: ('CH3SH', [59, 60]), 30: ('FURFURAL', [61]), 31: ('DOH', [62]), 32: ('I', [63]), 33: ('BR', [64]), 35: ('DMSO', [67]), 39: ('DMF', [72, 73]), 42: ('CY-CH2', [78, 79, 80]), 43: ('CY-CH20', [27, 83, 84]), 45: ('CHCL3', [50]), 46: ('CY-CONC', [86, 87, 88, 89]), 53: ('EPOXIDES', [107, 108, 109, 119, 153]), 57: ('AC-CHO', [116]), 68: ('CF2H', [139, 140]), 70: ('CF2Cl2', [142, 143, 148]), 73: ('CF4', [146]), 150: ('NH3', [300]), 151: ('CO2', [306]), 152: ('CH4', [307]), 153: ('O2', [308]), 154: ('Ar', [305]), 155: ('N2', [304]), 156: ('H2S', [303]), 157: ('D2', [302, 309]), 158: ('CO', [301]), 160: ('SO2', [310]), 162: ('N2O', [312]), 164: ('He', [314]), 165: ('Ne', [315]), 169: ('HCl', [319]), 185: ('Hg', [345])}

thermo.unifac.VTPRIP

Interaction parameters for the VTPRIP UNIFAC model.

**Type** dict[int: dict[int: tuple(float, 3)]]

# 7.30 Support for pint Quantities (thermo.units)

Basic module which wraps some of thermo functions and classes to be compatible with the pint unit handling library. All other object - dicts, lists, etc - are not wrapped.

```
>>> from fluids.units import *
>>> import thermo
>>> thermo.units.PRMIX
<class 'fluids.units.PRMIX'>
```

Note that values which can normally be numpy arrays or python lists, are required to always be numpy arrays in this interface.

This is interface is powerful but not complex enough to handle many of the objects in Thermo. A list of the types of classes which are not supported is as follows:

- TDependentProperty, TPDependentProperty, MixtureProperty
- · Phase objects
- · Flash object
- ChemicalConstantsPackage
- PropertyCorrelationsPackage

For further information on this interface, please see the documentation of fluids.units which is built in the same way.

# 7.31 Utilities and Base Classes (thermo.utils)

This module contains base classes for temperature T, pressure P, and composition zs dependent properties. These power the various interfaces for each property.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Temperature Dependent
- *Temperature and Pressure Dependent*
- Temperature, Pressure, and Composition Dependent

# 7.31.1 Temperature Dependent

### class thermo.utils.TDependentProperty(extrapolation, \*\*kwargs)

Class for calculating temperature-dependent chemical properties.

On creation, a *TDependentProperty* examines all the possible methods implemented for calculating the property, loads whichever coefficients it needs (unless *load\_data* is set to False), examines its input parameters, and selects the method it prefers. This method will continue to be used for all calculations until the method is changed by setting a new method to the to *method* attribute.

The default list of preferred method orderings is at *ranked\_methods* for all properties; the order can be modified there in-place, and this will take effect on all new *TDependentProperty* instances created but NOT on existing instances.

All methods have defined criteria for determining if they are valid before calculation, i.e. a minimum and maximum temperature for coefficients to be valid. For constant property values used due to lack of temperaturedependent data, a short range is normally specified as valid. It is not assumed that a specified method will succeed; for example many expressions are not mathematically valid past the critical point, and in some cases there is no easy way to determine the temperature where a property stops being reasonable.

Accordingly, all properties calculated are checked by a sanity function *test\_property\_validity*, which has basic sanity checks. If the property is not reasonable, None is returned.

This framework also supports tabular data, which is interpolated from if specified. Interpolation is cubic-spline based if 5 or more points are given, and linearly interpolated with if few points are given. A transform may be applied so that a property such as vapor pressure can be interpolated non-linearly. These are functions or lambda expressions which are set for the variables *interpolation\_T*, *interpolation\_property*, and *interpolation\_property\_inv*.

In order to calculate properties outside of the range of their correlations, a number of extrapolation method are available. Extrapolation is used by default on some properties but not all. The extrapolation methods available are as follows:

- 'constant' returns the model values as calculated at the temperature limits
- 'linear' fits the model at its temperature limits to a linear model
- 'nolimit' attempt to evaluate the model outside of its limits; this will error in most cases and return None
- 'interp1d' SciPy's interp1d is used to extrapolate
- 'AntoineAB' fits the model to Antoine's equation at the temperature limits using only the A and B coefficient
- 'DIPPR101\_ABC' fits the model at its temperature limits to the EQ101 equation
- 'Watson' fits the model to the Heat of Vaporization model Watson
- 'EXP\_POLY\_LN\_TAU2' uses the models's critical temperature and derivative to fit the model linearly in the equation prop =  $\exp(a + b \cdot \ln \tau)$ , so that it is always zero at the critical point; suitable for surface tension.
- 'DIPPR106\_AB' uses the models's critical temperature and derivative to fit the model linearly in the equation EQ106's equation at the temperature limits using only the A and B coefficient
- 'DIPPR106\_ABC' uses the models's critical temperature and first two derivatives to fit the model quadratically in the equation EQ106's equation at the temperature limits using only the A, B, and C coefficient.

It is possible to use different extrapolation methods for the low-temperature and the high-temperature region. Specify the extrapolation parameter with the '|' symbols between the two methods; the first method is used for low-temperature, and the second for the high-temperature.

# Attributes

name [str] The name of the property being calculated, [-]

units [str] The units of the property, [-]

- *method* [str] Method used to set a specific property method or to obtain the name of the method in use.
- **interpolation\_T** [callable or None] A function or lambda expression to transform the temperatures of tabular data for interpolation; e.g. 'lambda self, T: 1./T'
- **interpolation\_T\_inv** [callable or None] A function or lambda expression to invert the transform of temperatures of tabular data for interpolation; e.g. 'lambda self, x: self. $Tc^*(1 x)$ '
- **interpolation\_property** [callable or None] A function or lambda expression to transform tabular property values prior to interpolation; e.g. 'lambda self, P: log(P)'

- **interpolation\_property\_inv** [callable or None] A function or property expression to transform interpolated property values from the transform performed by *interpolation\_property* back to their actual form, e.g. 'lambda self, P: exp(P)'
- **Tmin** [float] Minimum temperature (K) at which the current method can calculate the property.
- **Tmax** [float] Maximum temperature (K) at which the current method can calculate the property.
- property\_min [float] Lowest value expected for a property while still being valid; this is a criteria used by test\_method\_validity.
- property\_max [float] Highest value expected for a property while still being valid; this is a
  criteria used by test\_method\_validity.
- ranked\_methods [list] Constant list of ranked methods by default
- **tabular\_data** [dict] Stores all user-supplied property data for interpolation in format {name: (Ts, properties)}, [-]
- **tabular\_data\_interpolators** [dict] Stores all interpolation objects, idexed by name and property transform methods with the format {(name, interpolation\_T, interpolation\_property, interpolation\_property\_inv): (extrapolator, spline)}, [-]
- all\_methods [set] Set of all methods available for a given CASRN and set of properties, [-]

### Methods

T_dependent_property(T)	Method to calculate the property with sanity check-
	ing and using the selected <i>method</i> .
T_dependent_property_derivative(T[, order])	Method to obtain a derivative of a property with re-
	spect to temperature, of a given order.
T_dependent_property_integral(T1, T2)	Method to calculate the integral of a property with
	respect to temperature, using the selected method.
T_dependent_property_integral_over_T(T1,	Method to calculate the integral of a property over
T2)	temperature with respect to temperature, using the se-
	lected method.
call(T)	Convenience method to calculate the property; calls
	T_dependent_property.
add_correlation(name, model, Tmin, Tmax,)	Method to add a new set of emperical fit equation co-
	efficients to the object and select it for future property
	calculations.
add_method(f[, Tmin, Tmax, f_der, f_der2,])	Define a new method and select it for future property
	calculations.
add_tabular_data(Ts, properties[, name,])	Method to set tabular data to be used for interpola-
	tion.
as_json([references])	Method to create a JSON serialization of the property
	model which can be stored, and reloaded later.
calculate(T, method)	Method to calculate a property with a specified
	method, with no validity checking or error handling.
<pre>calculate_derivative(T, method[, order])</pre>	Method to calculate a derivative of a property with
	respect to temperature, of a given order using a spec-
	ified method.
<pre>calculate_integral(T1, T2, method)</pre>	Method to calculate the integral of a property with
	respect to temperature, using a specified method.
	continues on next page

<pre>calculate_integral_over_T(T1, T2, method)</pre>	Method to calculate the integral of a property over
	temperature with respect to temperature, using a
	specified method.
<pre>extrapolate(T, method[, in_range])</pre>	Method to perform extrapolation on a given method
	according to the <i>extrapolation</i> setting.
fit_add_model(name, model, Ts, data, **kwargs)	Method to add a new emperical fit equation to the
	object by fitting its coefficients to specified data.
<pre>fit_data_to_model(Ts, data, model[,])</pre>	Method to fit T-dependent property data to one of the
	available model correlations.
<pre>from_json(json_repr)</pre>	Method to create a property model from a JSON se-
	rialization of another property model.
<i>interpolate</i> (T, name)	Method to perform interpolation on a given tabular
	data set previously added via add_tabular_data.
<pre>plot_T_dependent_property([Tmin, Tmax,])</pre>	Method to create a plot of the property vs temperature
	according to either a specified list of methods, or user
	methods (if set), or all methods.
<pre>polynomial_from_method(method[, n, start_n,</pre>	Method to fit a T-dependent property to a polynomial.
])	
solve_property(goal)	Method to solve for the temperature at which a prop-
	erty is at a specified value.
<pre>test_method_validity(T, method)</pre>	Method to test the validity of a specified method for
	a given temperature.
<pre>test_property_validity(prop)</pre>	Method to test the validity of a calculated property.
valid_methods([T])	Method to obtain a sorted list of methods that have
	data available to be used.

Table 97 – continued from previous page

#### **T\_dependent\_property**(*T*)

Method to calculate the property with sanity checking and using the selected *method*.

In the unlikely event the calculation of the property fails, None is returned.

The calculated result is checked with test\_property\_validity and None is returned if the calculated value is nonsensical.

## **Parameters**

T [float] Temperature at which to calculate the property, [K]

#### Returns

prop [float] Calculated property, [units]

# T\_dependent\_property\_derivative(T, order=1)

Method to obtain a derivative of a property with respect to temperature, of a given order.

Calls calculate\_derivative internally to perform the actual calculation.

derivative = 
$$\frac{d(\text{property})}{dT}$$

# **Parameters**

T [float] Temperature at which to calculate the derivative, [K]

**order** [int] Order of the derivative, >= 1

### Returns

derivative [float] Calculated derivative property, [units/K^order]

#### T\_dependent\_property\_integral(T1, T2)

Method to calculate the integral of a property with respect to temperature, using the selected method.

Calls calculate\_integral internally to perform the actual calculation.

integral = 
$$\int_{T_1}^{T_2}$$
 property  $dT$ 

Parameters

T1 [float] Lower limit of integration, [K]

T2 [float] Upper limit of integration, [K]

#### Returns

integral [float] Calculated integral of the property over the given range, [*units\*K*]

#### T\_dependent\_property\_integral\_over\_T(T1, T2)

Method to calculate the integral of a property over temperature with respect to temperature, using the selected method.

Calls calculate\_integral\_over\_T internally to perform the actual calculation.

integral = 
$$\int_{T_1}^{T_2} \frac{\text{property}}{T} dT$$

**Parameters** 

T1 [float] Lower limit of integration, [K]

T2 [float] Upper limit of integration, [K]

Returns

integral [float] Calculated integral of the property over the given range, [units]

#### T\_limits = {}

Dictionary containing method: (Tmin, Tmax) pairs for all methods applicable to the chemical

## \_\_call\_\_(T)

Convenience method to calculate the property; calls  $T\_dependent\_property$ . Caches previously calculated value, which is an overhead when calculating many different values of a property. See  $T\_dependent\_property$  for more details as to the calculation procedure.

# **Parameters**

T [float] Temperature at which to calculate the property, [K]

Returns

prop [float] Calculated property, [units]

```
__repr__()
```

Create and return a string representation of the object. The design of the return string is such that it can be eval'd into itself. This is very convinient for creating tests. Note that several methods are not compatible with the eval'ing principle.

Returns

repr [str] String representation, [-]

#### add\_correlation(name, model, Tmin, Tmax, \*\*kwargs)

Method to add a new set of emperical fit equation coefficients to the object and select it for future property calculations.

A number of hardcoded model names are implemented; other models are not supported.

#### Parameters

name [str] The name of the coefficient set; user specified, [-]

model [str] A string representing the supported models, [-]

Tmin [float] Minimum temperature to use the method at, [K]

Tmax [float] Maximum temperature to use the method at, [K]

kwargs [dict] Various keyword arguments accepted by the model, [-]

#### Notes

The correlation models and links to their functions, describing their parameters, are as follows:

- "Antoine": Antoine, required parameters ('A', 'B', 'C'), optional parameters ('base',).
- "TRC\_Antoine\_extended": TRC\_Antoine\_extended, required parameters ('Tc', 'to', 'A', 'B', 'C', 'n', 'E', 'F').
- "Wagner\_original": Wagner\_original, required parameters ('Tc', 'Pc', 'a', 'b', 'c', 'd').
- "Wagner": Wagner, required parameters ('Tc', 'Pc', 'a', 'b', 'c', 'd').
- "Yaws\_Psat": Yaws\_Psat, required parameters ('A', 'B', 'C', 'D', 'E').
- "TDE\_PVExpansion": TDE\_PVExpansion, required parameters ('a1', 'a2', 'a3'), optional parameters ('a4', 'a5', 'a6', 'a7', 'a8').
- "Alibakhshi": Alibakhshi, required parameters ('Tc', 'C').
- "PPDS12": PPDS12, required parameters ('Tc', 'A', 'B', 'C', 'D', 'E').
- "Watson": Watson, required parameters ('Hvap\_ref', 'T\_ref', 'Tc'), optional parameters ('exponent',).
- "Viswanath\_Natarajan\_2": Viswanath\_Natarajan\_2, required parameters ('A', 'B').
- "Viswanath\_Natarajan\_2\_exponential": Viswanath\_Natarajan\_2\_exponential, required parameters ('C', 'D').
- "Viswanath\_Natarajan\_3": Viswanath\_Natarajan\_3, required parameters ('A', 'B', 'C').
- "PPDS5": PPDS5, required parameters ('Tc', 'a0', 'a1', 'a2').
- "mu\_TDE": mu\_TDE, required parameters ('A', 'B', 'C', 'D').
- "PPDS9": PPDS9, required parameters ('A', 'B', 'C', 'D', 'E').
- "mu\_Yaws": mu\_Yaws, required parameters ('A', 'B'), optional parameters ('C', 'D').
- "Poling": Poling, required parameters ('a', 'b', 'c', 'd', 'e').
- "TRCCp": TRCCp, required parameters ('a0', 'a1', 'a2', 'a3', 'a4', 'a5', 'a6', 'a7').
- "Zabransky\_quasi\_polynomial": Zabransky\_quasi\_polynomial, required parameters ('Tc', 'a1', 'a2', 'a3', 'a4', 'a5', 'a6').
- "Zabransky\_cubic": Zabransky\_cubic, required parameters ('a1', 'a2', 'a3', 'a4').
- "REFPROP\_sigma": REFPROP\_sigma, required parameters ('Tc', 'sigma0', 'n0'), optional parameters ('sigma1', 'n1', 'sigma2', 'n2').
- "Somayajulu": Somayajulu, required parameters ('Tc', 'A', 'B', 'C').
- "Jasper": Jasper, required parameters ('a', 'b').
- "PPDS14": PPDS14, required parameters ('Tc', 'a0', 'a1', 'a2').

- "Watson\_sigma": Watson\_sigma, required parameters ('Tc', 'a1', 'a2', 'a3', 'a4', 'a5').
- "ISTExpansion": ISTExpansion, required parameters ('Tc', 'a1', 'a2', 'a3', 'a4', 'a5').
- "Chemsep\_16": Chemsep\_16, required parameters ('A', 'B', 'C', 'D', 'E').
- "PPDS8": PPDS8, required parameters ('Tc', 'a0', 'a1', 'a2', 'a3').
- "PPDS3": PPDS3, required parameters ('Tc', 'a1', 'a2', 'a3').
- "TDE\_VDNS\_rho": TDE\_VDNS\_rho, required parameters ('Tc', 'rhoc', 'a1', 'a2', 'a3', 'a4', 'MW').
- "PPDS17": PPDS17, required parameters ('Tc', 'a0', 'a1', 'a2', 'MW').
- "volume\_VDI\_PPDS": volume\_VDI\_PPDS, required parameters ('Tc', 'rhoc', 'a', 'b', 'c', 'd', 'MW').
- "Rackett\_fit": Rackett\_fit, required parameters ('Tc', 'rhoc', 'b', 'n', 'MW').
- "DIPPR100": EQ100, required parameters (), optional parameters ('A', 'B', 'C', 'D', 'E', 'F', 'G').
- "constant": EQ100, required parameters (), optional parameters ('A',).
- "linear": EQ100, required parameters (), optional parameters ('A', 'B').
- "quadratic": EQ100, required parameters (), optional parameters ('A', 'B', 'C').
- "cubic": EQ100, required parameters (), optional parameters ('A', 'B', 'C', 'D').
- "quintic": EQ100, required parameters (), optional parameters ('A', 'B', 'C', 'D', 'E').
- "polynomial": horner\_backwards, required parameters ('coeffs',).
- "exp\_polynomial": exp\_horner\_backwards, required parameters ('coeffs',).
- "polynomial\_ln\_tau": horner\_backwards\_ln\_tau, required parameters ('Tc', 'coeffs').
- "exp\_polynomial\_ln\_tau": exp\_horner\_backwards\_ln\_tau, required parameters ('Tc', 'coeffs').
- "DIPPR101": EQ101, required parameters ('A', 'B'), optional parameters ('C', 'D', 'E').
- "DIPPR102": EQ102, required parameters ('A', 'B', 'C', 'D').
- "DIPPR104": EQ104, required parameters ('A', 'B'), optional parameters ('C', 'D', 'E').
- "DIPPR105": EQ105, required parameters ('A', 'B', 'C', 'D').
- "DIPPR106": EQ106, required parameters ('Tc', 'A', 'B'), optional parameters ('C', 'D', 'E').
- "YawsSigma": EQ106, required parameters ('Tc', 'A', 'B'), optional parameters ('C', 'D', 'E').
- "DIPPR107": EQ107, required parameters (), optional parameters ('A', 'B', 'C', 'D', 'E').
- "DIPPR114": EQ114, required parameters ('Tc', 'A', 'B', 'C', 'D').
- "DIPPR115": EQ115, required parameters ('A', 'B'), optional parameters ('C', 'D', 'E').
- "DIPPR116": EQ116, required parameters ('Tc', 'A', 'B', 'C', 'D', 'E').
- "DIPPR127": EQ127, required parameters ('A', 'B', 'C', 'D', 'E', 'F', 'G').
- "Twu91\_alpha\_pure": Twu91\_alpha\_pure, required parameters ('Tc', 'c0', 'c1', 'c2').
- "Heyen\_alpha\_pure": *Heyen\_alpha\_pure*, required parameters ('Tc', 'c1', 'c2').
- "Harmens\_Knapp\_alpha\_pure": *Harmens\_Knapp\_alpha\_pure*, required parameters ('Tc', 'c1', 'c2').
- "Mathias\_Copeman\_untruncated\_alpha\_pure": Mathias\_Copeman\_untruncated\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Mathias\_1983\_alpha\_pure": Mathias\_1983\_alpha\_pure, required parameters ('Tc', 'c1', 'c2').

- "Soave\_1972\_alpha\_pure": Soave\_1972\_alpha\_pure, required parameters ('Tc', 'c0').
- "Soave\_1979\_alpha\_pure": Soave\_1979\_alpha\_pure, required parameters ('Tc', 'M', 'N').
- "Gibbons\_Laughton\_alpha\_pure": *Gibbons\_Laughton\_alpha\_pure*, required parameters ('Tc', 'c1', 'c2').
- "Soave\_1984\_alpha\_pure": Soave\_1984\_alpha\_pure, required parameters ('Tc', 'c1', 'c2').
- "Yu\_Lu\_alpha\_pure": Yu\_Lu\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3', 'c4').
- "Trebble\_Bishnoi\_alpha\_pure": Trebble\_Bishnoi\_alpha\_pure, required parameters ('Tc', 'c1').
- "Melhem\_alpha\_pure": Melhem\_alpha\_pure, required parameters ('Tc', 'c1', 'c2').
- "Androulakis\_alpha\_pure": Androulakis\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Schwartzentruber\_alpha\_pure": Schwartzentruber\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3', 'c4').
- "Almeida\_alpha\_pure": Almeida\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Soave\_1993\_alpha\_pure": Soave\_1993\_alpha\_pure, required parameters ('Tc', 'c1', 'c2').
- "Gasem\_alpha\_pure": Gasem\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Coquelet\_alpha\_pure": Coquelet\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Haghtalab\_alpha\_pure": Haghtalab\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Saffari\_alpha\_pure": Saffari\_alpha\_pure, required parameters ('Tc', 'c1', 'c2', 'c3').
- "Chen\_Yang\_alpha\_pure": Chen\_Yang\_alpha\_pure, required parameters ('Tc', 'omega', 'c1', 'c2', 'c3', 'c4', 'c5', 'c6', 'c7').
- "Wagner2,5": Wagner, required parameters ('Tc', 'Pc', 'a', 'b', 'c', 'd').
- "Wagner3,6": Wagner\_original, required parameters ('Tc', 'Pc', 'a', 'b', 'c', 'd').
- "Andrade": Viswanath\_Natarajan\_2, required parameters ('A', 'B').
- "YawsHvap": EQ106, required parameters ('Tc', 'A', 'B'), optional parameters ('C', 'D', 'E').

add\_method(f, Tmin=None, Tmax=None, f\_der=None, f\_der2=None, f\_der3=None, f\_int=None, f int over T=None, name=None)

Define a new method and select it for future property calculations.

#### Parameters

f [callable] Object which calculates the property given the temperature in K, [-]

Tmin [float, optional] Minimum temperature to use the method at, [K]

Tmax [float, optional] Maximum temperature to use the method at, [K]

- **f\_der** [callable, optional] If specified, should take as an argument the temperature and return the first derivative of the property, [-]
- **f\_der2** [callable, optional] If specified, should take as an argument the temperature and return the second derivative of the property, [-]
- **f\_der3** [callable, optional] If specified, should take as an argument the temperature and return the third derivative of the property, [-]
- **f\_int** [callable, optional] If specified, should take *T1* and *T2* and return the integral of the property from *T1* to *T2*, [-]

**f\_int\_over\_T** [callable, optional] If specified, should take *T1* and *T2* and return the integral of the property over T from *T1* to *T2*, [-]

name [str, optional] Name of method.

### Notes

Once a custom method has been added to an object, that object can no longer be serialized to json and the *TDependentProperty*.\_\_repr\_\_ method can no longer be used to reconstruct the object completely.

add\_tabular\_data(Ts, properties, name=None, check\_properties=True)

Method to set tabular data to be used for interpolation. Ts must be in increasing order. If no name is given, data will be assigned the name 'Tabular data series #x', where x is the number of previously added tabular data series.

After adding the data, this method becomes the selected method.

#### **Parameters**

Ts [array-like] Increasing array of temperatures at which properties are specified, [K]

properties [array-like] List of properties at Ts, [units]

name [str, optional] Name assigned to the data

**check\_properties** [bool] If True, the properties will be checked for validity with *test\_property\_validity* and raise an exception if any are not valid

#### as\_json(references=1)

Method to create a JSON serialization of the property model which can be stored, and reloaded later.

#### Parameters

references [int] How to handle references to other objects; internal parameter, [-]

#### Returns

json\_repr [dict] JSON-friendly representation, [-]

### calculate(T, method)

Method to calculate a property with a specified method, with no validity checking or error handling. Demo function for testing only; must be implemented according to the methods available for each individual method. Include the interpolation call here.

#### **Parameters**

T [float] Temperature at which to calculate the property, [K]

method [str] Method name to use

# Returns

prop [float] Calculated property, [units]

### calculate\_derivative(T, method, order=1)

Method to calculate a derivative of a property with respect to temperature, of a given order using a specified method. Uses SciPy's derivative function, with a delta of 1E-6 K and a number of points equal to 2\*order + 1.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### Parameters

**T** [float] Temperature at which to calculate the derivative, [K]

method [str] Method for which to find the derivative

**order** [int] Order of the derivative, >= 1

#### Returns

derivative [float] Calculated derivative property, [units/K^order]

#### calculate\_integral(T1, T2, method)

Method to calculate the integral of a property with respect to temperature, using a specified method. Uses SciPy's *quad* function to perform the integral, with no options.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### **Parameters**

T1 [float] Lower limit of integration, [K]

T2 [float] Upper limit of integration, [K]

method [str] Method for which to find the integral

#### Returns

integral [float] Calculated integral of the property over the given range, [units\*K]

#### calculate\_integral\_over\_T(T1, T2, method)

Method to calculate the integral of a property over temperature with respect to temperature, using a specified method. Uses SciPy's *quad* function to perform the integral, with no options.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### **Parameters**

T1 [float] Lower limit of integration, [K]

T2 [float] Upper limit of integration, [K]

**method** [str] Method for which to find the integral

#### Returns

integral [float] Calculated integral of the property over the given range, [units]

#### critical\_zero = False

Whether or not the property is declining and reaching zero at the critical point. This is used by numerical solvers.

### extrapolate(T, method, in\_range='error')

Method to perform extrapolation on a given method according to the extrapolation setting.

## Parameters

T [float] Temperature at which to extrapolate the property, [K]

method [str] The method to use, [-]

**in\_range** [str] How to handle inputs which are not outside the temperature limits; set to 'low' to use the low T extrapolation, 'high' to use the high T extrapolation, 'nearest' to use the nearest value, and 'error' or anything else to raise an error in those cases, [-]

#### Returns

prop [float] Calculated property, [units]

#### property extrapolation

The string setting of the current extrapolation settings. This can be set to a new value to change which extrapolation setting is used.

#### fit\_add\_model(name, model, Ts, data, \*\*kwargs)

Method to add a new emperical fit equation to the object by fitting its coefficients to specified data. Once added, the new method is set as the default.

A number of hardcoded model names are implemented; other models are not supported.

This is a wrapper around TDependentProperty.fit\_data\_to\_model and TDependentProperty. add\_correlation.

The data is also stored in the object as a tabular method with the name *name* '+'\_data', through :obj: 'TDependentProperty.add\_tabular\_data.

#### Parameters

name [str] The name of the coefficient set; user specified, [-]

model [str] A string representing the supported models, [-]

Ts [list[float]] Temperatures of the data points, [K]

data [list[float]] Data points, [units]

kwargs [dict] Various keyword arguments accepted by fit\_data\_to\_model, [-]

**classmethod fit\_data\_to\_model**(*Ts*, *data*, *model*, *model\_kwargs=None*, *fit\_method='lm'*, *sigma=None*,

use\_numba=False, do\_statistics=False, guesses=None, solver\_kwargs=None, objective='MeanSquareErr', multiple\_tries=False, multiple\_tries\_max\_err=1e-05, multiple\_tries\_max\_objective='MeanRelErr')

Method to fit T-dependent property data to one of the available model correlations.

### Parameters

Ts [list[float]] Temperatures of the data points, [K]

data [list[float]] Data points, [units]

model [str] A string representing the supported models, [-]

**model\_kwargs** [dict, optional] Various keyword arguments accepted by the model; not necessary for most models. Parameters which are normally fit, can be specified here as well with a constant value and then that fixed value will be used instead of fitting the parameter. [-]

fit\_method [str, optional] The fit method to use; one of {*lm*, *trf*, *dogbox*, *differen*-*tial\_evolution*}, [-]

sigma [None or list[float]] Uncertainty parameters used by curve\_fit, [-]

**use\_numba** [bool, optional] Whether or not to try to use numba to speed up the computation, [-]

**do\_statistics** [bool, optional] Whether or not to compute statistical measures on the outputs, [-]

**guesses** [dict[str: float], optional] Parameter guesses, by name; any number of parameters can be specified, [-]

solver\_kwargs [dict] Extra parameters to be passed to the solver chosen, [-]

objective [str] The minimimization criteria; supported by *differential\_evolution*. One of:

- 'MeanAbsErr': Mean absolute error
- 'MeanRelErr': Mean relative error
- 'MeanSquareErr': Mean squared absolute error
- · 'MeanSquareRelErr': Mean squared relative error
- 'MaxAbsErr': Maximum absolute error
- 'MaxRelErr': Maximum relative error
- 'MaxSquareErr': Maximum squared absolute error
- 'MaxSquareRelErr': Maximum squared relative error

**multiple\_tries** [bool or int] For most solvers, multiple initial guesses are available and the best guess is normally tried. When this is set to True, all guesses are tried until one is found with an error lower than *multiple\_tries\_max\_err*. If an int is supplied, the best *multiple\_tries* guesses are tried only. [-]

**multiple\_tries\_max\_err** [float] Only used when *multiple\_tries* is true; if a solution is found with lower error than this, no further guesses are tried, [-]

multiple\_tries\_max\_objective [str] The error criteria to use for minimization, [-]

#### Returns

coefficients [dict[str: float]] Calculated coefficients, [various]

statistics [dict[str: float]] Statistics, calculated and returned only if *do\_statistics* is True, [-]

#### classmethod from\_json(json\_repr)

Method to create a property model from a JSON serialization of another property model.

### Parameters

json\_repr [dict] JSON-friendly representation, [-]

#### Returns

**model** [*TDependentProperty* or *TPDependentProperty*] Newly created object from the json serialization, [-]

#### Notes

It is important that the input string be in the same format as that created by *TDependentProperty*. *as\_json*.

#### interpolate(T, name)

Method to perform interpolation on a given tabular data set previously added via *add\_tabular\_data*. This method will create the interpolators the first time it is used on a property set, and store them for quick future use.

Interpolation is cubic-spline based if 5 or more points are available, and linearly interpolated if not. Extrapolation is always performed linearly. This function uses the transforms *interpolation\_T*, *interpolation\_property*, and *interpolation\_property\_inv* if set. If any of these are changed after the interpolators were first created, new interpolators are created with the new transforms. All interpolation is performed via the *interp1d* function.

#### Parameters

**T** [float] Temperature at which to interpolate the property, [K]

name [str] The name assigned to the tabular data set

Returns

prop [float] Calculated property, [units]

interpolation\_T = None

interpolation\_T\_inv = None

interpolation\_property = None

# interpolation\_property\_inv = None

#### property method

Method used to set a specific property method or to obtain the name of the method in use.

When setting a method, an exception is raised if the method specified isnt't available for the chemical with the provided information.

If *method* is None, no calculations can be performed.

Parameters

method [str] Method to use, [-]

#### name = 'Property name'

Method to create a plot of the property vs temperature according to either a specified list of methods, or user methods (if set), or all methods. User-selectable number of points, and temperature range. If only\_valid is set,:obj:test\_method\_validity will be used to check if each temperature in the specified range is valid, and test\_property\_validity will be used to test the answer, and the method is allowed to fail; only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will not succeed if the method fails.

### Parameters

- Tmin [float] Minimum temperature, to begin calculating the property, [K]
- Tmax [float] Maximum temperature, to stop calculating the property, [K]

methods [list, optional] List of methods to consider

- **pts** [int, optional] A list of points to calculate the property at; if Tmin to Tmax covers a wide range of method validities, only a few points may end up calculated for a given method so this may need to be large
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds

show [bool] If True, displays the plot; otherwise, returns it

- **tabular\_points** [bool, optional] If True, tabular data will only be shows as the original points; otherwise interpolated values are shown, [-]

Method to fit a T-dependent property to a polynomial. The degree of the polynomial can be specified with the *n* parameter, or it will be automatically selected for maximum accuracy.

#### Parameters

method [str] Method name to fit, [-]

- **n** [int, optional] The degree of the polynomial, if specified
- start\_n [int] If n is not specified, all polynomials of degree start\_n to max\_n will be tried and the highest-accuracy will be selected; [-]
- **max\_n** [int] If *n* is not specified, all polynomials of degree *start\_n* to *max\_n* will be tried and the highest-accuracy will be selected; [-]
- eval\_pts [int] The number of points to evaluate the fitted functions at to check for accuracy; more is better but slower, [-]
- fit\_form [str] The shape of the polynomial; options are 'POLY\_FIT', 'EXP\_POLY\_FIT', 'EXP\_POLY\_FIT\_LN\_TAU', and 'POLY\_FIT\_LN\_TAU' [-]

#### Returns

coeffs [list[float]] Fit coefficients, [-]

Tmin [float] The minimum temperature used for the fitting, [K]

Tmax [float] The maximum temperature used for the fitting, [K]

err\_avg [float] Mean error in the evaluated points, [-]

err\_std [float] Standard deviation of errors in the evaluated points, [-]

**min\_ratio** [float] Lowest ratio of calc/actual in any found points, [-]

max\_ratio [float] Highest ratio of calc/actual in any found points, [-]

#### property\_max = 10000.0

property\_min = 0

#### ranked\_methods = []

#### solve\_property(goal)

Method to solve for the temperature at which a property is at a specified value. *T\_dependent\_property* is used to calculate the value of the property as a function of temperature.

Checks the given property value with *test\_property\_validity* first and raises an exception if it is not valid.

#### Parameters

goal [float] Propoerty value desired, [units]

#### Returns

T [float] Temperature at which the property is the specified value [K]

#### test\_method\_validity(T, method)

Method to test the validity of a specified method for a given temperature. Demo function for testing only; must be implemented according to the methods available for each individual method. Include the interpolation check here.

### Parameters

T [float] Temperature at which to determine the validity of the method, [K]

method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

#### classmethod test\_property\_validity(prop)

Method to test the validity of a calculated property. Normally, this method is used by a given property class, and has maximum and minimum limits controlled by the variables *property\_min* and *property\_max*.

#### Parameters

prop [float] property to be tested, [units]

Returns

validity [bool] Whether or not a specifid method is valid

units = 'Property units'

#### valid\_methods(T=None)

Method to obtain a sorted list of methods that have data available to be used. The methods are ranked in the following order:

- The currently selected method is first (if one is selected)
- Other available methods are ranked by the attribute *ranked\_methods*

If T is provided, the methods will be checked against the temperature limits of the correlations as well.

#### Parameters

T [float or None] Temperature at which to test methods, [K]

### Returns

sorted\_valid\_methods [list] Sorted lists of methods valid at T according to
 test\_method\_validity, [-]

# 7.31.2 Temperature and Pressure Dependent

#### class thermo.utils.TPDependentProperty(extrapolation, \*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for calculating temperature and pressure dependent chemical properties.

On creation, a *TPDependentProperty* examines all the possible methods implemented for calculating the property, loads whichever coefficients it needs (unless *load\_data* is set to False), examines its input parameters, and selects the method it prefers. This method will continue to be used for all calculations until the method is changed by setting a new method to the to *method* attribute.

Because many pressure dependent property methods are implemented as a low-pressure correlation and a highpressure correlation, this class works essentially the same as *TDependentProperty* but with extra methods that accept pressure as a parameter.

The object also selects the pressure-dependent method it prefers. This method will continue to be used for all pressure-dependent calculations until the pressure-dependent method is changed by setting a new method\_P to the to  $method_P$  attribute.

The default list of preferred pressure-dependent method orderings is at ranked\_methods\_P for all properties; the order can be modified there in-place, and this will take effect on all new *TPDependentProperty* instances created but NOT on existing instances.

Tabular data can be provided as either temperature-dependent or pressure-dependent data. The same *extrapolation* settings as in *TDependentProperty* are implemented here for the low-pressure correlations.

In addition to the methods and attributes shown here, all those from *TPDependentProperty* are also available.

#### Attributes

**method\_P** [str] Method used to set or get a specific property method.

*method* [str] Method used to set a specific property method or to obtain the name of the method in use.

all\_methods [set] All low-pressure methods available, [-]

all\_methods\_P [set] All pressure-dependent methods available, [-]

# Methods

TP_dependent_property(T, P)	Method to calculate the property given a temperature and pressure according to the selected <i>method_P</i> and <i>method</i> .
<pre>TP_dependent_property_derivative_P(T, P[, order])</pre>	Method to calculate a derivative of a temperature and pressure dependent property with respect to pressure at constant temperature, of a given order, according to the selected <i>method_P</i> .
<pre>TP_dependent_property_derivative_T(T, P[, order])</pre>	Method to calculate a derivative of a temperature and pressure dependent property with respect to temper- ature at constant pressure, of a given order, according to the selected <i>method_P</i> .
TP_or_T_dependent_property(T, P)	Method to calculate the property given a temperature and pressure according to the selected <i>method_P</i> and <i>method</i> .
call(T, P)	Convenience method to calculate the property; calls <i>TP_dependent_property</i> .
add_method(f[, Tmin, Tmax, f_der, f_der2,])	Define a new method and select it for future property calculations.
<pre>add_tabular_data(Ts, properties[, name,])</pre>	Method to set tabular data to be used for interpola- tion.
<pre>add_tabular_data_P(Ts, Ps, properties[,])</pre>	Method to set tabular data to be used for interpola- tion.
calculate(T, method)	Method to calculate a property with a specified method, with no validity checking or error handling.
<pre>calculate_derivative_P(P, T, method[, order])</pre>	Method to calculate a derivative of a temperature and pressure dependent property with respect to pressure at constant temperature, of a given order using a spec- ified method.
<pre>calculate_derivative_T(T, P, method[, order])</pre>	Method to calculate a derivative of a temperature and pressure dependent property with respect to temper- ature at constant pressure, of a given order using a specified method.
<pre>extrapolate(T, method[, in_range])</pre>	Method to perform extrapolation on a given method according to the <i>extrapolation</i> setting.
<pre>plot_TP_dependent_property([Tmin, Tmax, ])</pre>	Method to create a plot of the property vs tempera- ture and pressure according to either a specified list of methods, or user methods (if set), or all methods.
<pre>plot_isobar(P[, Tmin, Tmax, methods_P, pts,])</pre>	Method to create a plot of the property vs temperature at a specific pressure according to either a specified list of methods, or user methods (if set), or all meth- ods.

continues on next page

<pre>plot_isotherm(T[, Pmin, Pmax, methods_P,])</pre>	Method to create a plot of the property vs pressure at a
	specified temperature according to either a specified
	list of methods, or the user methods (if set), or all
	methods.
solve_property(goal)	Method to solve for the temperature at which a prop-
	erty is at a specified value.
<pre>test_method_validity(T, method)</pre>	Method to test the validity of a specified method for
	a given temperature.
<pre>test_property_validity(prop)</pre>	Method to test the validity of a calculated property.
valid_methods([T])	Method to obtain a sorted list of methods that have
	data available to be used.
valid_methods_P([T, P])	Method to obtain a sorted list of high-pressure meth-
	ods that have data available to be used.

# Table 98 – continued from previous page

### **TP\_dependent\_property**(*T*, *P*)

Method to calculate the property given a temperature and pressure according to the selected *method\_P* and *method*. The pressure-dependent method is always used and required to succeed. The result is checked with *test\_property\_validity*.

If the method does not succeed, returns None.

#### **Parameters**

T [float] Temperature at which to calculate the property, [K]

**P** [float] Pressure at which to calculate the property, [Pa]

#### Returns

prop [float] Calculated property, [units]

## TP\_dependent\_property\_derivative\_P(T, P, order=1)

Method to calculate a derivative of a temperature and pressure dependent property with respect to pressure at constant temperature, of a given order, according to the selected *method\_P*.

Calls calculate\_derivative\_P internally to perform the actual calculation.

derivative = 
$$\frac{d(\text{property})}{dP}|_T$$

# Parameters

T [float] Temperature at which to calculate the derivative, [K]

**P** [float] Pressure at which to calculate the derivative, [Pa]

**order** [int] Order of the derivative, >= 1

Returns

**dprop\_dP\_T** [float] Calculated derivative property, [*units/Pa^order*]

# **TP\_dependent\_property\_derivative\_T**(*T*, *P*, order=1)

Method to calculate a derivative of a temperature and pressure dependent property with respect to temperature at constant pressure, of a given order, according to the selected *method\_P*.

Calls *calculate\_derivative\_T* internally to perform the actual calculation.

derivative = 
$$\frac{d(\text{property})}{dT}|_P$$

**Parameters** 

**T** [float] Temperature at which to calculate the derivative, [K]

**P** [float] Pressure at which to calculate the derivative, [Pa]

**order** [int] Order of the derivative, >= 1

#### Returns

**dprop\_dT\_P** [float] Calculated derivative property, [*units/K^order*]

#### **TP\_or\_T\_dependent\_property**(*T*, *P*)

Method to calculate the property given a temperature and pressure according to the selected *method\_P* and *method*. The pressure-dependent method is always tried. The result is checked with *test\_property\_validity*.

If the pressure-dependent method does not succeed, the low-pressure method is tried and its result is returned.

**Warning:** It can seem like a good idea to switch between a low-pressure and a high-pressure method if the high pressure method is not working, however it can cause discontinuities and prevent numerical methods from converging

#### **Parameters**

T [float] Temperature at which to calculate the property, [K]

**P** [float] Pressure at which to calculate the property, [Pa]

#### Returns

prop [float] Calculated property, [units]

### T\_limits = {}

Dictionary containing method: (Tmin, Tmax) pairs for all methods applicable to the chemical

#### \_\_call\_\_(*T*, *P*)

Convenience method to calculate the property; calls *TP\_dependent\_property*. Caches previously calculated value, which is an overhead when calculating many different values of a property. See *TP\_dependent\_property* for more details as to the calculation procedure.

#### Parameters

**T** [float] Temperature at which to calculate the property, [K]

P [float] Pressure at which to calculate the property, [Pa]

### Returns

**prop** [float] Calculated property, [*units*]

add\_method(f, Tmin=None, Tmax=None, f\_der=None, f\_der2=None, f\_der3=None, f\_int=None, f int over T=None, name=None)

Define a new method and select it for future property calculations.

#### **Parameters**

f [callable] Object which calculates the property given the temperature in K, [-]

Tmin [float, optional] Minimum temperature to use the method at, [K]

Tmax [float, optional] Maximum temperature to use the method at, [K]

- **f\_der** [callable, optional] If specified, should take as an argument the temperature and return the first derivative of the property, [-]
- **f\_der2** [callable, optional] If specified, should take as an argument the temperature and return the second derivative of the property, [-]
- **f\_der3** [callable, optional] If specified, should take as an argument the temperature and return the third derivative of the property, [-]
- **f\_int** [callable, optional] If specified, should take *T1* and *T2* and return the integral of the property from *T1* to *T2*, [-]
- **f\_int\_over\_T** [callable, optional] If specified, should take *T1* and *T2* and return the integral of the property over T from *T1* to *T2*, [-]

name [str, optional] Name of method.

# Notes

Once a custom method has been added to an object, that object can no longer be serialized to json and the *TDependentProperty*.\_\_\_repr\_\_\_ method can no longer be used to reconstruct the object completely.

add\_tabular\_data(Ts, properties, name=None, check\_properties=True)

Method to set tabular data to be used for interpolation. Ts must be in increasing order. If no name is given, data will be assigned the name 'Tabular data series #x', where x is the number of previously added tabular data series.

After adding the data, this method becomes the selected method.

# Parameters

Ts [array-like] Increasing array of temperatures at which properties are specified, [K]

properties [array-like] List of properties at Ts, [units]

**name** [str, optional] Name assigned to the data

**check\_properties** [bool] If True, the properties will be checked for validity with *test\_property\_validity* and raise an exception if any are not valid

#### add\_tabular\_data\_P(Ts, Ps, properties, name=None, check\_properties=True)

Method to set tabular data to be used for interpolation. Ts and Psmust be in increasing order. If no name is given, data will be assigned the name 'Tabular data series #x', where x is the number of previously added tabular data series.

After adding the data, this method becomes the selected high-pressure method.

#### **Parameters**

Ts [array-like] Increasing array of temperatures at which properties are specified, [K]

**Ps** [array-like] Increasing array of pressures at which properties are specified, [Pa]

**properties** [array-like] List of properties at *Ts* and *Ps*; the data should be indexed [P][T], [*units*]

name [str, optional] Name assigned to the data

**check\_properties** [bool] If True, the properties will be checked for validity with *test\_property\_validity* and raise an exception if any are not valid

#### calculate(T, method)

Method to calculate a property with a specified method, with no validity checking or error handling. Demo function for testing only; must be implemented according to the methods available for each individual method. Include the interpolation call here.

# Parameters

T [float] Temperature at which to calculate the property, [K]

method [str] Method name to use

Returns

prop [float] Calculated property, [units]

# calculate\_derivative\_P(P, T, method, order=1)

Method to calculate a derivative of a temperature and pressure dependent property with respect to pressure at constant temperature, of a given order using a specified method. Uses SciPy's derivative function, with a delta of 0.01 Pa and a number of points equal to 2\* order + 1.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### **Parameters**

**P** [float] Pressure at which to calculate the derivative, [Pa]

**T** [float] Temperature at which to calculate the derivative, [K]

method [str] Method for which to find the derivative

**order** [int] Order of the derivative, >= 1

# Returns

**dprop\_dP\_T** [float] Calculated derivative property at constant temperature, [*units/Pa^order*]

# calculate\_derivative\_T(T, P, method, order=1)

Method to calculate a derivative of a temperature and pressure dependent property with respect to temperature at constant pressure, of a given order using a specified method. Uses SciPy's derivative function, with a delta of 1E-6 K and a number of points equal to 2\* order + 1.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### Parameters

T [float] Temperature at which to calculate the derivative, [K]

**P** [float] Pressure at which to calculate the derivative, [Pa]

**method** [str] Method for which to find the derivative

**order** [int] Order of the derivative, >= 1

#### Returns

**dprop\_dT\_P** [float] Calculated derivative property at constant pressure, [*units/K^order*]

#### extrapolate(T, method, in\_range='error')

Method to perform extrapolation on a given method according to the *extrapolation* setting.

#### Parameters

T [float] Temperature at which to extrapolate the property, [K]

**method** [str] The method to use, [-]

**in\_range** [str] How to handle inputs which are not outside the temperature limits; set to 'low' to use the low T extrapolation, 'high' to use the high T extrapolation, 'nearest' to use the nearest value, and 'error' or anything else to raise an error in those cases, [-]

#### Returns

prop [float] Calculated property, [units]

#### property extrapolation

The string setting of the current extrapolation settings. This can be set to a new value to change which extrapolation setting is used.

#### interpolation\_T = None

interpolation\_T\_inv = None

interpolation\_property = None

#### interpolation\_property\_inv = None

#### property method

Method used to set a specific property method or to obtain the name of the method in use.

When setting a method, an exception is raised if the method specified isnt't available for the chemical with the provided information.

If *method* is None, no calculations can be performed.

# Parameters

method [str] Method to use, [-]

#### property method\_P

Method used to set or get a specific property method.

An exception is raised if the method specified isnt't available for the chemical with the provided information.

#### **Parameters**

method [str or list] Methods by name to be considered or preferred

#### name = 'Property name'

# 

Method to create a plot of the property vs temperature and pressure according to either a specified list of methods, or user methods (if set), or all methods. User-selectable number of points for each variable. If only\_valid is set,:obj:test\_method\_validity\_P will be used to check if each condition in the specified range is valid, and test\_property\_validity will be used to test the answer, and the method is allowed to fail; only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will not succeed if the any method fails for any point.

#### **Parameters**

Tmin [float] Minimum temperature, to begin calculating the property, [K]

Tmax [float] Maximum temperature, to stop calculating the property, [K]

Pmin [float] Minimum pressure, to begin calculating the property, [Pa]

Pmax [float] Maximum pressure, to stop calculating the property, [Pa]

methods\_P [list, optional] List of methods to plot

- **pts** [int, optional] A list of points to calculate the property at for both temperature and pressure; pts<sup>2</sup> points will be calculated.
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds

**plot\_isobar**(*P*, *Tmin=None*, *Tmax=None*, *methods\_P=[]*, *pts=50*, *only\_valid=True*, *show=True*)

Method to create a plot of the property vs temperature at a specific pressure according to either a specified list of methods, or user methods (if set), or all methods. User-selectable number of points, and temperature range. If only\_valid is set,:obj:*test\_method\_validity\_P* will be used to check if each condition in the specified range is valid, and *test\_property\_validity* will be used to test the answer, and the method is allowed to fail; only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will not succeed if the method fails.

#### **Parameters**

**P** [float] Pressure for the isobar, [Pa]

Tmin [float] Minimum temperature, to begin calculating the property, [K]

Tmax [float] Maximum temperature, to stop calculating the property, [K]

methods\_P [list, optional] List of methods to consider

- **pts** [int, optional] A list of points to calculate the property at; if Tmin to Tmax covers a wide range of method validities, only a few points may end up calculated for a given method so this may need to be large
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds

**plot\_isotherm**(*T*, *Pmin=None*, *Pmax=None*, *methods\_P=[]*, *pts=50*, *only\_valid=True*, *show=True*)

Method to create a plot of the property vs pressure at a specified temperature according to either a specified list of methods, or the user methods (if set), or all methods. User-selectable number of points, and pressure range. If only\_valid is set, test\_method\_validity\_P will be used to check if each condition in the specified range is valid, and test\_property\_validity will be used to test the answer, and the method is allowed to fail; only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will not succeed if the method fails.

#### **Parameters**

T [float] Temperature at which to create the plot, [K]

Pmin [float] Minimum pressure, to begin calculating the property, [Pa]

**Pmax** [float] Maximum pressure, to stop calculating the property, [Pa]

methods\_P [list, optional] List of methods to consider

- **pts** [int, optional] A list of points to calculate the property at; if Pmin to Pmax covers a wide range of method validities, only a few points may end up calculated for a given method so this may need to be large
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds

show [bool] If True, displays the plot; otherwise, returns it

 $property_max = 10000.0$ 

# property\_min = 0

# ranked\_methods = []

# solve\_property(goal)

Method to solve for the temperature at which a property is at a specified value. *T\_dependent\_property* is used to calculate the value of the property as a function of temperature.

Checks the given property value with *test\_property\_validity* first and raises an exception if it is not valid.

#### **Parameters**

goal [float] Propoerty value desired, [units]

#### Returns

**T** [float] Temperature at which the property is the specified value [K]

# test\_method\_validity(T, method)

Method to test the validity of a specified method for a given temperature. Demo function for testing only; must be implemented according to the methods available for each individual method. Include the interpolation check here.

#### Parameters

T [float] Temperature at which to determine the validity of the method, [K]

method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

# classmethod test\_property\_validity(prop)

Method to test the validity of a calculated property. Normally, this method is used by a given property class, and has maximum and minimum limits controlled by the variables *property\_min* and *property\_max*.

#### Parameters

prop [float] property to be tested, [units]

Returns

validity [bool] Whether or not a specifid method is valid

# units = 'Property units'

# valid\_methods(T=None)

Method to obtain a sorted list of methods that have data available to be used. The methods are ranked in the following order:

- The currently selected method is first (if one is selected)
- Other available methods are ranked by the attribute *ranked\_methods*
- If T is provided, the methods will be checked against the temperature limits of the correlations as well.

# Parameters

T [float or None] Temperature at which to test methods, [K]

#### Returns

sorted\_valid\_methods [list] Sorted lists of methods valid at T according to
test\_method\_validity, [-]

valid\_methods\_P(T=None, P=None)

Method to obtain a sorted list of high-pressure methods that have data available to be used. The methods are ranked in the following order:

- The currently selected *method\_P* is first (if one is selected)
- Other available pressure-depenent methods are ranked by the attribute ranked\_methods\_P

If T and P are provided, the methods will be checked against the temperature and pressure limits of the correlations as well.

## **Parameters**

- T [float] Temperature at which to test methods, [K]
- **P** [float] Pressure at which to test methods, [Pa]

#### Returns

sorted\_valid\_methods\_P [list] Sorted lists of methods valid at T and P according to
test\_method\_validity\_P

# 7.31.3 Temperature, Pressure, and Composition Dependent

class thermo.utils.MixtureProperty(\*\*kwargs)

Bases: object

# Attributes

*correct\_pressure\_pure* Method to set the pressure-dependence of the model; if set to False, only temperature dependence is used, and if True, temperature and pressure dependence are used.

method Method to set the T, P, and composition dependent property method desired.

prop\_cached

# Methods

call(T, P[, zs, ws])	Convenience method to calculate the property; calls
	mixture_property.
as_json([references])	Method to create a JSON serialization of the mixture
	property which can be stored, and reloaded later.
<pre>calculate_derivative_P(P, T, zs, ws, method)</pre>	Method to calculate a derivative of a mixture prop-
	erty with respect to pressure at constant temperature
	and composition of a given order using a specified
	method.
<pre>calculate_derivative_T(T, P, zs, ws, method)</pre>	Method to calculate a derivative of a mixture prop-
	erty with respect to temperature at constant pressure
	and composition of a given order using a specified
	method.
<pre>excess_property(T, P[, zs, ws])</pre>	Method to calculate the excess property with sanity
	checking and without specifying a specific method.
<pre>from_j son(string)</pre>	Method to create a MixtureProperty from a JSON se-
-	rialization of another MixtureProperty.
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continues on next page

	ed from previous page
<pre>mixture_property(T, P[, zs, ws])</pre>	Method to calculate the property with sanity check-
	ing and without specifying a specific method.
<pre>partial_property(T, P, i[, zs, ws])</pre>	Method to calculate the partial molar property with
	sanity checking and without specifying a specific
	method for the specified compound index and com-
	position.
<pre>plot_isobar(P[, zs, ws, Tmin, Tmax,])</pre>	Method to create a plot of the property vs tempera-
	ture at a specific pressure and composition according
	to either a specified list of methods, or the selected
	method.
<pre>plot_isotherm(T[, zs, ws, Pmin, Pmax,])</pre>	Method to create a plot of the property vs pressure at
	a specified temperature and composition according to
	either a specified list of methods, or the set method.
<pre>plot_property([zs, ws, Tmin, Tmax, Pmin,])</pre>	Method to create a plot of the property vs tempera-
	ture and pressure according to either a specified list
	of methods, or the selected method.
<pre>property_derivative_P(T, P[, zs, ws, order])</pre>	Method to calculate a derivative of a mixture prop-
	erty with respect to pressure at constant temperature
	and composition, of a given order.
<pre>property_derivative_T(T, P[, zs, ws, order])</pre>	Method to calculate a derivative of a mixture prop-
	erty with respect to temperature at constant pressure
	and composition, of a given order.
<pre>test_property_validity(prop)</pre>	Method to test the validity of a calculated property.

Table 99 – continued from previous page

pure_objs	
<pre>set_poly_fit_coeffs</pre>	

# RAISE\_PROPERTY\_CALCULATION\_ERROR = False

TP\_zs\_ws\_cached = (None, None, None, None)

#### Tmax

Maximum temperature at which no method can calculate the property above.

#### Tmin

Minimum temperature at which no method can calculate the property under.

#### all\_methods

Set of all methods available for a given set of information; filled by load\_all\_methods.

## all\_poly\_fit = False

as\_json(references=1)

Method to create a JSON serialization of the mixture property which can be stored, and reloaded later.

## Parameters

references [int] How to handle references to other objects; internal parameter, [-]

## Returns

json\_repr [dict] JSON-friendly representation, [-]

# calculate\_derivative\_P(P, T, zs, ws, method, order=1)

Method to calculate a derivative of a mixture property with respect to pressure at constant temperature and composition of a given order using a specified method. Uses SciPy's derivative function, with a delta of 0.01 Pa and a number of points equal to 2\* order + 1.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### Parameters

- **P** [float] Pressure at which to calculate the derivative, [Pa]
- T [float] Temperature at which to calculate the derivative, [K]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method for which to find the derivative

**order** [int] Order of the derivative, >= 1

#### Returns

**d\_prop\_d\_P\_at\_T** [float] Calculated derivative property at constant temperature, [*units/Pa^order*]

#### calculate\_derivative\_T(T, P, zs, ws, method, order=1)

Method to calculate a derivative of a mixture property with respect to temperature at constant pressure and composition of a given order using a specified method. Uses SciPy's derivative function, with a delta of 1E-6 K and a number of points equal to 2\*order + 1.

This method can be overwritten by subclasses who may perfer to add analytical methods for some or all methods as this is much faster.

If the calculation does not succeed, returns the actual error encountered.

#### **Parameters**

T [float] Temperature at which to calculate the derivative, [K]

**P** [float] Pressure at which to calculate the derivative, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method for which to find the derivative

**order** [int] Order of the derivative, >= 1

#### Returns

**d\_prop\_d\_T\_at\_P** [float] Calculated derivative property at constant pressure, [*units/K^order*]

#### property correct\_pressure\_pure

Method to set the pressure-dependence of the model; if set to False, only temperature dependence is used, and if True, temperature and pressure dependence are used.

#### excess\_property(T, P, zs=None, ws=None)

Method to calculate the excess property with sanity checking and without specifying a specific method. This requires the calculation of the property as a function of composition at the limiting concentration of each component. One or both of *zs* and *ws* are required.

$$m^E = m_{mixing} = m - \sum_i m_{i,pure} \cdot z_i$$

Parameters

- **T** [float] Temperature at which to calculate the excess property, [K]
- P [float] Pressure at which to calculate the excess property, [Pa]
- zs [list[float], optional] Mole fractions of all species in the mixture, [-]
- ws [list[float], optional] Weight fractions of all species in the mixture, [-]

#### Returns

excess\_prop [float] Calculated excess property, [units]

#### classmethod from\_json(string)

Method to create a MixtureProperty from a JSON serialization of another MixtureProperty.

#### Parameters

json\_repr [dict] JSON-friendly representation, [-]

# Returns

constants [MixtureProperty] Newly created object from the json serialization, [-]

# Notes

It is important that the input string be in the same format as that created by *MixtureProperty.as\_json*.

#### property method

Method to set the T, P, and composition dependent property method desired. See the *all\_methods* attribute for a list of methods valid for the specified chemicals and inputs.

#### mixture\_property(T, P, zs=None, ws=None)

Method to calculate the property with sanity checking and without specifying a specific method. valid\_methods is used to obtain a sorted list of methods to try. Methods are then tried in order until one succeeds. The methods are allowed to fail, and their results are checked with *test\_property\_validity*. On success, the used method is stored in the variable *method*.

If *method* is set, this method is first checked for validity with test\_method\_validity for the specified temperature, and if it is valid, it is then used to calculate the property. The result is checked for validity, and returned if it is valid. If either of the checks fail, the function retrieves a full list of valid methods with valid\_methods and attempts them as described above.

If no methods are found which succeed, returns None. One or both of zs and ws are required.

#### **Parameters**

T [float] Temperature at which to calculate the property, [K]

**P** [float] Pressure at which to calculate the property, [Pa]

zs [list[float], optional] Mole fractions of all species in the mixture, [-]

ws [list[float], optional] Weight fractions of all species in the mixture, [-]

#### Returns

prop [float] Calculated property, [units]

name = 'Test'

#### partial\_property(T, P, i, zs=None, ws=None)

Method to calculate the partial molar property with sanity checking and without specifying a specific method for the specified compound index and composition.

$$\bar{m}_i = \left(\frac{\partial(n_T m)}{\partial n_i}\right)_{T,P,n_{j \neq i}}$$

#### **Parameters**

- T [float] Temperature at which to calculate the partial property, [K]
- **P** [float] Pressure at which to calculate the partial property, [Pa]
- i [int] Compound index, [-]
- zs [list[float], optional] Mole fractions of all species in the mixture, [-]
- ws [list[float], optional] Weight fractions of all species in the mixture, [-]

#### Returns

partial\_prop [float] Calculated partial property, [units]

- plot\_isobar(P, zs=None, ws=None, Tmin=None, Tmax=None, methods=[], pts=50, only\_valid=True)
- Method to create a plot of the property vs temperature at a specific pressure and composition according to either a specified list of methods, or the selected method. User-selectable number of points, and temperature range. If only\_valid is set,:obj:*test\_method\_validity* will be used to check if each condition in the specified range is valid, and *test\_property\_validity* will be used to test the answer, and the method is allowed to fail; only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will not succeed if the method fails. One or both of *zs* and *ws* are required.

#### **Parameters**

- **P** [float] Pressure for the isobar, [Pa]
- zs [list[float], optional] Mole fractions of all species in the mixture, [-]
- ws [list[float], optional] Weight fractions of all species in the mixture, [-]
- Tmin [float] Minimum temperature, to begin calculating the property, [K]
- Tmax [float] Maximum temperature, to stop calculating the property, [K]
- methods [list, optional] List of methods to consider
- **pts** [int, optional] A list of points to calculate the property at; if Tmin to Tmax covers a wide range of method validities, only a few points may end up calculated for a given method so this may need to be large
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds
- plot\_isotherm(T, zs=None, ws=None, Pmin=None, Pmax=None, methods=[], pts=50, only\_valid=True)
  Method to create a plot of the property vs pressure at a specified temperature and composition according to
  either a specified list of methods, or the set method. User-selectable number of points, and pressure range.
  If only\_valid is set, test\_method\_validity will be used to check if each condition in the specified range
  is valid, and test\_property\_validity will be used to test the answer, and the method is allowed to fail;
  only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will
  not succeed if the method fails. One or both of zs and ws are required.

#### Parameters

**T** [float] Temperature at which to create the plot, [K]

**zs** [list[float], optional] Mole fractions of all species in the mixture, [-]

ws [list[float], optional] Weight fractions of all species in the mixture, [-]

Pmin [float] Minimum pressure, to begin calculating the property, [Pa]

**Pmax** [float] Maximum pressure, to stop calculating the property, [Pa]

methods [list, optional] List of methods to consider

- **pts** [int, optional] A list of points to calculate the property at; if Pmin to Pmax covers a wide range of method validities, only a few points may end up calculated for a given method so this may need to be large
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds

Method to create a plot of the property vs temperature and pressure according to either a specified list of methods, or the selected method. User-selectable number of points for each variable. If only\_valid is set,:obj:*test\_method\_validity* will be used to check if each condition in the specified range is valid, and *test\_property\_validity* will be used to test the answer, and the method is allowed to fail; only the valid points will be plotted. Otherwise, the result will be calculated and displayed as-is. This will not succeed if the any method fails for any point. One or both of *zs* and *ws* are required.

#### Parameters

zs [list[float], optional] Mole fractions of all species in the mixture, [-]

ws [list[float], optional] Weight fractions of all species in the mixture, [-]

Tmin [float] Minimum temperature, to begin calculating the property, [K]

Tmax [float] Maximum temperature, to stop calculating the property, [K]

Pmin [float] Minimum pressure, to begin calculating the property, [Pa]

Pmax [float] Maximum pressure, to stop calculating the property, [Pa]

methods [list, optional] List of methods to consider

- **pts** [int, optional] A list of points to calculate the property at for both temperature and pressure; pts<sup>2</sup> points will be calculated.
- **only\_valid** [bool] If True, only plot successful methods and calculated properties, and handle errors; if False, attempt calculation without any checking and use methods outside their bounds

#### prop\_cached = None

#### property\_derivative\_P(T, P, zs=None, ws=None, order=1)

Method to calculate a derivative of a mixture property with respect to pressure at constant temperature and composition, of a given order. Methods found valid by valid\_methods are attempted until a method succeeds. If no methods are valid and succeed, None is returned.

Calls *calculate\_derivative\_P* internally to perform the actual calculation.

derivative = 
$$\frac{d(\text{property})}{dP}|_{T,z}$$

#### **Parameters**

**T** [float] Temperature at which to calculate the derivative, [K]

P [float] Pressure at which to calculate the derivative, [Pa]

zs [list[float], optional] Mole fractions of all species in the mixture, [-]

ws [list[float], optional] Weight fractions of all species in the mixture, [-]

**order** [int] Order of the derivative, >= 1

#### Returns

**d\_prop\_d\_P\_at\_T** [float] Calculated derivative property, [*units/Pa^order*]

#### property\_derivative\_T(T, P, zs=None, ws=None, order=1)

Method to calculate a derivative of a mixture property with respect to temperature at constant pressure and composition, of a given order. Methods found valid by valid\_methods are attempted until a method succeeds. If no methods are valid and succeed, None is returned.

Calls calculate\_derivative\_T internally to perform the actual calculation.

derivative = 
$$\frac{d(\text{property})}{dT}|_{P,z}$$

One or both of zs and ws are required.

#### **Parameters**

- T [float] Temperature at which to calculate the derivative, [K]
- P [float] Pressure at which to calculate the derivative, [Pa]

zs [list[float], optional] Mole fractions of all species in the mixture, [-]

ws [list[float], optional] Weight fractions of all species in the mixture, [-]

**order** [int] Order of the derivative, >= 1

#### Returns

**d\_prop\_d\_T\_at\_P** [float] Calculated derivative property, [*units/K^order*]

property\_max = 10.0

property\_min = 0.0

pure\_objs()

```
pure_reference_types = ()
```

```
pure_references = ()
```

```
ranked_methods = []
```

set\_poly\_fit\_coeffs()

```
skip_method_validity_check = False
```

Flag to disable checking the validity of the method at the specified conditions. Saves a little time.

#### skip\_prop\_validity\_check = False

Flag to disable checking the output of the value. Saves a little time.

#### classmethod test\_property\_validity(prop)

Method to test the validity of a calculated property. Normally, this method is used by a given property class, and has maximum and minimum limits controlled by the variables *property\_min* and *property\_max*.

#### Parameters

**prop** [float] property to be tested, [*units*]

Returns

validity [bool] Whether or not a specifid method is valid

units = 'test units'

# 7.32 Vapor Pressure and Sublimation Pressure (thermo.vapor\_pressure)

This module contains implementations of *thermo.utils.TDependentProperty* representing vapor pressure and sublimation pressure. A variety of estimation and data methods are available as included in the *chemicals* library.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Vapor Pressure
- Sublimation Pressure

# 7.32.1 Vapor Pressure

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with vapor pressure as a function of temperature. Consists of five coefficient-based methods and four data sources, one source of tabular information, four corresponding-states estimators, any provided equation of state, the external library CoolProp, and one substance-specific formulation.

#### Parameters

- **Tb** [float, optional] Boiling point, [K]
- Tc [float, optional] Critical temperature, [K]
- Pc [float, optional] Critical pressure, [Pa]

omega [float, optional] Acentric factor, [-]

CASRN [str, optional] The CAS number of the chemical

- eos [object, optional] Equation of State object after thermo.eos.GCEOS
- **load\_data** [bool, optional] If False, do not load property coefficients from data sources in files; this can be used to reduce the memory consumption of an object as well, [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

#### See also:

chemicals.vapor\_pressure.Wagner\_original

chemicals.vapor\_pressure.Wagner

chemicals.vapor\_pressure.TRC\_Antoine\_extended chemicals.vapor\_pressure.Antoine chemicals.vapor\_pressure.boiling\_critical\_relation chemicals.vapor\_pressure.Lee\_Kesler chemicals.vapor\_pressure.Ambrose\_Walton chemicals.vapor\_pressure.Sanjari chemicals.vapor\_pressure.Edalat chemicals.iapws.iapws95\_Psat

# Notes

To iterate over all methods, use the list stored in *vapor\_pressure\_methods*.

- **WAGNER\_MCGARRY:** The Wagner 3,6 original model equation documented in chemicals. vapor\_pressure.Wagner\_original, with data for 245 chemicals, from [1],
- **WAGNER\_POLING:** The Wagner 2.5, 5 model equation documented in chemicals.vapor\_pressure. Wagner in [2], with data for 104 chemicals.
- **ANTOINE\_EXTENDED\_POLING:** The TRC extended Antoine model equation documented in chemicals. vapor\_pressure.TRC\_Antoine\_extended with data for 97 chemicals in [2].
- **ANTOINE\_POLING:** Standard Antoine equation, as documented in the function chemicals. vapor\_pressure.Antoine and with data for 325 fluids from [2]. Coefficients were altered to be in units of Pa and Kelvin.
- **ANTOINE\_WEBBOOK:** Standard Antoine equation, as documented in the function chemicals. vapor\_pressure.Antoine and with data for ~1400 fluids from [6]. Coefficients were altered to be in units of Pa and Kelvin.
- **DIPPR\_PERRY\_8E:** A collection of 341 coefficient sets from the DIPPR database published openly in [5]. Provides temperature limits for all its fluids. chemicals.dippr.EQ101 is used for its fluids.
- VDI\_PPDS: Coefficients for a equation form developed by the PPDS, published openly in [4].
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [3]. Very slow.
- **BOILING\_CRITICAL:** Fundamental relationship in thermodynamics making several approximations; see chemicals.vapor\_pressure.boiling\_critical\_relation for details. Least accurate method in most circumstances.
- LEE\_KESLER\_PSAT: CSP method documented in chemicals.vapor\_pressure.Lee\_Kesler. Widely used.

AMBROSE\_WALTON: CSP method documented in chemicals.vapor\_pressure.Ambrose\_Walton.

SANJARI: CSP method documented in chemicals.vapor\_pressure.Sanjari.

EDALAT: CSP method documented in chemicals.vapor\_pressure.Edalat.

VDI\_TABULAR: Tabular data in [4] along the saturation curve; interpolation is as set by the user or the default.

EOS: Equation of state provided by user; must implement thermo.eos.GCEOS.Psat

IAPWS: IAPWS-95 formulation documented in chemicals.iapws.iapws95\_Psat.

# References

[1], [2], [3], [4], [5], [6]

# Methods

calculate(T, method)	Method to calculate vapor pressure of a fluid at temperature $T$ with a given method.
interpolation_T(T)	Function to make the data-based interpolation as lin-
	ear as possible.
interpolation_property(P)	log(P) interpolation transformation by default.
<pre>interpolation_property_inv(P)</pre>	exp(P) interpolation transformation by default; re-
	verses interpolation_property_inv.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

# calculate(T, method)

Method to calculate vapor pressure of a fluid at temperature T with a given method.

This method has no exception handling; see thermo.utils.TDependentProperty. T\_dependent\_property for that.

# **Parameters**

T [float] Temperature at calculate vapor pressure, [K]

method [str] Name of the method to use

Returns

Psat [float] Vapor pressure at T, [Pa]

# static interpolation\_T(T)

Function to make the data-based interpolation as linear as possible. This transforms the input T into the 1/T domain.

# static interpolation\_property(P)

log(P) interpolation transformation by default.

#### static interpolation\_property\_inv(P)

exp(P) interpolation transformation by default; reverses *interpolation\_property\_inv*.

#### name = 'Vapor pressure'

# property\_max = 10000000000.0

Maximum valid value of vapor pressure. Set slightly above the critical point estimated for Iridium; Mercury's 160 MPa critical point is the highest known.

#### property\_min = 0

Mimimum valid value of vapor pressure.

```
ranked_methods = ['IAPWS', 'WAGNER_MCGARRY', 'WAGNER_POLING',
'ANTOINE_EXTENDED_POLING', 'DIPPR_PERRY_8E', 'VDI_PPDS', 'COOLPROP',
'ANTOINE_POLING', 'VDI_TABULAR', 'ANTOINE_WEBBOOK', 'AMBROSE_WALTON',
'LEE_KESLER_PSAT', 'EDALAT', 'BOILING_CRITICAL', 'EOS', 'SANJARI']
Default rankings of the available methods.
```

#### test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For CSP methods, the models are considered valid from 0 K to the critical point. For tabular data, extrapolation

outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

## Parameters

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

units = 'Pa'

thermo.vapor\_pressure.vapor\_pressure\_methods = ['IAPWS', 'WAGNER\_MCGARRY',
'WAGNER\_POLING', 'ANTOINE\_EXTENDED\_POLING', 'DIPPR\_PERRY\_8E', 'VDI\_PPDS', 'COOLPROP',
'ANTOINE\_POLING', 'VDI\_TABULAR', 'ANTOINE\_WEBBOOK', 'AMBROSE\_WALTON', 'LEE\_KESLER\_PSAT',
'EDALAT', 'EOS', 'BOILING\_CRITICAL', 'SANJARI']

Holds all methods available for the VaporPressure class, for use in iterating over them.

# 7.32.2 Sublimation Pressure

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with sublimation pressure as a function of temperature. Consists of one estimation method.

# Parameters

CASRN [str, optional] The CAS number of the chemical

Tt [float, optional] Triple temperature, [K]

Pt [float, optional] Triple pressure, [Pa]

Hsub\_t [float, optional] Sublimation enthalpy at the triple point, [J/mol]

- **load\_data** [bool, optional] If False, do not load property coefficients from data sources in files; this can be used to reduce the memory consumption of an object as well, [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

See also:

chemicals.vapor\_pressure.Psub\_Clapeyron

# Notes

To iterate over all methods, use the list stored in *sublimation\_pressure\_methods*.

PSUB\_CLAPEYRON: Clapeyron thermodynamic identity, Psub\_Clapeyron

# References

[1]

# Methods

calculate(T, method)	Method to calculate sublimation pressure of a fluid at temperature $T$ with a given method.
interpolation_T(T)	Function to make the data-based interpolation as lin-
	ear as possible.
<pre>interpolation_property(P)</pre>	log(P) interpolation transformation by default.
<pre>interpolation_property_inv(P)</pre>	exp(P) interpolation transformation by default; re-
	verses interpolation_property_inv.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

# calculate(T, method)

Method to calculate sublimation pressure of a fluid at temperature T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature at calculate sublimation pressure, [K]

method [str] Name of the method to use

## Returns

Psub [float] Sublimation pressure at T, [Pa]

# static interpolation\_T(T)

Function to make the data-based interpolation as linear as possible. This transforms the input T into the 1/T domain.

# static interpolation\_property(P)

log(P) interpolation transformation by default.

# static interpolation\_property\_inv(P)

exp(P) interpolation transformation by default; reverses interpolation\_property\_inv.

# name = 'Sublimation pressure'

#### $property_max = 100000.0$

Maximum valid value of sublimation pressure. Set to 1 bar tentatively.

# property\_min = 1e-300

Mimimum valid value of sublimation pressure.

# ranked\_methods = ['PSUB\_CLAPEYRON']

Default rankings of the available methods.

#### test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For CSP methods, the models are considered valid from 0 K to the critical point. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### Parameters

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

units = 'Pa'

```
thermo.vapor_pressure.sublimation_pressure_methods = ['PSUB_CLAPEYRON']
Holds all methods available for the SublimationPressure class, for use in iterating over them.
```

# 7.33 Viscosity (thermo.viscosity)

This module contains implementations of *TPDependentProperty* representing liquid and vapor viscosity. A variety of estimation and data methods are available as included in the *chemicals* library. Additionally liquid and vapor mixture viscosity predictor objects are implemented subclassing *MixtureProperty*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Pure Liquid Viscosity
- Pure Gas Viscosity
- Mixture Liquid Viscosity
- Mixture Gas Viscosity

# 7.33.1 Pure Liquid Viscosity

Class for dealing with liquid viscosity as a function of temperature and pressure.

For low-pressure (at 1 atm while under the vapor pressure; along the saturation line otherwise) liquids, there are six coefficient-based methods from three data sources, one source of tabular information, two corresponding-states estimators, one group contribution method, and the external library CoolProp.

For high-pressure liquids (also, <1 atm liquids), there is one corresponding-states estimator, and the external library CoolProp.

#### Parameters

CASRN [str, optional] The CAS number of the chemical

MW [float, optional] Molecular weight, [g/mol]

Tm [float, optional] Melting point, [K]

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

Vc [float, optional] Critical volume, [m^3/mol]

omega [float, optional] Acentric factor, [-]

- **Psat** [float or callable, optional] Vapor pressure at a given temperature or callable for the same, [Pa]
- **Vml** [float or callable, optional] Liquid molar volume at a given temperature and pressure or callable for the same, [m^3/mol]
- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

#### See also:

chemicals.viscosity.Viswanath\_Natarajan\_3

chemicals.viscosity.Viswanath\_Natarajan\_2

chemicals.viscosity.Viswanath\_Natarajan\_2\_exponential

chemicals.viscosity.Letsou\_Stiel

chemicals.viscosity.Przedziecki\_Sridhar

chemicals.viscosity.Lucas

thermo.joback.Joback

# Notes

To iterate over all methods, use the lists stored in *viscosity\_liquid\_methods* and *viscosity\_liquid\_methods\_P* for low and high pressure methods respectively.

Low pressure methods:

- **DUTT\_PRASAD:** A simple function as expressed in [1], with data available for 100 fluids. Temperature limits are available for all fluids. See chemicals.viscosity.Viswanath\_Natarajan\_3 for details.
- VISWANATH\_NATARAJAN\_3: A simple function as expressed in [1], with data available for 432 fluids. Temperature limits are available for all fluids. See chemicals.viscosity.Viswanath\_Natarajan\_3 for details.
- VISWANATH\_NATARAJAN\_2: A simple function as expressed in [1], with data available for 135 fluids. Temperature limits are available for all fluids. See chemicals.viscosity.Viswanath\_Natarajan\_2 for details.

- VISWANATH\_NATARAJAN\_2E: A simple function as expressed in [1], with data available for 14 fluids. Temperature limits are available for all fluids. See chemicals.viscosity. Viswanath\_Natarajan\_2\_exponential for details.
- **DIPPR\_PERRY\_8E:** A collection of 337 coefficient sets from the DIPPR database published openly in [4]. Provides temperature limits for all its fluids. EQ101 is used for its fluids.
- LETSOU\_STIEL: CSP method, described in chemicals.viscosity.Letsou\_Stiel.

PRZEDZIECKI\_SRIDHAR: CSP method, described in chemicals.viscosity.Przedziecki\_Sridhar.

- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [2]. Very slow.
- VDI\_TABULAR: Tabular data in [3] along the saturation curve; interpolation is as set by the user or the default.
- **VDI\_PPDS:** Coefficients for a equation form developed by the PPDS, published openly in [3]. Provides no temperature limits, but has been designed for extrapolation. Extrapolated to low temperatures it provides a smooth exponential increase. However, for some chemicals such as glycerol, extrapolated to higher temperatures viscosity is predicted to increase above a certain point.
- **JOBACK:** An estimation method for organic substances in [5]; this also requires molecular weight as an input.

High pressure methods:

- LUCAS: CSP method, described in chemicals.viscosity.Lucas. Calculates a low-pressure liquid viscosity as its input.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [2]. Very slow, but unparalled in accuracy for pressure dependence.

A minimum viscosity value of 1e-5 Pa\*s is set according to [4]. This is also just above the lowest experimental values of viscosity of helium, 9.4e-6 Pa\*s. This excludes the behavior of superfluids, and also systems where the mean free path between moleules approaches the geometry of the system and then the viscosity is geometry-dependent.

#### References

#### [1], [2], [3], [4], [5], [6]

## Attributes

Tmax Maximum temperature (K) at which the current method can calculate the property.

*Tmin* Minimum temperature (K) at which the current method can calculate the property.

# Methods

calculate(T, method)	Method to calculate low-pressure liquid viscosity at tempearture $T$ with a given method.
calculate_P(T, P, method)	Method to calculate pressure-dependent liquid viscosity at temperature $T$ and pressure $P$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.
<pre>test_method_validity_P(T, P, method)</pre>	Method to check the validity of a high-pressure method.

#### property Tmax

Maximum temperature (K) at which the current method can calculate the property.

#### property Tmin

Minimum temperature (K) at which the current method can calculate the property.

#### calculate(T, method)

Method to calculate low-pressure liquid viscosity at tempearture T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### Parameters

T [float] Temperature at which to calculate viscosity, [K]

method [str] Name of the method to use

#### Returns

mu [float] Viscosity of the liquid at T and a low pressure, [Pa\*s]

#### calculate\_P(T, P, method)

Method to calculate pressure-dependent liquid viscosity at temperature T and pressure P with a given method.

This method has no exception handling; see TP\_dependent\_property for that.

#### **Parameters**

T [float] Temperature at which to calculate viscosity, [K]

**P** [float] Pressure at which to calculate viscosity, [K]

**method** [str] Name of the method to use

#### Returns

**mu** [float] Viscosity of the liquid at T and P, [Pa\*s]

```
name = 'liquid viscosity'
```

#### property\_max = 200000000.0

Maximum valid value of liquid viscosity. Generous limit, as the value is that of bitumen in a Pitch drop experiment.

#### property\_min = 0.0

Mimimum valid value of liquid viscosity.

```
ranked_methods = ['COOLPROP', 'DIPPR_PERRY_8E', 'VDI_PPDS', 'DUTT_PRASAD',
'VISWANATH_NATARAJAN_3', 'VISWANATH_NATARAJAN_2', 'VISWANATH_NATARAJAN_2E',
'VDI_TABULAR', 'LETSOU_STIEL', 'JOBACK', 'PRZEDZIECKI_SRIDHAR']
Defoult rankings of the low pressure methods
```

Default rankings of the low-pressure methods.

```
ranked_methods_P = ['COOLPROP', 'LUCAS']
```

Default rankings of the high-pressure methods.

#### test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For CSP methods, the models are considered valid from 0 K to the critical point. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### Parameters

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

## Returns

validity [bool] Whether or not a method is valid

# test\_method\_validity\_P(T, P, method)

Method to check the validity of a high-pressure method. For **COOLPROP**, the fluid must be both a liquid and under the maximum pressure of the fluid's EOS. **LUCAS** doesn't work on some occasions, due to something related to Tr and negative powers - but is otherwise considered correct for all circumstances.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures and pressures.

# **Parameters**

T [float] Temperature at which to test the method, [K]

**P** [float] Pressure at which to test the method, [Pa]

method [str] Name of the method to test

# Returns

validity [bool] Whether or not a method is valid

units = 'Pa\*s'

thermo.viscosity.viscosity\_liquid\_methods = ['COOLPROP', 'DIPPR\_PERRY\_8E', 'VDI\_PPDS',
'DUTT\_PRASAD', 'VISWANATH\_NATARAJAN\_3', 'VISWANATH\_NATARAJAN\_2',

'VISWANATH\_NATARAJAN\_2E', 'VDI\_TABULAR', 'LETSOU\_STIEL', 'JOBACK', 'PRZEDZIECKI\_SRIDHAR'] Holds all low-pressure methods available for the ViscosityLiquid class, for use in iterating over them.

thermo.viscosity.viscosity\_liquid\_methods\_P = ['COOLPROP', 'LUCAS'] Holds all high-pressure methods available for the ViscosityLiquid class, for use in iterating over them.

# 7.33.2 Pure Gas Viscosity

Bases: thermo.utils.tp\_dependent\_property.TPDependentProperty

Class for dealing with gas viscosity as a function of temperature and pressure.

For gases at atmospheric pressure, there are 4 corresponding-states estimators, two sources of coefficient-based models, one source of tabular information, and the external library CoolProp.

For gases under the fluid's boiling point (at sub-atmospheric pressures), and high-pressure gases above the boiling point, there are zero corresponding-states estimators, and the external library CoolProp.

# Parameters

CASRN [str, optional] The CAS number of the chemical

MW [float, optional] Molecular weight, [g/mol]

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

Zc [float, optional] Critical compressibility, [-]

dipole [float, optional] Dipole moment of the fluid, [debye]

Vmg [float, optional] Molar volume of the fluid at a pressure and temperature, [m^3/mol]

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

# See also:

chemicals.viscosity.Gharagheizi\_gas\_viscosity

chemicals.viscosity.Yoon\_Thodos

chemicals.viscosity.Stiel\_Thodos

chemicals.viscosity.Lucas\_gas

## Notes

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the lists stored in *viscosity\_gas\_methods* and *viscosity\_gas\_methods\_P* for low and high pressure methods respectively.

Low pressure methods:

GHARAGHEIZI: CSP method, described in chemicals.viscosity.Gharagheizi\_gas\_viscosity.

YOON\_THODOS: CSP method, described in chemicals.viscosity.Yoon\_Thodos.

**STIEL\_THODOS:** CSP method, described in chemicals.viscosity.Stiel\_Thodos.

LUCAS\_GAS: CSP method, described in chemicals.viscosity.Lucas\_gas.

- **DIPPR\_PERRY\_8E:** A collection of 345 coefficient sets from the DIPPR database published openly in [3]. Provides temperature limits for all its fluids. chemicals.dippr.EQ102 is used for its fluids.
- **VDI\_PPDS:** Coefficients for a equation form developed by the PPDS, published openly in [2]. Provides no temperature limits, but provides reasonable values at fairly high and very low temperatures.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [1]. Very slow.

VDI\_TABULAR: Tabular data in [2] along the saturation curve; interpolation is as set by the user or the default.

High pressure methods:

**COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [1]. Very slow, but unparalled in accuracy for pressure dependence.

A minimum viscosity value of 1e-5 Pa\*s is set according to [4]. This is also just above the lowest experimental values of viscosity of helium, 9.4e-6 Pa\*s.

# References

# [1], [2], [3], [4]

# Attributes

Tmax Maximum temperature (K) at which the current method can calculate the property.

Tmin Minimum temperature (K) at which the current method can calculate the property.

# Methods

calculate(T, method)	Method to calculate low-pressure gas viscosity at tempearture $T$ with a given method.
calculate_P(T, P, method)	Method to calculate pressure-dependent gas viscosity
	at temperature $T$ and pressure $P$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a temperature-
	dependent low-pressure method.
<pre>test_method_validity_P(T, P, method)</pre>	Method to check the validity of a high-pressure
	method.

## property Tmax

Maximum temperature (K) at which the current method can calculate the property.

#### property Tmin

Minimum temperature (K) at which the current method can calculate the property.

#### calculate(T, method)

Method to calculate low-pressure gas viscosity at tempearture T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature of the gas, [K]

method [str] Name of the method to use

#### Returns

mu [float] Viscosity of the gas at T and a low pressure, [Pa\*s]

#### calculate\_P(T, P, method)

Method to calculate pressure-dependent gas viscosity at temperature T and pressure P with a given method.

This method has no exception handling; see *TP\_dependent\_property* for that.

## Parameters

T [float] Temperature at which to calculate gas viscosity, [K]

P [float] Pressure at which to calculate gas viscosity, [K]

method [str] Name of the method to use

#### Returns

mu [float] Viscosity of the gas at T and P, [Pa\*]

```
name = 'Gas viscosity'
```

#### property\_max = 0.001

Maximum valid value of gas viscosity. Might be too high, or too low.

# property\_min = 0.0

Mimimum valid value of gas viscosity; limiting condition at low pressure is 0.

```
ranked_methods = ['COOLPROP', 'DIPPR_PERRY_8E', 'VDI_PPDS', 'VDI_TABULAR',
'GHARAGHEIZI', 'YOON_THODOS', 'STIEL_THODOS', 'LUCAS_GAS']
Default rankings of the low-pressure methods.
```

#### ranked\_methods\_P = ['COOLPROP']

Default rankings of the high-pressure methods.

#### test\_method\_validity(T, method)

Method to check the validity of a temperature-dependent low-pressure method. For CSP most methods, the all methods are considered valid from 0 K up to 5000 K. For method **GHARAGHEIZI**, the method is considered valud from 20 K to 2000 K.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### **Parameters**

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

#### Returns

validity [bool] Whether or not a method is valid

#### test\_method\_validity\_P(T, P, method)

Method to check the validity of a high-pressure method. For **COOLPROP**, the fluid must be both a gas and under the maximum pressure of the fluid's EOS. No other methods are implemented.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures and pressures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### Parameters

T [float] Temperature at which to test the method, [K]

**P** [float] Pressure at which to test the method, [Pa]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

```
units = 'Pa*s'
```

```
thermo.viscosity.viscosity_gas_methods = ['COOLPROP', 'DIPPR_PERRY_8E', 'VDI_PPDS',
'VDI_TABULAR', 'GHARAGHEIZI', 'YOON_THODOS', 'STIEL_THODOS', 'LUCAS_GAS']
```

Holds all low-pressure methods available for the ViscosityGas class, for use in iterating over them.

thermo.viscosity.viscosity\_gas\_methods\_P = ['COOLPROP']

Holds all high-pressure methods available for the ViscosityGas class, for use in iterating over them.

# 7.33.3 Mixture Liquid Viscosity

class thermo.viscosity.ViscosityLiquidMixture(CASs=[], ViscosityLiquids=[], MWs=[], \*\*kwargs)
Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with the viscosity of a liquid mixture as a function of temperature, pressure, and composition. Consists of one electrolyte-specific method, and logarithmic rules based on either mole fractions of mass fractions.

Prefered method is mixing\_logarithmic with mole fractions, or **Laliberte** if the mixture is aqueous and has electrolytes.

#### Parameters

- CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]
- **ViscosityLiquids** [list[ViscosityLiquid], optional] ViscosityLiquid objects created for all species in the mixture, [-]
- MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]
- **correct\_pressure\_pure** [bool, optional] Whether to try to use the better pressure-corrected pure component models or to use only the T-only dependent pure species models, [-]

# See also:

thermo.electrochem.Laliberte\_viscosity

#### **Notes**

To iterate over all methods, use the list stored in viscosity\_liquid\_mixture\_methods.

- LALIBERTE\_MU: Electrolyte model equation with coefficients; see thermo.electrochem. Laliberte\_viscosity for more details.
- MIXING\_LOG\_MOLAR: Logarithmic mole fraction mixing rule described in chemicals.utils. mixing\_logarithmic.
- MIXING\_LOG\_MASS: Logarithmic mole fraction mixing rule described in chemicals.utils. mixing\_logarithmic.

LINEAR: Linear mole fraction mixing rule described in mixing\_simple.

#### References

[1]

# **Methods**

calculate(T, P, zs, ws, method)	Method to calculate viscosity of a liquid mixture
	at temperature $T$ , pressure $P$ , mole fractions $zs$ and
	weight fractions ws with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for
	the given conditions.

Tmax

Maximum temperature at which no method can calculate the property above.

#### Tmin

Minimum temperature at which no method can calculate the property under.

# calculate(T, P, zs, ws, method)

Method to calculate viscosity of a liquid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

#### Parameters

- T [float] Temperature at which to calculate the property, [K]
- P [float] Pressure at which to calculate the property, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

#### Returns

mu [float] Viscosity of the liquid mixture, [Pa\*s]

name = 'liquid viscosity'

#### $property_max = 20000000.0$

Maximum valid value of liquid viscosity. Generous limit, as the value is that of bitumen in a Pitch drop experiment.

#### property\_min = 0

Mimimum valid value of liquid viscosity.

# ranked\_methods = ['Laliberte', 'Logarithmic mixing, molar', 'Logarithmic mixing, mass', 'LINEAR']

#### test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. If **Laliberte** is applicable, all other methods are returned as inapplicable. Otherwise, there are no checks or strict ranges of validity.

#### **Parameters**

- T [float] Temperature at which to check method validity, [K]
- P [float] Pressure at which to check method validity, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]
- method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

#### units = 'Pa\*s'

thermo.viscosity.viscosity\_liquid\_mixture\_methods = ['Laliberte', 'Logarithmic mixing, molar', 'Logarithmic mixing, mass', 'LINEAR']

Holds all mixing rules available for the ViscosityLiquidMixture class, for use in iterating over them.

# 7.33.4 Mixture Gas Viscosity

class thermo.viscosity.ViscosityGasMixture(MWs=[], molecular\_diameters=[], Stockmayers=[],

CASs=[], ViscosityGases=[], \*\*kwargs)

 $Bases: \ thermo.utils.mixture\_property.MixtureProperty$ 

Class for dealing with the viscosity of a gas mixture as a function of temperature, pressure, and composition. Consists of three gas viscosity specific mixing rules and a mole-weighted simple mixing rule.

Prefered method is Brokaw.

# Parameters

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

molecular\_diameters [list[float], optional] Lennard-Jones molecular diameters, [angstrom]

- **Stockmayers** [list[float], optional] Lennard-Jones depth of potential-energy minimum over k or epsilon\_k, [K]
- CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]
- **ViscosityGases** [list[ViscosityGas], optional] ViscosityGas objects created for all species in the mixture, [-]
- **correct\_pressure\_pure** [bool, optional] Whether to try to use the better pressure-corrected pure component models or to use only the T-only dependent pure species models, [-]

# See also:

chemicals.viscosity.Brokaw

chemicals.viscosity.Herning\_Zipperer

chemicals.viscosity.Wilke

# Notes

To iterate over all methods, use the list stored in *viscosity\_liquid\_mixture\_methods*.

BROKAW: Mixing rule described in Brokaw.

HERNING\_ZIPPERER: Mixing rule described in Herning\_Zipperer.

WILKE: Mixing rule described in Wilke.

LINEAR: Mixing rule described in mixing\_simple.

# References

[1]

# **Methods**

calculate(T, P, zs, ws, method)	Method to calculate viscosity of a gas mixture at temperature $T$ , pressure $P$ , mole fractions $zs$ and weight
	fractions ws with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for
	the given conditions.

# Tmax

Maximum temperature at which no method can calculate the property above.

#### Tmin

Minimum temperature at which no method can calculate the property under.

#### calculate(T, P, zs, ws, method)

Method to calculate viscosity of a gas mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

#### **Parameters**

- T [float] Temperature at which to calculate the property, [K]
- P [float] Pressure at which to calculate the property, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

#### Returns

mu [float] Viscosity of gas mixture, [Pa\*s]

#### name = 'gas viscosity'

#### property\_max = 0.001

Maximum valid value of gas viscosity. Might be too high, or too low.

#### property\_min = 0

Mimimum valid value of gas viscosity; limiting condition at low pressure is 0.

ranked\_methods = ['BROKAW', 'HERNING\_ZIPPERER', 'LINEAR', 'WILKE']

#### test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

#### Parameters

- T [float] Temperature at which to check method validity, [K]
- P [float] Pressure at which to check method validity, [Pa]

**zs** [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

```
units = 'Pa*s'
```

```
thermo.viscosity.viscosity_gas_mixture_methods = ['BROKAW', 'HERNING_ZIPPERER', 'WILKE',
'LINEAR']
```

Holds all mixing rules available for the ViscosityGasMixture class, for use in iterating over them.

# 7.34 Density/Volume (thermo.volume)

This module contains implementations of *TDependentProperty* representing liquid, vapor, and solid volume. A variety of estimation and data methods are available as included in the *chemicals* library. Additionally liquid, vapor, and solid mixture volume predictor objects are implemented subclassing *MixtureProperty*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Pure Liquid Volume
- Pure Gas Volume
- Pure Solid Volume
- Mixture Liquid Volume
- Mixture Gas Volume
- Mixture Solid Volume

# 7.34.1 Pure Liquid Volume

Class for dealing with liquid molar volume as a function of temperature and pressure.

For low-pressure (at 1 atm while under the vapor pressure; along the saturation line otherwise) liquids, there are six coefficient-based methods from five data sources, one source of tabular information, one source of constant values, eight corresponding-states estimators, the external library CoolProp and the equation of state.

For high-pressure liquids (also, <1 atm liquids), there is one corresponding-states estimator, and the external library CoolProp.

# Parameters

CASRN [str, optional] The CAS number of the chemical

MW [float, optional] Molecular weight, [g/mol]

**Tb** [float, optional] Boiling point, [K]

Tc [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

Vc [float, optional] Critical volume, [m^3/mol]

Zc [float, optional] Critical compressibility

omega [float, optional] Acentric factor, [-]

dipole [float, optional] Dipole, [debye]

- **Psat** [float or callable, optional] Vapor pressure at a given temperature, or callable for the same [Pa]
- eos [object, optional] Equation of State object after thermo.eos.GCEOS
- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

# See also:

chemicals.volume.Yen\_Woods\_saturation

chemicals.volume.Rackett

chemicals.volume.Yamada\_Gunn

chemicals.volume.Townsend\_Hales

chemicals.volume.Bhirud\_normal

chemicals.volume.COSTALD

chemicals.volume.Campbell\_Thodos

chemicals.volume.SNM0

chemicals.volume.CRC\_inorganic

chemicals.volume.COSTALD\_compressed

#### **Notes**

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the lists stored in *volume\_liquid\_methods* and *volume\_liquid\_methods\_P* for low and high pressure methods respectively.

Low pressure methods:

- **DIPPR\_PERRY\_8E:** A simple polynomial as expressed in [1], with data available for 344 fluids. Temperature limits are available for all fluids. Believed very accurate.
- **VDI\_PPDS:** Coefficients for a equation form developed by the PPDS (EQ116 in terms of mass density), published openly in [3]. Valid up to the critical temperature, and extrapolates to very low temperatures well.
- **MMSNM0FIT:** Uses a fit coefficient for better accuracy in the SNM0 method, Coefficients available for 73 fluids from [2]. Valid to the critical point.
- **HTCOSTALDFIT:** A method with two fit coefficients to the COSTALD method. Coefficients available for 192 fluids, from [3]. Valid to the critical point.
- **RACKETTFIT:** The Rackett method, with a fit coefficient Z\_RA. Data is available for 186 fluids, from [3]. Valid to the critical point.
- **CRC\_INORG\_L:** Single-temperature coefficient linear model in terms of mass density for the density of inorganic liquids; converted to molar units internally. Data is available for 177 fluids normally valid over a narrow range above the melting point, from [4]; described in CRC\_inorganic.

MMSNM0: CSP method, described in SNM0.

HTCOSTALD: CSP method, described in COSTALD.

YEN\_WOODS\_SAT: CSP method, described in Yen\_Woods\_saturation.

RACKETT: CSP method, described in Rackett.

YAMADA\_GUNN: CSP method, described in Yamada\_Gunn.

BHIRUD\_NORMAL: CSP method, described in Bhirud\_normal.

TOWNSEND\_HALES: CSP method, described in Townsend\_Hales.

CAMPBELL\_THODOS: CSP method, described in Campbell\_Thodos.

**COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [5]. Very slow.

CRC\_INORG\_L\_CONST: Constant inorganic liquid densities, in [4].

VDI\_TABULAR: Tabular data in [6] along the saturation curve; interpolation is as set by the user or the default.

**EOS:** Equation of state provided by user.

High pressure methods:

- **COSTALD\_COMPRESSED:** CSP method, described in COSTALD\_compressed. Calculates a low-pressure molar volume first, using *T\_dependent\_property*.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [5]. Very slow, but unparalled in accuracy for pressure dependence.

EOS: Equation of state provided by user.

#### References

# [1], [2], [3], [4], [5], [6]

#### Attributes

Tmax Maximum temperature (K) at which the current method can calculate the property.

Tmin Minimum temperature (K) at which the current method can calculate the property.

# Methods

calculate(T, method)	Method to calculate low-pressure liquid molar volume at tempearture $T$ with a given method.
<pre>calculate_P(T, P, method)</pre>	Method to calculate pressure-dependent liquid molar volume at temperature $T$ and pressure $P$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.
<pre>test_method_validity_P(T, P, method)</pre>	Method to check the validity of a high-pressure method.

# property Tmax

Maximum temperature (K) at which the current method can calculate the property.

#### property Tmin

Minimum temperature (K) at which the current method can calculate the property.

#### calculate(T, method)

Method to calculate low-pressure liquid molar volume at tempearture T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

**T** [float] Temperature at which to calculate molar volume, [K]

method [str] Name of the method to use

# Returns

Vm [float] Molar volume of the liquid at T and a low pressure, [m^3/mol]

#### calculate\_P(T, P, method)

Method to calculate pressure-dependent liquid molar volume at temperature T and pressure P with a given method.

This method has no exception handling; see TP\_dependent\_property for that.

#### Parameters

T [float] Temperature at which to calculate molar volume, [K]

**P** [float] Pressure at which to calculate molar volume, [K]

method [str] Name of the method to use

#### Returns

Vm [float] Molar volume of the liquid at T and P, [m^3/mol]

#### name = 'Liquid molar volume'

```
property_max = 0.002
```

Maximum valid value of liquid molar volume. Generous limit.

#### property\_min = 0

Mimimum valid value of liquid molar volume. It should normally occur at the triple point, and be well above this.

```
ranked_methods = ['DIPPR_PERRY_8E', 'VDI_PPDS', 'COOLPROP', 'MMSNM0FIT',
'VDI_TABULAR', 'HTCOSTALDFIT', 'RACKETTFIT', 'CRC_INORG_L', 'CRC_INORG_L_CONST',
'COMMON_CHEMISTRY', 'MMSNM0', 'HTCOSTALD', 'YEN_WOODS_SAT', 'RACKETT',
'YAMADA_GUNN', 'BHIRUD_NORMAL', 'TOWNSEND_HALES', 'CAMPBELL_THODOS', 'EOS']
```

Default rankings of the low-pressure methods.

```
ranked_methods_P = ['COOLPROP', 'COSTALD_COMPRESSED', 'EOS']
```

Default rankings of the high-pressure methods.

## test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For CSP methods, the models are considered valid from 0 K to the critical point. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

**BHIRUD\_NORMAL** behaves poorly at low temperatures and is not used under 0.35Tc. The constant value available for inorganic chemicals, from method **CRC\_INORG\_L\_CONST**, is considered valid for all temperatures.

Parameters

T [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

# Returns

validity [bool] Whether or not a method is valid

# test\_method\_validity\_P(T, P, method)

Method to check the validity of a high-pressure method. For **COOLPROP**, the fluid must be both a liquid and under the maximum pressure of the fluid's EOS. **COSTALD\_COMPRESSED** is considered valid for all values of temperature and pressure. However, it very often will not actually work, due to the form of the polynomial in terms of Tr, the result of which is raised to a negative power. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures and pressures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### **Parameters**

T [float] Temperature at which to test the method, [K]

**P** [float] Pressure at which to test the method, [Pa]

method [str] Name of the method to test

# Returns

validity [bool] Whether or not a method is valid

```
units = 'm^3/mol'
```

thermo.volume.volume\_liquid\_methods = ['DIPPR\_PERRY\_8E', 'VDI\_PPDS', 'COOLPROP',
'MMSNM0FIT', 'VDI\_TABULAR', 'HTCOSTALDFIT', 'RACKETTFIT', 'CRC\_INORG\_L',
'CRC\_INORG\_L\_CONST', 'COMMON\_CHEMISTRY', 'MMSNM0', 'HTCOSTALD', 'YEN\_WOODS\_SAT',
'RACKETT', 'YAMADA\_GUNN', 'BHIRUD\_NORMAL', 'TOWNSEND\_HALES', 'CAMPBELL\_THODOS', 'EOS']
Holds all low-pressure methods available for the VolumeLiquid class, for use in iterating over them.

thermo.volume.volume\_liquid\_methods\_P = ['COOLPROP', 'COSTALD\_COMPRESSED', 'EOS'] Holds all high-pressure methods available for the *VolumeLiquid* class, for use in iterating over them.

# 7.34.2 Pure Gas Volume

**class** thermo.volume.**VolumeGas**(*CASRN=''*, *MW=None*, *Tc=None*, *Pc=None*, *omega=None*, *dipole=None*, *eos=None*, *extrapolation=None*, \*\*kwargs)

Bases: thermo.utils.tp\_dependent\_property.TPDependentProperty

Class for dealing with gas molar volume as a function of temperature and pressure.

All considered methods are both temperature and pressure dependent. Included are four CSP methods for calculating second virial coefficients, one source of polynomials for calculating second virial coefficients, one equation of state (Peng-Robinson), and the ideal gas law.

# Parameters

CASRN [str, optional] The CAS number of the chemical

MW [float, optional] Molecular weight, [g/mol]

**Tc** [float, optional] Critical temperature, [K]

Pc [float, optional] Critical pressure, [Pa]

omega [float, optional] Acentric factor, [-]

dipole [float, optional] Dipole, [debye]

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

# See also:

chemicals.virial.BVirial\_Pitzer\_Curl
chemicals.virial.BVirial\_Abbott
chemicals.virial.BVirial\_Tsonopoulos
chemicals.virial.BVirial\_Tsonopoulos\_extended

## Notes

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the list stored in *volume\_gas\_methods*.

PR: Peng-Robinson Equation of State. See the appropriate module for more information.

CRC\_VIRIAL: Short polynomials, for 105 fluids from [1]. The full expression is:

$$B = \sum_{1}^{4} a_i \left[ T_0 / 298.15 - 1 \right]^{i-1}$$

- **TSONOPOULOS\_EXTENDED:** CSP method for second virial coefficients, described in chemicals. virial.BVirial\_Tsonopoulos\_extended
- **TSONOPOULOS:** CSP method for second virial coefficients, described in chemicals.virial. BVirial\_Tsonopoulos
- **ABBOTT:** CSP method for second virial coefficients, described in chemicals.virial.BVirial\_Abbott. This method is the simplest CSP method implemented.
- **PITZER\_CURL:** CSP method for second virial coefficients, described in chemicals.virial. BVirial\_Pitzer\_Curl.
- **COOLPROP:** CoolProp external library; with select fluids from its library. Range is limited to that of the equations of state it uses, as described in [2]. Very slow, but unparalled in accuracy for pressure dependence.

# References

# [1], [2]

# Attributes

Tmax Maximum temperature (K) at which the current method can calculate the property.

Tmin Minimum temperature (K) at which the current method can calculate the property.

# **Methods**

calculate(T, method)	Method to calculate a property with a specified
	method, with no validity checking or error handling.
calculate_P(T, P, method)	Method to calculate pressure-dependent gas molar
	volume at temperature $T$ and pressure $P$ with a given
	method.
<pre>test_method_validity(T, method)</pre>	Method to test the validity of a specified method for
	a given temperature.
<pre>test_method_validity_P(T, P, method)</pre>	Method to check the validity of a pressure and tem-
	perature dependent gas molar volume method.

#### property Tmax

Maximum temperature (K) at which the current method can calculate the property.

#### property Tmin

Minimum temperature (K) at which the current method can calculate the property.

# calculate(T, method)

Method to calculate a property with a specified method, with no validity checking or error handling. Demo function for testing only; must be implemented according to the methods available for each individual method. Include the interpolation call here.

#### Parameters

T [float] Temperature at which to calculate the property, [K]

method [str] Method name to use

#### Returns

prop [float] Calculated property, [units]

# calculate\_P(T, P, method)

Method to calculate pressure-dependent gas molar volume at temperature T and pressure P with a given method.

This method has no exception handling; see *TP\_dependent\_property* for that.

#### **Parameters**

T [float] Temperature at which to calculate molar volume, [K]

**P** [float] Pressure at which to calculate molar volume, [K]

**method** [str] Name of the method to use

## Returns

Vm [float] Molar volume of the gas at T and P, [m^3/mol]

name = 'Gas molar volume'

# property\_max = 1000000000.0

Maximum valid value of gas molar volume. Set roughly at an ideal gas at 1 Pa and 2 billion K.

## property\_min = 0

Mimimum valid value of gas molar volume. It should normally be well above this.

#### ranked\_methods = []

Default rankings of the low-pressure methods.

```
ranked_methods_P = ['COOLPROP', 'EOS', 'TSONOPOULOS_EXTENDED', 'TSONOPOULOS',
'ABBOTT', 'PITZER_CURL', 'CRC_VIRIAL', 'IDEAL']
```

Default rankings of the pressure-dependent methods.

#### test\_method\_validity(T, method)

Method to test the validity of a specified method for a given temperature. Demo function for testing only; must be implemented according to the methods available for each individual method. Include the interpolation check here.

#### Parameters

T [float] Temperature at which to determine the validity of the method, [K]

method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

#### test\_method\_validity\_P(T, P, method)

Method to check the validity of a pressure and temperature dependent gas molar volume method. For the four CSP methods that calculate second virial coefficient, the method is considered valid for all temperatures and pressures, with validity checking based on the result only. For **CRC\_VIRIAL**, there is no limit but there should be one; at some conditions, a negative volume will result! For **COOLPROP**, the fluid must be both a gas at the given conditions and under the maximum pressure of the fluid's EOS.

For the equation of state **PR**, the determined phase must be a gas. For **IDEAL**, there are no limits.

For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures and pressures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

## Parameters

T [float] Temperature at which to test the method, [K]

**P** [float] Pressure at which to test the method, [Pa]

method [str] Name of the method to test

#### Returns

validity [bool] Whether or not a method is valid

```
units = 'm^3/mol'
```

```
thermo.volume.volume_gas_methods = ['COOLPROP', 'EOS', 'CRC_VIRIAL',
```

'TSONOPOULOS\_EXTENDED', 'TSONOPOULOS', 'ABBOTT', 'PITZER\_CURL', 'IDEAL']

Holds all methods available for the *VolumeGas* class, for use in iterating over them.

# 7.34.3 Pure Solid Volume

class thermo.volume.VolumeSolid(CASRN=", MW=None, Tt=None, Vml\_Tt=None, extrapolation='linear',

\*\*kwargs)

Bases: thermo.utils.t\_dependent\_property.TDependentProperty

Class for dealing with solid molar volume as a function of temperature. Consists of one constant value source, and one simple estimator based on liquid molar volume.

### **Parameters**

CASRN [str, optional] CAS number

MW [float, optional] Molecular weight, [g/mol]

Tt [float, optional] Triple temperature

Vml\_Tt [float, optional] Liquid molar volume at the triple point

- load\_data [bool, optional] If False, do not load property coefficients from data sources in files
  [-]
- **extrapolation** [str or None] None to not extrapolate; see *TDependentProperty* for a full list of all options, [-]
- **method** [str or None, optional] If specified, use this method by default and do not use the ranked sorting; an exception is raised if this is not a valid method for the provided inputs, [-]

## See also:

chemicals.volume.Goodman

### **Notes**

A string holding each method's name is assigned to the following variables in this module, intended as the most convenient way to refer to a method. To iterate over all methods, use the list stored in *volume\_solid\_methods*.

**CRC\_INORG\_S:** Constant values in [1], for 1872 chemicals.

**GOODMAN:** Simple method using the liquid molar volume. Good up to 0.3\*Tt. See Goodman for details.

## References

[1]

#### **Methods**

calculate(T, method)	Method to calculate the molar volume of a solid at
	tempearture $T$ with a given method.
<pre>test_method_validity(T, method)</pre>	Method to check the validity of a method.

## calculate(T, method)

Method to calculate the molar volume of a solid at tempearture T with a given method.

This method has no exception handling; see *T\_dependent\_property* for that.

#### **Parameters**

**T** [float] Temperature at which to calculate molar volume, [K]

method [str] Name of the method to use

## Returns

Vms [float] Molar volume of the solid at T, [m^3/mol]

```
name = 'Solid molar volume'
```

#### property\_max = 0.002

Maximum value of Heat capacity; arbitrarily set to 0.002, as the largest in the data is 0.00136.

## property\_min = 0.0

Molar volume cannot be under 0.

#### ranked\_methods = ['CRC\_INORG\_S', 'GOODMAN']

Default rankings of the available methods.

#### test\_method\_validity(T, method)

Method to check the validity of a method. Follows the given ranges for all coefficient-based methods. For tabular data, extrapolation outside of the range is used if tabular\_extrapolation\_permitted is set; if it is, the extrapolation is considered valid for all temperatures.

It is not guaranteed that a method will work or give an accurate prediction simply because this method considers the method valid.

#### Parameters

**T** [float] Temperature at which to test the method, [K]

method [str] Name of the method to test

Returns

validity [bool] Whether or not a method is valid

```
units = 'm^3/mol'
```

```
thermo.volume.volume_solid_methods = ['GOODMAN', 'CRC_INORG_S']
```

Holds all methods available for the VolumeSolid class, for use in iterating over them.

# 7.34.4 Mixture Liquid Volume

```
class thermo.volume.VolumeLiquidMixture(MWs=[], Tcs=[], Pcs=[], Vcs=[], Zcs=[], omegas=[],
```

CASs=[], VolumeLiquids=[], \*\*kwargs)

Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with the molar volume of a liquid mixture as a function of temperature, pressure, and composition. Consists of one electrolyte-specific method, four corresponding states methods which do not use purecomponent volumes, and one mole-weighted averaging method.

Prefered method is LINEAR, or LALIBERTE if the mixture is aqueous and has electrolytes.

## Parameters

**MWs** [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

Tcs [list[float], optional] Critical temperatures of all species in the mixture, [K]

**Pcs** [list[float], optional] Critical pressures of all species in the mixture, [Pa]

Vcs [list[float], optional] Critical molar volumes of all species in the mixture, [m^3/mol]

Zcs [list[float], optional] Critical compressibility factors of all species in the mixture, [Pa]

- omegas [list[float], optional] Accentric factors of all species in the mixture, [-]
- CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]
- **VolumeLiquids** [list[VolumeLiquid], optional] VolumeLiquid objects created for all species in the mixture, [-]
- **correct\_pressure\_pure** [bool, optional] Whether to try to use the better pressure-corrected pure component models or to use only the T-only dependent pure species models, [-]

To iterate over all methods, use the list stored in *volume\_liquid\_mixture\_methods*.

LALIBERTE: Aqueous electrolyte model equation with coefficients; see thermo.electrochem. Laliberte\_density for more details.

**COSTALD\_MIXTURE:** CSP method described in COSTALD\_mixture.

- **COSTALD\_MIXTURE\_FIT:** CSP method described in COSTALD\_mixture, with two mixture composition independent fit coefficients, *Vc* and *omega*.
- **RACKETT:** CSP method described in Rackett\_mixture.
- **RACKETT\_PARAMETERS:** CSP method described in Rackett\_mixture, but with a mixture independent fit coefficient for compressibility factor for each species.

LINEAR: Linear mole fraction mixing rule described in mixing\_simple; also known as Amgat's law.

#### References

[1]

#### Methods

calculate(T, P, zs, ws, method)	Method to calculate molar volume of a liquid mixture at temperature <i>T</i> , pressure <i>P</i> , mole fractions <i>zs</i> and weight fractions <i>ws</i> with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for the given conditions.

#### Tmax

Maximum temperature at which no method can calculate the property above.

#### Tmin

Minimum temperature at which no method can calculate the property under.

## calculate(T, P, zs, ws, method)

Method to calculate molar volume of a liquid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

#### Parameters

- T [float] Temperature at which to calculate the property, [K]
- **P** [float] Pressure at which to calculate the property, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

**method** [str] Name of the method to use

#### Returns

Vm [float] Molar volume of the liquid mixture at the given conditions, [m^3/mol]

# name = 'Liquid volume'

## property\_max = 0.002

Maximum valid value of liquid molar volume. Generous limit.

#### property\_min = 0

Mimimum valid value of liquid molar volume. It should normally occur at the triple point, and be well above this.

ranked\_methods = ['LALIBERTE', 'LINEAR', 'COSTALD\_MIXTURE\_FIT',
'RACKETT\_PARAMETERS', 'COSTALD\_MIXTURE', 'RACKETT']

#### test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

## Parameters

T [float] Temperature at which to check method validity, [K]

**P** [float] Pressure at which to check method validity, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

## Returns

validity [bool] Whether or not a specifid method is valid

## units = 'm^3/mol'

thermo.volume.volume\_liquid\_mixture\_methods = ['LALIBERTE', 'LINEAR',

'COSTALD\_MIXTURE\_FIT', 'RACKETT\_PARAMETERS', <function COSTALD>, 'RACKETT']

Holds all low-pressure methods available for the VolumeLiquidMixture class, for use in iterating over them.

# 7.34.5 Mixture Gas Volume

class thermo.volume.VolumeGasMixture(eos=None, CASs=[], VolumeGases=[], MWs=[], \*\*kwargs)
Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with the molar volume of a gas mixture as a function of temperature, pressure, and composition. Consists of an equation of state, the ideal gas law, and one mole-weighted averaging method.

Prefered method is **EOS**, or **IDEAL** if critical properties of components are unavailable.

#### Parameters

CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]

VolumeGases [list[VolumeGas], optional] VolumeGas objects created for all species in the mixture, [-] eos [container[EOS Object], optional] Equation of state mixture object, [-]

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

## See also:

chemicals.volume.ideal\_gas
thermo.eos\_mix

## **Notes**

To iterate over all methods, use the list stored in *volume\_gas\_mixture\_methods*.

EOS: Equation of state mixture object; see thermo.eos\_mix for more details.

LINEAR: Linear mole fraction mixing rule described in mixing\_simple; more correct than the ideal gas law. **IDEAL:** The ideal gas law.

#### References

[1]

## Methods

calculate(T, P, zs, ws, method)	Method to calculate molar volume of a gas mixture
	at temperature T, pressure P, mole fractions zs and
	weight fractions ws with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for
	the given conditions.

#### Tmax

Maximum temperature at which no method can calculate the property above.

## Tmin

Minimum temperature at which no method can calculate the property under.

# calculate(T, P, zs, ws, method)

Method to calculate molar volume of a gas mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

## Parameters

- T [float] Temperature at which to calculate the property, [K]
- **P** [float] Pressure at which to calculate the property, [Pa]
- zs [list[float]] Mole fractions of all species in the mixture, [-]
- ws [list[float]] Weight fractions of all species in the mixture, [-]
- method [str] Name of the method to use

#### Returns

Vm [float] Molar volume of the gas mixture at the given conditions, [m^3/mol]

name = 'Gas volume'

#### $property_max = 1000000000.0$

Maximum valid value of gas molar volume. Set roughly at an ideal gas at 1 Pa and 2 billion K.

property\_min = 0.0

Mimimum valid value of gas molar volume. It should normally be well above this.

ranked\_methods = ['EOS', 'LINEAR', 'IDEAL', 'LINEAR\_MISSING\_IDEAL']

#### test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

#### Parameters

T [float] Temperature at which to check method validity, [K]

**P** [float] Pressure at which to check method validity, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

#### Returns

validity [bool] Whether or not a specifid method is valid

units = 'm^3/mol'

```
thermo.volume.volume_gas_mixture_methods = ['EOS', 'LINEAR', 'IDEAL']
```

Holds all methods available for the VolumeGasMixture class, for use in iterating over them.

# 7.34.6 Mixture Solid Volume

class thermo.volume.VolumeSolidMixture(CASs=[], VolumeSolids=[], MWs=[], \*\*kwargs)
Bases: thermo.utils.mixture\_property.MixtureProperty

Class for dealing with the molar volume of a solid mixture as a function of temperature, pressure, and composition. Consists of only mole-weighted averaging.

## Parameters

CASs [list[str], optional] The CAS numbers of all species in the mixture, [-]

**VolumeSolids** [list[VolumeSolid], optional] VolumeSolid objects created for all species in the mixture, [-]

MWs [list[float], optional] Molecular weights of all species in the mixture, [g/mol]

To iterate over all methods, use the list stored in *volume\_solid\_mixture\_methods*.

LINEAR: Linear mole fraction mixing rule described in mixing\_simple.

## **Methods**

calculate(T, P, zs, ws, method)	Method to calculate molar volume of a solid mixture at temperature <i>T</i> , pressure <i>P</i> , mole fractions <i>zs</i> and weight fractions <i>ws</i> with a given method.
<pre>test_method_validity(T, P, zs, ws, method)</pre>	Method to test the validity of a specified method for the given conditions.

#### Tmax

Maximum temperature at which no method can calculate the property above.

#### Tmin

Minimum temperature at which no method can calculate the property under.

## calculate(T, P, zs, ws, method)

Method to calculate molar volume of a solid mixture at temperature T, pressure P, mole fractions zs and weight fractions ws with a given method.

This method has no exception handling; see *mixture\_property* for that.

#### Parameters

T [float] Temperature at which to calculate the property, [K]

**P** [float] Pressure at which to calculate the property, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Name of the method to use

## Returns

Vm [float] Molar volume of the solid mixture at the given conditions, [m^3/mol]

## name = 'Solid molar volume'

## property\_max = 0.002

Maximum value of Heat capacity; arbitrarily set to 0.002, as the largest in the data is 0.00136.

# property\_min = 0

Molar volume cannot be under 0.

#### ranked\_methods = ['LINEAR']

### test\_method\_validity(T, P, zs, ws, method)

Method to test the validity of a specified method for the given conditions. No methods have implemented checks or strict ranges of validity.

#### Parameters

T [float] Temperature at which to check method validity, [K]

P [float] Pressure at which to check method validity, [Pa]

zs [list[float]] Mole fractions of all species in the mixture, [-]

ws [list[float]] Weight fractions of all species in the mixture, [-]

method [str] Method name to use

Returns

validity [bool] Whether or not a specifid method is valid

units = 'm^3/mol'

## thermo.volume.volume\_solid\_mixture\_methods = ['LINEAR']

Holds all methods available for the VolumeSolidMixture class, for use in iterating over them.

# 7.35 Wilson Gibbs Excess Model (thermo.wilson)

This module contains a class *Wilson* for performing activity coefficient calculations with the Wilson model. An older, functional calculation for activity coefficients only is also present, *Wilson\_gammas*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Wilson Class
- Wilson Functional Calculations
- Wilson Regression Calculations

# 7.35.1 Wilson Class

Bases: thermo.activity.GibbsExcess

Class for representing an a liquid with excess gibbs energy represented by the Wilson equation. This model is capable of representing most nonideal liquids for vapor-liquid equilibria, but is not recommended for liquid-liquid equilibria.

The two basic equations are as follows; all other properties are derived from these.

$$g^{E} = -RT \sum_{i} x_{i} \ln \left( \sum_{j} x_{j} \lambda_{i,j} \right)$$
$$\Lambda_{ij} = \exp \left[ a_{ij} + \frac{b_{ij}}{T} + c_{ij} \ln T + d_{ij}T + \frac{e_{ij}}{T^{2}} + f_{ij}T^{2} \right]$$

**Parameters** 

- T [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]
- **lambda\_coeffs** [list[list[list[float]]], optional] Wilson parameters, indexed by [i][j] and then each value is a 6 element list with parameters (*a*, *b*, *c*, *d*, *e*, *f*); either *lambda\_coeffs* or the lambda parameters are required, [various]

- **ABCDEF** [tuple(list[list[float]], 6), optional] The lamba parameters can be provided as a tuple, [various]
- lambda\_as [list[list[float]], optional] a parameters used in calculating Wilson.lambdas, [-]
- lambda\_bs [list[list[float]], optional] b parameters used in calculating Wilson.lambdas, [K]
- **lambda\_cs** [list[list[float]], optional] *c* parameters used in calculating *Wilson.lambdas*, [-]
- **lambda\_ds** [list[list[float]], optional] *d* paraemeters used in calculating *Wilson.lambdas*, [1/K]
- **lambda\_es** [list[list[float]], optional] *e* parameters used in calculating *Wilson.lambdas*, [K<sup>2</sup>]
- **lambda\_fs** [list[float]], optional] f parameters used in calculating *Wilson.lambdas*, [1/K^2]

In addition to the methods presented here, the methods of its base class thermo.activity.GibbsExcess are available as well.

**Warning:** If parameters are ommited for all interactions, this model reverts to *thermo.activity*. *IdealSolution*. In large systems it is common to only regress parameters for the most important components; set *lambda* parameters for other components to 0 to "ignore" them and treat them as ideal components.

This class works with python lists, numpy arrays, and can be accelerated with Numba or PyPy quite effectively.

### References

[1], [2], [3]

## **Examples**

# Example 1

This object-oriented class provides access to many more thermodynamic properties than *Wilson\_gammas*, but it can also be used like that function. In the following example, *gammas* are calculated with both functions. The *lambdas* cannot be specified in this class; but fixed values can be converted with the *log* function so that fixed values will be obtained.

```
>>> Wilson_gammas([0.252, 0.748], [[1, 0.154], [0.888, 1]])
[1.881492608717, 1.165577493112]
>>> GE = Wilson(T=300.0, xs=[0.252, 0.748], lambda_as=[[0, log(0.154)], [log(0.888),
→ 0]])
>>> GE.gammas()
[1.881492608717, 1.165577493112]
```

We can check that the same lambda values were computed as well, and that there is no temperature dependency:

```
>>> GE.lambdas()
[[1.0, 0.154], [0.888, 1.0]]
>>> GE.dlambdas_dT()
[[0.0, 0.0], [0.0, 0.0]]
```

In this case, there is no temperature dependency in the Wilson model as the *lambda* values are fixed, so the excess enthalpy is always zero. Other properties are not always zero.

>>> GE.HE(), GE.CpE()
(0.0, 0.0)
>>> GE.GE(), GE.SE(), GE.dGE\_dT()
(683.165839398, -2.277219464, 2.2772194646)

## Example 2

ChemSep is a (partially) free program for modeling distillation. Besides being a wonderful program, it also ships with a permissive license several sets of binary interaction parameters. The Wilson parameters in it can be accessed from Thermo as follows. In the following case, we compute activity coefficients of the ethanol-water system at mole fractions of [.252, 0.748].

In ChemSep, the form of the Wilson lambda equation is

$$\Lambda_{ij} = \frac{V_j}{V_i} \exp\left(\frac{-A_{ij}}{RT}\right)$$

The parameters were converted to the form used by Thermo as follows:

$$a_{ij} = \log\left(\frac{V_j}{V_i}\right)$$
$$b_{ij} = \frac{-A_{ij}}{R} = \frac{-A_{ij}}{1.9872042586408316}$$

This system was chosen because there is also a sample problem for the same components from the DDBST which can be found here: http://chemthermo.ddbst.com/Problems\_Solutions/Mathcad\_Files/P05.01a% 20VLE%20Behavior%20of%20Ethanol%20-%20Water%20Using%20Wilson.xps

In that example, with different data sets and parameters, they obtain at the same conditions activity coefficients of [1.881, 1.165]. Different sources of parameters for the same system will generally have similar behavior if regressed in the same temperature range. As higher order *lambda* parameters are added, models become more likely to behave differently. It is recommended in [3] to regress the minimum number of parameters required.

#### Example 3

The DDBST has published some sample problems which are fun to work with. Because the DDBST uses a different equation form for the coefficients than this model implements, we must initialize the *Wilson* object with a different method.

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```
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```

```
>>> bs_ddbst = [[0, -3.78434, -0.67704], [6.405502, 0, 2.59359], [-0.256645, -6.
→2234, 0]]
>>> cs_ddbst = [[0.0, 7.91073e-3, 8.68371e-4], [-7.47788e-3, 0.0, 3.1e-5], [-1.
→24796e-3, 3e-5, 0.0]]
>>> dis = eis = fis = [[0.0]*N for _ in range(N)]
>>> params = Wilson.from_DDBST_as_matrix(Vs=Vs_ddbst, ais=as_ddbst, bis=bs_ddbst,_
>>> xs = [0.229, 0.175, 0.596]
>>> GE = Wilson(T=T, xs=xs, lambda_as=params[0], lambda_bs=params[1], lambda_
→cs=params[2], lambda_ds=params[3], lambda_es=params[4], lambda_fs=params[5])
>>> GE
Wilson(T=331.42, xs=[0.229, 0.175, 0.596], lambda_as=[[0.0, 3.870101271243586, 0.
→07939943395502425], [-6.491263271243587, 0.0, -3.276991837288562], [0.
→8542855660449756, 6.906801837288562, 0.0]], lambda_bs=[[0.0, -375.2835, -31.1208],
→ [1722.58, 0.0, 1140.79], [-747.217, -3596.17, -0.0]], lambda_ds=[[-0.0, -0.
→00791073, -0.000868371], [0.00747788, -0.0, -3.1e-05], [0.00124796, -3e-05, -0.
→0]])
>>> GE_GE(), GE_dGE_dT(), GE_d2GE_dT2()
(480.2639266306882, 4.355962766232997, -0.029130384525017247)
>>> GE_HE(), GE_SE(), GE_dHE_dT(), GE_dSE_dT()
(-963.3892533542517, -4.355962766232997, 9.654392039281216, 0.029130384525017247)
>>> GE.gammas()
[1.2233934334, 1.100945902470, 1.205289928117]
```

The solution given by the DDBST has the same values [1.223, 1.101, 1.205], and can be found here: http://chemthermo.ddbst.com/Problems\_Solutions/Mathcad\_Files/05.09%20Compare%20Experimental% 20VLE%20to%20Wilson%20Equation%20Results.xps

# Example 4

A simple example is given in [1]; other textbooks sample problems are normally in the same form as this - with only volumes and the a term specified. The system is 2-propanol/water at 353.15 K, and the mole fraction of 2-propanol is 0.25.

```
>>> T = 353.15
>>> N = 2
>>> Vs = [76.92, 18.07] # cm^3/mol
>>> ais = [[0.0, 437.98],[1238.0, 0.0]] # cal/mol
>>> bis = cis = dis = eis = fis = [[0.0]*N for _ in range(N)]
>>> params = Wilson.from_DDBST_as_matrix(Vs=Vs, ais=ais, bis=bis, cis=cis, dis=dis,_
...eis=eis, fis=fis, unit_conversion=True)
>>> xs = [0.25, 0.75]
>>> GE = Wilson(T=T, xs=xs, lambda_as=params[0], lambda_bs=params[1], lambda_
...cs=params[2], lambda_ds=params[3], lambda_es=params[4], lambda_fs=params[5])
>>> GE.gammas()
[2.124064516, 1.1903745834]
```

The activity coefficients given in [1] are [2.1244, 1.1904]; matching (with a slight deviation from their use of 1.987 as a gas constant).

## Attributes

- **T** [float] Temperature, [K]
- **xs** [list[float]] Mole fractions, [-]

model\_id [int] Unique identifier for the Wilson activity model, [-]

# Methods

GE()	Calculate and return the excess Gibbs energy of a liq-
	uid phase represented with the Wilson model.
d2GE_dT2()	Calculate and return the second temperature deriva-
	tive of excess Gibbs energy of a liquid phase using
	the Wilson activity coefficient model.
d2GE_dTdxs()	Calculate and return the temperature derivative of
, , , , , , , , , , , , , , , , , , ,	mole fraction derivatives of excess Gibbs energy of
	a liquid represented by the Wilson model.
d2GE_dxixjs()	Calculate and return the second mole fraction deriva-
	tives of excess Gibbs energy for the Wilson model.
d2lambdas_dT2()	Calculate and return the second temperature deriva-
	tive of the lambda termsfor the Wilson model at the
	system temperature.
d3GE_dT3()	Calculate and return the third temperature derivative
	of excess Gibbs energy of a liquid phase using the
	Wilson activity coefficient model.
d3GE_dxixjxks()	Calculate and return the third mole fraction deriva-
	tives of excess Gibbs energy using the Wilson model.
d3lambdas_dT3()	Calculate and return the third temperature derivative
	of the lambda terms for the Wilson model at the sys-
	tem temperature.
dGE_dT()	Calculate and return the temperature derivative of ex-
	cess Gibbs energy of a liquid phase represented by the
	Wilson model.
dGE_dxs()	Calculate and return the mole fraction derivatives of
	excess Gibbs energy for the Wilson model.
dlambdas_dT()	Calculate and return the temperature derivative of the
	lambda terms for the Wilson model at the system
	temperature.
<i>from_DDBST</i> (Vi, Vj, a, b, c[, d, e, f,])	Converts parameters for the wilson equation in the
	DDBST to the basis used in this implementation.
<pre>from_DDBST_as_matrix(Vs[, ais, bis, cis,])</pre>	Converts parameters for the wilson equation in the
	DDBST to the basis used in this implementation.
lambdas()	Calculate and return the <i>lambda</i> terms for the Wilson
	model for at system temperature.
to_T_xs(T, xs)	Method to construct a new Wilson instance at tem-
	perature T, and mole fractions xs with the same pa-
	rameters as the existing object.

# GE()

Calculate and return the excess Gibbs energy of a liquid phase represented with the Wilson model.

$$g^E = -RT \sum_i x_i \ln\left(\sum_j x_j \lambda_{i,j}\right)$$

Returns

GE [float] Excess Gibbs energy of an ideal liquid, [J/mol]

#### $d2GE_dT2()$

Calculate and return the second temperature derivative of excess Gibbs energy of a liquid phase using the Wilson activity coefficient model.

$$\frac{\partial^2 G^E}{\partial T^2} = -R \left[ T \sum_i \left( \frac{x_i \sum_j (x_j \frac{\partial^2 \Lambda_{ij}}{\partial T^2})}{\sum_j x_j \Lambda_{ij}} - \frac{x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})^2}{(\sum_j x_j \Lambda_{ij})^2} \right) + 2 \sum_i \left( \frac{x_i \sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T}}{\sum_j x_j \Lambda_{ij}} \right) \right]$$

Returns

## d2GE\_dTdxs()

Calculate and return the temperature derivative of mole fraction derivatives of excess Gibbs energy of a liquid represented by the Wilson model.

$$\frac{\partial^2 G^E}{\partial x_k \partial T} = -R \left[ T \left( \sum_i \left( \frac{x_i \frac{\partial n_{ik}}{\partial T}}{\sum_j x_j \Lambda_{ij}} - \frac{x_i \Lambda_{ik} (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\partial_j x_j \Lambda_{ij})^2} \right) + \frac{\sum_i x_i \frac{\partial \Lambda_{ki}}{\partial T}}{\sum_j x_j \Lambda_{kj}} \right) + \ln \left( \sum_i x_i \Lambda_{ki} \right) + \sum_i \frac{x_i \Lambda_{ik}}{\sum_j x_j \Lambda_{ij}} \right] \right]$$

Returns

**d2GE\_dTdxs** [list[float]] Temperature derivative of mole fraction derivatives of excess Gibbs energy, [J/mol/K]

# d2GE\_dxixjs()

Calculate and return the second mole fraction derivatives of excess Gibbs energy for the Wilson model.

$$\frac{\partial^2 G^E}{\partial x_k \partial x_m} = RT \left( \sum_i \frac{x_i \Lambda_{ik} \Lambda_{im}}{(\sum_j x_j \Lambda_{ij})^2} - \frac{\Lambda_{km}}{\sum_j x_j \Lambda_{kj}} - \frac{\Lambda_{mk}}{\sum_j x_j \Lambda_{mj}} \right)$$

Returns

**d2GE\_dxixjs** [list[list[float]]] Second mole fraction derivatives of excess Gibbs energy, [J/mol]

#### d2lambdas\_dT2()

Calculate and return the second temperature derivative of the *lambda* termsfor the Wilson model at the system temperature.

$$\frac{\partial^2 \Lambda_{ij}}{\partial^2 T} = \left(2f_{ij} + \left(2Tf_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3}\right)^2 - \frac{c_{ij}}{T^2} + \frac{2b_{ij}}{T^3} + \frac{6e_{ij}}{T^4}\right) e^{T^2 f_{ij} + Td_{ij} + a_{ij} + c_{ij} \ln\left(T\right) + \frac{b_{ij}}{T} + \frac{e_{ij}}{T^2} + \frac{e_{ij}}{T^2} + \frac{2e_{ij}}{T^3} + \frac{2e_{ij}}{T^3} + \frac{2e_{ij}}{T^4} + \frac{e_{ij}}{T^4} + \frac{e_{ij}}$$

Returns

**d2lambdas\_dT2** [list[list[float]]] Second temperature deriavtives of Lambda terms, asymmetric matrix, [1/K^2]

## **Notes**

These Lambda ij values (and the coefficients) are NOT symmetric.

## d3GE\_dT3()

Calculate and return the third temperature derivative of excess Gibbs energy of a liquid phase using the Wilson activity coefficient model.

$$\frac{\partial^3 G^E}{\partial T^3} = -R \left[ 3 \left( \frac{x_i \sum_j (x_j \frac{\partial^2 \Lambda_{ij}}{\partial T^2})}{\sum_j x_j \Lambda_{ij}} - \frac{x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})^2}{(\sum_j x_j \Lambda_{ij})^2} \right) + T \left( \sum_i \frac{x_i (\sum_j x_j \frac{\partial^3 \Lambda_{ij}}{\partial T^3})}{\sum_j x_j \Lambda_{ij}} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T})}{(\sum_j x_j \Lambda_{ij})^2} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}{(\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})} - \frac{3x_i (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2}) (\sum_j x_j \frac{\partial \Lambda_{ij}}{\partial T^2})}$$

## Returns

d3GE\_dT3 [float] Third temperature derivative of excess Gibbs energy, [J/(mol\*K^3)]

### d3GE\_dxixjxks()

Calculate and return the third mole fraction derivatives of excess Gibbs energy using the Wilson model.

$$\frac{\partial^3 G^E}{\partial x_k \partial x_m \partial x_n} = -RT \left[ \sum_i \left( \frac{2x_i \Lambda_{ik} \Lambda_{im} \Lambda_{in}}{(\sum x_j \Lambda_{ij})^3} \right) - \frac{\Lambda_{km} \Lambda_{kn}}{(\sum_j x_j \Lambda_{kj})^2} - \frac{\Lambda_{mk} \Lambda_{mn}}{(\sum_j x_j \Lambda_{mj})^2} - \frac{\Lambda_{nk} \Lambda_{nm}}{(\sum_j x_j \Lambda_{mj})^2} \right] \right]$$

Returns

**d3GE\_dxixjxks** [list[list[float]]]] Third mole fraction derivatives of excess Gibbs energy, [J/mol]

### d3lambdas\_dT3()

Calculate and return the third temperature derivative of the *lambda* terms for the Wilson model at the system temperature.

$$\frac{\partial^3 \Lambda_{ij}}{\partial^3 T} = \left( 3 \left( 2f_{ij} - \frac{c_{ij}}{T^2} + \frac{2b_{ij}}{T^3} + \frac{6e_{ij}}{T^4} \right) \left( 2Tf_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3} \right) + \left( 2Tf_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3} \right)^3$$

Returns

**d3lambdas\_dT3** [list[list[float]]] Third temperature deriavtives of Lambda terms, asymmetric matrix, [1/K^3]

## Notes

These Lambda ij values (and the coefficients) are NOT symmetric.

### dGE\_dT()

Calculate and return the temperature derivative of excess Gibbs energy of a liquid phase represented by the Wilson model.

$$\frac{\partial G^E}{\partial T} = -R\sum_i x_i \ln\left(\sum_j x_i \Lambda_{ij}\right) - RT\sum_i \frac{x_i \sum_j x_j \frac{\Lambda_{ij}}{\partial T}}{\sum_j x_j \Lambda_{ij}}$$

#### Returns

**dGE\_dT** [float] First temperature derivative of excess Gibbs energy of a liquid phase represented by the Wilson model, [J/(mol\*K)]

dGE\_dxs()

Calculate and return the mole fraction derivatives of excess Gibbs energy for the Wilson model.

$$\frac{\partial G^E}{\partial x_k} = -RT \left[ \sum_i \frac{x_i \Lambda_{ik}}{\sum_j \Lambda_{ij} x_j} + \ln \left( \sum_j x_j \Lambda_{kj} \right) \right]$$

Returns

dGE\_dxs [list[float]] Mole fraction derivatives of excess Gibbs energy, [J/mol]

dlambdas\_dT()

Calculate and return the temperature derivative of the *lambda* terms for the Wilson model at the system temperature.

$$\frac{\partial \Lambda_{ij}}{\partial T} = \left(2Th_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3}\right)e^{T^2h_{ij} + Td_{ij} + a_{ij} + c_{ij}\ln(T) + \frac{b_{ij}}{T} + \frac{e_{ij}}{T^2}}$$

#### Returns

**dlambdas\_dT** [list[list[float]]] Temperature deriavtives of Lambda terms, asymmetric matrix [1/K]

## Notes

These Lambda ij values (and the coefficients) are NOT symmetric.

**static from\_DDBST**(*Vi*, *Vj*, *a*, *b*, *c*, d=0.0, e=0.0, f=0.0,  $unit\_conversion=True$ ) Converts parameters for the wilson equation in the DDBST to the basis used in this implementation.

$$\Lambda_{ij} = \frac{V_j}{V_i} \exp\left(\frac{-\Delta\lambda_{ij}}{RT}\right)$$
$$\Delta\lambda_{ij} = a_{ij} + b_{ij}T + cT^2 + d_{ij}T\ln T + e_{ij}T^3 + f_{ij}/T$$

#### **Parameters**

Vi [float] Molar volume of component i; needs only to be in the same units as Vj, [cm^3/mol]

Vj [float] Molar volume of component j; needs only to be in the same units as Vi, [cm^3/mol]

- a [float] a parameter in DDBST form, [K]
- **b** [float] *b* parameter in DDBST form, [-]
- **c** [float] *c* parameter in DDBST form, [1/K]
- **d** [float, optional] *d* parameter in DDBST form, [-]
- e [float, optional] e parameter in DDBST form, [1/K^2]
- **f** [float, optional] *f* parameter in DDBST form, [K<sup>2</sup>]

**unit\_conversion** [bool] If True, the input coefficients are in units of cal/K/mol, and a *R* gas constant of 1.9872042... is used for the conversion; the DDBST uses this generally, [-]

## Returns

- **a** [float] *a* parameter in *Wilson* form, [-]
- **b** [float] *b* parameter in *Wilson* form, [K]
- c [float] c parameter in Wilson form, [-]
- **d** [float] *d* parameter in *Wilson* form, [1/K]
- e [float] e parameter in Wilson form, [K^2]
- **f** [float] *f* parameter in *Wilson* form, [1/K^2]

#### Notes

The units show how the different variables are related to each other.

```
>>> Wilson.from_DDBST(Vi=74.04, Vj=80.67, a=375.2835, b=-3.78434, c=0.00791073,

→d=0.0, e=0.0, f=0.0, unit_conversion=False)

(3.8701012712, -375.2835, -0.0, -0.00791073, -0.0, -0.0)
```

Converts parameters for the wilson equation in the DDBST to the basis used in this implementation. Matrix wrapper around *Wilson.from\_DDBST*.

## Parameters

Vs [list[float]] Molar volume of component; needs only to be in consistent units, [cm^3/mol]

**ais** [list[list[float]]] *a* parameters in DDBST form, [K]

- **bis** [list[list[float]]] *b* parameters in DDBST form, [-]
- **cis** [list[float]]] *c* parameters in DDBST form, [1/K]
- dis [list[list[float]], optional] d parameters in DDBST form, [-]
- eis [list[list[float]], optional] *e* parameters in DDBST form, [1/K<sup>2</sup>]
- **fis** [list[float]], optional] *f* parameters in DDBST form, [K^2]
- **unit\_conversion** [bool] If True, the input coefficients are in units of cal/K/mol, and a *R* gas constant of 1.9872042... is used for the conversion; the DDBST uses this generally, [-]

## Returns

- **a** [list[list[float]]] *a* parameters in *Wilson* form, [-]
- **b** [list[list[float]]] *b* parameters in *Wilson* form, [K]
- c [list[list[float]]] c parameters in *Wilson* form, [-]
- **d** [list[list[float]]] *d* paraemeters in *Wilson* form, [1/K]
- e [list[list[float]]] e parameters in *Wilson* form, [K^2]
- **f** [list[list[float]]] *f* parameters in *Wilson* form, [1/K^2]

## lambdas()

Calculate and return the lambda terms for the Wilson model for at system temperature.

$$\Lambda_{ij} = \exp\left[a_{ij} + \frac{b_{ij}}{T} + c_{ij}\ln T + d_{ij}T + \frac{e_{ij}}{T^2} + f_{ij}T^2\right]$$

## Returns

lambdas [list[list[float]]] Lambda terms, asymmetric matrix [-]

These Lambda ij values (and the coefficients) are NOT symmetric.

#### $to_T_xs(T, xs)$

Method to construct a new *Wilson* instance at temperature *T*, and mole fractions *xs* with the same parameters as the existing object.

#### Parameters

T [float] Temperature, [K]

xs [list[float]] Mole fractions of each component, [-]

#### Returns

obj [Wilson] New Wilson object at the specified conditions [-]

#### Notes

If the new temperature is the same temperature as the existing temperature, if the *lambda* terms or their derivatives have been calculated, they will be set to the new object as well.

# 7.35.2 Wilson Functional Calculations

## thermo.wilson.Wilson\_gammas(xs, params)

Calculates the activity coefficients of each species in a mixture using the Wilson method, given their mole fractions, and dimensionless interaction parameters. Those are normally correlated with temperature, and need to be calculated separately.

$$\ln \gamma_i = 1 - \ln \left( \sum_{j}^{N} \Lambda_{ij} x_j \right) - \sum_{j}^{N} \frac{\Lambda_{ji} x_j}{\sum_{k}^{N} \Lambda_{jk} x_k}$$

#### **Parameters**

xs [list[float]] Liquid mole fractions of each species, [-]

**params** [list[list[float]]] Dimensionless interaction parameters of each compound with each other, [-]

### Returns

gammas [list[float]] Activity coefficient for each species in the liquid mixture, [-]

## Notes

This model needs N^2 parameters.

The original model correlated the interaction parameters using the standard pure-component molar volumes of each species at 25°C, in the following form:

$$\Lambda_{ij} = \frac{V_j}{V_i} \exp\left(\frac{-\lambda_{i,j}}{RT}\right)$$

If a compound is not liquid at that temperature, the liquid volume is taken at the saturated pressure; and if the component is supercritical, its liquid molar volume should be extrapolated to 25°C.

However, that form has less flexibility and offered no advantage over using only regressed parameters.

Most correlations for the interaction parameters include some of the terms shown in the following form:

$$\ln \Lambda_{ij} = a_{ij} + \frac{b_{ij}}{T} + c_{ij} \ln T + d_{ij}T + \frac{e_{ij}}{T^2} + h_{ij}T^2$$

The Wilson model is not applicable to liquid-liquid systems.

For this model to produce ideal acitivty coefficients (gammas = 1), all interaction parameters should be 1.

The specific process simulator implementations are as follows:

## References

[1], [2]

#### **Examples**

Ethanol-water example, at 343.15 K and 1 MPa, from [2] also posted online http://chemthermo.ddbst. com/Problems\_Solutions/Mathcad\_Files/P05.01a%20VLE%20Behavior%20of%20Ethanol%20-%20Water% 20Using%20Wilson.xps :

```
>>> Wilson_gammas([0.252, 0.748], [[1, 0.154], [0.888, 1]])
[1.881492608717, 1.165577493112]
```

# 7.35.3 Wilson Regression Calculations

#### thermo.wilson.wilson\_gammas\_binaries(xs, lambda12, lambda21, calc=None)

Calculates activity coefficients at fixed *lambda* values for a binary system at a series of mole fractions. This is used for regression of *lambda* parameters. This function is highly optimized, and operates on multiple points at a time.

$$\ln \gamma_1 = -\ln(x_1 + \Lambda_{12}x_2) + x_2 \left(\frac{\Lambda_{12}}{x_1 + \Lambda_{12}x_2} - \frac{\Lambda_{21}}{x_2 + \Lambda_{21}x_1}\right)$$
$$\ln \gamma_2 = -\ln(x_2 + \Lambda_{21}x_1) - x_1 \left(\frac{\Lambda_{12}}{x_1 + \Lambda_{12}x_2} - \frac{\Lambda_{21}}{x_2 + \Lambda_{21}x_1}\right)$$

#### **Parameters**

xs [list[float]] Liquid mole fractions of each species in the format x0\_0, x1\_0, (component 1 point1, component 2 point 1), x0\_1, x1\_1, (component 1 point2, component 2 point 2), ... [-]

lambda12 [float] lambda parameter for 12, [-]

lambda21 [float] *lambda* parameter for 21, [-]

**gammas** [list[float], optional] Array to store the activity coefficient for each species in the liquid mixture, indexed the same as *xs*; can be omitted or provided for slightly better performance [-]

# Returns

**gammas** [list[float]] Activity coefficient for each species in the liquid mixture, indexed the same as *xs*, [-]

The lambda values are hard-coded to replace values under zero which are mathematically impossible, with a very small number. This is helpful for regression which might try to make those values negative.

#### **Examples**

```
>>> wilson_gammas_binaries([.1, .9, 0.3, 0.7, .85, .15], 0.1759, 0.7991)
[3.42989, 1.03432, 1.74338, 1.21234, 1.01766, 2.30656]
```

# 7.36 UNIQUAC Gibbs Excess Model (thermo.uniquac)

This module contains a class *UNIQUAC* for performing activity coefficient calculations with the UNIQUAC model. An older, functional calculation for activity coefficients only is also present, *UNIQUAC\_gammas*.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- UNIQUAC Class
- UNIQUAC Functional Calculations

# 7.36.1 UNIQUAC Class

**class** thermo.uniquac.**UNIQUAC**(*T*, *xs*, *rs*, *qs*, *tau\_coeffs=None*, *ABCDEF=None*, *tau\_as=None*, *tau\_bs=None*, *tau\_cs=None*, *tau\_ds=None*, *tau\_es=None*, *tau\_fs=None*)

Bases: thermo.activity.GibbsExcess

Class for representing an a liquid with excess gibbs energy represented by the UNIQUAC equation. This model is capable of representing VL and LL behavior.

$$\frac{G^E}{RT} = \sum_i x_i \ln \frac{\phi_i}{x_i} + \frac{z}{2} \sum_i q_i x_i \ln \frac{\theta_i}{\phi_i} - \sum_i q_i x_i \ln \left(\sum_j \theta_j \tau_{ji}\right)$$
$$\phi_i = \frac{r_i x_i}{\sum_j r_j x_j}$$
$$\theta_i = \frac{q_i x_i}{\sum_j q_j x_j}$$
$$\tau_{ij} = \exp\left[a_{ij} + \frac{b_{ij}}{T} + c_{ij} \ln T + d_{ij}T + \frac{e_{ij}}{T^2} + f_{ij}T^2\right]$$

**Parameters** 

- **T** [float] Temperature, [K]
- xs [list[float]] Mole fractions, [-]
- **rs** [list[float]] r parameters  $r_i = \sum_{k=1}^{n} \nu_k R_k$  if from UNIFAC, otherwise regressed, [-]
- **qs** [list[float]] q parameters  $q_i = \sum_{k=1}^{n} \nu_k Q_k$  if from UNIFAC, otherwise regressed, [-]

- **tau\_coeffs** [list[list[float]]], optional] UNIQUAC parameters, indexed by [i][j] and then each value is a 6 element list with parameters [*a*, *b*, *c*, *d*, *e*, *f*]; either *tau\_coeffs* or *ABCDEF* are required, [-]
- **ABCDEF** [tuple[list[list[float]], 6], optional] Contains the following. One of *tau\_coeffs* or *ABCDEF* or some of the *tau\_as*, etc parameters are required, [-]
- tau\_as [list[list[float]] or None, optional] a parameters used in calculating UNIQUAC.taus, [-]
- tau\_bs [list[float]] or None, optional] b parameters used in calculating UNIQUAC. taus, [K]
- tau\_cs [list[list[float]] or None, optional] c parameters used in calculating UNIQUAC.taus, [-]
- tau\_ds [list[list[float]] or None, optional] d paraemeters used in calculating UNIQUAC.taus,
   [1/K]
- **tau\_es** [list[list[float]] or None, optional] *e* parameters used in calculating *UNIQUAC.taus*, [K^2]
- **tau\_fs** [list[list[float]] or None, optional] *f* parameters used in calculating UNIQUAC.taus, [1/K^2]

In addition to the methods presented here, the methods of its base class thermo.activity.GibbsExcess are available as well.

**Warning:** There is no such thing as a missing parameter in the UNIQUAC model. It is possible to find  $\tau_{ij}$  and  $\tau_{ji}$  which make  $\gamma_i = 1$  and  $\gamma_j = 1$ , but those tau values depend on *rs*, *qs*, and *xs* - the composition, which obviously will change. It is therefore impossible to make an interaction parameter "missing"; whatever value it has will always impact the phase equilibria problem. At best, the tau values can produce close to ideal behavior.

## References

[1], [2]

## **Examples**

#### **Example 1**

Example 5.19 in [2] includes the calculation of liquid-liquid activity coefficients for the water-ethanol-benzene system. Two calculations are reproduced accurately here. Note that the DDBST-style coefficients assume a negative sign; for compatibility, their coefficients need to have their sign flipped.

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```
>>> ABCDEF = (tausA, tausB, tausC, tausD, tausE, tausF)
>>> GE = UNIQUAC(T=T, xs=xs, rs=rs, qs=qs, ABCDEF=ABCDEF)
>>> GE.gammas()
[1.570393328, 0.2948241614, 18.114329048]
```

The given values in [2] are [1.570, 0.2948, 18.11], matching exactly. The second phase has a different composition; the expected values are [8.856, 0.860, 1.425]. Once the *UNIQUAC* object has been constructed, it is very easy to obtain properties at different conditions:

```
>>> GE.to_T_xs(T=T, xs=[1/6., 1/6., 2/3.]).gammas()
[8.8559908058, 0.8595242462, 1.42546014081]
```

The string representation of the object presents enough information to reconstruct it as well.

```
>>> GE
UNIQUAC(T=298.15, xs=[0.7273, 0.0909, 0.1818], rs=[0.92, 2.1055, 3.1878], qs=[1.4,
→1.972, 2.4], ABCDEF=([[0.0, 0.0, 0.0], [0.0, 0.0, 0.0], [0.0, 0.0, 0.0]], [[0, -
→526.02, -309.64], [318.06, 0, 91.532], [-1325.1, -302.57, 0]], [[0.0, 0.0, 0.0],
→[0.0, 0.0, 0.0], [0.0, 0.0, 0.0]], [[0.0, 0.0, 0.0], [0.0, 0.0, 0.0], [0.0, 0.0, 0.0],
→0.0]], [[0.0, 0.0, 0.0], [0.0, 0.0, 0.0], [0.0, 0.0, 0.0]], [[0.0, 0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]], [0.0, 0.0]]]))
```

The phase exposes many properties and derivatives as well.

```
>>> GE.GE(), GE.dGE_dT(), GE.d2GE_dT2()
(1843.96486834, 6.69851118521, -0.015896025970)
>>> GE.HE(), GE.SE(), GE.dHE_dT(), GE.dSE_dT()
(-153.19624152, -6.69851118521, 4.7394001431, 0.0158960259705)
```

## Example 2

Another problem is 8.32 in [1] - acetonitrile, benzene, n-heptane at 45 °C. The sign flip is needed here as well to convert their single temperature-dependent values into the correct form, but it has already been done to the coefficients:

```
>>> N = 3
>>> T = 45 + 273.15
>>> rs = [.1311, .0330, .8359]
>>> rs = [1.87, 3.19, 5.17]
>>> qs = [1.72, 2.4, 4.4]
>>> tausA = tausC = tausD = tausE = tausF = [[0.0]*N for i in range(N)]
>>> tausB = [[0.0, -60.28, -23.71], [-89.57, 0.0, 135.9], [-545.8, -245.4, 0.0]]
>>> ABCDEF = (tausA, tausB, tausC, tausD, tausE, tausF)
>>> GE = UNIQUAC(T=T, xs=xs, rs=rs, qs=qs, ABCDEF=ABCDEF)
>>> GE.gammas()
[7.1533533992, 1.25052436922, 1.060392792605]
```

The given values in [1] are [7.15, 1.25, 1.06].

## Example 3

ChemSep is a program for modeling distillation. Chemsep ships with a permissive license several sets of binary interaction parameters. The UNIQUAC parameters in it can be accessed from Thermo as follows. In the following case, we compute activity coefficients of the ethanol-water system at mole fractions of [.252, 0.748].

>>> from thermo.interaction\_parameters import IPDB >>> CAS1, CAS2 = '64-17-5', '7732-18-5' >>> xs = [0.252, 0.748] >>> rs = [2.11, 0.92] >>> qs = [1.97, 1.400] >>> N = 2 >>> T = 343.15 >>> tau\_bs = IPDB.get\_ip\_asymmetric\_matrix(name='ChemSep UNIQUAC', CASs=['64-17-5', -, '7732-18-5'], ip='bij') >>> GE = UNIQUAC(T=T, xs=xs, rs=rs, qs=qs, tau\_bs=tau\_bs) >>> GE.gammas() [1.977454, 1.1397696]

In ChemSep, the form of the UNIQUAC tau equation is

$$\tau_{ij} = \exp\left(\frac{-A_{ij}}{RT}\right)$$

The parameters were converted to the form used by Thermo as follows:

$$b_{ij} = \frac{-A_{ij}}{R} = \frac{-A_{ij}}{1.9872042586408316}$$

This system was chosen because there is also a sample problem for the same components from the DDBST which can be found here: http://chemthermo.ddbst.com/Problems\_Solutions/Mathcad\_Files/P05.01c% 20VLE%20Behavior%20of%20Ethanol%20-%20Water%20Using%20UNIQUAC.xps

In that example, with different data sets and parameters, they obtain at the same conditions activity coefficients of [2.359, 1.244].

# Attributes

T [float] Temperature, [K]

xs [list[float]] Mole fractions, [-]

## Methods

<i>GE</i> ()	Calculate and return the excess Gibbs energy of a liq-
U U	uid phase using the UNIQUAC model.
d2GE_dT2()	Calculate and return the second temperature deriva-
	tive of excess Gibbs energy of a liquid phase using
	the UNIQUAC model.
d2GE_dTdxs()	Calculate and return the temperature derivative of
	mole fraction derivatives of excess Gibbs energy us-
	ing the UNIQUAC model.
d2GE_dxixjs()	Calculate and return the second mole fraction deriva-
	tives of excess Gibbs energy using the UNIQUAC
	model.
d2taus_dT2()	Calculate and return the second temperature deriva-
	tive of the <i>tau</i>
d3GE_dT3()	Calculate and return the third temperature derivative
	of excess Gibbs energy of a liquid phase using the
	UNIQUAC model.
	continues on post page

continues on next page

Table 113 – continued from previous page	
d3taus_dT3()	Calculate and return the third temperature derivative
	of the tau terms for the UNIQUAC model for a spec-
	ified temperature.
$dGE_dT()$	Calculate and return the temperature derivative of ex-
	cess Gibbs energy of a liquid phase using the UNI-
	QUAC model.
dGE_dxs()	Calculate and return the mole fraction derivatives of
	excess Gibbs energy using the UNIQUAC model.
dtaus_dT()	Calculate and return the temperature derivative of the
	tau terms for the UNIQUAC model for a specified
	temperature.
phis()	Calculate and return the <i>phi</i> parameters at the system
	composition and temperature.
<pre>regress_binary_parameters(gammas, xs, rs, qs)</pre>	Perform a basic regression to determine the values of
	the <i>tau</i> terms in the UNIQUAC model, given a series
	of known or predicted activity coefficients and mole
	fractions.
taus()	Calculate and return the <i>tau</i> terms for the UNIQUAC
	model for the system temperature.
thetas()	Calculate and return the <i>theta</i> parameters at the sys-
	tem composition and temperature.
$to_T_xs(T, xs)$	Method to construct a new UNIQUAC instance at tem-
	perature T, and mole fractions xs with the same pa-
	rameters as the existing object.

# **GE**()

Calculate and return the excess Gibbs energy of a liquid phase using the UNIQUAC model.

$$\frac{G^E}{RT} = \sum_i x_i \ln \frac{\phi_i}{x_i} + \frac{z}{2} \sum_i q_i x_i \ln \frac{\theta_i}{\phi_i} - \sum_i q_i x_i \ln \left(\sum_j \theta_j \tau_{ji}\right)$$

Returns

GE [float] Excess Gibbs energy, [J/mol]

# $d2GE_dT2()$

Calculate and return the second temperature derivative of excess Gibbs energy of a liquid phase using the UNIQUAC model.

$$\frac{\partial G^E}{\partial T^2} = -R \left[ T \sum_i \left( \frac{q_i x_i (\sum_j \theta_j \frac{\partial^2 \tau_{ji}}{\partial T^2})}{\sum_j \theta_j \tau_{ji}} - \frac{q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})^2}{(\sum_j \theta_j \tau_{ji})^2} \right) + 2 \left( \sum_i \frac{q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{\sum_j \theta_j \tau_{ji}} \right) \right]$$

Returns

d2GE\_dT2 [float] Second temperature derivative of excess Gibbs energy, [J/(mol\*K^2)]

# d2GE\_dTdxs()

Calculate and return the temperature derivative of mole fraction derivatives of excess Gibbs energy using the UNIQUAC model.

$$\frac{\partial G^E}{\partial x_i \partial T} = R \left[ -T \left\{ \frac{q_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{\sum_j \tau_{ki} \theta_k} + \sum_j \frac{q_j x_j (\sum_k \frac{\partial \tau_{kj}}{\partial T} \frac{\partial \theta_k}{\partial x_i})}{\sum_k \tau_{kj} \theta_k} - \sum_j \frac{q_j x_j (\sum_k \tau_{kj} \frac{\partial \theta_k}{\partial x_i}) (\sum_k \theta_k \frac{\partial \tau_{kj}}{\partial T})}{(\sum_k \tau_{kj} \theta_k)^2} \right\} + \sum_j \frac{q_j x_j z \left(\frac{\partial \theta_j}{\partial x_i} \frac{\partial \theta_k}{\partial x_i}\right)}{2\theta_j} \left(\sum_k \tau_{kj} \frac{\partial \theta_k}{\partial x_i}\right) \left(\sum_k \theta_k \frac{\partial \tau_{kj}}{\partial T}\right)}{2\theta_j} \right\}$$

Returns

**d2GE\_dTdxs** [list[float]] Temperature derivative of mole fraction derivatives of excess Gibbs energy, [J/(mol\*K)]

#### d2GE\_dxixjs()

Calculate and return the second mole fraction derivatives of excess Gibbs energy using the UNIQUAC model.

$$\frac{\partial^2 g^E}{\partial x_i \partial x_j}$$

#### Returns

**d2GE\_dxixjs** [list[list[float]]] Second mole fraction derivatives of excess Gibbs energy, [J/mol]

## Notes

The formula is extremely long and painful; see the source code for details.

# d2taus\_dT2()

**Calculate and return the second temperature derivative of the** *tau* terms for the UNIQUAC model for a specified temperature.

$$\frac{\partial^2 \tau_{ij}}{\partial^2 T} = \left(2f_{ij} + \left(2Tf_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^2}\right)^2 - \frac{c_{ij}}{T^2} + \frac{2b_{ij}}{T^3} + \frac{6e_{ij}}{T^4}\right)e^{T^2f_{ij} + Td_{ij} + a_{ij} + c_{ij}\ln(T) + \frac{b_{ij}}{T} + \frac{e_{ij}}{T^2} + \frac{e_{ij}}{T^2} + \frac{2e_{ij}}{T^2} + \frac{2e_{ij}}{T^4} + \frac{e_{ij}}{T^4}\right)e^{T^2f_{ij} + Td_{ij} + a_{ij} + c_{ij}\ln(T) + \frac{b_{ij}}{T} + \frac{e_{ij}}{T^2} + \frac{e_{ij}}{T^4} + \frac{e_{$$

Returns

**d2taus\_dT2** [list[list[float]]] Second temperature derivatives of tau terms, asymmetric matrix [1/K^2]

#### Notes

These values (and the coefficients) are NOT symmetric.

## d3GE\_dT3()

Calculate and return the third temperature derivative of excess Gibbs energy of a liquid phase using the UNIQUAC model.

$$\frac{\partial^3 G^E}{\partial T^3} = -R \left[ T \sum_i \left( \frac{q_i x_i (\sum_j \theta_j \frac{\partial^3 \tau_{ji}}{\partial T^3})}{(\sum_j \theta_j \tau_{ji})} - \frac{3q_i x_i (\sum_j \theta_j \frac{\partial^2 \tau_{ji}}{\partial T^2}) (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} + \frac{2q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})^3}{(\sum_j \theta_j \tau_{ji})^3} \right) + \sum_i \left( \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} - \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} + \frac{2q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})^3}{(\sum_j \theta_j \tau_{ji})^3} \right) + \sum_i \left( \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} - \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} + \frac{2q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^3} \right) + \sum_i \left( \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} - \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} + \frac{2q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^3} \right) + \sum_i \left( \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} - \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} + \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^3} \right) + \sum_i \left( \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} - \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} + \frac{3q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{(\sum_j \theta_j \tau_{ji})^2} \right) \right]$$

Returns

**d3GE\_dT3** [float] Third temperature derivative of excess Gibbs energy, [J/(mol\*K^3)]

## d3taus\_dT3()

Calculate and return the third temperature derivative of the *tau* terms for the UNIQUAC model for a specified temperature.

$$\frac{\partial^3 \tau_{ij}}{\partial^3 T} = \left( 3\left(2f_{ij} - \frac{c_{ij}}{T^2} + \frac{2b_{ij}}{T^3} + \frac{6e_{ij}}{T^4}\right) \left(2Tf_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3}\right) + \left(2Tf_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3}\right)^3 - \frac{2e_{ij}}{T^3} + \frac{$$

Returns

**d3taus\_dT3** [list[list[float]]] Third temperature derivatives of tau terms, asymmetric matrix [1/K^3]

These values (and the coefficients) are NOT symmetric.

dGE\_dT()

Calculate and return the temperature derivative of excess Gibbs energy of a liquid phase using the UNI-QUAC model.

$$\frac{\partial G^E}{\partial T} = \frac{G^E}{T} - RT\left(\sum_i \frac{q_i x_i (\sum_j \theta_j \frac{\partial \tau_{ji}}{\partial T})}{\sum_j \theta_j \tau_{ji}}\right)$$

Returns

dGE\_dT [float] First temperature derivative of excess Gibbs energy, [J/(mol\*K)]

dGE\_dxs()

Calculate and return the mole fraction derivatives of excess Gibbs energy using the UNIQUAC model.

$$\frac{\partial G^E}{\partial x_i} = RT \left[ \sum_j \frac{q_j x_j \phi_j z}{2\theta_j} \left( \frac{1}{\phi_j} \cdot \frac{\partial \theta_j}{\partial x_i} - \frac{\theta_j}{\phi_j^2} \cdot \frac{\partial \phi_j}{\partial x_i} \right) - \sum_j \left( \frac{q_j x_j (\sum_k \tau_{kj} \frac{\partial \theta_k}{\partial x_i})}{\sum_k \tau_{kj} \theta_k} \right) + 0.5zq_i \ln \left( \frac{\theta_i}{\phi_i} \right) - q_i \ln \left( \sum_j \tau_{ji} \theta_j \right) \right] \right]$$

Returns

dGE\_dxs [list[float]] Mole fraction derivatives of excess Gibbs energy, [J/mol]

## dtaus\_dT()

Calculate and return the temperature derivative of the *tau* terms for the UNIQUAC model for a specified temperature.

$$\frac{\partial \tau_{ij}}{\partial T} = \left(2Th_{ij} + d_{ij} + \frac{c_{ij}}{T} - \frac{b_{ij}}{T^2} - \frac{2e_{ij}}{T^3}\right)e^{T^2h_{ij} + Td_{ij} + a_{ij} + c_{ij}\ln(T) + \frac{b_{ij}}{T} + \frac{e_{ij}}{T^2}}$$

#### Returns

**dtaus\_dT** [list[list[float]]] First temperature derivatives of tau terms, asymmetric matrix [1/K]

## Notes

These values (and the coefficients) are NOT symmetric.

## phis()

Calculate and return the *phi* parameters at the system composition and temperature.

$$\phi_i = \frac{r_i x_i}{\sum_j r_j x_j}$$

Returns

phis [list[float]] phi parameters, [-]

classmethod regress\_binary\_parameters(gammas, xs, rs, qs, use\_numba=False, do\_statistics=True,

\*\*kwargs)

Perform a basic regression to determine the values of the *tau* terms in the UNIQUAC model, given a series of known or predicted activity coefficients and mole fractions.

#### **Parameters**

gammas [list[list[float, 2]]] List of activity coefficient pairs, [-]

- xs [list[list[float, 2]]] List of binary mole fraction pairs, [-]
- rs [list[float]] Van der Waals volume parameters for each species, [-]
- qs [list[float]] Surface area parameters for each species, [-]
- **use\_numba** [bool, optional] Whether or not to try to use numba to speed up the computation, [-]
- **do\_statistics** [bool, optional] Whether or not to compute statistical measures on the outputs, [-]

kwargs [dict] Extra parameters to be passed to the fitting function (not yet documented), [-]

#### Returns

- **parameters** [dict[str, float]] Dimentionless interaction parameters of each compound with each other; these are the actual *tau* values. [-]
- statistics [dict[str: float]] Statistics, calculated and returned only if *do\_statistics* is True, [-]

#### Notes

Notes on getting fitting coefficients that yield gammas of 1:

- This is possible some of the time to a pretty high accuracy
- This is not possible whatsoever in some cases
- The values of rs, and qs determine how close the fitting can be
- If *rs* and *qs* are close to each other, it may well fit nicely
- If they are distant (1.2-1.5x) they usually will not fit

## **Examples**

In the following example, the *tau* values required to zero-out the coefficients for the n-pentane and nhexane system are calculated. The parameters are converted back into *aij* parameters as used by this activity coefficient object, and then the calculated values are verified to be fairly nearly one.

```
>>> from thermo import UNIQUAC
>>> import numpy as np
>>> pts = 30
>>> rs = [3.8254, 4.4998]
>>> qs = [3.316, 3.856]
>>> xs = [[xi, 1.0 - xi] for xi in np.linspace(1e-7, 1-1e-7, pts)]
>>> gammas = [[1, 1] for i in range(pts)]
>>> coeffs, stats = UNIQUAC.regress_binary_parameters(gammas, xs, rs, qs)
>>> coeffs
{ 'tau12': 1.04220685, 'tau21': 0.95538082}
>>> assert stats['MAE'] < 1e-6</pre>
>>> tausB = tausC = tausD = tausE = tausF = [[0.0]*2 for i in range(2)]
>>> tausA = [[0, np.log(coeffs['tau12'])], [np.log(coeffs['tau21']), 0]]
>>> ABCDEF = (tausA, tausB, tausC, tausD, tausE, tausF)
>>> GE = UNIQUAC(T=300, xs=[.5, .5], rs=rs, qs=qs, ABCDEF=ABCDEF)
>>> GE.gammas()
[1.000000466, 1.000000180]
```

Note how the *tau* coefficients need to be converted into the *a* parameters of the *tau* equation. They could also have been converted into any of the other parameters, but then the activity coefficients predicted would no longer be close to 1 at other temperatures.

$$\tau_{ij} = \exp\left[a_{ij} + \frac{b_{ij}}{T} + c_{ij}\ln T + d_{ij}T + \frac{e_{ij}}{T^2} + f_{ij}T^2\right]$$

The UNIQUAC model's r and q parameters create their own biases in the model, based on the structure of each of the pure species. Water and n-pentane are not miscible liquids; they will form two liquid phases except when one component is present in trace amounts. No matter the values of *tau*, it is not possible to make the UNIQUAC equation predict activity coefficients very close to one for this system, as shown in the following sample.

>>> rs = [3.8254, 0.92]
>>> qs = [3.316, 1.4]
>>> pts = 6
>>> xs = [[xi, 1.0 - xi] for xi in np.linspace(1e-7, 1-1e-7, pts)]
>>> gammas = [[1, 1] for i in range(pts)]
>>> coeffs, stats = UNIQUAC.regress\_binary\_parameters(gammas, xs, rs, qs)
>>> stats['MAE']
0.0254

#### taus()

Calculate and return the tau terms for the UNIQUAC model for the system temperature.

$$\tau_{ij} = \exp\left[a_{ij} + \frac{b_{ij}}{T} + c_{ij}\ln T + d_{ij}T + \frac{e_{ij}}{T^2} + f_{ij}T^2\right]$$

#### Returns

taus [list[list[float]]] tau terms, asymmetric matrix [-]

## **Notes**

These *tau ij* values (and the coefficients) are NOT symmetric.

#### thetas()

Calculate and return the *theta* parameters at the system composition and temperature.

$$\theta_i = \frac{q_i x_i}{\sum_j q_j x_j}$$

#### Returns

thetas [list[float]] theta parameters, [-]

 $to_T_xs(T, xs)$ 

Method to construct a new UNIQUAC instance at temperature T, and mole fractions xs with the same parameters as the existing object.

#### Parameters

T [float] Temperature, [K]

xs [list[float]] Mole fractions of each component, [-]

#### Returns

obj [UNIQUAC] New UNIQUAC object at the specified conditions [-]

If the new temperature is the same temperature as the existing temperature, if the *tau* terms or their derivatives have been calculated, they will be set to the new object as well.

# 7.36.2 UNIQUAC Functional Calculations

## thermo.uniquac.UNIQUAC\_gammas(xs, rs, qs, taus)

Calculates the activity coefficients of each species in a mixture using the Universal quasi-chemical (UNIQUAC) equation, given their mole fractions, *rs*, *qs*, and dimensionless interaction parameters. The interaction parameters are normally correlated with temperature, and need to be calculated separately.

$$\ln \gamma_i = \ln \frac{\Phi_i}{x_i} + \frac{z}{2} q_i \ln \frac{\theta_i}{\Phi_i} + l_i - \frac{\Phi_i}{x_i} \sum_j^N x_j l_j - q_i \ln \left(\sum_j^N \theta_j \tau_{ji}\right) + q_i - q_i \sum_j^N \frac{\theta_j \tau_{ij}}{\sum_k^N \theta_k \tau_{kj}}$$
$$\theta_i = \frac{x_i q_i}{\sum_{j=1}^N x_j q_j}$$
$$\Phi_i = \frac{x_i r_i}{\sum_{j=1}^N x_j r_j}$$
$$l_i = \frac{z}{2} (r_i - q_i) - (r_i - 1)$$

#### Parameters

xs [list[float]] Liquid mole fractions of each species, [-]

- rs [list[float]] Van der Waals volume parameters for each species, [-]
- qs [list[float]] Surface area parameters for each species, [-]
- taus [list[list[float]]] Dimensionless interaction parameters of each compound with each other,
   [-]

## Returns

gammas [list[float]] Activity coefficient for each species in the liquid mixture, [-]

## Notes

This model needs N^2 parameters.

The original expression for the interaction parameters is as follows:

$$\tau_{ji} = \exp\left(\frac{-\Delta u_{ij}}{RT}\right)$$

However, it is seldom used. Most correlations for the interaction parameters include some of the terms shown in the following form:

$$\ln \tau_{ij} = a_{ij} + \frac{b_{ij}}{T} + c_{ij} \ln T + d_{ij}T + \frac{e_{ij}}{T^2}$$

This model is recast in a slightly more computationally efficient way in [2], as shown below:

$$\ln \gamma_i = \ln \gamma_i^{res} + \ln \gamma_i^{comb}$$
$$\ln \gamma_i^{res} = q_i \left( 1 - \ln \frac{\sum_j^N q_j x_j \tau_{ji}}{\sum_j^N q_j x_j} - \sum_j \frac{q_k x_j \tau_{ij}}{\sum_k q_k x_k \tau_{kj}} \right)$$
$$\ln \gamma_i^{comb} = (1 - V_i + \ln V_i) - \frac{z}{2} q_i \left( 1 - \frac{V_i}{F_i} + \ln \frac{V_i}{F_i} \right)$$
$$V_i = \frac{r_i}{\sum_j^N r_j x_j}$$
$$F_i = \frac{q_i}{\sum_j q_j x_j}$$

There is no global set of parameters which will make this model yield ideal acitivty coefficients (gammas = 1) for this model.

#### References

[1], [2], [3]

## **Examples**

Ethanol-water example, at 343.15 K and 1 MPa:

```
>>> UNIQUAC_gammas(xs=[0.252, 0.748], rs=[2.1055, 0.9200], qs=[1.972, 1.400],
... taus=[[1.0, 1.0919744384510301], [0.37452902779205477, 1.0]])
[2.35875137797083, 1.2442093415968987]
```

# 7.37 Joback Group Contribution Method (thermo.group\_contribution.joback)

This module contains an implementation of the Joback group-contribution method. This functionality requires the RDKit library to work.

For submitting pull requests, please use the GitHub issue tracker.

**Warning:** The Joback class method does not contain all the groups for every chemical. There are often multiple ways of fragmenting a chemical. Other times, the fragmentation algorithm will fail. These limitations are present in both the implementation and the method itself. You are welcome to seek to improve this code but no to little help can be offered.

class thermo.group\_contribution.joback.Joback(mol, atom\_count=None, MW=None, Tb=None)
Bases: object

Class for performing chemical property estimations with the Joback group contribution method as described in [1] and [2]. This is a very common method with low accuracy but wide applicability. This routine can be used with either its own automatic fragmentation routine, or user specified groups. It is applicable to organic compounds only, and has only 41 groups with no interactions between them. Each method's documentation describes its accuracy. The automatic fragmentation routine is possible only because of the development of SMARTS expressions to match the Joback groups by Dr. Jason Biggs. The list of SMARTS expressions was posted publically on the RDKit mailing list.

#### Parameters

mol [rdkitmol or smiles str] Input molecule for the analysis, [-]

- **atom\_count** [int, optional] The total number of atoms including hydrogen in the molecule; this will be counted by rdkit if it not provided, [-]
- **MW** [float, optional] Molecular weight of the molecule; this will be calculated by rdkit if not provided, [g/mol]
- **Tb** [float, optional] An experimentally known boiling temperature for the chemical; this increases the accuracy of the calculated critical point if provided. [K]

## Notes

Be sure to check the status of the automatic fragmentation; not all chemicals with the Joback method are applicable.

Approximately 68% of chemcials in the thermo database seem to be able to be estimated with the Joback method.

If a group which was identified is missign a regressed contribution, the estimated property will be None. However, if not all atoms of a molecule are identified as particular groups, property estimation will go ahead with heavily reduced accuracy. Check the *status* attribute to be sure a molecule was properly fragmented.

## References

[1], [2]

## **Examples**

Analysis of Acetone:

```
>>> J = Joback('CC(=0)C')
>>> J.Hfus(J.counts)
5125.0
>>> J.Cpig(350)
84.69109750000001
>>> J.status
'OK'
```

All properties can be obtained in one go with the *estimate* method:

The results for propionic anhydride (if the status is not OK) should not be used.

```
>>> J = Joback('CCC(=0)OC(=0)CC')
>>> J.status
'Matched some atoms repeatedly: [4]'
>>> J.Cpig(300)
175.859999999999999
```

None of the routines need to use the automatic routine; they can be used manually too:

```
>>> Joback.Tb({1: 2, 24: 1})
322.11
```

# Attributes

calculated\_Cpig\_coeffs calculated\_mul\_coeffs

# Methods

Cpig(T)	Computes ideal-gas heat capacity at a specified tem-
	perature of an organic compound using the Joback
	method as a function of chemical structure only.
Cpig_coeffs(counts)	Computes the ideal-gas polynomial heat capacity co-
	efficients of an organic compound using the Joback
	method as a function of chemical structure only.
<i>Gf</i> (counts)	Estimates the ideal-gas Gibbs energy of formation at
	298.15 K of an organic compound using the Joback
	method as a function of chemical structure only.
<i>Hf</i> (counts)	Estimates the ideal-gas enthalpy of formation at
	298.15 K of an organic compound using the Joback
	method as a function of chemical structure only.
Hfus(counts)	Estimates the enthalpy of fusion of an organic com-
	pound at its melting point using the Joback method
	as a function of chemical structure only.
<i>Hvap</i> (counts)	Estimates the enthalpy of vaporization of an or-
	ganic compound at its normal boiling point using the
	Joback method as a function of chemical structure
	only.
<i>Pc</i> (counts, atom_count)	Estimates the critcal pressure of an organic com-
	pound using the Joback method as a function of
	chemical structure only.
<i>Tb</i> (counts)	Estimates the normal boiling temperature of an or-
	ganic compound using the Joback method as a func-
	tion of chemical structure only.
<i>Tc</i> (counts[, Tb])	Estimates the critcal temperature of an organic com-
	pound using the Joback method as a function of
	chemical structure only, or optionally improved by
_ /	using an experimental boiling point.
Tm(counts)	Estimates the melting temperature of an organic com-
	pound using the Joback method as a function of
	chemical structure only.
Vc(counts)	Estimates the critcal volume of an organic compound
	using the Joback method as a function of chemical
	structure only.
estimate([callables])	Method to compute all available properties with the
	Joback method; returns their results as a dict.

	Table 114 continued nom previous page
mul(T)	Computes liquid viscosity at a specified temperature
	of an organic compound using the Joback method as
	a function of chemical structure only.
<pre>mul_coeffs(counts)</pre>	Computes the liquid phase viscosity Joback coef-
	ficients of an organic compound using the Joback
	method as a function of chemical structure only.

# Table 114 - continued from previous page

## Cpig(T)

Computes ideal-gas heat capacity at a specified temperature of an organic compound using the Joback method as a function of chemical structure only.

$$C_p^{ig} = \sum_i a_i - 37.93 + \left[\sum_i b_i + 0.210\right] T + \left[\sum_i c_i - 3.91 \cdot 10^{-4}\right] T^2 + \left[\sum_i d_i + 2.06 \cdot 10^{-7}\right] T^3$$

**Parameters** 

T [float] Temperature, [K]

Returns

Cpig [float] Ideal-gas heat capacity, [J/mol/K]

## **Examples**

```
>>> J = Joback('CC(=0)C')
>>> J.Cpig(300)
75.32642000000001
```

## static Cpig\_coeffs(counts)

Computes the ideal-gas polynomial heat capacity coefficients of an organic compound using the Joback method as a function of chemical structure only.

$$C_p^{ig} = \sum_i a_i - 37.93 + \left[\sum_i b_i + 0.210\right] T + \left[\sum_i c_i - 3.91 \cdot 10^{-4}\right] T^2 + \left[\sum_i d_i + 2.06 \cdot 10^{-7}\right] T^3$$

288 compounds were used by Joback in this determination. No overall error was reported.

The ideal gas heat capacity values used in developing the heat capacity polynomials used 9 data points between 298 K and 1000 K.

## **Parameters**

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

## Returns

**coefficients** [list[float]] Coefficients which will result in a calculated heat capacity in in units of J/mol/K, [-]

```
>>> c = Joback.Cpig_coeffs({1: 2, 24: 1})
>>> c
[7.52000000000003, 0.26084, -0.0001207, 1.5459999999999998e-08]
>>> Cp = lambda T : c[0] + c[1]*T + c[2]*T**2 + c[3]*T**3
>>> Cp(300)
75.32642000000001
```

#### static Gf(counts)

Estimates the ideal-gas Gibbs energy of formation at 298.15 K of an organic compound using the Joback method as a function of chemical structure only.

$$G_{formation} = 53.88 + \sum G_{f,i}$$

In the above equation, Gibbs energy of formation is calculated in kJ/mol; it is converted to J/mol here.

328 compounds were used by Joback in this determination, with an absolute average error of 2.0 kcal/mol, standard devaition 4.37 kcal/mol, and AARE of 15.7%.

## **Parameters**

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

Gf [float] Estimated ideal-gas Gibbs energy of formation at 298.15 K, [J/mol]

## **Examples**

```
>>> Joback.Gf({1: 2, 24: 1})
-154540.0000000003
```

## static Hf(counts)

Estimates the ideal-gas enthalpy of formation at 298.15 K of an organic compound using the Joback method as a function of chemical structure only.

$$H_{formation} = 68.29 + \sum_{i} H_{f,i}$$

In the above equation, enthalpy of formation is calculated in kJ/mol; it is converted to J/mol here.

370 compounds were used by Joback in this determination, with an absolute average error of 2.2 kcal/mol, standard devaition 2.0 kcal/mol, and AARE of 15.2%.

#### Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

Hf [float] Estimated ideal-gas enthalpy of formation at 298.15 K, [J/mol]

```
>>> Joback.Hf({1: 2, 24: 1})
-217829.99999999997
```

# static Hfus(counts)

Estimates the enthalpy of fusion of an organic compound at its melting point using the Joback method as a function of chemical structure only.

$$\Delta H_{fus} = -0.88 + \sum_{i} H_{fus,i}$$

In the above equation, enthalpy of fusion is calculated in kJ/mol; it is converted to J/mol here.

For 155 compounds tested by Joback, the absolute average error was 485.2 cal/mol and standard deviation was 661.4 cal/mol; the average relative error was 38.7%.

#### **Parameters**

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

Hfus [float] Estimated enthalpy of fusion of the compound at its melting point, [J/mol]

## **Examples**

```
>>> Joback.Hfus({1: 2, 24: 1})
5125.0
```

#### static Hvap(counts)

Estimates the enthalpy of vaporization of an organic compound at its normal boiling point using the Joback method as a function of chemical structure only.

$$\Delta H_{vap} = 15.30 + \sum_{i} H_{vap,i}$$

In the above equation, enthalpy of fusion is calculated in kJ/mol; it is converted to J/mol here.

For 368 compounds tested by Joback, the absolute average error was 303.5 cal/mol and standard deviation was 429 cal/mol; the average relative error was 3.88%.

#### Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

## Returns

**Hvap** [float] Estimated enthalpy of vaporization of the compound at its normal boiling point, [J/mol]

```
>>> Joback.Hvap({1: 2, 24: 1})
29018.0
```

# static Pc(counts, atom\_count)

Estimates the critcal pressure of an organic compound using the Joback method as a function of chemical structure only. This correlation was developed using the actual number of atoms forming the molecule as well.

$$P_c = \left[0.113 + 0.0032N_A - \sum_i P_{c,i}\right]^{-2}$$

In the above equation, critical pressure is calculated in bar; it is converted to Pa here.

392 compounds were used by Joback in this determination, with an absolute average error of 2.06 bar, standard devaition 3.2 bar, and AARE of 5.2%.

#### Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

atom\_count [int] Total number of atoms (including hydrogens) in the molecule, [-]

#### Returns

Pc [float] Estimated critical pressure, [Pa]

#### **Examples**

```
>>> Joback.Pc({1: 2, 24: 1}, 10)
4802499.604994407
```

## static Tb(counts)

Estimates the normal boiling temperature of an organic compound using the Joback method as a function of chemical structure only.

$$T_b = 198.2 + \sum_i T_{b,i}$$

For 438 compounds tested by Joback, the absolute average error was 12.91 K and standard deviation was 17.85 K; the average relative error was 3.6%.

## Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

**Tb** [float] Estimated normal boiling temperature, [K]

#### **Examples**

```
>>> Joback.Tb({1: 2, 24: 1})
322.11
```

#### static Tc(counts, Tb=None)

Estimates the critcal temperature of an organic compound using the Joback method as a function of chemical structure only, or optionally improved by using an experimental boiling point. If the experimental boiling point is not provided it will be estimated with the Joback method as well.

$$T_{c} = T_{b} \left[ 0.584 + 0.965 \sum_{i} T_{c,i} - \left( \sum_{i} T_{c,i} \right)^{2} \right]^{-1}$$

For 409 compounds tested by Joback, the absolute average error was 4.76 K and standard deviation was 6.94 K; the average relative error was 0.81%.

Appendix BI of Joback's work lists 409 estimated critical temperatures.

#### Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

**Tb** [float, optional] Experimental normal boiling temperature, [K]

#### Returns

Tc [float] Estimated critical temperature, [K]

#### **Examples**

```
>>> Joback.Tc({1: 2, 24: 1}, Tb=322.11)
500.5590049525365
```

#### static Tm(counts)

Estimates the melting temperature of an organic compound using the Joback method as a function of chemical structure only.

$$T_m = 122.5 + \sum_i T_{m,i}$$

For 388 compounds tested by Joback, the absolute average error was 22.6 K and standard deviation was 24.68 K; the average relative error was 11.2%.

#### Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

Tm [float] Estimated melting temperature, [K]

#### **Examples**

```
>>> Joback.Tm({1: 2, 24: 1})
173.5
```

#### static Vc(counts)

Estimates the critcal volume of an organic compound using the Joback method as a function of chemical structure only.

$$V_c = 17.5 + \sum_i V_{c,i}$$

In the above equation, critical volume is calculated in cm<sup>3</sup>/mol; it is converted to m<sup>3</sup>/mol here.

310 compounds were used by Joback in this determination, with an absolute average error of 7.54 cm<sup>3</sup>/mol, standard devaition 13.16 cm<sup>3</sup>/mol, and AARE of 2.27%.

#### **Parameters**

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

Vc [float] Estimated critical volume, [m^3/mol]

#### **Examples**

```
>>> Joback.Vc({1: 2, 24: 1})
0.0002095
```

#### calculated\_Cpig\_coeffs = None

#### calculated\_mul\_coeffs = None

#### estimate(callables=True)

Method to compute all available properties with the Joback method; returns their results as a dict. For the tempearture dependent values Cpig and mul, both the coefficients and objects to perform calculations are returned.

#### mul(T)

Computes liquid viscosity at a specified temperature of an organic compound using the Joback method as a function of chemical structure only.

$$\mu_{liq} = \mathbf{MW} \exp\left(\frac{\sum_{i} \mu_a - 597.82}{T} + \sum_{i} \mu_b - 11.202\right)$$

#### **Parameters**

T [float] Temperature, [K]

#### Returns

mul [float] Liquid viscosity, [Pa\*s]

#### **Examples**

```
>>> J = Joback('CC(=0)C')
>>> J.mul(300)
0.0002940378347162687
```

#### static mul\_coeffs(counts)

Computes the liquid phase viscosity Joback coefficients of an organic compound using the Joback method as a function of chemical structure only.

$$\mu_{liq} = \mathbf{MW} \exp\left(\frac{\sum_{i} \mu_a - 597.82}{T} + \sum_{i} \mu_b - 11.202\right)$$

288 compounds were used by Joback in this determination. No overall error was reported.

The liquid viscosity data used was specified to be at "several temperatures for each compound" only. A small and unspecified number of compounds were used in this estimation.

#### Parameters

**counts** [dict] Dictionary of Joback groups present (numerically indexed) and their counts, [-]

#### Returns

**coefficients** [list[float]] Coefficients which will result in a liquid viscosity in in units of Pa\*s, [-]

#### **Examples**

```
>>> mu_ab = Joback.mul_coeffs({1: 2, 24: 1})
>>> mu_ab
[839.1099999999998, -14.99]
>>> MW = 58.041864812
>>> mul = lambda T : MW*exp(mu_ab[0]/T + mu_ab[1])
>>> mul(300)
0.0002940378347162687
```

```
thermo.group_contribution.joback.J_BIGGS_JOBACK_SMARTS = [['Methyl', '-CH3', '[CX4H3]'],
['Secondary acyclic', '-CH2-', '[!R;CX4H2]'], ['Tertiary acyclic', '>CH-', '[!R;CX4H]'],
['Quaternary acyclic', '>C<', '[!R;CX4H0]'], ['Primary alkene', '=CH2', '[CX3H2]'],
['Secondary alkene acyclic', '=CH-', '[!R;CX3H1;!$([CX3H1](=0))]'], ['Tertiary alkene
acyclic', '=C<', '[$([!R;CX3H0]);!$([!R;CX3H0]=[#8])]'], ['Cumulative alkene', '=C=',</pre>
'[$([CX2H0](=*)=*)]'], ['Terminal alkyne', 'CH', '[$([CX2H1]#[!#7])]'], ['Internal
alkyne', 'C-', '[$([CX2H0]#[!#7])]'], ['Secondary cyclic', '-CH2- (ring)', '[R;CX4H2]'],
['Tertiary cyclic', '>CH- (ring)', '[R;CX4H]'], ['Quaternary cyclic', '>C< (ring)',
'[R;CX4H0]'], ['Secondary alkene cyclic', '=CH- (ring)', '[R;CX3H1,cX3H1]'], ['Tertiary
alkene cyclic', '=C< (ring)', '[$([R;CX3H0]);!$([R;CX3H0]=[#8])]'], ['Fluoro', '-F',</pre>
'[F]'], ['Chloro', '-Cl', '[Cl]'], ['Bromo', '-Br', '[Br]'], ['Iodo', '-I', '[I]'],
['Alcohol', '-OH (alcohol)', '[OX2H;!$([OX2H]-[#6]=[0]);!$([OX2H]-a)]'], ['Phenol', '-OH
(phenol)', '[$([0X2H]-a)]'], ['Ether acyclic', '-0- (nonring)',
'[OX2H0;!R;!$([OX2H0]-[#6]=[#8])]'], ['Ether cyclic', '-0- (ring)',
'[#8X2H0;R;!$([#8X2H0]~[#6]=[#8])]'], ['Carbonyl acyclic', '>C=O (nonring)',
'[$([CX3H0](=[0X1]));!$([CX3](=[0X1])-[0X2]);!R]=0'], ['Carbonyl cyclic', '>C=0 (ring)',
'[$([#6X3H0](=[0X1]));!$([#6X3](=[#8X1])~[#8X2]);R]=0'], ['Aldehyde', '0=CH- (aldehyde)',
'[CX3H1](=0)'], ['Carboxylic acid', '-COOH (acid)', '[OX2H]-[C]=0'], ['Ester', '-COO-
(ester)', '[#6X3H0;!$([#6X3H0](~0)(~0)(~0))](=[#8X1])[#8X2H0]'], ['Oxygen double bond
other', '=0 (other than above)', '[OX1H0;!$([OX1H0]~[#6X3]);!$([OX1H0]~[#7X3]~[#8])]'],
['Primary amino', '-NH2', '[NX3H2]'], ['Secondary amino acyclic', '>NH (nonring)',
'[NX3H1;!R]'], ['Secondary amino cyclic', '>NH (ring)', '[#7X3H1;R]'], ['Tertiary amino',
'>N- (nonring)', '[#7X3H0;!$([#7](~0)~0)]'], ['Imine acyclic', '-N= (nonring)',
'[#7X2H0;!R]'], ['Imine cyclic', '-N= (ring)', '[#7X2H0;R]'], ['Aldimine', '=NH',
'[#7X2H1]'], ['Cyano', '-CN', '[#6X2]#[#7X1H0]'], ['Nitro', '-NO2',
'[$([#7X3,#7X3+][!#8])](=[0])~[0-]'], ['Thiol', '-SH', '[SX2H]'], ['Thioether acyclic',
'-S- (nonring)', '[#16X2H0;!R]'], ['Thioether cyclic', '-S- (ring)', '[#16X2H0;R]']]
    Metadata for the Joback groups. The first element is the group name; the second is the group symbol; and the
    third is the SMARTS matching string.
thermo.group_contribution.joback.J_BIGGS_JOBACK_SMARTS_id_dict = {1: '[CX4H3]', 2:
'[!R;CX4H2]', 3: '[!R;CX4H]', 4: '[!R;CX4H0]', 5: '[CX3H2]', 6:
'[!R;CX3H1;!$([CX3H1](=0))]', 7: '[$([!R;CX3H0]);!$([!R;CX3H0]=[#8])]', 8:
'[$([CX2H0](=*)=*)]', 9: '[$([CX2H1]#[!#7])]', 10: '[$([CX2H0]#[!#7])]', 11: '[R;CX4H2]',
12: '[R;CX4H]', 13: '[R;CX4H0]', 14: '[R;CX3H1,cX3H1]', 15:
'[$([R;CX3H0]);!$([R;CX3H0]=[#8])]', 16: '[F]', 17: '[Cl]', 18: '[Br]', 19: '[I]', 20:
'[OX2H;!$([OX2H]-[#6]=[0]);!$([OX2H]-a)]', 21: '[$([OX2H]-a)]', 22:
'[OX2H0;!R;!$([OX2H0]-[#6]=[#8])]', 23: '[#8X2H0;R;!$([#8X2H0]~[#6]=[#8])]', 24:
'[$([CX3H0](=[OX1]));!$([CX3](=[OX1])-[OX2]);!R]=O', 25:
'[$([#6X3H0](=[0X1]));!$([#6X3](=[#8X1])~[#8X2]);R]=0', 26: '[CX3H1](=0)', 27:
'[0X2H]-[C]=0', 28: '[#6X3H0;!$([#6X3H0](~0)(~0)(~0))](=[#8X1])[#8X2H0]', 29:
'[0X1H0;!$([0X1H0]~[#6X3]);!$([0X1H0]~[#7X3]~[#8])]', 30: '[NX3H2]', 31: '[NX3H1;!R]',
32: '[#7X3H1;R]', 33: '[#7X3H0;!$([#7](~0)~0)]', 34: '[#7X2H0;!R]', 35: '[#7X2H0;R]', 36:
'[#7X2H1]', 37: '[#6X2]#[#7X1H0]', 38: '[$([#7X3,#7X3+][!#8])](=[0])~[0-]', 39: '[SX2H]',
```

```
40: '[#16X2H0;!R]', 41: '[#16X2H0;R]'}
```

## 7.38 Fedors Group Contribution Method (thermo.group\_contribution.fedors)

This module contains an implementation of the Fedors group-contribution method. This functionality requires the RDKit library to work.

thermo.group\_contribution.Fedors(mol)

Estimate the critical volume of a molecule using the Fedors [1] method, which is a basic group contribution method that also uses certain bond count features and the number of different types of rings.

#### Parameters

**mol** [str or rdkit.Chem.rdchem.Mol, optional] Smiles string representing a chemical or a rdkit molecule, [-]

#### Returns

- Vc [float] Estimated critical volume, [m^3/mol]
- **status** [str] A string holding an explanation of why the molecule failed to be fragmented, if it fails; 'OK' if it succeds, [-]
- **unmatched\_atoms** [bool] Whether or not all atoms in the molecule were matched successfully; if this is True, the results should not be trusted, [-]
- **unrecognized\_bond** [bool] Whether or not all bonds in the molecule were matched successfully; if this is True, the results should not be trusted, [-]
- **unrecognized\_ring\_size** [bool] Whether or not all rings in the molecule were matched successfully; if this is True, the results should not be trusted, [-]

#### Notes

Raises an exception if rdkit is not installed, or smi or rdkitmol is not defined.

#### References

[1], [2]

#### **Examples**

Example for sec-butanol in [2]:

```
>>> Vc, status, _, _, _ = Fedors('CCC(C)0')
>>> Vc, status
(0.000274024, 'OK')
```

# 7.39 Wilson-Jasperson Group Contribution Method (thermo.group\_contribution.wilson\_jasperson)

This module contains an implementation of the Wilson-Jasperson group-contribution method. This functionality requires the RDKit library to work.

#### thermo.group\_contribution.Wilson\_Jasperson(mol, Tb, second\_order=True)

Estimate the critical temperature and pressure of a molecule using the molecule itself, and a known or estimated boiling point using the Wilson-Jasperson method.

#### Parameters

**mol** [str or rdkit.Chem.rdchem.Mol, optional] Smiles string representing a chemical or a rdkit molecule, [-]

Tb [float] Known or estimated boiling point, [K]

second\_order [bool] Whether to use the first order method (False), or the second order method,
[-]

#### Returns

Tc [float] Estimated critical temperature, [K]

Pc [float] Estimated critical pressure, [Pa]

**missing\_Tc\_increments** [bool] Whether or not there were missing atoms for the *Tc* calculation, [-]

**missing\_Pc\_increments** [bool] Whether or not there were missing atoms for the *Pc* calculation, [-]

#### Notes

Raises an exception if rdkit is not installed, or smi or rdkitmol is not defined.

Calculated values were published in [3] for 448 compounds, as calculated by NIST TDE. There appear to be further modifications to the method in NIST TDE, as  $\sim 25\%$  of values have differences larger than 5 K.

#### References

[1], [2], [3]

#### **Examples**

Example for 2-ethylphenol in [2]:

```
>>> Tc, Pc, _, _ = Wilson_Jasperson('CCC1=CC=CC=C10', Tb=477.67)
>>> (Tc, Pc)
(693.567, 3743819.6667)
>>> Tc, Pc, _, _ = Wilson_Jasperson('CCC1=CC=CC=C10', Tb=477.67, second_order=False)
>>> (Tc, Pc)
(702.883, 3794106.49)
```

## **EXAMPLE USES OF THERMO**

The following Jupyter notebooks show some of the many calculations that can be done with Thermo.

These problems often make use of fluids, ht, chemicals, and pint so make sure you have them installed! More details on the unit handling library can be found at fluids.units.

## 8.1 Working with Heat Transfer Fluids - Therminol LT

Heat transfer fluids are pure species or chemical mixtures with specially tailored properties that make them suitable for use in heat exchangers. Usually this means not fouling, requiring little heat transfer area because of a high heat capacity, thermal conductivity, and potentially high density and low flammability.

Therminol LT is a fluid chosen for the demonstration. It is in fact a pure chemical, 1,2-diethylbenzene.

The data comes from therminol itself, in the following PDF.

```
https://web.archive.org/web/20210615044602/https://www.therminol.com/sites/therminol/files/documents/TF-8726_Therminol_LT.pdf
```

```
[1]: from fluids.core import C2K, F2K
    from fluids.constants import R
    import numpy as np
    from chemicals import rho_to_Vm, Vm_to_rho, property_mass_to_molar, omega_definition,_
     → simple_formula_parser, similarity_variable, molecular_weight
    from thermo import (TDependentProperty, VaporPressure, VolumeLiquid,
     → ChemicalConstantsPackage, PropertyCorrelationsPackage,
                         HeatCapacityLiquid, HeatCapacityGas, ThermalConductivityLiquid,
                         ThermalConductivityGas, ViscosityGas, ViscosityLiquid,
     → EnthalpyVaporization,
                         SurfaceTension)
    name = '1,2-diethylbenzene'
    CAS = "25340 - 17 - 4"
    formula = "C10H14"
    atoms = simple_formula_parser(formula)
    sv = similarity_variable(atoms)
    MW = molecular_weight(atoms)
    Tc = 377.0 + 273.15
    Pc = 34.5e5
    rhoc_mass = 298.0 # kg/m^3
    Vc = rho_to_Vm(rhoc_mass, MW)
    Zc = Pc*Vc/(R*Tc)
                                                                                  (continues on next page)
```

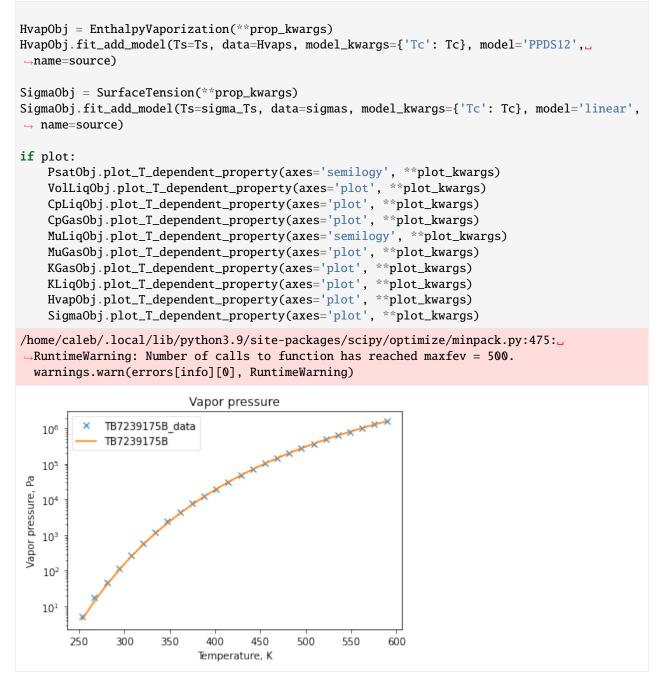
tindes on next page

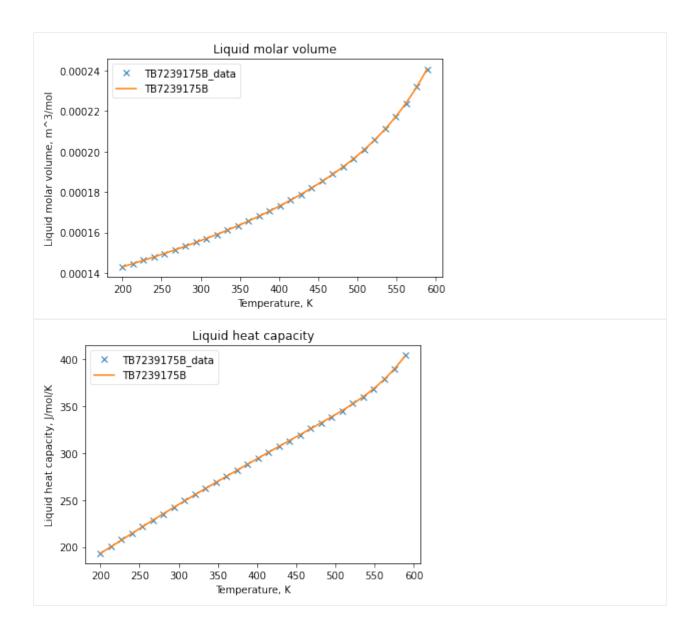
Tm = C2K(-75.0)Ts = [-73, -62, -51, -40, -29, -18, -7, 4, 16, 27, 38, 49, 60, 71, 82, 93, 104, 116, 127, → 138, 149, 160, 171, 181, 182, 193, 204, 216, 227, 238, 249, 260, 271, 282, 293, 304, **1 →**316] Ts = [C2K(v) for v in Ts]Psats = [0.002, 0.006, 0.016, 0.038, 0.084, 0.175, 0.345, 0.649, 1.17, 2.02, 3.37, 5.43, 0.084, 0.175, 0.345, 0.649, 1.17, 2.02, 3.37, 5.43, 0.084, 0.016, 0.016, 0.016, 0.016, 0.016, 0.016, 0.016, 0.016, 0.008, 0.016,→ 740, 904, 1090, 1310, 1570] Psats = [v\*1e3 for v in Psats] # kPa to Pa Ts\_Psats = Ts[len(Ts)-len(Psats):] # Obtain the acentric factor from linear interpolation for convenience  $Psat_07 = float(np.interp(0.7*Tc, Ts_Psats, Psats))$ omega = omega\_definition(Psat\_07, Pc) # Interpolate on pressure to find the normal boiling point Tb = float(np.interp(101325.0, Psats, Ts\_Psats)) rhols\_mass = [938, 930, 921, 913, 904, 896, 887, 878, 869, 860, 852, 843, 833, 824, 815, →806, 796, 786, 776, 766, 756, 746, 735, 726, 724, 713, 702, 690, 678, 666, 652, 639, ·  $\leftrightarrow 625, 610, 594, 576, 558$ ] Vms = [rho\_to\_Vm(rho, MW) for rho in rhols\_mass]  $Cpls_mass = [1.44, 1.48, 1.53, 1.57, 1.61, 1.66, 1.70, 1.74, 1.78, 1.83, 1.87, 1.91, 1.$ →95, 1.99, 2.03, 2.07, 2.11, 2.15, 2.19, 2.23, 2.27, 2.30, 2.34, 2.38, 2.38, 2.42, 2.46, → 2.50, 2.54, 2.58, 2.63, 2.67, 2.72, 2.78, 2.84, 2.91, 3.01] Cpls\_mass =  $[v*1000 \text{ for } v \text{ in } Cpls_mass] \# kJ/(kg*K)$ Cpls = [property\_mass\_to\_molar(Cp, MW) for Cp in Cpls\_mass] # J/(mol\*K)  $Cpgs_mass = [0.766, 0.813, 0.860, 0.908, 0.955, 1.002, 1.049, 1.095, 1.142, 1.188, 1.234, 1.234, 1.049, 1$ → 1.280, 1.325, 1.370, 1.415, 1.459, 1.503, 1.547, 1.590, 1.634, 1.676, 1.719, 1.761, 1. →799, 1.803, 1.845, 1.886, 1.928, 1.970, 2.012, 2.055, 2.099, 2.144, 2.191, 2.241, 2. →297, 2.362] Cpgs\_mass =  $[v*1000 \text{ for } v \text{ in } Cpgs_mass] \# kJ/(kg*K)$ Cpgs = [property\_mass\_to\_molar(Cp, MW) for Cp in Cpgs\_mass] # J/(mol\*K) kls = [0.1426, 0.1405, 0.1384, 0.1362, 0.1341, 0.1320, 0.1298, 0.1277, 0.1255, 0.1233, 0.→1212, 0.1190, 0.1168, 0.1146, 0.1124, 0.1102, 0.1080, 0.1058, 0.1036, 0.1013, 0.0991, J →0.0968, 0.0946, 0.0926, 0.0923, 0.0901, 0.0878, 0.0855, 0.0832, 0.0810, 0.0786, 0.0763,  $\leftrightarrow$  0.0740, 0.0717, 0.0694, 0.0670, 0.0647] muls = [10.09, 6.03, 3.99, 2.84, 2.13, 1.67, 1.35, 1.12, 0.947, 0.814, 0.708, 0.624, 0. →554, 0.496, 0.447, 0.405, 0.369, 0.338, 0.310, 0.286, 0.265, 0.246, 0.229, 0.215, 0. →213, 0.199, 0.187, 0.175, 0.165, 0.155, 0.146, 0.138, 0.131, 0.124, 0.117, 0.112, 0. **→106**] muls = [v\*1e-3 for v in muls] # mPa\*s to Pa\*s Hvaps\_mass = [492.7, 485.2, 477.8, 470.4, 463.0, 455.7, 448.5, 441.3, 434.1, 427.0, 420. →0, 412.9, 405.9, 399.0, 392.1, 385.2, 378.4, 371.6, 364.7, 357.9, 351.0, 344.1, 337.2, **.** -330.9, 330.1, 323.0, 315.7, 308.2, 300.5, 292.5, 284.3, 275.6, 266.4, 256(continue for dext page) →234.7, 221.8]

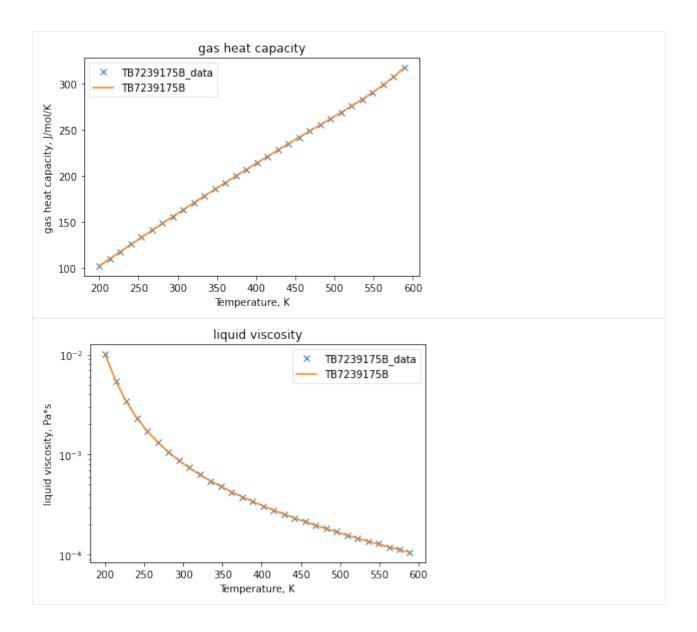
```
Hvaps_mass = [v*1000 \text{ for } v \text{ in } Hvaps_mass] \# kJ/(kg)
Hvaps = [property_mass_to_molar(Hvap, MW) for Hvap in Hvaps_mass] # J/(mol)
kgs = [0.0051, 0.0057, 0.0063, 0.0069, 0.0075, 0.0082, 0.0088, 0.0095, 0.0101, 0.0108, ]
→0.0115, 0.0122, 0.0130, 0.0137, 0.0144, 0.0152, 0.0160, 0.0168, 0.0176, 0.0184, 0.0192,
→ 0.0200, 0.0209, 0.0216, 0.0217, 0.0226, 0.0235, 0.0244, 0.0253, 0.0262, 0.0272, 0.
↔0281, 0.0291, 0.0301, 0.0310, 0.0321, 0.0331]
mugs = [0.00434, 0.00458, 0.00482, 0.00506, 0.00530, 0.00554, 0.00578, 0.00603, 0.00628, ...
→0.00652. 0.00677. 0.00702. 0.00727. 0.00752. 0.00777. 0.00802. 0.00828. 0.00853. 0.
→00878, 0.00903, 0.00928, 0.00952, 0.00977, 0.01000, 0.01002, 0.01027, 0.01051, 0.01076,
→ 0.01100, 0.01124, 0.01148, 0.01172, 0.01196, 0.01220, 0.01243, 0.01267, 0.01290]
mugs = [v*1e-3 for v in mugs] # mPa*s to Pa*s
sigmas = [0.028, 0.0]
sigma_Ts = [298.15, Tc]
prop_kwargs = {'Tc': Tc, 'Pc': Pc, 'Vc': Vc, 'Zc': Zc, 'omega': omega,
               'MW': MW, 'Tb': Tb, 'Tm': Tm, 'CASRN': CAS}
prop_kwargs = {} # Comment this out to show the estimation method results
plot_kwargs = {'pts': 30, 'Tmin': Ts[0]}
```

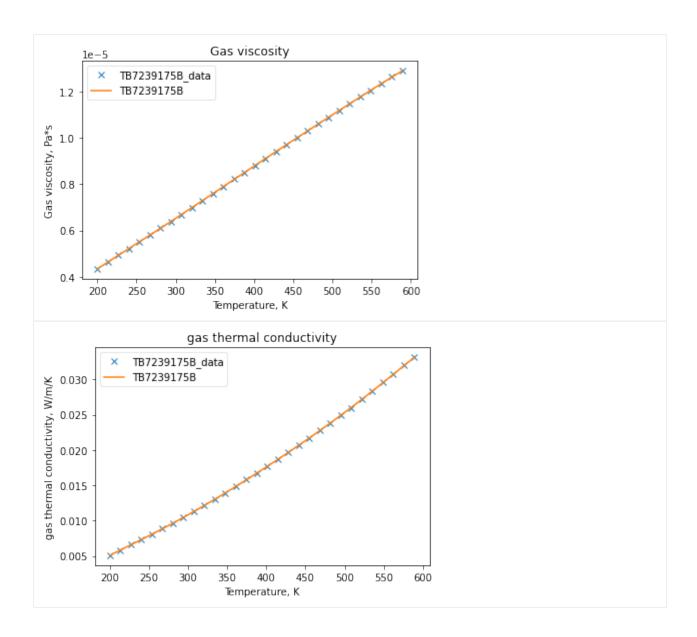
Now that the data has been added into Python objects, we can fit them to equations. The plots below show how good the fits are.

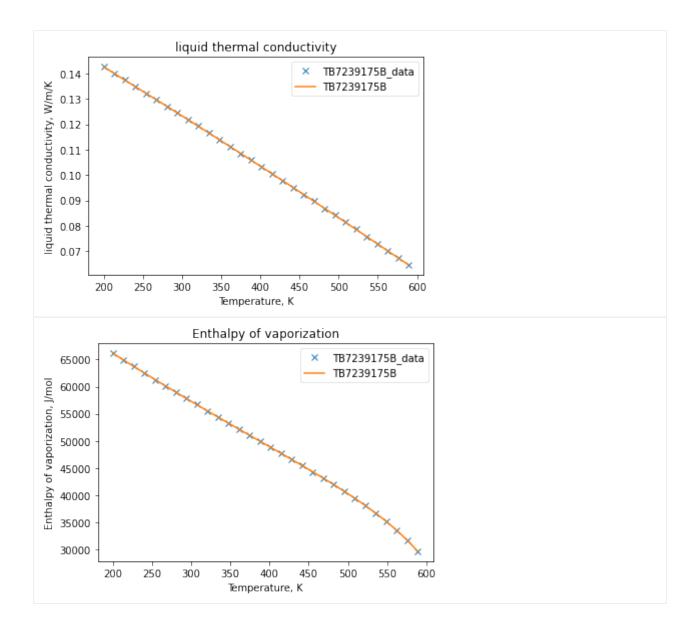
```
[2]: source = 'TB7239175B'
    plot = True
    Psat0bj = VaporPressure(**prop_kwargs)
    PsatObj.fit_add_model(Ts=Ts_Psats, data=Psats, model='DIPPR101', name=source)
    VolLiqObj = VolumeLiquid(**prop_kwargs)
    VolLigObj.fit_add_model(Ts=Ts, data=Vms, model='DIPPR100', name=source)
    CpLiqObj = HeatCapacityLiquid(**prop_kwargs)
    CpLiqObj.fit_add_model(Ts=Ts, data=Cpls, model='DIPPR100', name=source)
    CpGasObj = HeatCapacityGas(**prop_kwargs)
    CpGasObj.fit_add_model(Ts=Ts, data=Cpgs, model='DIPPR100', name=source)
    MuLiqObj = ViscosityLiquid(**prop_kwargs)
    MuLiqObj.fit_add_model(Ts=Ts, data=muls, model='mu_TDE', name=source)
    MuGasObj = ViscosityGas(**prop_kwargs)
    MuGasObj.fit_add_model(Ts=Ts, data=mugs, model='DIPPR100', name=source)
    KGasObj = ThermalConductivityGas(**prop_kwargs)
    KGasObj.fit_add_model(Ts=Ts, data=kgs, model='DIPPR100', name=source)
    KLiqObj = ThermalConductivityLiquid(**prop_kwargs)
    KLigObj.fit_add_model(Ts=Ts, data=kls, model='DIPPR100', name=source)
```

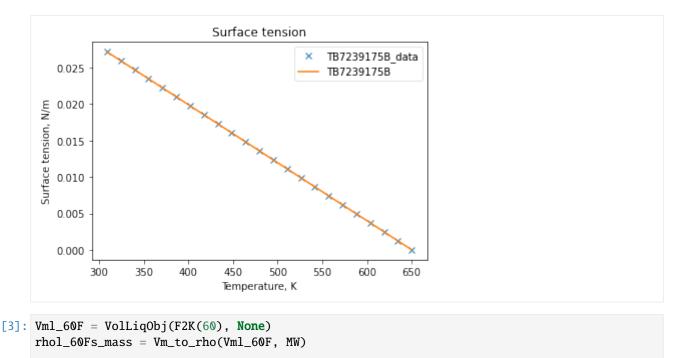












```
Vml_STP = VolLiqObj(298.15, None)
rhol_STPs_mass = Vm_to_rho(Vml_STP, MW)
```

```
constants = ChemicalConstantsPackage(Tcs=[Tc], Pcs=[Pc], Vcs=[Vc], Zcs=[Zc],
\leftrightarrow omegas=[omega], MWs=[MW],
                                      Vml_60Fs=[Vml_60F], rhol_60Fs=[1/Vml_60F], rhol_
\rightarrow 60Fs_mass=[rhol_60Fs_mass],
                                      Vml_STPs=[Vml_STP], rhol_STPs_mass=[rhol_STPs_mass],
                                      similarity_variables=[sv])
correlations = PropertyCorrelationsPackage(constants=constants, VaporPressures=[Psat0bj],
→ VolumeLiquids=[VolLiqObj],
                                         HeatCapacityLiquids=[CpLiqObj],_
→HeatCapacityGases=[CpGas0bj],
                                          ViscosityLiquids=[MuLiqObj],_
→ViscosityGases=[MuGasObj],
                                          ThermalConductivityGases=[KGasObj],
→ ThermalConductivityLiquids=[KLiqObj],
                                          EnthalpyVaporizations=[HvapObj],_
→SurfaceTensions=[SigmaObj])
```

Now that the ChemicalConstantsPackage and PropertyCorrelationsPackage have been created, we are ready to make packages and do calculations with them.

```
print(flasher_PR.flash(T=300, P=1e5))
```

```
<EquilibriumState, T=300.0000, P=100000.0000, zs=[1.0], betas=[1.0], phases=[<CEOSLiquid,

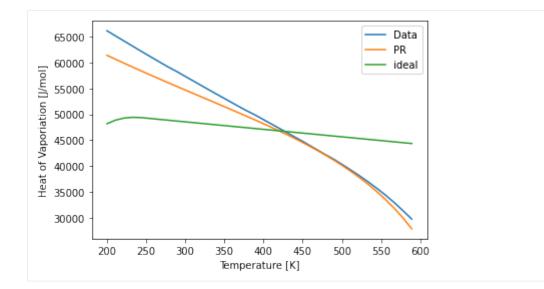
→ T=300 K, P=100000 Pa>]>
```

Using a thermodynamically consistent model is much more challenging than directly predicting a property. Liquid heat capacity, heat of vaporization, and density are all particularly challenging properties. The following plots show the accuracy of the models.

```
[9]: Cpls_calc_PR = []
    Cpls_calc_ideal = []
    for T in Ts:
        Cpls_calc_PR.append(flasher_PR.flash(T=T, VF=0).Cp())
        Cpls_calc_ideal.append(flasher_ideal.flash(T=T, VF=0).Cp())
    Hvaps_calc_PR = []
    Hvaps_calc_ideal = []
    for T in Ts:
        Hvaps_calc_PR.append(flasher_PR.flash(T=T, VF=1).H() - flasher_PR.flash(T=T, VF=0).
     →H())
        Hvaps_calc_ideal.append(flasher_ideal.flash(T=T, VF=1).H() - flasher_ideal.flash(T=T,
     → VF=(0).H())
    Vl_calc_PR = []
    Vl_calc_ideal = []
    for T in Ts:
        Vl_calc_PR.append(flasher_PR.flash(T=T, VF=0).V())
        Vl_calc_ideal.append(flasher_ideal.flash(T=T, VF=0).V())
[7]: import matplotlib.pyplot as plt
    plt.plot(Ts, Hvaps, label='Data')
    plt.plot(Ts, Hvaps_calc_PR, label='PR')
    plt.plot(Ts, Hvaps_calc_ideal, label='ideal')
    plt.xlabel("Temperature [K]")
```

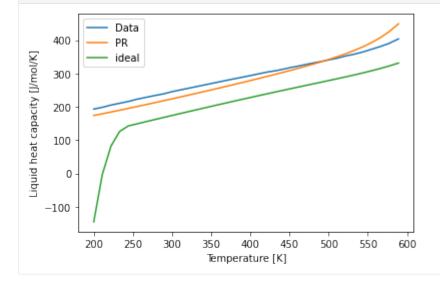
plt.legend()
plt.show()

plt.ylabel("Heat of Vaporiation [J/mol]")

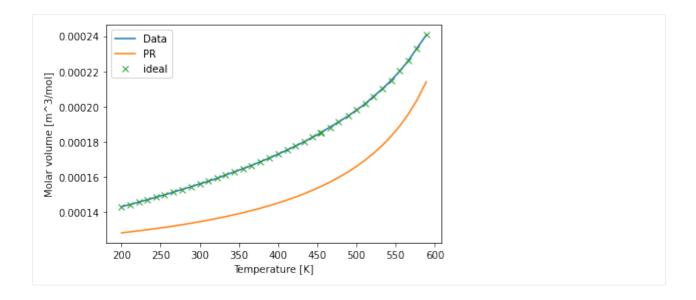


```
[8]: import matplotlib.pyplot as plt
plt.plot(Ts, Cpls, label='Data')
```

```
plt.plot(Ts, Cpls_calc_PR, label='PR')
plt.plot(Ts, Cpls_calc_ideal, label='ideal')
plt.xlabel("Temperature [K]")
plt.ylabel("Liquid heat capacity [J/mol/K]")
plt.legend()
plt.show()
```



```
[11]: import matplotlib.pyplot as plt
plt.plot(Ts, Vms, label='Data')
plt.plot(Ts, Vl_calc_PR, label='PR')
plt.plot(Ts, Vl_calc_ideal, 'x', label='ideal')
plt.xlabel("Temperature [K]")
plt.ylabel("Molar volume [m^3/mol]")
plt.legend()
plt.show()
```



## 8.2 Validating Flash Calculations

Finding the solution to multiphase equilibrium calculations is challenging and the topic of continuing research. Many commercial packages offer users a great deal of confidence in their answers, but can they be trusted? Thermo can be used to validate the results from other software or identify defects in them.

The following example uses a natural gas mixture two pseudocomponents C7-C16 and C17+. The properties of pure components are taken from Thermo. To do a perfect comparison, the critical properties from other software packages should be substituted into Thermo. This is example S3 from Fonseca-Pérez (2021). The kijs are from Harding and Floudas (2000), and the original pseudocomponents are from Nagarajan, Cullick, and Griewank (1991).

Fonseca-Pérez, R. M., A. Bonilla-Petriciolet, J. C. Tapia-Picazo, and J. E. Jaime-Leal. "A Reconsideration on the Resolution of Phase Stability Analysis Using Stochastic Global Optimization Methods: Proposal of a Reliable Set of Benchmark Problems." Fluid Phase Equilibria 548 (November 15, 2021): 113180. https://doi.org/10.1016/j.fluid. 2021.113180.

Harding, S. T., and C. A. Floudas. "Phase Stability with Cubic Equations of State: Global Optimization Approach." AIChE Journal 46, no. 7 (July 1, 2000): 1422–40. https://doi.org/10.1002/aic.690460715.

Nagarajan, N. R., A. S. Cullick, and A. Griewank. "New Strategy for Phase Equilibrium and Critical Point Calculations by Thermodynamic Energy Analysis. Part I. Stability Analysis and Flash." Fluid Phase Equilibria 62, no. 3 (January 1, 1991): 191–210. https://doi.org/10.1016/0378-3812(91)80010-S.

```
(continued from previous page)
```

```
P = 38500e3
      zs = [0.7212, 0.09205, 0.04455, 0.03123, 0.01273, 0.01361, 0.07215, 0.01248]
      kijs = [[0.0, 0.002, 0.017, 0.015, 0.02, 0.039, 0.05, 0.09],
      [0.002, 0.0, 0.0, 0.025, 0.01, 0.056, 0.04, 0.055],
      [0.017, 0.0, 0.0, 0.0, 0.0, 0.0, 0.01, 0.01],
      [0.015, 0.025, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0],
      [0.02, 0.01, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0],
      [0.039, 0.056, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0],
      [0.05, 0.04, 0.01, 0.0, 0.0, 0.0, 0.0, 0.0],
      [0.09, 0.055, 0.01, 0.0, 0.0, 0.0, 0.0, 0.0]]
      eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas,_
      →kijs=kijs)
      gas = CEOSGas(PRMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases, T=T,
      \rightarrow P=P, zs=zs)
      liq = CEOSLiquid(PRMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases, T=T,
      \rightarrow P=P, zs=zs)
      liq2 = CEOSLiquid(PRMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases, T=T,
      \rightarrow P=P, zs=zs)
      phase_list = [gas, liq, liq]
      flashN = FlashVLN(constants, properties, liquids=[liq, liq2], gas=gas)
      # flashN.PT_SS_TOL = 1e-18
      res = flashN.flash(T=T, P=P, zs=zs)
      print('There are %s phases present' %(res.phase_count))
      print('Mass densities of each liquid are %f and %f kg/m^3' %(res.liquid0.rho_mass(),_

→res.liquid0.rho_mass()))

      There are 2 phases present
      Mass densities of each liquid are 527.867861 and 527.867861 kg/m^3
[45]: import numpy as np
      max_fugacity_err = np.max(np.abs(1-np.array(res.liquid0.fugacities())/res.liquid1.
      →fugacities()))
```

print('The maximum relative difference in fugacity is %e.' %(max\_fugacity\_err,))

The maximum relative difference in fugacity is 2.773985e-07.

## 8.3 High Molecular Weight Petroleum Pseudocomponents

Thermo is a general phase equilibrium engine, and if the user provides enough properties for the components, there is no issue adding your own components. In this basic example below, a made-up extended gas analysis is used to specify a gas consisting of the standard real components and three heavier fractions, C10+, C12+ and C15+.

A bare minimum of basic properties are estimated using the Kesler-Lee method (1976), and the estimated fraction molecular weights are turned into atomic compositions. The heat capacities of each pseudocomponent is found with the similarity variable concept of Lastovka and Shaw (2013) based on atomic composition.

This example ends with calculating a flash at 270 Kelvin and 1 bar.

```
[72]: from math import log, exp
      import numpy as np
      from scipy.constants import psi
      from thermo import *
      from chemicals import *
      def Tc_Kesler_Lee_SG_Tb(SG, Tb):
         r"Estimates critical temperature of a hydrocarbon compound or petroleum
         fraction using only its specific gravity and boiling point, from
          [1]_ as presented in [2]_.
          .. math::
             T_c = 341.7 + 811.1SG + [0.4244 + 0.1174SG]T_b
              + \int [0.4669 - 3.26238SG] 10^{5} \{T_b\}
         Parameters
         SG : float
              Specific gravity of the fluid at 60 degrees Farenheight [-]
          Tb : float
              Boiling point the fluid [K]
         Returns
         Tc : float
              Estimated critical temperature [K]
         Notes
         Model shows predictions for Tc, Pc, MW, and omega.
          Original units in degrees Rankine.
         Examples
         Example 2.2 from [2]_, but with K instead of R.
         >>> Tc_Kesler_Lee_SG_Tb(0.7365, 365.555)
          545.0124354151242
         References
          .. [1] Kesler, M. G., and B. I. Lee. "Improve Prediction of Enthalpy of
             Fractions." Hydrocarbon Processing (March 1976): 153-158.
          .. [2] Ahmed, Tarek H. Equations of State and PVT Analysis: Applications
             for Improved Reservoir Modeling. Gulf Pub., 2007.
         Tb = 9/5.*Tb \# K to R
         Tc = 341.7 + 811.1*SG + (0.4244 + 0.1174*SG)*Tb + ((0.4669 - 3.26238*SG)*1E5)/Tb
         Tc = 5/9.*Tc \# R to K
         return Tc
      def Pc_Kesler_Lee_SG_Tb(SG, Tb):
         r"Estimates critical pressure of a hydrocarbon compound or petroleum
                                                                                  (continues on next page)
```

```
fraction using only its specific gravity and boiling point, from
    [1]_ as presented in [2]_.
    .. math::
       {SG} + \frac{0.11857}{SG^2}\right]10^{-3}T_b
       + \left[1.4685 + \frac{3.648}{SG} + \frac{0.47227}{SG^2}\right]
       10^{-7}T_b^2 - left[0.42019 + frac{1.6977}{SG^2} right]10^{-10}T_b^3
   Parameters
     _____
   SG : float
       Specific gravity of the fluid at 60 degrees Farenheight [-]
   Tb : float
       Boiling point the fluid [K]
   Returns
   Pc : float
       Estimated critical pressure [Pa]
   Notes
    ____
   Model shows predictions for Tc, Pc, MW, and omega.
   Original units in degrees Rankine and psi.
   Examples
   Example 2.2 from [2]_, but with K instead of R and Pa instead of psi.
   >>> Pc_Kesler_Lee_SG_Tb(0.7365, 365.555)
   3238323.346840464
   References
    .. [1] Kesler, M. G., and B. I. Lee. "Improve Prediction of Enthalpy of
      Fractions." Hydrocarbon Processing (March 1976): 153-158.
    .. [2] Ahmed, Tarek H. Equations of State and PVT Analysis: Applications
      for Improved Reservoir Modeling. Gulf Pub., 2007.
   Tb = 9/5.*Tb \# K to R
   Pc = exp(8.3634 - 0.0566/SG - (0.24244 + 2.2898/SG + 0.11857/SG**2)*1E-3*Tb
   + (1.4685 + 3.648/SG + 0.47227/SG**2)*1E-7*Tb**2
    -(0.42019 + 1.6977/SG^{**2})^{*1E-10^{*}Tb^{**3}})
   Pc = Pc*psi
   return Pc
def MW_Kesler_Lee_SG_Tb(SG, Tb):
   r"Estimates molecular weight of a hydrocarbon compound or petroleum
   fraction using only its specific gravity and boiling point, from
    [1]_ as presented in [2]_.
```

```
.. math::
        MW = -12272.6 + 9486.4SG + [4.6523 - 3.3287SG]T_b + [1-0.77084SG]
        - 0.02058SG^2]\left[1.3437 - \frac{720.79}{T_b}\right]\frac{10^7}{T_b}
        + [1-0.80882SG + 0.02226SG^2][1.8828 - frac{181.98}{T_b}]
        frac{10^{12}}{T_b^3}
    Parameters
    _____
    SG : float
        Specific gravity of the fluid at 60 degrees Farenheight [-]
    Tb : float
       Boiling point the fluid [K]
    Returns
    _____
    MW : float
        Estimated molecular weight [g/mol]
    Notes
    Model shows predictions for Tc, Pc, MW, and omega.
    Original units in degrees Rankine.
    Examples
    Example 2.2 from [2]_, but with K instead of R and Pa instead of psi.
    >>> MW_Kesler_Lee_SG_Tb(0.7365, 365.555)
    98.70887589833501
    References
    _____
    .. [1] Kesler, M. G., and B. I. Lee. "Improve Prediction of Enthalpy of
       Fractions." Hydrocarbon Processing (March 1976): 153-158.
    .. [2] Ahmed, Tarek H. Equations of State and PVT Analysis: Applications
       for Improved Reservoir Modeling. Gulf Pub., 2007.
    Tb = 9/5.*Tb \# K to R
    MW = (-12272.6 + 9486.4 \text{*}\text{SG} + (4.6523 - 3.3287 \text{*}\text{SG}) \text{*}\text{Tb} + (1.-0.77084 \text{*}\text{SG} - 0.
→02058*SG**2)*
    (1.3437 - 720.79/Tb)*1E7/Tb + (1.-0.80882*SG + 0.02226*SG**2)*
    (1.8828 - 181.98/Tb)*1E12/Tb**3)
    return MW
def omega_Kesler_Lee_SG_Tb_Tc_Pc(SG, Tb, Tc=None, Pc=None):
    r"Estimates accentric factor of a hydrocarbon compound or petroleum
    fraction using only its specific gravity and boiling point, from
    [1]_ as presented in [2]_. If Tc and Pc are provided, the Kesler-Lee
    routines for estimating them are not used.
    For Tbr > 0.8:
    .. math::
```

```
+ ([1.408-0.01063K]/T_{br})
Otherwise:
.. math::
   + 1.28862\ln T_{br} - 0.169347T_{br}^6}{15.2518 - \frac{15.6875}{T_{br}}
    - 13.4721 \ln T_{br} + 0.43577T_{br}^{6}
   K = \frac{frac{T_b^{1/3}}}{SG}
   T_{br} = \int frac \{T_b\} \{T_c\}
Parameters
_____
SG : float
   Specific gravity of the fluid at 60 degrees Farenheight [-]
Tb : float
   Boiling point the fluid [K]
Tc : float, optional
   Estimated critical temperature [K]
Pc : float, optional
   Estimated critical pressure [Pa]
Returns
_____
omega : float
   Acentric factor [-]
Notes
_ _ _ _ _
Model shows predictions for Tc, Pc, MW, and omega.
Original units in degrees Rankine and psi.
Examples
Example 2.2 from [2]_, but with K instead of R and Pa instead of psi.
>>> omega_Kesler_Lee_SG_Tb_Tc_Pc(0.7365, 365.555, 545.012, 3238323.)
0.306392118159797
References
_____
.. [1] Kesler, M. G., and B. I. Lee. "Improve Prediction of Enthalpy of
  Fractions." Hydrocarbon Processing (March 1976): 153-158.
.. [2] Ahmed, Tarek H. Equations of State and PVT Analysis: Applications
  for Improved Reservoir Modeling. Gulf Pub., 2007.
if Tc is None:
   Tc = Tc_Kesler_Lee_SG_Tb(SG, Tb)
if Pc is None:
   Pc = Pc_Kesler_Lee_SG_Tb(SG, Tb)
```

Tb = 9/5.\*Tb # K to R Tc = 9/5.\*Tc # K to R  $K = Tb^{**}(1/3.)/SG$  Tbr = Tb/Tcif Tbr > 0.8: omega = -7.904 + 0.1352\*K - 0.007465\*K^{\*\*2} + 8.359\*Tbr + ((1.408-0.01063\*K)/Tbr)
else: omega = ((-log(Pc/101325.) - 5.92714 + 6.09648/Tbr + 1.28862\*log(Tbr) - 0.169347\*Tbr\*\*6) / (15.2518 - 15.6875/Tbr - 13.4721\*log(Tbr) +0.43577\*Tbr\*\*6)) return omega

[112]: # Basic composition and names. All pure component properties are obtained from Chemicals.  $\rightarrow$  and Thermo. pure\_constants = ChemicalConstantsPackage.constants\_from\_IDs( ['water', 'hydrogen', 'helium', 'nitrogen', 'carbon dioxide', 'hydrogen sulfide',  $\rightarrow$  'methane'. 'ethane', 'propane', 'isobutane', 'n-butane', 'isopentane', 'n-pentane', 'hexane', 'heptane', 'octane', 'nonane']) pure\_fractions = [.02, .00005, .00018, .009, .02, .002, .82, .08, .031, .009, .0035, .0033, .0003, .0007, .0004, .00005, .00002] [105]: pseudo\_names = ['C10-C11', 'C12-C14', 'C15+']  $pseudo_carbon_numbers = [10.35, 12.5, 16.9]$ pseudo\_SGs = [.73, .76, .775] # Specific gravity values are based of the alkane series  $pseudo_Tbs = [447, 526, 589]$ # Using the estimation methods defined earlier, we obtain some critical properties pseudo\_Tcs = [Tc\_Kesler\_Lee\_SG\_Tb(SG, Tb) for SG, Tb in zip(pseudo\_SGs, pseudo\_Tbs)] pseudo\_Pcs = [Pc\_Kesler\_Lee\_SG\_Tb(SG, Tb) for SG, Tb in zip(pseudo\_SGs, pseudo\_Tbs)] pseudo\_MWs = [MW\_Kesler\_Lee\_SG\_Tb(SG, Tb) for SG, Tb in zip(pseudo\_SGs, pseudo\_Tbs)] pseudo\_omegas = [omega\_Kesler\_Lee\_SG\_Tb\_Tc\_Pc(SG, Tb) for SG, Tb in zip(pseudo\_SGs, →pseudo\_Tbs)] # Estimate the hydroen counts hydrogen\_counts = [(MW - C\*periodic\_table.C.MW)/periodic\_table.H.MW for C, MW in zip(pseudo\_carbon\_numbers, pseudo\_MWs)] # Get the atomic compositions pseudo\_atoms = [{'C': C, 'H': H} for C, H in zip(pseudo\_carbon\_numbers, hydrogen\_counts)] # Calculate the similarity variable of each species similarity\_variables = [similarity\_variable(atoms=atoms) for atoms in pseudo\_atoms] pseudo\_fractions = [.0003, .00015, .00005] [113]: pseudos = ChemicalConstantsPackage(names=pseudo\_names, MWs=pseudo\_MWs, Tbs=pseudo\_Tbs, atomss=pseudo\_atoms, Tcs=pseudo\_Tcs, Pcs=pseudo\_Pcs, omegas=pseudo\_omegas,

```
# Obtain the temperature and pressure dependent objects
properties = PropertyCorrelationsPackage(constants=constants)
# This is the feed composition
zs = normalize(pure_fractions + pseudo_fractions)
T = 270 # K
P = 1e5 # bar
```

```
[132]: kijs = np.zeros((constants.N, constants.N)).tolist() # kijs left as zero in this example
      eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas,
       →kijs=kijs)
       # The API SRK equation of state is used, but other cubic equations of state can be uesd
       \rightarrow instead
      gas = CEOSGas(APISRKMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases, T=T,
       \rightarrow P=P, zs=zs)
      liq = CEOSLiquid(APISRKMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases,___
       \hookrightarrow T=T, P=P, zs=zs)
      liq2 = CEOSLiquid(APISRKMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases,__
       \rightarrow T=T, P=P, zs=zs)
      phase_list = [gas, liq, liq]
      # Set up the three phase flash engine
      flashN = FlashVLN(constants, properties, liquids=[liq, liq2], gas=gas)
[133]: # Do the flash, and get some properties
      res = flashN.flash(T=T, P=P, zs=zs)
      res_phase_count, res_gas_beta, res_liquids_betas
[133]: (3, 0.9827041561275568, [0.01683884003998437, 0.0004570038324588659])
[134]: res.H(), res.Cp_mass(), res.MW(), res.gas.mu(), res.gas.k()
[134]: (-1961.508963322489.
       1989.3915447041693,
       19.675910651652533,
        1.0011888443404098e-05,
       0.027073401138714016)
[135]: res.heaviest_liquid.rho_mass(), res.lightest_liquid.rho_mass()
```

```
[135]: (769.2525386053419, 599.2086838769083)
```

# 8.4 Performing Large Numbers of Calculations with Thermo in Parallel

A common request is to obtain a large number of properties from Thermo at once. Thermo is not NumPy - it cannot just automatically do all of the calculations in parallel.

If you have a specific property that does not require phase equilibrium calculations to obtain, it is possible to use the chemicals.numba interface to in your own numba-accelerated code. https://chemicals.readthedocs.io/chemicals.numba.html

For those cases where lots of flashes are needed, your best bet is to brute force it - use multiprocessing (and maybe a beefy machine) to obtain the results faster. The following code sample uses joblib to facilitate the calculation. Note that joblib won't show any benefits on sub-second calculations. Also note that the threading backend of joblib will not offer any performance improvements due to the CPython GIL.

```
[1]: import numpy as np
    from thermo import *
    from chemicals import *
    constants, properties = ChemicalConstantsPackage.from_IDs(
         ['methane', 'ethane', 'propane', 'isobutane', 'n-butane', 'isopentane',
          'n-pentane', 'hexane', 'heptane', 'octane', 'nonane', 'nitrogen'])
    T, P = 200, 5e6
    zs = [.8, .08, .032, .00963, .0035, .0034, .0003, .0007, .0004, .00005, .00002, .07]
    eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
    gas = CEOSGas(SRKMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases, T=T, _
     \rightarrow P=P, zs=zs)
    liq = CEOSLiquid(SRKMIX, eos_kwargs, HeatCapacityGases=properties.HeatCapacityGases, T=T,
     \rightarrow P=P, zs=zs)
     # Set up a two-phase flash engine, ignoring kijs
    flasher = FlashVL(constants, properties, liquid=liq, gas=gas)
     # Set a composition - it could be modified in the inner loop as well
     # Do a test flash
    flasher.flash(T=T, P=P, zs=zs).gas_beta
[1]: 0.4595970727935113
```

```
[2]: def get_properties(T, P):
    # This is the function that will be called in parallel
    # note that Python floats are faster than numpy floats
    res = flasher.flash(T=float(T), P=float(P), zs=zs)
    return [res.rho_mass(), res.Cp_mass(), res.gas_beta]
```

43.9 s  $\pm$  0 ns per loop (mean  $\pm$  std. dev. of 1 run, 1 loop each)

[7]: # Use the multiprocessing feature of joblib # We were able to improve the speed by 5x %timeit -r 1 -n 1 processed\_data = Parallel(n\_jobs=16, batch\_size=30)(delayed(get\_ →properties)(T, P) for T, P in zip(Ts\_grid.flat, Ps\_grid.flat))

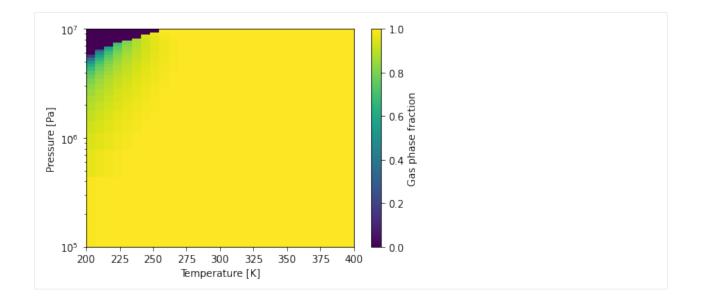
```
3.55 s \pm 0 ns per loop (mean \pm std. dev. of 1 run, 1 loop each)
```

4.42 s  $\pm$  0 ns per loop (mean  $\pm$  std. dev. of 1 run, 1 loop each)

[9]: # Joblib returns the data as a flat structure, but we can re-construct it into a grid processed\_data = Parallel(n\_jobs=16, batch\_size=30)(delayed(get\_properties)(T, P) for T,\_ →P in zip(Ts\_grid.flat, Ps\_grid.flat)) phase\_fractions = np.array([[processed\_data[j\*pts+i][2] for j in range(pts)] for i in\_ →range(pts)])

```
[10]: # Make a plot to show the results
```

```
import matplotlib.pyplot as plt
from matplotlib import ticker, cm
from matplotlib.colors import LogNorm
fig, ax = plt.subplots()
color_map = cm.viridis
im = ax.pcolormesh(Ts_grid, Ps_grid, phase_fractions T, cmap=color_map)
cbar = fig.colorbar(im, ax=ax)
cbar.set_label('Gas phase fraction')
ax.set_yscale('log')
ax.set_xlabel('Temperature [K]')
ax.set_ylabel('Pressure [Pa]')
plt.show()
<ipython-input-10-719d0a113f9b>:8: MatplotlibDeprecationWarning: shading='flat' when X_
\rightarrow and Y have the same dimensions as C is deprecated since 3.3. Either specify the
\rightarrow corners of the quadrilaterals with X and Y, or pass shading='auto', 'nearest' or
→ 'gouraud', or set rcParams['pcolor.shading']. This will become an error two minor.
\rightarrow releases later.
  im = ax.pcolormesh(Ts_grid, Ps_grid, phase_fractions.T, cmap=color_map)
```



## 8.5 Example 14.2 Joule-Thomson Effect

A stream of nitrogen is expanded from T1 = 300 K, P1 = 200 bar, to 1 bar by a throttling valve. An ideal throttling valve has the conditions of being adiabatic (no heat loss, energy is conserved); and is either solved using a valve Cv to solve for pressure or solved with the outlet pressure directly specified.

Calculate the outlet temperature using:

- (1) A high precision (helmholtz fundamental) equation of state
- (2) The Peng-Robinson equation of state

```
[1]: # Set the conditions and imports
    from scipy.constants import bar
    from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CoolPropLiquid, CEOSGas,
     →CoolPropGas, FlashPureVLS
    fluid = 'nitrogen'
    constants, correlations = ChemicalConstantsPackage from_IDs([fluid])
    T1 = 300.0
    P1 = 200*bar
    P2 = 1*bar
    zs = [1]
[2]: # Thermo can use CoolProp to provide properties of one or all phases
    # For pure species this is quite reliable within the temperature,
    # pressure, etc. limits of the EOSs implemented by CoolProp
    backend = 'HEOS'
    gas = CoolPropGas(backend, fluid, T=T1, P=P1, zs=zs)
    liquid = CoolPropLiquid(backend, fluid, T=T1, P=P1, zs=zs)
    flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
```

```
state_1 = flasher.flash(T=T1, P=P1)
state_2 = flasher.flash(H=state_1.H(), P=P2)
T2_precise = state_2.T
T2_precise
```

[2]: 269.1866854380218

```
[3]: # Use the default originally published Peng-Robinson models
```

The outlet temperature anwsers given in the book are 269.19 K for the high-precision EOS, and for the PR EOS they used a very low precision Cp of 1  $J/(g^*K)$  and obtained an outlet temperature of 283.05 K.

The book textbook cites this 14 K difference as coming from the cubic EOS's lack of precision but the above calculation shows that if an accurate heat capacity is used the difference is only  $\sim 4$ K.

## 8.6 Example 14.3 Adiabatic Compression and Expansion

A heat pump using the refrigerant R-22 operates with a mass flow rate of 100 kg/hr. The fluid enters the compressor at T1 = 300 K and P1 = 1 bar. The compressor heat loss is neglected. The outlet pressure of the compressor is 5 bar. If the isentropic efficiency of the compressor is 0.7 and the mechanical efficiency is 0.9, what is the power draw of the compressor and how how is the refrigerant when it exits the compressor?

The textbook uses the Peng-Robinson EOS, so to compare, use that as well.

```
[1]: # Set the conditions and imports
```

```
from scipy.constants import bar, hour
from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CEOSGas, FlashPureVLS
fluid = 'R-22'
constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
T1 = 300.0
P1 = 1*bar
P2 = 5*bar
eta_isentropic = 0.7
eta_mechanical = 0.9
[2]: # Use the default originally published Peng-Robinson models
```

```
(continued from previous page)
gas = CEOSGas(PRMIX, HeatCapacityGases=correlations.HeatCapacityGases, eos_kwargs=eos_
→kwargs)
flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
# Flash at inlet conditions to obtain initial enthalpy
state_1 = flasher.flash(T=T1, P=P1)
# Flash at outlet condition - entropy is conserved by compressors and expanders!
state_2_ideal = flasher.flash(S=state_1.S(), P=P2)
# Compute the change in enthalpy
delta_H_ideal = (state_2_ideal.H()-state_1.H())
# The definition of isentropic efficiency means that the actual amount of heat added is
# dH_actual = dH_idea/eta_isentropic
H_added_to_fluid_actual = delta_H_ideal/eta_isentropic
state_2 = flasher.flash(H=state_1.H() + H_added_to_fluid_actual, P=P2)
# To compute the actual power, it is more convinient to use the mass enthalpy
actual_power_per_kg = (state_2.H_mass() - state_1.H_mass())/(eta_mechanical) # W/kg
actual_power = actual_power_per_kg*100/hour
print(f'The actual power is {actual_power:.0f} W')
print(f'The actual outlet temperature is {state_2.T: .2f} K')
The actual power is 2252 W
The actual outlet temperature is 406.60 K
```

The power given in the textbook is 2257 W and 405.68 K out. No details as to the liquid heat capacity are given. As refrigerants are well defined substances, it is recommended for anyone doing modeling with them to use a high-accuracy model wherever possible.

# 8.7 Problem 14.02 Work and Temperature Change Upon Isentropic Compression of Oxygen

A stream of gaseous oxygen is compressed from 1 bar to 10 bar. The inlet temperature is 25 °C. Calculate the specific work and the temperature of the outlet gas if the process as an isentropic efficiency of 1, using both the ideal gas law and the SRK equation of state.

### 8.7.1 Solution

This requires a PT and then a PS flash only. This problem is also good for contrasting simple engineering formulas for compression vs. rigorous thermodynamics.

P1 = 1\*barP2 = 10\*bar

```
[2]: # Use the Ideal-Gas EOS
    gas = IdealGas(HeatCapacityGases=correlations.HeatCapacityGases)
    # Note that we can set-up a flasher object with only a gas phase
    # This obviously has much more performance!
    flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[], solids=[])
    # Flash at inlet conditions to obtain initial enthalpy
    state_1 = state_1_ideal = flasher.flash(T=T1, P=P1)
    # Flash at outlet condition - entropy is conserved by compressors and expanders!
    state_2 = state_2_ideal = flasher.flash(S=state_1.S(), P=P2)
    actual_power = (state_2.H() - state_1.H()) # W/mol
    print('With the ideal-gas EOS:')
    print(f'The actual power is {actual_power:.4f} J/mol')
    print(f'The actual outlet temperature is {state_2.T: .2f} K')
    With the ideal-gas EOS:
    The actual power is 7991.2798 J/mol
    The actual outlet temperature is 560.70 K
[3]: # SRK
    eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
    liquid = CEOSLiquid(SRKMIX, HeatCapacityGases=correlations.HeatCapacityGases, eos_
     →kwargs=eos_kwargs)
    gas = CEOSGas(SRKMIX, HeatCapacityGases=correlations.HeatCapacityGases, eos_kwargs=eos_
     →kwargs)
    flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
    # Flash at inlet conditions to obtain initial enthalpy
    state_1 = flasher.flash(T=T1, P=P1)
    # Flash at outlet condition - entropy is conserved by compressors and expanders!
    state_2 = state_2_ideal = flasher.flash(S=state_1.S(), P=P2)
    actual_power = (state_2.H() - state_1.H()) # W/mol
    print('With the SRK EOS:')
    print(f'The actual power is {actual_power:.4f} J/mol')
    print(f'The actual outlet temperature is {state_2.T: .2f} K')
    With the SRK EOS:
    The actual power is 8000.1749 J/mol
    The actual outlet temperature is 561.06 K
```

These calculations make use of the full power of the Thermo engine. It is also possible to use simpler calculations to calculate, as shown below.

```
[4]: from fluids import isentropic_work_compression, isentropic_T_rise_compression
    k = state_1_ideal.isentropic_exponent()
    Z = state_1_ideal.Z()
    print(f'Using the ideal isentropic exponent {k:.3f}')
    print(f'Using the ideal compressibility {Z:.3f}')
```

```
molar_work = isentropic_work_compression(T1=T1, k=state_1_ideal.isentropic_exponent(),_

Z=state_1_ideal.Z(), P1=P1, P2=P2, eta=1)

T2 = isentropic_T_rise_compression(T1=T1, P1=P1, P2=P2, k=k, eta=1)

print(f'The simple power is {molar_work:.4f} J/mol')

print(f'The simple outlet temperature is {T2: .2f} K')

Using the ideal isentropic exponent 1.395

Using the ideal compressibility 1.000

The simple power is 8047.9387 J/mol

The simple outlet temperature is 572.15 K
```

From these results, we can see that for small pressure increases, the ideal-gas and SRK equations work quite similarly. There is also a very large difference in outlet temperature between the simplified equations given in many textbooks, and the real isentropic calculations when a temperature-dependent heat capacity is used. Therefore, there are substantial advantages to rigorous modeling, regardless of the complexity of the EOS for the gas phase.

# 8.8 Problem 14.03 Reversible and Isothermal Compression of Liquid Water

A flow of 2000 kg/h liquid water at 25 °C and 1 bar is pumped to a pressure of 100 bar. The pump is "cooled", so the process is reversible and isothermal. What is the duty of the pump shaft, and the energy that must be removed from the water being compressed?

### 8.8.1 Solution

We can use the high-accuracy IAPWS-95 implementation of the properties of water to easily and extremely accurately calculate these values.

```
[87]: from scipy.constants import bar, hour
     import numpy as np
     from thermo import FlashPureVLS, IAPWS95Liquid, IAPWS95Gas, iapws_constants, iapws_
      →correlations
      from scipy.integrate import quad
     import numpy as np
     T1 = T2 = 25 + 273.15
     P1 = 1*bar
     P2 = 100*bar
     liquid = IAPWS95Liquid(T=T1, P=P1, zs=[1])
     gas = IAPWS95Gas(T=T1, P=P1, zs=[1])
     flasher = FlashPureVLS(iapws_constants, iapws_correlations, gas, [liquid], [])
     mass_flow = 2000/hour
     mole_flow = property_molar_to_mass(mass_flow, MW=iapws_constants.MWs[0])
     entry = flasher.flash(T=T1, P=P1)
     leaving = flasher.flash(T=T2, P=P2)
```

```
def to_int(P, flasher):
    state = flasher.flash(T=T1, P=P)
    return state.V()
integral_result = quad(to_int, P1, P2, args=(flasher,))[0]
shaft_duty = integral_result*mole_flow
cooling_duty = shaft_duty - (leaving.H() - entry.H())*mole_flow
print(f'The shaft power is {shaft_duty:.8f} W')
print(f'The cooling duty is {cooling_duty:.4f} W')
The shaft power is 5504.05633851 W
The cooling duty is 431.1770 W
```

The above shows the numerical integral calculation. That is the correct formulation.

However, it can be a little unintuitive. We can contrast this with another calculation - a series of tiny isentropic compression, then cooling steps.

```
[86]: cooling_duty = 0
     compressing_duty = 0
     increments = 30 # Number of increments
     dP = (P2 - P1)/increments
     old_state = entry
     for i in range(increments):
         P = P1 + (i+1) * dP
          # Compress another increment of pressure
         new_compressed_state = flasher.flash(S=old_state.S(), P=P)
         compressing_duty += (new_compressed_state.H() - old_state.H())*mole_flow
          # Cool back to T1 at new pressure
         new_cooled_state = flasher.flash(T=T1, P=P)
         cooling_duty += (new_compressed_state.H() - new_cooled_state.H())*mole_flow
         old_state = new_cooled_state
     print(f'The shaft power is {compressing_duty:.4f} W')
     print(f'The cooling duty is {cooling_duty:.4f} W')
     The shaft power is 5504.0608 W
     The cooling duty is 431.1815 W
```

# 8.9 Problem 14.04 Heat Effect Upon Mixing of Methane and Dodecane at Elevated Temperature and Pressure Using SRK

1600 kg/hr of methane is mixed with 170 kg/hr of dodecane. The inlet temperature of both streams is 160  $^{\circ}$ C, and each enter at a pressure of 2 MPa. The mixing process is isobaric. What is the temperature of the combined stream? Use the SRK EOS with no binary interaction parameters.

## 8.9.1 Solution

This is a straightforward calculation. The energy of both streams is combined; and the outlet pressure is known. The calculation only requires calculating the inlet energy of both streams, adding it up, and finding the mole fractions of the outlet.

```
[12]: from thermo import ChemicalConstantsPackage, SRKMIX, FlashVL, CEOSLiquid, CEOSGas
      from chemicals import ws_to_zs, mixing_simple
      constants, correlations = ChemicalConstantsPackage.from_IDs(['methane', 'dodecane'])
      eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
      liquid = CEOSLiquid(SRKMIX, HeatCapacityGases=correlations.HeatCapacityGases, eos_
      →kwargs=eos_kwargs)
      gas = CEOSGas(SRKMIX, HeatCapacityGases=correlations.HeatCapacityGases, eos_kwargs=eos_
      \rightarrowkwargs)
      flasher = FlashVL(constants, correlations, liquid=liquid, gas=gas)
      P1 = P2 = 2e6
      T1 = 160 + 273.15
      ws = [1600, 170]
      zs = ws_to_zs(ws=ws, MWs=constants.MWs)
      methane_H = flasher.flash(T=T1, P=P1, zs=[1, 0]).H()
      dodecane_H = flasher.flash(T=T1, P=P1, zs=[0, 1]).H()
      H = zs[0]*methane_H + zs[1]*dodecane_H
      res = flasher.flash(P=P2, H=H, zs=zs)
      print(f'The outlet temperature is {res.T-273.15:.4f} °C')
      The outlet temperature is 150.2259 °C
```

# 8.10 Problem 14.05 Required Power for R134a Compression Using a High Precision Equation of State

Refrigerant R134a is compressed from a saturated vapor at 5 °C to an outlet pressure of 1 MPa. Calculate the power of the compressor, using a high-precision EOS.

The mechanical efficiency is 0.95, and the isentropic efficiency 0.7; the mass flow rate is 3000 kg/hr.

### 8.10.1 Solution

This is straightforward.

```
[8]: # Set the conditions and imports
     from scipy.constants import bar, hour
     from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CoolPropLiquid, CEOSGas,
      →CoolPropGas, FlashPureVLS
      fluid = 'R134a'
     constants, correlations = ChemicalConstantsPackage from_IDs([fluid])
     T1 = 5 + 273.15
     VF1 = 1
     P2 = 10*bar
     zs = [1]
     eta_isentropic = 0.7
     eta_mechanical = 0.9
[10]: backend = 'HEOS'
     gas = CoolPropGas(backend, fluid, T=T1, P=1e5, zs=zs)
     liquid = CoolPropLiquid(backend, fluid, T=T1, P=1e5, zs=zs)
     flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
      # Flash at inlet conditions to obtain initial enthalpy
     state_1 = flasher.flash(T=T1, VF=VF1)
      # Flash at outlet condition - entropy is conserved by compressors and expanders!
     state_2_ideal = flasher.flash(S=state_1.S(), P=P2)
      # Compute the change in enthalpy
     delta_H_ideal = (state_2_ideal.H()-state_1.H())
      # The definition of isentropic efficiency means that the actual amount of heat added is
      # dH_actual = dH_idea/eta_isentropic
     H_added_to_fluid_actual = delta_H_ideal/eta_isentropic
     state_2 = flasher.flash(H=state_1.H() + H_added_to_fluid_actual, P=P2)
     # To compute the actual power, it is more convinient to use the mass enthalpy
     actual_power_per_kg = (state_2.H_mass() - state_1.H_mass())/(eta_mechanical) # W/kg
     actual_power = actual_power_per_kg*3000/hour
     print(f'The actual power is {actual_power:.0f} W')
     print(f'The actual outlet temperature is {state_2.T: .2f} K')
     The actual power is 28858 W
     The actual outlet temperature is 324.80 K
```

# 8.11 Problem 14.06 Required Volume for a Gas Storage Tank for Ammonia

 $50 \text{ m}^3$  of liquid ammonia is stored at the conditions 50 °C and 100 bar. The vessel fails, and the contents empties into a backup containment vessel. The backup vessel has a maximum pressure of 10 bar. What volume must be vessel be to not exceed this pressure?

## 8.11.1 Solution

This is straightforward; energy is conserved and a pressure is specified. Find the amount of ammonia in the original vessel; find the molar volume of ammonia in the new vessel; and multiply that by the amount of ammonia.

Ammonia is a highly non-ideal fluid, so we use a high-precision EOS.

```
[10]: # Set the conditions and imports
      from scipy.constants import bar
      from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CoolPropLiquid, CEOSGas,
      →CoolPropGas, FlashPureVLS
      fluid = 'ammonia'
      constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
      T1 = 50 + 273.15
      P1 = 100*bar
      P2 = 10*bar
      zs = [1]
      volume_1 = 50
      backend = 'HEOS'
      gas = CoolPropGas(backend, fluid, T=T1, P=1e5, zs=zs)
      liquid = CoolPropLiquid(backend, fluid, T=T1, P=1e5, zs=zs)
      flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
[12]: # Flash at inlet conditions to obtain initial enthalpy
      state_1 = flasher.flash(T=T1, P=P1)
      moles = volume_1/state_1.V()
      state_2 = flasher.flash(P=P2, H=state_1.H())
      volume 2 = moles*state 2.V()
      print(f'The thermodynamically required secondary containment volume is {volume_2: .2f} m^
      →3')
      The thermodynamically required secondary containment volume is 433.83 m<sup>3</sup>
```

## 8.12 Problem 14.07 Liquid Nitrogen Production Via Volume Expansion of the Compressed Gas

Nitrogen at -104 °C and 250 bar flows through a valve to a pressure of 1 bar. What fraction of the stream becomes liquid?

### 8.12.1 Solution

This is straightforward; energy is conserved and outlet presure is specified, making this a PH flash. This problem is also an important application that can show the results of different equations of state and how important good thermodynamics are.

We can compare many different EOSs with Thermo easily.

```
[1]: from thermo import *
    from thermo.interaction_parameters import SPDB
    fluid = 'nitrogen'
     constants, correlations = ChemicalConstantsPackage from_IDs([fluid])
    T1 = -104 + 273.15
    P1 = 240 * 1e5
    zs = [1]
    P2 = 1e5
[2]: flasher_objects = []
    flasher_names = []
    gas = CoolPropGas('HEOS', fluid, T=T1, P=P1, zs=zs)
    liquid = CoolPropLiquid('HEOS', fluid, T=T1, P=P1, zs=zs)
    high_precision = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid],
     \rightarrow solids=[])
    flasher_objects.append(high_precision)
    flasher_names.append('High-Precision')
    # Add the Peng-Robinson Pina-Martinez parameters EOS
    Ls = SPDB.get_parameter_vector(name='PRTwu_PinaMartinez', CASs=constants.CASs, parameter=
     \leftrightarrow 'TwuPRL')
    Ms = SPDB.get_parameter_vector(name='PRTwu_PinaMartinez', CASs=constants.CASs, parameter=
     \leftrightarrow 'TwuPRM')
    Ns = SPDB.get_parameter_vector(name='PRTwu_PinaMartinez', CASs=constants.CASs, parameter=
     \leftrightarrow 'TwuPRN')
    cs = SPDB.get_parameter_vector(name='PRTwu_PinaMartinez', CASs=constants.CASs, parameter=
     \rightarrow 'TwuPRc')
    alpha_coeffs = [(Ls[i], Ms[i], Ns[i]) for i in range(constants.N)]
    eos_kwargs = { 'Pcs': constants.Pcs, 'Tcs': constants.Tcs, 'omegas': constants.omegas,
     'cs': cs, 'alpha_coeffs':alpha_coeffs}
    gas = CEOSGas(PRMIXTranslatedConsistent, eos_kwargs=eos_kwargs,__
     →HeatCapacityGases=correlations.HeatCapacityGases)
    liquid = CEOSLiquid(PRMIXTranslatedConsistent, eos_kwargs=eos_kwargs,_
     Generations.HeatCapacityGases
    eos_obj = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
                                                                                   (continues on next page)
```

```
flasher_objects.append(eos_obj)
    flasher_names.append('PR-Pina-Martinez')
    # Add the SRK Pina-Martinez parameters EOS
    Ls = SPDB.get_parameter_vector(name='SRKTwu_PinaMartinez', CASs=constants.CASs,
     →parameter='TwuSRKL')
    Ms = SPDB.get_parameter_vector(name='SRKTwu_PinaMartinez', CASs=constants.CASs,_
     →parameter='TwuSRKM')
    Ns = SPDB.get_parameter_vector(name='SRKTwu_PinaMartinez', CASs=constants.CASs,
     \rightarrow parameter='TwuSRKN')
    cs = SPDB.get_parameter_vector(name='SRKTwu_PinaMartinez', CASs=constants.CASs,
     →parameter='TwuSRKc')
    alpha_coeffs = [(Ls[i], Ms[i], Ns[i]) for i in range(constants.N)]
    eos_kwargs = { 'Pcs': constants.Pcs, 'Tcs': constants.Tcs, 'omegas': constants.omegas,
    'cs': cs, 'alpha_coeffs':alpha_coeffs}
    gas = CEOSGas(SRKMIXTranslatedConsistent, eos_kwargs=eos_kwargs,_
     →HeatCapacityGases=correlations.HeatCapacityGases)
    liquid = CEOSLiquid(SRKMIXTranslatedConsistent, eos_kwargs=eos_kwargs,_
     →HeatCapacityGases=correlations.HeatCapacityGases)
    eos_obj = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
    flasher_objects append(eos_obj)
    flasher_names.append('SRK-Pina-Martinez')
    # Add a bunch of EOSs that don't require any parameters
    eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
    cubic_EOSs = [('PR', PRMIX), ('SRK', SRKMIX),
                   ('VDW', VDWMIX),
                  ('PRSV', PRSVMIX), ('PRSV2', PRSV2MIX),
                  ('TWUPR', TWUPRMIX), ('TWUSRK', TWUSRKMIX),
                  ('PRTranslatedConsistent', PRMIXTranslatedConsistent),
                  ('SRKTranslatedConsistent', SRKMIXTranslatedConsistent)]
    for eos_name, eos_obj in cubic_EOSs:
        liquid = CEOSLiquid(eos_obj, HeatCapacityGases=correlations.HeatCapacityGases, eos_
     →kwargs=eos_kwargs)
        gas = CEOSGas(eos_obj, HeatCapacityGases=correlations.HeatCapacityGases, eos_
     \rightarrow kwargs=eos_kwargs)
        eos_obj = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
         flasher_objects.append(eos_obj)
         flasher_names.append(eos_name)
[3]: for obj, obj_name in zip(flasher_objects, flasher_names):
```

```
state_1 = obj.flash(T=T1, P=P1, zs=zs)
state_2 = obj.flash(P=P2, H=state_1.H(), zs=zs)
print(f'The {obj_name} EOS predicted liquid molar fraction is {state_2.LF:.8f}.')
```

The High-Precision EOS predicted liquid molar fraction is 0.03887228. The PR-Pina-Martinez EOS predicted liquid molar fraction is 0.05536129.

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```
The SRK-Pina-Martinez EOS predicted liquid molar fraction is 0.06765522.
The PR EOS predicted liquid molar fraction is 0.05963486.
The SRK EOS predicted liquid molar fraction is 0.04341557.
The VDW EOS predicted liquid molar fraction is 0.06000000.
The PRSV EOS predicted liquid molar fraction is 0.06011654.
The PRSV2 EOS predicted liquid molar fraction is 0.06011654.
The TWUPR EOS predicted liquid molar fraction is 0.05491152.
The TWUSRK EOS predicted liquid molar fraction is 0.04670591.
The PRTranslatedConsistent EOS predicted liquid molar fraction is 0.07069564.
```

As can be see, the equation of state used changes the results drastically. Even the best of the cubic equations of state given results 30-50% off from the high-precision equation of state. This problem was admittedly constructed to show off the importance of using higher precision models, but the point applies elsewhere also.

## 8.13 Problem 14.08 Required Compressor Power for Isothermal and Adiabatic Compression of a Gas Mixture (CO2, O2) Using the Ideal Gas Law

A stream of 1000 mol/hour CO2 and 1000 mol/hour O2 is compressed from 290 K and 1 bar to 5 bar. Calculate the compression power for both adiabatic compression, and isothermal compression. The compression is reversible (assumed) in each case - no efficiencies are necessary.

#### 8.13.1 Solution

This is a straightforward calculation. Using Thermo, working with complicated mixtures can be about as easy as pure components - if binary interaction parameters are zero. In this case, we try to load a parameter from a sample ChemSep database, but no values are available.

The values in that database are just a sample - it is entirely the user's responsibility to provide the correct data to Thermo. If garbage is put in, garbage will come out!

The problem says to use the ideal-gas law, so we can do that too and see how the answers compare.

#### Adiabatic compression

```
[2]: # Solve with Peng-Robinson
state_1 = flasher.flash(T=T1, P=P1, zs=zs)
state_2 = flasher.flash(S=state_1.S(), P=P2, zs=zs)
shaft_duty = (state_2.H() - state_1.H())*flow
print(f'The shaft power with Peng-Robinson is {shaft_duty:.4f} W')
state_1 = flasher_ideal.flash(T=T1, P=P1, zs=zs)
state_2 = flasher_ideal.flash(S=state_1.S(), P=P2, zs=zs)
shaft_duty = (state_2.H() - state_1.H())*flow
print(f'The shaft power with ideal-gas is {shaft_duty:.4f} W')
The shaft power with Peng-Robinson is 2632.7895 W
The shaft power with ideal-gas is 2639.9248 W
```

#### **Isothermal Compression**

This problem is more interesting, because there is the cooling duty as well as the compressing duty.

From theory, in an ideal gas, the cooling duty will be exactly equal to the compressing duty.

For a real-gas, it will be different as enthalpy is pressure-dependent.

In both cases, the evaluation of the following integral is required.

$$\operatorname{duty} = \operatorname{flow} \int_{P1}^{P2} V \partial P$$

[3]: from scipy.integrate import quad

```
def to_int(P, flasher):
    state = flasher.flash(T=T1, P=P, zs=zs)
    return state.V()
shaft_duty = cooling_duty = quad(to_int, P1, P2, args=(flasher_ideal,))[0]*flow
```

(continues on next page)

```
print(f'The shaft power with ideal-gas is {shaft_duty:.4f} W')
print(f'The cooling duty with ideal-gas is {cooling_duty:.4f} W')
entry = flasher.flash(T=T1, P=P1, zs=zs)
exit = flasher.flash(T=T1, P=P2, zs=zs)
shaft_duty = quad(to_int, P1, P2, args=(flasher,))[0]*flow
cooling_duty = shaft_duty - (exit.H() - entry.H())*flow
print(f'The shaft power with Peng-Robinson is {shaft_duty:.8f} W')
print(f'The cooling duty with Peng-Robinson is {cooling_duty:.8f} W')
The shaft power with ideal-gas is 2155.9263 W
The cooling duty with Peng-Robinson is 2139.44610002 W
The cooling duty with Peng-Robinson is 2192.57596810 W
```

The above shows the numerical integral calculation. That is the correct formulation.

However, it can be a little unintuitive. We can contrast this with another calculation - a series of tiny isentropic compression, then cooling steps.

```
[4]: cooling_duty = \emptyset
    compressing_duty = 0
    increments = 3 # Number of increments
    dP = (P2 - P1)/increments
    old_state = entry
    for i in range(increments):
        P = P1 + (i+1) * dP
         # Compress another increment of pressure
        new_compressed_state = flasher.flash(S=old_state.S(), P=P, zs=zs)
        compressing_duty += (new_compressed_state.H() - old_state.H())*flow
         # Cool back to T1 at new pressure
        new_cooled_state = flasher.flash(T=T1, P=P, zs=zs)
        cooling_duty += (new_compressed_state.H() - new_cooled_state.H())*flow
        old_state = new_cooled_state
    print(f'The shaft power is {compressing_duty:.8f} W')
    print(f'The cooling duty is {cooling_duty:.8f} W')
    The shaft power is 2322.61227046 W
    The cooling duty is 2375.74213854 W
```

# 8.14 Problem 14.09 Temperature Change Upon Ethylene Expansion in Throttle Valves Using a High Precision EOS

Ethylene is expanded from P1 = 3000 bar, T1 = 600 K to P2 = 300 bar by a first valve, and then to P3 = 1 bar by a second valve. What are the temperatures T2 and T3? Neglect the velocity term in the solution.

### 8.14.1 Solution

This is straightforward - an initial PT flash calculation, followed by two separate PH flash calculations.

```
[1]: # Set the conditions and imports
    from scipy.constants import bar, hour
    from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CoolPropLiquid, CEOSGas,
     →CoolPropGas, FlashPureVLS
    fluid = 'ethylene'
    constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
    T1 = 600
    P1 = 3000*bar
    P2 = 300*bar
    P3 = 1*bar
    zs = [1]
[2]: backend = 'HEOS'
    gas = CoolPropGas(backend, fluid, T=T1, P=P1, zs=zs)
    liquid = CoolPropLiquid(backend, fluid, T=T1, P=P1, zs=zs)
    flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
    # Flash at inlet conditions to obtain initial enthalpy
    state_1 = flasher.flash(T=T1, P=P1)
    state_2 = flasher.flash(H=state_1.H(), P=P2)
    state_3 = flasher.flash(H=state_1.H(), P=P3)
    print(f'The second temperature is {state_2.T: .2f} K')
    print(f'The third temperature is {state_3.T: .2f} K')
    The second temperature is 676.94 K
    The third temperature is 651.47 K
```

# 8.15 Problem 14.10 Leakage Rate Change in Vacuum Distillation When Lowering the Column Pressure

In sub-atmospheric pressure distillation columns, a vacuum system removes entering air by removing a vapor stream, usually near the top of the column. If air is not removed the pressure will continue to increase, as the air itself won't condense through the condenser (unless it is cryogenic). Air can also pose a fire hazard in some cases.

How will the leakage rate into the column change if the pressure of the column is lowered from 0.4 bar to 0.1 bar? Assume the ambient pressure is 1.013 bar.

#### 8.15.1 Solution

Leaks into a column are usually around flanges, through valve or pump packings, inspection or sampling ports, or manholes.

There are a variety of empirical correlations that can be used to estimate leakage depending on pressure. The first answer uses one of those. These are not truly mechanistic, however.

We can also imagine a single hole, and treat the flow as through an orifice. This is the second answer.

We can also treat the hole as an isothermal compressible gas flow problem. The third answer uses that.

```
[18]: from math import pi
     from scipy.constants import hour
     from fluids import *
     V = 10
     P1 = 0.4*1e5
     P2 = 0.1*1e5
     P_{ambient} = 101325
     rho = 1.2
     D = .8
     H = 15
     V = pi/4*D**2*H
     m1 = vacuum_air_leakage_Seider(V=V, P=P1)*hour
     m2 = vacuum_air_leakage_Seider(V=V, P=P2)*hour
     m_ratio = m2/m1
     print(f'Using an emperical correlation, the ratio of air increase is {m_ratio: .3f}.')
     Using an emperical correlation, the ratio of air increase is 1.029.
[21]: # Imagine a 0.1 m hole in the tower
     D_hole = 1e-7
     beta = D_hole/D
     m1 = differential_pressure_meter_solver(D=D_hole/beta, D2=D_hole, P1=P_ambient, P2=P1,
                                              rho=rho, mu=1e-3, k=1.3, meter_type='ISO 5167_

→orifice', taps='D')

     m2 = differential_pressure_meter_solver(D=D_hole/beta, D2=D_hole, P1=P_ambient, P2=P2,
                                              rho=rho, mu=1e-3, k=1.3, meter_type='ISO 5167_

→orifice', taps='D')

     m_ratio = m2/m1
     print(f'Using a flow meter correlation, the ratio of air increase is {m_ratio: .3f}.')
     Using a flow meter correlation, the ratio of air increase is 1.031.
[22]: t_hole = 0.008 # 0.8 mm thick wall
```

Using isothermal compressible gas flow, the ratio of air increase is 1.081.

### 8.16 Problem 14.11 Pressure Rise In a Storage Tank Upon Heating

500 kg of propylene is contained in a 1 m<sup>3</sup> vessel stored at 30 °C. The vessel is heated - from solar radiation in the problem statement. What is the initial pressure?

The safety value of the tank activates at 60 bar. If the cooling system is disabled, what temperature will the contents of the vessel be when the value actuates?

#### 8.16.1 Solution

This is straightforward - an initial solution with total volume, mass, and temperature specified, followed by solving for the end temperature to obtain a specified pressure.

From experience the vessel is known to be liquid. Because of that, we can skip the flash calculations and work directly with the liquid phase object. That is normally much faster than the flash calculations.

```
[1]: from scipy.constants import bar, hour
    from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CoolPropLiquid, CEOSGas,
     →CoolPropGas, FlashPureVLS
    fluid = 'propylene'
    constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
    T1 = 30 + 273.15
    P2 = 60*bar
    zs = [1]
    V_total = 1 \# m^3
    m = 500 \# kg
    backend = 'HEOS'
    gas = CoolPropGas(backend, fluid, T=T1, P=1e5, zs=zs)
    liquid = CoolPropLiquid(backend, fluid, T=T1, P=1e5, zs=zs)
    flasher = FlashPureVLS(constants, correlations, gas=gas, liquids=[liquid], solids=[])
    # Calculate the total number of moles
    moles = m/(1e-3*constants.MWs[0])
    # Calculate the molar volume
    Vm_initial = V_total/moles
    # We know the phase is liquid, so we can skip the flash and solve for the liquid at this.
     ⇔state
    state_1 = liquid.to(T=T1, V=Vm_initial, zs=zs)
    print(f'The initial pressure is {state_1.P/1e6: .3f} MPa')
    state_2 = liquid.to(P=P2, V=Vm_initial, zs=zs)
    print(f'The end tempererature is {state_2.T: .3f} K')
    The initial pressure is 1.979 MPa
    The end tempererature is 311.102 K
```

# 8.17 Problem 14.12 Work and Temperature Change Upon Adiabatic Compression of Oxygen

A stream of oxygen is compressed by a compressor from a pressure P1 = 1 bar to P2 = 10 bar. The flow rate of the oxygen stream is 250 kg/h and the temperature is 25°C.

What is the power of the compressor, and the outlet temperature of the gas?

#### 8.17.1 Solution

This is a series of PH, PS and PT flashes.

```
[1]: from scipy.constants import bar, hour
from thermo import ChemicalConstantsPackage, SRKMIX, IGMIX, CEOSGas, CEOSLiquid,
...,FlashPureVLS
fluid = 'oxygen'
constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
T1 = 25 + 273.15
P1 = 1*bar
P2 = 10*bar
zs = [1]
eta_isentropic = 0.75
eta_mechanical = 0.95
```

```
[3]: # Flash at inlet conditions to obtain initial enthalpy
state_1 = SRK_flasher.flash(T=T1, P=P1)
# Flash at outlet condition - entropy is conserved by compressors and expanders!
state_2_ideal = SRK_flasher.flash(S=state_1.S(), P=P2)
# Compute the change in enthalpy
delta_H_ideal = (state_2_ideal.H()-state_1.H())
# The definition of isentropic efficiency means that the actual amount of heat added is
# dH_actual = dH_idea/eta_isentropic
H_added_to_fluid_actual = delta_H_ideal/eta_isentropic
state_2 = SRK_flasher.flash(H=state_1.H() + H_added_to_fluid_actual, P=P2)
# To compute the actual power, itis more convinient to use the mass enthalpy
actual_power_per_kg = (state_2.H_mass() - state_1.H_mass())/(eta_mechanical) # W/kg
(continues on next page)
```

```
actual_power = actual_power_per_kg*250/hour
    print('With the SRK EOS:')
    print(f'The actual power is {actual_power:.0f} W')
    print(f'The actual outlet temperature is {state_2.T: .2f} K')
    With the SRK EOS:
    The actual power is 24368 W
    The actual outlet temperature is 643.85 K
[4]: # Flash at inlet conditions to obtain initial enthalpy
    state_1 = ideal_flasher.flash(T=T1, P=P1)
    # Flash at outlet condition - entropy is conserved by compressors and expanders!
    state_2_ideal = ideal_flasher.flash(S=state_1.S(), P=P2)
    # Compute the change in enthalpy
    delta_H_ideal = (state_2_ideal.H()-state_1.H())
    # The definition of isentropic efficiency means that the actual amount of heat added is
    # dH_actual = dH_idea/eta_isentropic
    H_added_to_fluid_actual = delta_H_ideal/eta_isentropic
    state_2 = ideal_flasher.flash(H=state_1.H() + H_added_to_fluid_actual, P=P2)
    # To compute the actual power, it is more convinient to use the mass enthalpy
    actual_power_per_kg = (state_2.H_mass() - state_1.H_mass())/(eta_mechanical) # W/kg
    actual_power = actual_power_per_kg*250/hour
    print('With the ideal EOS:')
    print(f'The actual power is {actual_power:.0f} W')
    print(f'The actual outlet temperature is {state_2.T: .2f} K')
    With the ideal EOS:
    The actual power is 24341 W
    The actual outlet temperature is 643.68 K
```

### 8.18 Problem 14.13 Thermodynamic Cycle Calculation Using a High-Precision EOS

A thermodynamic cycle with water as the working fluid consists of the following steps:

- Constant-pressure heating to P1 = 100 bar and T1 =  $350 \degree C$
- Isentropic expansion of the gas in a turbine to P2 = 1 bar (reversible; efficiency = 100%)
- Constant pressure condensation
- Isentropic compression of the liquid to P4 = 100 bar

What is the thermal efficiency of the process?

$$\eta_{th} = -\frac{P_{12} + P_{34}}{Q_{41}}$$

#### 8.18.1 Solution

This is quite straightforward.

```
[1]: import numpy as np
    from thermo import FlashPureVLS, IAPWS95Liquid, IAPWS95Gas, iapws_constants, iapws_
     →correlations
    from scipy.integrate import quad
    import numpy as np
    T1 = 350 + 273.15
    P1 = 100*1e5
    P2 = 1e5
    # Entropy conserved in step 2 as well
    VF3 = ≬
    P3 = P2
    P4 = P1
    # entropy conserved in step 5 as well
    liquid = IAPWS95Liquid(T=T1, P=P1, zs=[1])
    gas = IAPWS95Gas(T=T1, P=P1, zs=[1])
    flasher = FlashPureVLS(iapws_constants, iapws_correlations, gas, [liquid], [])
    stage_1 = flasher.flash(P=P1, T=T1)
    stage_2 = flasher.flash(P=P2, S=stage_1.S())
    stage_3 = flasher.flash(VF=VF3, P=P3)
    stage_4 = flasher.flash(P=P4, S=stage_3.S())
    expander_duty = stage_2.H() - stage_1.H()
    pump_duty = stage_4.H() - stage_3.H()
    heating_duty = stage_1.H() - stage_4.H()
    cooling_duty = stage_3.H() - stage_2.H()
    heating_duty, cooling_duty, expander_duty, pump_duty
[1]: (44969.97634439414,
     -31180.343551697508,
     -13975.281899345828,
     185.64910664919353)
[2]: # it is easy to check the cycle converged
    cycle_error = sum([heating_duty, cooling_duty, expander_duty, pump_duty])
    cycle_error
[2]: -9.094947017729282e-13
[3]: # Not quite sure what definition is being suggested by the textbook
    eta_th = -expander_duty/heating_duty
    print(f'The thermal efficiency is {eta_th*100:.2f} %')
    The thermal efficiency is 31.08 %
```

## 8.19 Problem 14.14 Refrigeration Cycle Calculation Using the Peng-Robinson EOS

A refrigerator uses the refrigerant R-12, dichlorodifluoromethane. The steps and conditions of the cycle are as follows:

- Isobaric condensation to saturation temperature 30°C
- Adiabatic let-down to P2 = 20 degrees subcooling
- Isobaric evaporation to saturation temperature of 20  $^{\circ}\mathrm{C}$
- Isentropic compression to  $P4 = 30 \ ^{\circ}C$

Use the Peng-Robinson EOS.

### 8.19.1 Solution

This is quite straightforward, with the only complication coming from the degrees of subcooling.

```
[1]: # Set the conditions and imports
    from scipy.constants import bar
    from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CEOSGas, FlashPureVLS
    fluid = 'dichlorodifluoromethane'
    constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
    zs = [1]
    eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
    liquid = CEOSLiquid(PRMIX, HeatCapacityGases=correlations.HeatCapacityGases,
                         eos_kwargs=eos_kwargs)
    gas = CEOSGas(PRMIX, HeatCapacityGases=correlations.HeatCapacityGases,
                   eos_kwargs=eos_kwargs)
    flasher = FlashPureVLS(constants, correlations, liquids=[liquid], gas=gas, solids=[])
    T1 = 273.15+30
    state_1 = flasher.flash(VF=0, T=T1)
    saturation_state_1 = flasher.flash(T=-20+273.15, VF=1)
    # Wording is unclear for state 2 but thermodynamically his is what makes sense
    state_2 = flasher.flash(H=state_1.H(), P=saturation_state_1.P)
    # Check the flash lowers the pressure
    assert state_2.P < state_1.P</pre>
    state_3 = flasher.flash(P=state_2.P, VF=1)
    saturation_state_2 = flasher.flash(T=30+273.15, VF=1)
    state_4 = flasher.flash(P=saturation_state_2.P, S=state_3.S())
    states = [state_1, state_2, state_3, state_4]
    condensation_duty = (state_1.H() - state_4.H())
    heating_duty = state_3.H() - state_2.H()
    compressing_duty = state_4.H() - state_3.H()
    condensation_duty, heating_duty, compressing_duty
[1]: (-17242.594866461008, 13841.52397663936, 3401.0708898216462)
```

```
[2]: # Check the cycle convergence
cycle_error = sum([condensation_duty, heating_duty, compressing_duty])
cycle_error
```

[2]: -9.094947017729282e-13

```
[3]: for state in states:
    print(f'T={state.T:.2f} K, P={state.P:.2f} Pa, VF={state.VF:.2f}, S={state.S():.2f}_
    →J/(mol*K), H={state.H():.2f} J/(mol)')
T=303.15 K, P=746445.43 Pa, VF=0.00, S=-72.22 J/(mol*K), H=-17223.28 J/(mol)
T=253.15 K, P=152387.52 Pa, VF=0.29, S=-70.06 J/(mol*K), H=-17223.28 J/(mol)
T=253.15 K, P=152387.52 Pa, VF=1.00, S=-15.38 J/(mol*K), H=-3381.75 J/(mol)
T=312.16 K, P=746445.43 Pa, VF=1.00, S=-15.38 J/(mol*K), H=19.32 J/(mol)
```

## 8.20 Problem 14.15 Joule-Thomson Coefficient for Methane Using the Peng-Robinson EOS

Calculate the Joule-Thomson coefficient of methane at 300 K and 30 bar, using the Peng Robinson model.

#### 8.20.1 Solution

This is straightforward.

```
[1]: # Set the conditions and imports
    from scipy.constants import bar
    from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CEOSGas, FlashPureVLS
    fluid = 'methane'
    constants, correlations = ChemicalConstantsPackage from_IDs([fluid])
    T = 300
    P = 30*bar
    zs = [1]
    eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
    liquid = CEOSLiquid(PRMIX, HeatCapacityGases=correlations HeatCapacityGases,
                        eos_kwargs=eos_kwargs)
    gas = CEOSGas(PRMIX, HeatCapacityGases=correlations HeatCapacityGases,
                  eos_kwargs=eos_kwargs)
    flasher = FlashPureVLS(constants, correlations, liquids=[liquid], gas=gas, solids=[])
    res = flasher.flash(T=T, P=P, zs=zs)
    print(f'The JT coefficient at the specified conditions is {res.Joule_Thomson():.4g} K/Pa
     ')
    The JT coefficient at the specified conditions is 4.652e-06 K/Pa
```

# 8.21 Problem 14.16 Compressor Duty and State Properties after Ammonia Compression

Ammonia at 100 °C and 5 bar is compressed to a pressure of 10 bar. The thermal efficiency of the process is 0.8; and the mechanical efficiency is 0.9. What is the compressor duty per mole and the temperature of the outlet?

### 8.21.1 Solution

This is just another compression problem.

```
[1]: # Set the conditions and imports
    from scipy.constants import bar
    from thermo import ChemicalConstantsPackage, PRMIX, CEOSLiquid, CEOSGas, FlashPureVLS
    fluid = 'ammonia'
    constants, correlations = ChemicalConstantsPackage.from_IDs([fluid])
    T1 = 100 + 273.15
    P1 = 5*bar
    P2 = 10*bar
    zs = [1]
    eta_isentropic = 0.8
    eta_mechanical = 0.9
    eos_kwargs = dict(Tcs=constants.Tcs, Pcs=constants.Pcs, omegas=constants.omegas)
    liquid = CEOSLiquid(PRMIX, HeatCapacityGases=correlations.HeatCapacityGases,
                        eos_kwargs=eos_kwargs)
    gas = CEOSGas(PRMIX, HeatCapacityGases=correlations HeatCapacityGases,
                   eos_kwargs=eos_kwargs)
    flasher = FlashPureVLS(constants, correlations, liquids=[liquid], gas=gas, solids=[])
    state_1 = flasher.flash(T=T1, P=P1)
    state_2_ideal = flasher.flash(S=state_1.S(), P=P2)
    # Compute the change in enthalpy
    delta_H_ideal = (state_2_ideal.H()-state_1.H())
    H_added_to_fluid_actual = delta_H_ideal/eta_isentropic
    state_2 = flasher.flash(H=state_1.H() + H_added_to_fluid_actual, P=P2)
    specific_power = (state_2.H() - state_1.H())/(eta_mechanical)
    print(f'The actual power is {specific_power:.0f} W/mol')
    print(f'The actual outlet temperature is {state_2.T: .2f} K')
    The actual power is 3148 W/mol
    The actual outlet temperature is 448.20 K
```

### NINE

## INSTALLATION

Get the latest version of Thermo from https://pypi.python.org/pypi/thermo/

If you have an installation of Python with pip, simple install it with:

\$ pip install thermo

Alternatively, if you are using conda as your package management, you can simply install thermo in your environment from conda-forge channel with:

\$ conda install -c conda-forge thermo

To get the git version, run:

\$ git clone git://github.com/CalebBell/thermo.git

### TEN

## LATEST SOURCE CODE

The latest development version of Thermo's sources can be obtained at

https://github.com/CalebBell/thermo

### **ELEVEN**

## **BUG REPORTS**

#### To report bugs, please use the Thermo's Bug Tracker at:

https://github.com/CalebBell/thermo/issues

If you have further questions about the usage of the library, feel free to contact the author at Caleb.Andrew.Bell@gmail.com.

### TWELVE

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Although not required by the Thermo license, if it is convenient for you, please cite Thermo if used in your work. Please also consider contributing any changes you make back, and benefit the community.

### THIRTEEN

## CITATION

To cite Thermo in publications use:

Caleb Bell and Contributors (2016-2021). Thermo: Chemical properties component of →Chemical Engineering Design Library (ChEDL) https://github.com/CalebBell/thermo.

# FOURTEEN

## **INDICES AND TABLES**

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